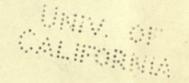


# SMITHSONIAN

# CONTRIBUTIONS TO KNOWLEDGE.

VOL. XIX.





EVERY MAN IS A VALUABLE MEMBER OF SOCIETY, WHO, BY HIS OBSERVATIONS, RESEARCHES, AND EXPERIMENTS, PROCURES KNOWLEDGE FOR MEN.—SMITHSON.

CITY OF WASHINGTON:

PUBLISHED BY THE SMITHSONIAN INSTITUTION.

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COLLINS, PRINTER,
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## ADVERTISEMENT.

This volume forms the nineteenth of a series, composed of original memoirs on different branches of knowledge, published at the expense, and under the direction, of the Smithsonian Institution. The publication of this series forms part of a general plan adopted for carrying into effect the benevolent intentions of James Smithson, Esq., of England. This gentleman left his property in trust to the United States of America, to found, at Washington, an institution which should bear his own name, and have for its objects the "increase and diffusion of knowledge among men." This trust was accepted by the Government of the United States, and an Act of Congress was passed August 10, 1846, constituting the President and the other principal executive officers of the general government, the Chief Justice of the Supreme Court, the Mayor of Washington, and such other persons as they might elect honorary members, an establishment under the name of the "SMITHSONIAN INSTITUTION FOR THE INCREASE AND DIFFUSION OF KNOWLEDGE AMONG MEN." The members and honorary members of this establishment are to hold stated and special meetings for the supervision of the affairs of the Institution, and for the advice and instruction of a Board of Regents, to whom the financial and other affairs are intrusted.

The Board of Regents consists of three members ex officio of the establishment, namely, the Vice-President of the United States, the Chief Justice of the Supreme Court, and the Mayor of Washington, together with twelve other members, three of whom are appointed by the Senate from its own body, three by the House of Representatives from its members, and six persons appointed by a joint resolution of both houses. To this Board is given the power of electing a Secretary and other officers, for conducting the active operations of the Institution.

To carry into effect the purposes of the testator, the plan of organization should evidently embrace two objects: one, the increase of knowledge by the addition of new truths to the existing stock; the other, the diffusion of knowledge, thus increased, among men. No restriction is made in favor of any kind of knowledge; and, hence, each branch is entitled to, and should receive, a share of attention.

The Act of Congress, establishing the Institution, directs, as a part of the plan of organization, the formation of a Library, a Museum, and a Gallery of Art, together with provisions for physical research and popular lectures, while it leaves to the Regents the power of adopting such other parts of an organization as they may deem best suited to promote the objects of the bequest.

After much deliberation, the Regents resolved to divide the annual income into two parts—one part to be devoted to the increase and diffusion of knowledge by means of original research and publications—the other part of the income to be applied in accordance with the requirements of the Act of Congress, to the gradual formation of a Library, a Museum, and a Gallery of Art.

The following are the details of the parts of the general plan of organization provisionally adopted at the meeting of the Regents, Dec. 8, 1847.

#### DETAILS OF THE FIRST PART OF THE PLAN.

- I. To increase Knowledge.—It is proposed to stimulate research, by offering rewards for original memoirs on all subjects of investigation.
- 1. The memoirs thus obtained, to be published in a series of volumes, in a quarto form, and entitled "Smithsonian Contributions to Knowledge."
- 2. No memoir, on subjects of physical science, to be accepted for publication, which does not furnish a positive addition to human knowledge, resting on original research; and all unverified speculations to be rejected.
- 3. Each memoir presented to the Institution, to be submitted for examination to a commission of persons of reputation for learning in the branch to which the memoir pertains; and to be accepted for publication only in case the report of this commission is favorable.
- 4. The commission to be chosen by the officers of the Institution, and the name of the author, as far as practicable, concealed, unless a favorable decision be made.
- 5. The volumes of the memoirs to be exchanged for the Transactions of literary and scientific societies, and copies to be given to all the colleges, and principal libraries, in this country. One part of the remaining copies may be offered for sale; and the other carefully preserved, to form complete sets of the work, to supply the demand from new institutions.
- 6. An abstract, or popular account, of the contents of these memoirs to be given to the public, through the annual report of the Regents to Congress.

- II. To increase Knowledge.—It is also proposed to appropriate a portion of the income, annually, to special objects of research, under the direction of suitable persons.
- 1. The objects, and the amount appropriated, to be recommended by counsellors of the Institution.
- 2. Appropriations in different years to different objects; so that, in course of time, each branch of knowledge may receive a share.
- 3. The results obtained from these appropriations to be published, with the memoirs before mentioned, in the volumes of the Smithsonian Contributions to Knowledge.
  - 4. Examples of objects for which appropriations may be made:-
- (1.) System of extended meteorological observations for solving the problem of American storms.
- (2.) Explorations in descriptive natural history, and geological, mathematical, and topographical surveys, to collect material for the formation of a Physical Atlas of the United States.
- (3.) Solution of experimental problems, such as a new determination of the weight of the earth, of the velocity of electricity, and of light; chemical analyses of soils and plants; collection and publication of articles of science, accumulated in the offices of Government.
- (4.) Institution of statistical inquiries with reference to physical, moral, and political subjects.
- (5.) Historical researches, and accurate surveys of places celebrated in American history.
- (6.) Ethnological researches, particularly with reference to the different races of men in North America; also explorations, and accurate surveys, of the mounds and other remains of the ancient people of our country.
- I. To diffuse Knowledge.—It is proposed to publish a series of reports, giving an account of the new discoveries in science, and of the changes made from year to year in all branches of knowledge not strictly professional.
- 1. Some of these reports may be published annually, others at longer intervals, as the income of the Institution or the changes in the branches of knowledge may indicate.
- 2. The reports are to be prepared by collaborators, eminent in the different branches of knowledge.

- 3. Each collaborator to be furnished with the journals and publications, domestic and foreign, necessary to the compilation of his report; to be paid a certain sum for his labors, and to be named on the title-page of the report.
- 4. The reports to be published in separate parts, so that persons interested in a particular branch, can procure the parts relating to it, without purchasing the whole.
- 5. These reports may be presented to Congress, for partial distribution, the remaining copies to be given to literary and scientific institutions, and sold to individuals for a moderate price.

The following are some of the subjects which may be embraced in the reports:—

### I. PHYSICAL CLASS.

- 1. Physics, including astronomy, natural philosophy, chemistry, and meteorology.
- 2. Natural history, including botany, zoology, geology, &c
- 3. Agriculture.
- 4. Application of science to arts.

#### II. MORAL AND POLITICAL CLASS.

- 5. Ethnology, including particular history, comparative philology, antiquities, &c.
- 6. Statistics and political economy.
- 7. Mental and moral philosophy.
- 8. A survey of the political events of the world; penal reform, &c.

### III. LITERATURE AND THE FINE ARTS.

- 9. Modern literature.
- 10. The fine arts, and their application to the useful arts.
- 11. Bibliography.
- 12. Obituary notices of distinguished individuals.
- II. To diffuse Knowledge.—It is proposed to publish occasionally separate treatises on subjects of general interest.
- 1. These treatises may occasionally consist of valuable memoirs translated from foreign languages, or of articles prepared under the direction of the Institution, or procured by offering premiums for the best exposition of a given subject.
- 2. The treatises to be submitted to a commission of competent judges, previous to their publication.

## DETAILS OF THE SECOND PART OF THE PLAN OF ORGANIZATION.

This part contemplates the formation of a Library, a Museum, and a Gallery of Art.

- 1. To carry out the plan before described, a library will be required, consisting, 1st, of a complete collection of the transactions and proceedings of all the learned societies of the world; 2d, of the more important current periodical publications, and other works necessary in preparing the periodical reports.
- 2. The Institution should make special collections, particularly of objects to verify its own publications. Also a collection of instruments of research in all branches of experimental science.
- 3. With reference to the collection of books, other than those mentioned above, catalogues of all the different libraries in the United States should be procured, in order that the valuable books first purchased may be such as are not to be found elsewhere in the United States.
- 4. Also catalogues of memoirs, and of books in foreign libraries, and other materials, should be collected, for rendering the Institution a centre of bibliographical knowledge, whence the student may be directed to any work which he may require.
- 5. It is believed that the collections in natural history will increase by donation, as rapidly as the income of the Institution can make provision for their reception; and, therefore, it will seldom be necessary to purchase any article of this kind.
- 6. Attempts should be made to procure for the gallery of art, casts of the most celebrated articles of ancient and modern sculpture.
- 7. The arts may be encouraged by providing a room, free of expense, for the exhibition of the objects of the Art-Union, and other similar societies.
- 8. A small appropriation should annually be made for models of antiquity, such as those of the remains of ancient temples, &c.
- 9. The Secretary and his assistants, during the session of Congress, will be required to illustrate new discoveries in science, and to exhibit new objects of art; distinguished individuals should also be invited to give lectures on subjects of general interest.

In accordance with the rules adopted in the programme of organization, each memoir in this volume has been favorably reported on by a Commission appointed

for its examination. It is however impossible, in most cases, to verify the statements of an author; and, therefore, neither the Commission nor the Institution can be responsible for more than the general character of a memoir.

The following rules have been adopted for the distribution of the quarto volumes of the Smithsonian Contributions:—

- 1. They are to be presented to all learned societies which publish Transactions, and give copies of these, in exchange, to the Institution.
- 2. Also, to all foreign libraries of the first class, provided they give in exchange their catalogues or other publications, or an equivalent from their duplicate volumes.
- 3. To all the colleges in actual operation in this country, provided they furnish, in return, meteorological observations, catalogues of their libraries and of their students, and all other publications issued by them relative to their organization and history.
- 4. To all States and Territories, provided there be given, in return, copies of all documents published under their authority.
- 5. To all incorporated public libraries in this country, not included in any of the foregoing classes, now containing more than 10,000 volumes; and to smaller libraries, where a whole State or large district would be otherwise unsupplied.

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AN

## INVESTIGATION

OF THE

# ORBIT OF URANUS,

WITH GENERAL TABLES OF ITS MOTION.

BY

SIMON NEWCOMB,

PROFESSOR OF MATHEMATICS, UNITED STATES NAVY.

[ACCEPTED FOR PUBLICATION, FEBRUARY, 1873.]

## ADVERTISEMENT.

In the investigation of the Orbit of Uranus which forms the subject of the accompanying memoir, as well as in that of the Orbit of Neptune previously published in the Smithsonian Contributions, a large amount of arithmetical computation has been required, especially in the reduction and comparison of observations. The cost of this, in accordance with the spirit of the Institution in advancing science, has been defrayed from the income of the Smithson fund.

As required by the rules of the Institution, the accompanying memoir was referred to competent authority for examination, and the persons selected for this purpose were Professor J. H. C. Coffin, of the Nautical Almanac Office, and Professor Asaph Hall, of the Naval Observatory.

JOSEPH HENRY, Secretary S. I.

WASHINGTON, 1873.

PHILADELPHIA: COLLINS, PRINTER, 705 Jayne Street.

## PREFACE.

THE present work was undertaken as far back as the year 1859. But the labor devoted to it at first amounted to little more than tentative efforts to obtain numerical data of sufficient accuracy, and to decide upon a satisfactory method of computing the general perturbations of the planet. The elements of Neptune employed in the earlier computations were found to deviate too widely from the truth to be used in computing the perturbations of Uranus with the first order of accuracy, and it became necessary to correct them. This was done during the years 1864 and 1865, and the investigation was printed by the Smithsonian Institution in the latter year. It was then found that the adopted elements of Uranus also differed too widely from the truth to serve as the basis of the work, and they were provisionally corrected by a series of heliocentric longitudes derived from observations extending from 1781 to 1861. Finally it was found that the adopted method of computing the perturbations, that of the "variation of elements," though not deserving of the disfavor into which it has fallen of late years, was practically inapplicable to the computation of the most difficult terms, namely, those of the second order with respect to the disturbing forces. Indeed, it appeared to the author that the only method of computing those terms which was at the same time general, practicable, and fully developed, was that of Hansen. But, were this method adopted, all that had previously been done would have been useless, even for the purpose of comparison and verification, owing to the expression of the coordinates in terms of a disturbed mean anomaly. It appeared to the author that, although this form of theory led to expressions having fewer terms than the other, it was not without its relative disadvantages. Other considerations being equal, he conceived that astronomers generally would greatly prefer to see the perturbations expressed directly in terms of the time, owing to the ease with which the results of different investigators could then be compared, and with which corrections to the theory may be introduced.

Under these circumstances the method described in the first chapter of the present paper was worked out. The question how much it contains that is essentially new is one that the author has never closely examined: it is, however, certain

that the mode of considering the subject is well known, being that employed by La Place, Herschel, De Pontécoulant, Encke, and perhaps others. The method of forming the required derivations of the perturbative function from the analytical development of that quantity, he has not seen elsewhere.

With these improved elements and methods the work was recommenced in 1868. The earlier investigations being merely provisional, it has not been deemed necessary to present them in the present work. Some of the results, corrected for errors of the older elements, are, however, given for the purpose of comparison.

Although this investigation has absorbed the greater part of the author's leisure for more than five years, it is only through the aid of the Smithsonian Institution and Nautical Almanac that he has been enabled to bring it to a conclusion within that time. At an early stage of the work Professor Henry responded favorably to a request for aid by the employment of computers; it was, however, not found practicable to use such aid until the perturbations had been completed, and the provisional theory concluded. Then, the comparison of theory and observation, and the construction of the tables, involved a large amount of mechanical computation, and on this part of the work a number of persons have been employed by the Institution at various times, among whom may be mentioned Professor F. W. Bardwell, of the University of Kansas, and Dr. C. L. F. Kampf, late of the Observatory of Leiden. Every part of the work has, however, been done under the author's immediate direction, and, as nearly as possible, in the same way as if he had done it himself, a result which, in one or two cases, has been attained only by the expenditure of an amount of labor approximating that saved by the employment of the computer.

In presenting the steps of the investigation, the end has been kept constantly in view to render as easy as possible the detection and correction of any error, or the introduction of any alteration in the elements or other data. It is, of course, impossible to present the steps of the computation with any approach to fulness without far transcending the limits of the printed work: The results given are, therefore, those which it was supposed would be most useful to the future investigator of the same subject. There is reason to believe that the original computations will ultimately become the property of the National Academy of Sciences, so that they may always be referred to for the clearing up of any difficulty in the printed text.

The author's acknowledgments are due to Professor J. H. C. Coffin, Superintendent of the Nautical Almanac, and Mr. E. J. Loomis, of the Nautical Almanac Office, for reading the proof sheets of the last twelve tables during the absence of the former abroad.

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#### ERRATA.

Pages 100 to 105. In computing the latitude from the provisional theory the values of the secular terms of  $\delta\eta$  and  $\delta k$  on page 97 have been interchanged. The provisional latitude, therefore, requires the correction

 $-0''.53 T \sin v + 0''.53 T \cos v$ 

where

 $v = g + 12^{\circ} 45' + 2e \sin g$ .

This correction is not applied in the subsequent investigation. Its effect would have been to change the value of b deduced on p. 176 by probably 0".2 or 0".3. The effect on the other elements of latitude would have been much smaller, and therefore unimportant.

Page 122, line 15. Add: the corrections in the sixth column being omitted.

Page 151. Add foot-note: In forming these comparisons the corrections to the heliocentric longitude in the sixth column of the provisional ephemeris, pages 100 to 105, are not applied.

Page 159. Equation 7. In this equation the coefficients of  $\delta \lambda$  and  $\delta \rho$  have been multiplied by  $\frac{1}{6}$ , instead of  $\frac{2}{6}$ , the factor of  $\delta l$ . The effect of this error enters into all the subsequent results, but in the comparisons of theory and observation it is corrected.

Page 184. The element here represented by x (kappa) is the same which, in the preceding chapters, has by mistake been represented by k, and which is defined on p. 24. The k of Chapter VIII is, therefore, not the same with that of preceding chapters.

## ON THE ORBIT OF URANUS.

#### INTRODUCTION.

The connection of the planet Uranus with the most brilliant astronomical achievement of the century lends a peculiar interest to its theory. The researches of Adams and Le Verrier showed that the observed motions of that planet were represented, at least approximately, by the action of a theoretical planet having the longitude of Neptune. Peirce showed that the action of Neptune itself accounted for these motions within the limits of possible error of the observations used by Le Verrier. It remains to be seen whether the agreement between theory and observation still subsists when the comparatively few observations used by those investigators are reduced with the more refined data now at our disposal, and when the great mass of additional observations made both before and since the date of Le Verrier's researches are included.

The circumstances connected with the discovery of Neptune have been so exhaustively recounted by a number of authors that it would be difficult to add anything not already familiar to astronomers without transcending our present limits. I shall therefore confine myself to such an account of previous researches on the theory of Uranus as may give an idea of their nature and extent, and facilitate their comparison with the methods and results of the present investigation.

The perturbations used by Bouvard in his tables are those of the Mécanique Céleste. Although not affected with any striking error, the numerical methods adopted in their computation are necessarily too rough to allow of much interest attaching to their comparison with the results of the more recent researches.

It is essential to a clear understanding of subsequent researches that we classify the methods which have been or may be adopted in the computation of the general perturbations of the planets. This computation comprises two distinct operations: (1) the development of the disturbing forces, or some quantities of which these forces are functions; (2) the integration of the equations of motion under the influence of these forces. In each of these operations three methods have been employed.

In developing the perturbative function, we have first the purely analytic method used by the great geometers of the last century. In this method this function is developed in powers of the eccentricities and mutual inclination of the orbits of the two planets, and the numerical coefficients are found by substituting the values of the elements in these expressions. It is only applicable when the eccentricities

1 March, 1873. (1)

and mutual inclination are small, and has for that reason fallen, of late, into a certain disrepute. The extended tables published by Le Verrier<sup>1</sup> have, however, added so much to its facility for use that it is not wholly unworthy of attention.

At the other extreme stands the purely mechanical method, in which special values of the disturbing force are computed for many combinations of the mean anomalies of the two planets, and the values of the coefficients in the general expression for the force thence deduced.

Between these two stands what I conceive we may designate as the Cauchy-Hansen method, in which the development is made mechanically with respect to the one planet, but the eccentric anomaly of the other is retained as an undetermined quantity. The germ of this method is found in several papers, by Cauchy, in the earlier volumes of the Comptes Rendus of the French Academy, which have since been combined into a homogeneous memoir by Puiseux.<sup>2</sup> The object had in view by these authors is only the computation of inequalities of long period. But Hansen has taken up the essential principle of the method, first, in his prize memoir on the perturbations of comets, crowned by the French Academy of Sciences, about 1848, and afterwards in his "Auseinandersetzung einer zweckmässigen Methode zur Berechnung der Störungen der kleinen Planeten," and applied it to the general development of perturbations.

Among the three methods of integration, the first in point of analytical elegance and generality, but the last in order of convenience in use, is that of the variation of elements, a method with which the name of La Grange is inseparably associated.

In the second the direct integration of the differential equations which express the perturbations of longitude, latitude, and radius vector is effected by special devices.

In the first of these methods the problem is presented in this form: The equations of motion being completely integrated for the action of the principal forces only, how must the arbitrary constants of integration vary in order that the same expressions may represent the motion of the planet under the influence of the disturbing forces? In the second method, the same thing being presupposed, the question is, what expressions must be added to the integrals of undisturbed motion in order that the sum may represent the integrals of the disturbed motion?

The third is Hansen's method, in which the co-ordinates are partly expressed in terms of a certain function of the time known as the disturbed mean anomaly, determined by the condition that the true longitude in the disturbed orbit shall be the same function of the disturbed time that the longitude in the elliptic orbit is of the simple time.

Although the last two methods have a great advantage over the first in the computation of the periodic perturbations, I conceive the first to be best adapted to the computation of the secular variations, and perhaps, of terms of very long period in the mean longitude and the elements of the orbit.

<sup>&</sup>lt;sup>1</sup> Annales de l'Observatoire Impérial de Paris. Tome I.

<sup>&</sup>lt;sup>2</sup> Annales de l'Observatoire Impérial de Paris. Tome VII.

<sup>&</sup>lt;sup>3</sup> Abhandlungen der Königlich Sächsischen Gesellschaft der Wissenschaften. Band V. VI, VII.

In his researches on the motion of Uranus, the first thing done by Le Verrier was to recompute the perturbations by Jupiter and Saturn. It will sufficiently describe his method of doing this to say that in the developments he used the purely mechanical method for the action of Saturn, and the algebraic development of the perturbative function for the action of Jupiter, while in the integration he used the method of the variation of elements. After completing the perturbations of the first order he made the earliest attempt at a complete determination of those of the second order. Beginning with the terms of this order which arise from the secular variations of the elements, he determines them by recomputing the terms of the first order for the epoch 2300, and assuming that the general term will then be given by interpolating between the two terms thus found, supposing them to increase uniformly with the time. This proceeding has the sanction of such high authority that it is worth while to call attention to its want of rigor. The differential coefficient of each element being given in the form

$$\frac{da}{dt} = k \cos bt,$$

k being a function of the elements, the perturbation of the first order will be

$$\delta a = \frac{k}{b} \sin bt.$$

When we take into account the variation of k, and suppose it of the form  $k_0 + k't$ , the process is equivalent to supposing that in this case

$$\delta a = \frac{k_0 + k't}{b} \sin bt,$$

whereas it really contains the additional term,

$$\frac{k'}{b^2}\cos bt,$$

which appears to be neglected in the process in question. It will be seen that the neglected coefficient is equal to the secular variation of the term during the time that its argument requires to increase by an amount equal to the unit radius. It is therefore the more important the longer the period of the inequality.

To obtain the periodic terms of the second order Le Verrier begins by determining the ten principal terms of the perturbations of the elements of Saturn produced by Jupiter. Next he takes up the terms in the mean longitude of Uranus which depend on the square of the mass of Saturn. The only sensible terms he finds are

$$-1''.17 \sin (\zeta^* - 3\zeta) - 0''.35 \cos (\zeta' - 3\zeta) + 0''.43 \sin (\zeta'' - 4\zeta' + 4\zeta) - 0''.21 \cos (\zeta'' - 4\zeta' + 4\zeta),$$

 $\zeta$ ,  $\zeta'$ , and  $\zeta''$  being the mean anomalies of Uranus, Saturn, and Jupiter, respectively. The terms depending on the product of the masses of Jupiter and Saturn are then taken up. Fifteen arguments are found the coefficients of which vary from a small fraction of a second to one or two seconds, while a single one of long period amounts to 32''.

When the method of variation of elements is used, it is necessary not only to determine these variations to quantities of the second order, but, in the transforma-

tion of the perturbations of the elements into perturbations of the co-ordinates, to carry this transformation to terms of the second order also. This Le Verrier avoids by showing that the terms of the lowest order with respect to the eccentricities thus introduced are destroyed by certain terms in the perturbations of the elements, so that it is only necessary to omit both classes of terms. These terms are of that fictitious class which disappear of themselves by a simple change of elements. When, instead of the eccentricity and longitude of the perihelion, we take h and k, which represent the products of the eccentricity into the sine and cosine of this longitude respectively, these terms disappear of themselves both from the perturbations of the elements and of the co-ordinates. It is not likely that any of the neglected terms of this class exceed 0".1.

As soon as the elements of Neptune were known, the nature of its general action on Uranus became of interest. This subject was taken up by Prof. Peirce, whose results are found in the Proceedings of the American Academy of Arts and Sciences, Vol. I, pp. 334–337. This paper is accompanied with a comparison of his theory of Uranus with observations, to which similar comparisons of the theories of Adams and Le Verrier are added. This comparative exhibit is of sufficient interest to be given here. The numbers given are probably excesses of computed over observed longitudes.

RESIDUAL DIFFERENCES BETWEEN THE THEORETICAL AND OBSERVED LONGITUDES OF URANUS, FROM THE THEORIES OF PEIRCE, LE VERRIER, AND ADAMS.								
Year.	From Le Verrier's best orbit of Uranus from the modern observations without any external planet.	rier's original theory with his best orbit of hypotheti-	original the- ory with his second hypo- thetical planet	That of Struve from his own observations of the satellite	That deduced by Peirce from Bond's & Las-	That deduced by Peirce from Bond's obser- vations of Las-		
1690 1715 1756 1769 1782 1787 1792 1797 1803 1808 1813 1819 1824 1829 1835 1840 1845	+ 289.0 + 279.6 + 230.9 + 123.3 + 20.5 + 2.0 - 7.8 - 6.7 - 3.4 + 3.8 + 4.5 + 3.8 - 7.6 - 7.8 - 4.5 + 0.7 + 6.5		+ 50.0 - 6.6 - 4.0 + 1.8 0.0 - 0.2 - 1.1 - 0.5 + 1.6 0.0 - 1.0 - 2.2 + 1.7 + 2.0 - 1.2 + 1.3		$\begin{array}{c} \\ \\ +13.0 \\ +10.0 \\ -12.7 \\ -16.0 \\ -5.6 \\ -12 \\ +0.5 \\ +0.8 \\ +1.2 \\ -0.6 \\ +1.1 \\ +0.7 \\ -1.9 \\ +1.3 \\ +2.4 \\ -1.3 \\ -1.2 \\ \end{array}$	$ \begin{array}{c}                                     $		

In this paper Professor Peirce presents the results of a complete computation of the general perturbations of Uranus by Neptune in longitude and radius vector, but without any details whatever of the investigation, or any statement of the methods employed. The minuteness of the residuals in the last column of the preceding table shows that employing these perturbations by Neptune, and those of Le Verrier by Jupiter and Saturn, we had a theory of Uranus from which quite accurate tables might have been constructed. But this never seems to have been done. The ephemeris of Uranus in the American Nautical Almanac was intended to be founded on this theory, but the proper definitive elements do not seem to have been adopted in the computations, as the ephemeris does not correspond with the theory.

Although twenty-five years have elapsed since the epoch of these researches, I am not aware of any published work of importance on the theory of Uranus during the interval. Mr. T. H. Safford has, however, made a very extended investigation of the subject, but has published nothing more than a brief general description of his work, which may be found in the Monthly Notices of the Royal Astronomical Society, Vol. 22. Like Professor Peirce, he took Le Verrier's perturbations by Jupiter and Saturn, but, instead of using general perturbations by Neptune, he computed the effect of the action of this planet by mechanical quadratures for the whole period of the observations of Uranus, and thus corrected the elements and the mass of Neptune from modern observations alone. The mass in question deduced was

 $\frac{1}{20039}$ 

Mr. Safford does not give the representation of the modern observations, but presents the following comparison of the ancient ones, alongside which we place for comparison the corresponding numbers of Peirce's theory and those of the present investigation.

	Excess o	F OBSERVATION	OVER THEORY.	
Date.	No. of obs.	Safford.	Peirce.	Newcomb.
1690	1	+ 5".0	<b>—</b> 0".8	- 11"
1715	3	- 4.2	— 8.7	- 8
1750	2	-12	}	+ 2.9
1753	1	_ 0.2		T 2.0
1756	1	- 0.9	- 4.0	
1764	1	+ 0.4		
1769	8	+ 4.5	+ 6.0	-1.4

## CHAPTER I.

METHOD OF DETERMINING THE PERTURBATIONS OF LONGITUDE, RADIUS VECTOR, AND LATITUDE OF A PLANET BY DIRECT INTEGRATION.

Let us conceive a plane determined by the condition that it shall pass through the sun and contain the tangent to the orbit of a planet at any moment. If the planet were acted on by the sun alone, the position of this plane would be invariable, but, under the influence of the disturbing forces of the other planets, it is subject, at each instant, to a motion of rotation around the radius vector of the planet. We may regard this as the instantaneous plane of the planet's orbit. The disturbing and the disturbed planet will each have its own instantaneous plane.

Let us now put:-

- v, the longitude of a planet counted from a determinate point in the instantaneous plane of its orbit.
- v, its distance from the node of intersection of its own orbit with that of another planet.
- y, the mutual inclination of the two orbits.
- $\sigma$ ,  $\sin \frac{1}{2} \gamma$ .
- r, the radius vector of the planet.
- ρ, its logarithm.
- $\mu$ , the attractive force of the sun upon unit of matter at unit distance.
- a, the mean distance corresponding to the observed mean motion of the planet, determined by the condition

$$a^3 = \frac{\mu \left(1 + m\right)}{n^2},$$

m and n being as usual the mass and mean motion.

 $a_0$ , the value of a corrected for the constants introduced by the perturbations, so that, as in the elliptic motion, we have

$$\rho = \log a + f(l, e, \varpi),$$

we shall have in the disturbed motion

$$\rho = \log a_0 + f(l, e, \varpi) + \text{periodic terms only.}$$

- $a_1$ , the mean distance of an outer planet, whether it be a disturbing or disturbed planet.
- v, the logarithm of a.
- a, the ratio of two mean distances, taken less than unity.
- R, the perturbative function.

h, the coefficient of any term of  $\frac{a_1}{m'}R$ , so that we have

$$R = \sum \frac{m'h}{a_1} \cos N$$

m' being here the mass of the disturbing planet.

- 2, the mean distance of the planet from the node, or the mean value of v.
- ω, the distance of the perihelion from the node.
- g, the mean anomaly.
- l, the mean longitude, or the mean value of v.
- $\psi$ , the angle of eccentricity so that  $e = \sin \psi$ .
- r<sub>3</sub>, the radius of the planet in the undisturbed ellipse.
- $r_1$ , the quotient of  $r_0$  divided by the mean distance, which is a function of the eccentricity and mean anomaly only.
- T, the time after the epoch 1850, Jan. 0, Greenwich mean noon, counted in Julian centuries.
- $\nu$ , the integrating factors of the periodic terms, or the ratio  $\frac{n}{N}$ , N being the change of the angle in unit of time.
- u, the eccentric anomaly, and, in the tables, the argument of latitude. We have for the value of R

$$R = \frac{m'}{\sqrt{r^2 - 2rr'(\cos v \cos v' + \sin v \sin v' \cos \gamma) + r'^2}} - \frac{m'r}{r'^2} (\cos v \cos v' + \sin v \sin v' \cos \gamma)$$

or, if we suppose r replaced by its value in  $\rho$ , namely

$$r = c'$$

we shall have

$$R = m'f(\mathbf{v}, \mathbf{v}', \rho, \rho', \gamma).$$

With this value of R it is well known that the differential equations for the longitude and radius vector of a planet are

$$r\frac{d^{2}r}{dt^{2}} - r^{2}\frac{dv^{2}}{dt^{2}} + \frac{\mu(1+m)}{r} = \mu\frac{\partial R}{\partial \rho};$$

$$r^{2}\frac{d^{2}v}{dt^{2}} + 2r\frac{dr}{dt}\frac{dv}{dt} = \mu\frac{\partial R}{\partial v}.$$
(1)

If we multiply the first of these equations by  $2\frac{d\rho}{dt}$  and the second by  $2\frac{dv}{dt}$  and add them together, putting, for brevity,

$$\frac{\partial R}{\partial \rho} \frac{d\rho}{dt} + \frac{\partial R}{\partial v} \frac{dv}{dt} = D_t R, \qquad (2)$$

and then integrate, we shall have

$$\frac{dr^{2}}{dt^{2}} + r^{2} \frac{dv^{2}}{dt^{2}} - \frac{2\mu (1+m)}{r} = 2\mu (C + \int D_{t} R dt)$$

C being the arbitrary constant added to the integral. Adding this equation to the first of equations (1) we have

$$\frac{1}{2} \frac{d^2(r^2)}{dt^2} - \frac{\mu(1+m)}{r} = \mu \left( 2C + 2 \int D' R dt + \frac{\partial R}{\partial \rho} \right)$$
 (3)

Let us now represent by  $r_0$  that elliptic value of r which satisfies the equation

$$\frac{1}{2}\frac{d^2(r_0^2)}{dt^2} - \frac{\mu(1+m)}{r_0} = 2\mu C.$$

Subtracting this equation from the last we have

$$\frac{1}{2} \frac{d^2 (r^2 - r_0^2)}{dt^2} - \mu (1 + m) \left( \frac{1}{r_0} - \frac{1}{r_0} \right) = \mu \left( 2 \int D_t R dt + \frac{\partial R}{\partial \rho} \right).$$

in which no constant is to be added to the integral, and both sides of the equation are of the order of the disturbing forces. As there is a decided advantage in taking the logarithm of the radius vector as the variable instead of r itself, we substitute for the latter its value

 $r=c_{\rm P},\quad r_{\rm o}=c_{\rm PO}$ 

and put

 $\delta \rho = \rho - \rho_0$ .

Then

$$\begin{split} r^2 &= c^{\frac{2r_0}{2} + \frac{2\delta\rho}{2}} = r_0^2 \ c^{\frac{2\delta\rho}{2}} = r_0^2 \ \left(1 + 2^{\varsigma}\rho + \frac{2^2}{1.2} \ \delta\rho^2 + \text{etc.}\right) \\ &\frac{1}{2} \left(r^2 - r_0^2\right) = r_0^2 \delta\rho + r_0^2 \delta\rho^2 + \text{etc.} \\ &\frac{1}{r} - \frac{1}{r_0} = -\frac{\delta\rho}{r_0} + \frac{\delta\rho^2}{2r_0} + \text{etc.} \end{split}$$

Substituting these values in the above equation, carrying the development only to terms of the second order, and transposing those terms to the right hand side of the equation, and putting  $\mu' = \mu (1 + m)$ , we find

$$\frac{d^{2}(r_{0}^{2}\delta\rho)}{dt^{2}} + \frac{\mu'}{r_{0}^{3}}(r_{0}^{2}\delta\rho) = \mu\left(2\int D'_{t}Rdt + \frac{\partial R}{\partial\rho}\right) - \frac{d^{2}(r_{0}^{2}\delta\rho^{2})}{dt^{2}} + \frac{\mu\delta\rho^{2}}{2r_{0}},$$
 (4)

an equation which gives the perturbations of radius vector.

The general mode of solving this equation by successive approximation is familiar. The principles on which the successive approximations are made being the same, we shall begin by assuming that we have obtained first approximations to the values of  $\delta v$ ,  $\delta v$ ,  $\delta \rho$ ,  $\delta \rho'$ ,  $\delta \gamma$ , and that from these we wish to pass to a second approximation. We must first carry this approximation into the functions of R in the second member of (4). To effect this we must show how, from the development of R in terms of the elements and the time, we may form its successive derivatives with respect to the quantities which enter into it. R, while originally a function of v, v',  $\rho$ ,  $\rho'$ , and  $\gamma$ , is, in its developed form, a function of  $\lambda$ ,  $\lambda'$ ,  $\omega$ ,  $\omega'$ , e, e', v, v, and  $\gamma$ , the development being effected by substituting for the first set of quantities their values in terms of the second. The substitution is as follows:

$$v = \lambda + Fg,$$

$$v' = \lambda' + Fg',$$

$$\rho = \nu + \varphi g,$$

$$\rho' = \nu' + \varphi g',$$
(5)

Fg being the equation of the centre, and  $\phi g$  the part of  $\rho$  depending on the eccentricity in the elliptic motion. It follows that if we express the developed expression for R as a function of  $\lambda$ ,  $\lambda'$ , g, g', n, n', which we may do by putting

$$\omega = \lambda - g$$
,  $\omega' = \lambda' - g'$ ;  
 $a = c^{\nu}$ ,  $a' = c^{\nu'}$ ;

we shall have by successive differentiation

$$\frac{\partial R}{\partial \lambda} = \frac{\partial R}{\partial \mathbf{v}} \frac{\partial \mathbf{v}}{\partial \lambda} = \frac{\partial R}{\partial \mathbf{v}}$$

$$\frac{\partial^{2} R}{\partial \lambda^{2}} = \frac{\partial^{2} R}{\partial \mathbf{v}^{2}} \frac{\partial \mathbf{v}}{\partial \lambda} = \frac{\partial^{2} R}{\partial \mathbf{v}^{2}}$$

$$\frac{\partial R}{\partial n} = \frac{\partial R}{\partial \rho} \frac{\partial \rho}{\partial n} = \frac{\partial R}{\partial \rho}$$

$$\frac{\partial^{2} R}{\partial n^{2}} = \frac{\partial^{2} R}{\partial \rho^{2}} \frac{\partial \rho}{\partial n} = \frac{\partial^{2} R}{\partial \rho^{2}}$$
etc. etc. etc.

and in general

$$\frac{\partial^{m+n+m'+n'}R}{\partial \lambda^m \partial \nu^n \partial \lambda'^{m'} \partial \nu'^{n'}} = \frac{\partial^{m+n+m'+n'}R}{\partial v^m \partial \rho^n \partial v'^{m'} \partial \rho'^{n'}}$$

Thus, by expressing the developed R in the above form, we may find the derivative of any order with respect to v, v',  $\rho$  and  $\rho'$ , by taking the corresponding derivative with respect to  $\lambda$ ,  $\lambda'$ ,  $\nu$  and  $\nu'$ .

The developed R is usually expressed in the form

$$R = \sum \frac{m'h}{a_1} \cos (i'\lambda' + i\lambda + j'\omega' + j\omega)$$

 $a_1$  being the mean distance of the outer planet, whether disturbing or disturbed, and h a function of e, e', a, and  $\gamma$ . Substituting for  $\omega$  its value in g, this equation will become

$$R = \sum \frac{m'h}{a_1} \cos \left( (i'+j') \lambda' + (i+j) \lambda - j'g' - jg \right).$$

Putting for brevity

$$N = i\lambda' + i\lambda + j\omega' + j\omega,$$

the formulæ (6) give

$$\frac{\partial R}{\partial \mathbf{v}} = -\sum \frac{m'h}{a_1} (i+j) \sin N$$

$$\frac{\partial^2 R}{\partial \mathbf{v}^2} = -\sum \frac{m'h}{a_1} (i+j)^2 \cos N$$

$$\frac{\partial R}{\partial \rho} = \sum m' \frac{\partial \frac{h}{a_1}}{\partial \rho} \cos N$$
(7)

and in general

$$\frac{\partial^{u+u'+n+n'}R}{\partial v^u \partial v'^{u'} \partial \rho^n \partial \rho'^{n'}} = \Sigma \pm m'(i+j)^u (i+j')^{u'} \frac{\partial^{n+n'}\frac{h}{a_1}}{\partial n^n \partial n'^{n'}} \sin N$$

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The formation of the derivatives in the second member of this equation demands attention. In the analytic development of the perturbative function each value of h is composed of a series of terms each of the form

$$E \times A$$

E being a function of the eccentricities and mutual inclination, and A a function of  $\alpha$  of the form

$$(0) \alpha^{s-\frac{1}{2}} b_s^{(i)} + (1) \alpha^{s+\frac{1}{2}} \frac{\partial b_s^{(i)}}{\partial \alpha} + (2) \alpha^{s+\frac{3}{2}} \frac{\partial^2 b_s^{(i)}}{\partial \alpha^2} + \text{etc.} + \alpha^{\frac{2s+2n-1}{2}} \frac{\partial^n b_s^{(i)}}{\partial \alpha^n}, \quad (8)$$

(0), (1), etc., being numerical coefficients connected with the coefficients  $V^{(i)}$  tabulated by Le Verrier, in Tome I of his Annales de l'Observatoire, by the relation

$$(n) \stackrel{\cdot}{=} \frac{V_n^{(i)}}{1.2.3 \dots n},$$

and  $b_s^{(i)}$  being, as usual, the coefficient of  $\cos i\phi$  in the development of

$$(1-2\alpha\cos\phi+\alpha^2)^{-s}$$

in multiples of  $\cos \phi$ , and n-1 the sum of the exponents of the eccentricities in E. It would have been much more convenient if in effecting this development the derivatives of  $b^{(i)}_s$  had been taken with respect to n instead of n. In fact the derivative  $\frac{\partial^n b^{(i)}_s}{\partial n}$  when expressed in terms of the derivatives with respect to n is of the form

$$\alpha^n \frac{\partial^n b_s^{(i)}}{\partial \alpha^n} = n_1 \frac{\partial b_s^{(i)}}{\partial p} + n_2 \frac{\partial^2 b_s^{(i)}}{\partial p^2} + \text{etc.} + n_n \frac{\partial^n b_s^{(i)}}{\partial p^n}$$

Therefore, when expressed in terms of the derivatives with respect to p, A will be of the form

$$\alpha^{s-\frac{1}{2}}\Big((0)'b_s^{(i)}+(1)'\frac{\partial b_s^{(i)}}{\partial n}+(2)'\frac{\partial^2 b_s^{(i)}}{\partial n^2}+\text{etc.}\Big),$$

from which the derivatives  $\frac{\partial A}{\partial n}$ ,  $\frac{\partial^2 A}{\partial n^2}$ , etc., may be found with great facility.

As in the actual developments of R which we possess, the values of A are given in the form (8), we must find the expression for the first two derivatives of its several terms with respect to p, which we easily do by the application of the symbolic formulæ

$$D_{x} = \alpha D_{a}$$

$$D_{x}^{2} = \alpha (D_{a} + \alpha D_{a}^{2}).$$

Beginning with the case of  $s = \frac{1}{2}$ , we have

$$\frac{\partial b_{\frac{1}{4}}^{(i)}}{\partial n} = \alpha \frac{\partial b_{\frac{1}{4}}^{(i)}}{\partial \alpha}$$

$$\frac{\partial^2 b_{\frac{1}{4}}^{(i)}}{\partial n^2} = \alpha \frac{\partial b_{\frac{1}{4}}^{(i)}}{\partial \alpha} + \alpha^2 \frac{\partial^2 b_{\frac{1}{4}}^{(i)}}{\partial \alpha^2}$$

$$\frac{\partial \left(\alpha^{n} \frac{\partial^{n} b_{\frac{1}{4}}^{(i)}}{\partial \alpha^{n}}\right)}{\partial \nu} = n\alpha^{n} \frac{\partial^{n} b_{\frac{1}{4}}^{(i)}}{\partial \alpha^{n}} + \alpha^{n+1} \frac{\partial^{n+1} b_{\frac{1}{4}}^{(i)}}{\partial \alpha^{n+1}}$$

$$\frac{\partial^{2} \left(\alpha^{n} \frac{\partial^{n} b_{\frac{1}{4}}^{(i)}}{\partial \alpha^{n}}\right)}{\partial \nu^{2}} = n^{2} \alpha^{n} \frac{\partial^{n} b_{\frac{1}{4}}^{(i)}}{\partial \alpha^{n}} + (2n+1) \alpha^{n+1} \frac{\partial^{n+1} b_{\frac{1}{4}}^{(i)}}{\partial \alpha^{n+1}} + \alpha^{n+2} \frac{\partial^{n+2} b_{\frac{1}{4}}^{(i)}}{\partial \alpha^{n+2}}$$

$$= n \frac{\partial \left(\alpha^{n} \frac{\partial^{n} b_{\frac{1}{4}}^{(i)}}{\partial \alpha^{n}}\right)}{\partial \nu} + \frac{\partial \left(\alpha^{n+1} \frac{\partial^{n+1} b_{\frac{1}{4}}^{(i)}}{\partial \alpha^{n+1}}\right)}{\partial \nu}$$

consequently we have for the derivatives of A from formulæ (8)

$$\frac{\partial A}{\partial p} = (0) \alpha \frac{\partial b_{\frac{1}{4}}^{(i)}}{\partial \alpha} + (1) \left( \alpha \frac{\partial b_{\frac{1}{4}}^{(i)}}{\partial \alpha} + \alpha^2 \frac{\partial^2 b_{\frac{1}{4}}^{(i)}}{\partial \alpha^2} \right) + (2) \left( 2\alpha^2 \frac{\partial^2 b_{\frac{1}{4}}^{(i)}}{\partial \alpha^2} + \alpha^3 \frac{\partial^3 b_{\frac{1}{4}}^{(i)}}{\partial \alpha^3} \right) + \text{etc.}$$

$$\frac{\partial^2 A}{\partial p^2} = (0) \left( \alpha \frac{\partial b_{\frac{1}{4}}^{(i)}}{\partial \alpha} + \alpha^2 \frac{\partial^2 b_{\frac{1}{4}}^{(i)}}{\partial \alpha^2} \right) + (1) \left( \alpha \frac{\partial b_{\frac{1}{4}}^{(i)}}{\partial \alpha} + 3\alpha^2 \frac{\partial^2 b_{\frac{1}{4}}^{(i)}}{\partial \alpha^2} + \alpha^3 \frac{\partial^3 b_{\frac{1}{4}}^{(i)}}{\partial \alpha^3} \right) + \text{etc.}$$
(9)

The derivatives of A being formed in this way, those of h are immediately deduced from the equations

$$rac{\partial h}{\partial n} = \Sigma E rac{\partial A}{\partial n},$$
 $rac{\partial^2 h}{\partial p^2} = \Sigma E rac{\partial^2 A}{\partial p^2}.$ 

When s is equal to  $\frac{3}{2}$ , A is of the form

$$\alpha \left\{ (0') b_{\frac{3}{2}}^{(i)} + (1)' \alpha \frac{\partial b_{\frac{3}{2}}^{(i)}}{\partial \alpha} + (2)' \alpha^3 \frac{\partial b_{\frac{3}{2}}^{(i)}}{\partial \alpha^2} + \text{etc.} \right\}$$

The quantity within parentheses is of the same form with A, in the case of  $s = \frac{1}{2}$ . If we represent it by A' we shall have

$$\frac{\partial A}{\partial n} = \alpha \left( \frac{\partial A'}{\partial n} + A' \right) = \alpha \frac{\partial A'}{\partial n} + A$$
$$\frac{\partial^2 A}{\partial n^3} = A + 2\alpha \frac{\partial A'}{\partial n} + \alpha \frac{\partial^2 A'}{\partial n^2}$$

A' being the same form with A, the derivatives  $\frac{\partial A'}{\partial n}$  and  $\frac{\partial^2 A'}{\partial n^2}$  will be of the form (9), substituting  $\frac{3}{2}$  for the index  $\frac{1}{2}$ , and (0)', (1)', etc., for (0), (1), etc.

In the case of  $s = \frac{5}{2}$  the derivatives are obtained in the same way, which is too simple to need elucidation.

We have now to pass from the derivatives of h to those of  $\frac{mh}{a_1}$ , the coefficients of the perturbative function. The form of these derivatives will depend not on whether the planet is disturbing or disturbed, but on whether it is an outer or

inner one. Let us then suppose for the present, that a and p refer to the inner planet, and put  $p_1$  for the logarithm of the mean distance of the outer one. We then have for the derivatives relatively to p

$$\frac{\partial^n \frac{h}{a_1}}{\partial n^n} = \frac{1}{a_1} \frac{\partial^n h}{\partial n^n},$$

and for the first derivative relatively to v, using the symbolic notation,

$$\frac{\partial \frac{h}{a_1}}{\partial p_1} = \frac{1}{a_1} (D_{a_1} - 1) h.$$

The symbols in the second member being distributive, we have by successive differentiation

$$\frac{\partial^n \frac{h}{a_1}}{\partial n_1^n} = \frac{1}{a_1} (D_{n_1} - 1)^n h.$$

The quantity h is a function of  $\alpha$ , the ratio of the mean distances or of  $C^{\nu-\nu_1}$ , C being the neperian base. Hence

$$D_{v_1}h = -D_vh,$$

which substituted in the last equation gives

$$\frac{\partial^n \frac{h}{a_1}}{\partial n_1^n} = \frac{(-1)^n}{a_1} (D_n + 1)^n h. \tag{10}$$

This formula gives for the first two derivatives

$$\frac{\partial \frac{h}{a_1}}{\partial n_1} = -\frac{1}{a_1} \left( h + \frac{\partial h}{\partial n} \right)$$

$$\frac{\partial^2 \frac{h}{a_1}}{\partial n_1^2} = \frac{1}{a_1} \left( h + 2 \frac{\partial h}{\partial n} + \frac{\partial^2 h}{\partial n^2} \right).$$

In order to compute the perturbations of the second order we must carry R and such of its derivatives as enter into the differential equations (1) to quantities of the first order with respect to the perturbations. Let us then represent by  $v_0$ ,  $v_0'$ ,  $\rho_0$ ,  $\rho'_0$ 

added to  $v_0$ ,  $v_0'$ , etc., to make the true values of v, v', etc., whether perturbations or corrections of the elements. We shall then have

$$\delta R = \frac{\partial R_0}{\partial \mathbf{v}_0} \delta \mathbf{v} + \frac{\partial R_0}{\partial \mathbf{v}_0'} \delta \mathbf{v}' + \frac{\partial R_0}{\partial \rho_0} \delta \rho + \frac{\partial R_0}{\partial \rho_0'} \delta \rho' + \frac{\partial R_0}{\partial \gamma_0} \delta \gamma 
\delta \frac{\partial R}{\partial \mathbf{v}} = \frac{\partial^2 R_0}{\partial \mathbf{v}_0^2} \delta \mathbf{v} + \frac{\partial^2 R_0}{\partial \mathbf{v}_0 \partial \mathbf{v}_0'} \delta \mathbf{v}' + \frac{\partial^2 R_0}{\partial \mathbf{v}_0 \partial \rho_0} \delta \rho + \frac{\partial^2 R_0}{\partial \mathbf{v}_0 \partial \rho_0'} \delta \rho' + \frac{\partial^2 R_0}{\partial \mathbf{v}_0 \partial \gamma_0} \delta \gamma 
\delta \frac{\partial R}{\partial \rho} = \frac{\partial^2 R_0}{\partial \rho_0 \partial \mathbf{v}_0} \delta \mathbf{v} + \frac{\partial^2 R_0}{\partial \rho_0 \partial \mathbf{v}_0'} \delta \mathbf{v}' + \frac{\partial^2 R_0}{\partial \rho_0 \partial \rho'_0} \delta \rho + \frac{\partial^2 R_0}{\partial \rho_0 \partial \rho'_0} \delta \rho' + \frac{\partial^2 R_0}{\partial \rho_0 \partial \rho'_0} \delta \gamma$$
(11)

The value of  $D_tR$  may be found either by equation (2), or by differentiating with respect to the time as introduced by the co-ordinates of the disturbed planet. When quantities of the first order only are considered the latter operation is very simple, but it is different when terms of the second order come in, because the true longitude of the planet is then expressed in terms not only of its own mean longitude, but also of the mean longitude of all the disturbing planets. The result can still be obtained in the same way by separating all the mean longitudes introduced by the co-ordinates of the disturbed planet from those introduced by the co-ordinates of the differentiation relatively to  $\ell$ .

Let us now resume the equation (4), representing its second member by  $\mu Q$ , so that it becomes

$$\frac{d^{2}\left(r_{0}^{2}\delta\rho\right)}{dt^{2}} + \frac{\mu\left(1+m\right)}{r_{0}^{3}}r_{0}^{2}\delta\rho = \mu Q \tag{12}$$

where

$$Q = 2 \int \!\! D'_{\rm t} R dt + \frac{\partial R}{\partial \rho} - \frac{1}{\mu} \frac{d^2 \left( r_0^{\ 2} \delta \rho^2 \right)}{dt^2} + \frac{1}{2} \frac{\delta \rho^2}{r_0}$$

By the operations already given Q has become a known function of the time.

It is well known that the integration of (12) may be effected by finding two values of  $r_0^2 \delta \rho$  which satisfy this equation when the second member is neglected, or, in other words, by finding two variables x and y which satisfy the equations

$$\frac{d^2x}{dt^2} + \frac{\mu(1+m)}{r_0^3} x = 0,$$

$$\frac{d^2y}{dt^2} + \frac{\mu(1+m)}{r_0^3} y = 0,$$

when the required integral is

$$r_0^2 \delta \rho = \frac{\mu}{x \frac{dy}{dt} - y \frac{dx}{dt}} \left\{ y \int x Q dt - x \int y Q dt \right\}.$$

The above differential equations are satisfied by the rectangular co-ordinates of the planet in its assumed elliptic orbit. The position of the axes of co-ordinates being arbitrary we shall take the line of apsides for the axis of X, the perihelion being on the positive side. If we put

$$e_0 = \sin \psi$$

we have

$$x\frac{dy}{dt} - y\frac{dx}{dt} = \sqrt{a\mu(1+m)\cos\psi} = \frac{\mu(1+m)\cos\psi}{an}$$

Let us, for convenience, replace x and y by two other variables  $\xi$  and  $\eta$  connected with them by the equations

 $x = a\xi,$ <br/> $y = a\eta \cos \psi.$ 

 $\xi$  and  $\eta$  are then functions of the eccentricity and mean anomaly only, and may be developed according to the multiples of the latter. Substituting the last three expressions in the preceding value of  $r_0^2 \delta \rho$  it becomes

$$r_0^2 \delta \rho = \frac{a^3 n}{1+m} \left\{ \eta \int \xi Q dt - \xi \int \eta Q dt \right\}.$$

If we put  $r_1^2$  for the value of  $r_0$  when the mean distance of the planet is put equal to unity, so that  $r_1$ , like  $\xi$  and  $\eta$  contains only the eccentricity and mean anomaly, we shall have

$$\delta \rho = \frac{nr_1^{-2}}{1+m} \left\{ \eta \int \xi a \, Q dt - \xi \int \eta a \, Q dt \right\}$$
 (13)

We must now express  $\xi$  and  $\eta$  in terms of the time, or of the mean anomaly. Putting for the present u for the eccentric and v for the true anomaly, we have, by the theory of the elliptic motion,

$$x = r \cos v = a (\cos u - e),$$
  
 $y = r \sin v = a \cos \psi \sin u,$ 

from which follow

$$\xi = \cos u - e,$$

$$\eta = \sin u.$$

As  $\xi$  and  $\eta$  are to be expressed in the form

$$\xi = \frac{1}{2} \sum p_i \cos ig,$$
  

$$\eta = \frac{1}{2} \sum q_i \sin ig,$$

the finite integrals extending to all values of i from  $-\infty$  to  $+\infty$ , we shall deduce general expressions from  $p_i$  and  $q_i$  arranged according to the power of the eccentricity. Since

$$u = g + e \sin u$$
,

we have by Lagrange's theorem

$$\cos u = \cos g - e \sin^2 g - \frac{e^2}{2!} \frac{\partial \sin^3 g}{\partial g} - \frac{e^3}{3!} \frac{\partial^2 \sin^4 g}{\partial g^2} - \text{etc.};$$

or

$$\cos u = \frac{\sum_{n=0}^{\infty} \frac{e^n}{n!} \frac{\partial^{n-1} \sin^{n+1} g}{\partial g^{n-1}}$$

using the notation

$$n! = 1.2.3 \dots n = \Gamma(n+1).$$

We then have

$$0! = 1! = 1.$$

Substituting in the general term of the above series for  $\sin g$  its value in imaginary exponential functions

$$2 \sin g = \sqrt{-1} (c^{-g\sqrt{-1}} - c^{g\sqrt{-1}})$$

we find by the binomial theorem, using the notation of combinations,

$$\overset{\bullet}{C} = \frac{n (n-1) \dots (n-s+1)}{1 \cdot 2 \cdot 3 \dots s} = \frac{n!}{s! (n-s)!}$$

$$2^{n+1} \sin^{n+1} g = (\sqrt{-1})^{n+1} \left\{ e^{-(n+1)g\sqrt{-1}} - \overset{1}{C} e^{-(n-1)g\sqrt{-1}} + \overset{2}{C} e^{-(n-3)g\sqrt{-1}} - \dots + (-1)^n \overset{1}{C} e^{(n-1)g\sqrt{-1}} + (-1)^{n+1} e^{(n+1)g\sqrt{-1}} \right\}$$

Differentiating n-1 times with respect to g, and putting together the first and last terms, the one after the first, and that before the last, and so on, we find

$$-2^{n+1} \frac{\partial^{n-1} \sin^{n+1} g}{\partial g^{n-1}} = (n+1)^{n-1} \left( c^{(n+1)g\sqrt{-1}} + c^{-(n+1)g\sqrt{-1}} \right)$$
$$-\frac{c}{n+1} (n-1)^{n-1} \left( c^{(n-1)g\sqrt{-1}} + c^{-(n-1)g\sqrt{-1}} \right) + \text{etc.}$$

Substituting for the exponentials their values in circular functions, and dividing by  $2^{n+1}$  we have

$$\frac{\partial^{n-1} \sin^{n+1} g}{\partial g^{n-1}} = -\frac{1}{2^n} \left\{ (n+1)^{n-1} \cos(n+1) g - \frac{1}{C} (n-1)^{n-1} \cos(n-1) g + \frac{2}{C} (n-3)^{n-1} \cos(n-3) g - \text{etc.} \right\}$$

the series terminating at the last positive coefficient of g. Substituting this last value in the general term of the series which gives  $\cos u$ , we have

$$\cos u = \sum_{n=0}^{n=\infty} \frac{e^n}{n! \, 2^n} \left\{ (n+1)^{n-1} \cos (n+1) \, g - \frac{1}{C} (n-1)^{n-1} \cos (n-1) \, g + \text{etc.} \right\}$$

Let us now substitute for n another variable i, putting in the first term of the last factor i = n + 1, in the second i = n - 1, in the third i = n - 3, etc. The limits of finite integration with respect to i will then be

in the first term, 
$$+1$$
 to  $+\infty$ , in the second term,  $-1$  to  $+\infty$ , in the third term,  $-3$  to  $+\infty$ , etc.

But all the coefficients of g will then be i, and the formula supposes the factor of  $\cos ig$  to vanish whenever i is zero or negative; whence, those elements of the finite integral in which i is negative must be omitted, and all the terms must be taken between the limits +1 and  $+\infty$ . Making the proposed substitution we have

$$\cos u = \sum_{i=1}^{i-\kappa} \left\{ \frac{i^{i-2}}{(i-1)! \ 2^{i-1}} e^{i-1} - \frac{i^i}{(i+1)! \ 2^{i+1}} \frac{1}{i+2} e^{i+1} + \frac{i^{i+2}}{(i+3)! \ 2^{i+3}} \frac{1}{i+4} e^{i+3} - \text{etc.} \right\} \cos ig$$

$$= \sum_{i=1}^{i-\kappa} \frac{i^{i-2} e^{i-1}}{(i-1)! \ 2^{i-1}} \left\{ 1 - \frac{i^2 e^2}{2^2 \ i(i+1)} \frac{1}{i+2} + \frac{i^4 e^4}{2^4 \ i(i+1)(i+2)(i+3)} \frac{1}{i+4} e^{i-1} - \text{e.c.} \right\} \cos ig$$

We have, therefore, for all values of i different from zero

$$p_{i} = p_{-i} = \frac{i^{i-2}e^{i-1}}{(i-1)! \, 2^{i-1}} \left\{ 1 - \frac{1}{C} \frac{i \, e^{2}}{2^{2}(i+1)} + \frac{2}{C} \frac{i^{3} \, e^{4}}{2^{4}(i+1)(i+2)(i+3)} - \text{etc.} \right\}$$
(14)

To obtain the value of  $p_0$  we remark that the only constant term in  $\cos u$  arises from the term  $-e\sin^2 g$ ; its value is therefore  $-\frac{1}{2}e$ . The constant term in  $\xi = \cos u - e$  is therefore  $\frac{3}{2}e$ , whence

$$p_0 = -3e. (15)$$

The values of  $q_i$  may be obtained in a similar way by developing  $\sin u$  by La Grange's theorem. But the development is rather more complex, and it is easier to derive them from  $p_i$ . Let us take up the equations

$$\xi = \cos u - e$$

$$\eta = \sin u$$

$$u - e \sin u = g$$

Considering u, like  $\xi$  and  $\eta$ , as a function of the independent variables e and g, we have by differentiation

$$\frac{\partial u}{\partial e} - \frac{\partial (e \sin u)}{\partial e} = 0$$

$$\therefore \frac{\partial u}{\partial e} = \frac{\partial (e\eta)}{\partial e} = \frac{\sin u}{1 - e \cos u}$$

$$\frac{\partial u}{\partial g} = \frac{1}{1 - e \cos u}$$

$$\therefore \frac{\partial u}{\partial e} = \sin u \frac{\partial u}{\partial g} = -\frac{\partial \xi}{\partial u} \frac{\partial u}{\partial g} = -\frac{\partial \xi}{\partial g}$$
(b)

Comparing (a) and (b)

$$\frac{\partial \xi}{\partial g} = -\frac{\partial (e\eta)}{\partial e}$$

Putting in this equation for  $\xi$  and  $\eta$  their developed values this equation becomes

$$\sum i p_i \sin ig = \sum \frac{\partial (eq_i)}{\partial e} \sin ig$$

which gives by equating the coefficients of sin ig

$$q_i = \frac{i}{e} \int p_i de. \tag{16}$$

The following are special values of  $p_i$  and  $q_i$ , developed to the sixth power of the eccentricities, as derived from the preceding formulæ:

$$p_{0} = -3e$$

$$p_{1} = 1 - \frac{3}{8}e^{2} + \frac{5}{192}e^{4} - \frac{7}{9216}e^{6}$$

$$p_{2} = \frac{1}{2}e - \frac{1}{3}e^{3} + \frac{1}{16}e^{5}$$

$$p_{3} = \frac{3}{8}e^{2} - \frac{45}{128}e^{4} + \frac{567}{5120}e^{6}$$

$$p_{4} = \frac{1}{3}e^{3} - \frac{6}{15}e^{5}$$

$$p_{5} = \frac{125}{384}e^{4} - \frac{4375}{9216}e^{6}$$

$$p_{6} = \frac{27}{80}e^{5}$$

$$p_{7} = \frac{16807}{46080}e^{6}$$

$$q_{1} = 1 - \frac{1}{8}e^{2} + \frac{1}{192}e^{4} - \frac{1}{9216}e^{6}$$

$$q_{3} = \frac{1}{2}e - \frac{1}{6}e^{3} + \frac{1}{48}e^{5}$$

$$q_{3} = \frac{3}{8}e^{2} - \frac{27}{128}e^{4} + \frac{243}{5120}e^{6}$$

$$q_{4} = \frac{1}{3}e^{3} - \frac{4}{15}e^{5}$$

$$q_{5} = \frac{125}{384}e^{4} - \frac{3125}{9216}e^{6}$$

$$q_{6} = \frac{27}{80}e^{5}$$

$$q_{7} = \frac{16807}{46080}e^{5}$$

Having the developed  $\xi$  and  $\eta$  in terms of time, let us resume the equation (13). As only purely linear operations are performed on Q in this equation, it follows that if we represent its several parts by  $Q_1$ ,  $Q_2$ , etc., and by  $\delta \rho_1$ ,  $\delta \rho_2$ , etc., the values  $\delta \rho$  obtained by putting  $Q = Q_1$ ,  $Q = Q_2$ , etc., we shall have

$$\delta \rho = \delta \rho_1 + \delta \rho_2 + {\rm etc.}$$

We have, therefore, only to find the separate values of  $r_0^2 \delta \rho$  corresponding to the different terms of Q, and to take their sum. Let us then represent, as before, by

$$\frac{m'}{a_1}h\cos(i'\lambda'+i\lambda+j'\omega'+j\omega)$$

any one term of R. 3 April, 1873.

We then have, considering only terms of the first order with respect to the dis-

turbing forces,

$$D_{t}R = -\frac{m'i\hbar n}{a_{1}}\sin N,$$

$$\int D_{t}R = \frac{m'i\hbar \nu}{a_{1}}\cos N;$$

$$\frac{\partial R}{\partial \rho} = m'\frac{\partial \frac{\hbar}{a_{1}}}{\partial \nu}\cos N;$$
(17)

where we put for brevity,

$$v = \frac{n}{i'n' + in}$$

$$N = i'\lambda' + i\lambda + j'\omega' + j\omega.$$

Let us represent by  $Q_0$  the terms in Q which are of the first order with respect to the disturbing forces, so that we have

$$Q_0 = 2 \int D_{\iota} R_0 + \frac{\partial R_0}{\partial \rho_0}.$$

The general term in R will then give rise in  $Q_0$  to the term

$$m'\left(\frac{2ih\nu}{a_1}+\frac{\partial\frac{h}{a_1}}{\partial p}\right)\cos N.$$

In the case of the action of an outer on an inner planet this expression becomes

$$\frac{m'}{a_i} \left( 2i\nu h + \frac{\partial h}{\partial p} \right) \cos N;$$

while in the contrary case it is

$$\frac{m'}{a_1} \left( 2ivh - h - \frac{\partial h}{\partial n'} \right) \cos N,$$

both derivatives being taken with respect to the logarithm of the mean distance of the inner planet.

In the integration it will be more convenient to substitute for  $\lambda'$  and  $\lambda$  the mean longitudes counted from the perihelion of the disturbed planet. If we put

$$\lambda = g + \omega$$
$$\lambda' = l' + \omega$$

the angle N will become,

$$i'l' + ig + j'\omega' + (i + i' + j)\omega.$$

Since corresponding to each set of values of i and i there are several values of j and j, it will be convenient in the numerical computation to combine these different terms into a single one, because after forming the derivatives of R there is no need that  $\omega$ ,  $\omega$  and the other elements should appear in an analytical form. If we put

k for the coefficient of  $\frac{m'}{a_1}\cos N$  in the preceding general term of  $Q_0$ , this term will become

$$Q_0 = \frac{m'}{a_1} k \cos \left[ j'\omega' + (i'+i+j)\omega \right] \cos \left[ il' + ig \right]$$
$$-\frac{m'}{a_1} k \sin \left[ j'\omega' + (i'+i+j)\omega \right] \sin \left[ il' + ig \right]$$

If we put

$$k_c = \sum k \cos [j'\omega' + (i'+i+j)\omega],$$
  
 $k_s = \sum k \sin [j'\omega' + (i'+i+j)\omega],$ 

the sign  $\Sigma$  being extended so as to include all values of j and j' which correspond to the given values of i and i', we shall have for the general terms of  $Q_0$ 

$$\frac{m'}{a_1} \left\{ k_e \cos (i'l' + ig) + k_s \sin (i'l' + ig) \right\},\,$$

or, when we represent the angle il'+ig by  $N_1$ 

$$Q_0 = \frac{m'}{a_1} \left\{ k_c \cos N_1 + k_s \sin N_1 \right\}.$$

This we are to combine with the values of  $\xi$  and  $\eta$ 

$$\xi = \frac{1}{2} \sum p_i \cos ig,$$
 $\eta = \frac{1}{2} \sum q_j \sin jg,$ 

in the general integral formula (13). If we substitute them in this formula, and represent by  $\mu$  the coefficient of t in the value of N we shall have to integrate differentials of the form

$$\sin \left(N_1 \pm ig\right)$$

in which the coefficient of the time t in the angle is  $\mu + in$ . Let us represent by  $v_t$  the integrating factor

$$\frac{n}{\mu + in}$$

The formula (13) will become by these substitutions, which, though a little complex, offer no difficulty,

$$\begin{split} \delta \rho = & \frac{1}{16} \frac{m' a r_1^{-2}}{a_1 \left(1+m\right)} \sum_{-\infty}^{+\infty} p_i q_j \times \\ & \left\{ \begin{aligned} & \left\{ v_{+j} - v_{+i} \right\} \left\{ k_c \cos \left[ N_1 + (i+j)g \right] + k_s \sin \left[ N_1 + (i+j)g \right] \right\} \\ & + \left\{ v_{+i} - v_{-j} \right\} \left\{ k_c \cos \left[ N_1 + (i-j)g \right] + k_s \sin \left[ N_1 + (i-j)g \right] \right\} \\ & + \left\{ v_{+j} - v_{-i} \right\} \left\{ k_c \cos \left[ N_1 - (i-j)g \right] + k_s \sin \left[ N_1 - (i-j)g \right] \right\} \\ & + \left\{ v_{-i} - v_{-j} \right\} \left\{ k_c \cos \left[ N_1 - (i+j)g \right] + k_s \sin \left[ N_1 - (i+j)g \right] \right\} \end{aligned} \end{split}$$

The sign  $\Sigma$  of finite integration here includes the separate combination of every value of i with every value of j, except those combinations which make the

<sup>\*</sup> The indices i and j, in these equations, are not to be confounded with the coefficients of  $\lambda$  and  $\omega$  in the general terms of R and Q. We need not use the latter at present.

coefficient of the time under the sign sin or cos vanish, and so render the corresponding value of  $\nu$  infinite. These cases have to be treated separately.

To find, from the expression, the coefficient of the sine or cosine of cosine  $N_1 + ug$ in  $r_1^2 \delta \rho$ , we put, in the four lines of this equation, as follows:

In the first, 
$$i+j=u$$
  $\therefore$   $j=u-i$ ; second,  $i-j=u$   $\therefore$   $j=i-u$ ; third,  $-i+j=u$   $\therefore$   $j=u+i$ ; fourth,  $-i-j=u$   $\therefore$   $j=-u-i$ .

In the above expressions i and j being independent, and including all values from  $-\infty$  to  $+\infty$ , i and u will also be independent, and include the same range of values. Substituting for j its value in u the coefficient of

$$\frac{1}{16} \frac{m'a r_1^{-2}}{a_i (1+m)} [k_c \cos (N_1 + ug) + k_s \sin (N_1 + ug)]$$

becomes

$$\Sigma \begin{cases} p_i q_{(u-i)} (\nu_{(u-i)} - \nu_i) \\ + p_i q_{(i-u)} (\nu_i - \nu_{(u-i)}) \\ + p_i q_{(u+i)} (\nu_{(u+i)} - \nu_{-i}) \\ + p_i q_{-(u+i)} (\nu_{-i} - \nu_{(u+i)}). \end{cases}$$

Since  $q_j = -q_{-j}$  this expression reduces immediately to

$$2\Sigma \left\{ \begin{array}{c} p_i q_{(i-u)} (\nu_i - \nu_{(u-i)}) \\ + p_i q_{(i+u)} (\nu_{(u+i)} - \nu_{-i}), \end{array} \right.$$

or, substituting i - u for i in the second line

$$2\Sigma \left(p_{i}q_{(i-u)}+p_{(i-u)}q_{i}\right)\left(\nu_{i}-\nu_{u-i}\right).$$
 Hence, writing  $N$  instead of  $N_{i}$ ,

$$\delta \rho = \frac{1}{8} \frac{m' a r_1^{-2}}{a_1 (1+m)} \sum_{i,u}^{2} (p_i q_{(i-u)} + p_{(i-u)} q_i) (\nu_i - \nu_{(u-i)}) [k_c \cos(N + ug) + k_s \sin(N + ug)]$$
(19)

This expression fails for the particular case N = ug, where the value of  $\nu_{-u}$  will be infinite. If we take each term of Q of the form

$$\frac{m'}{a_1}(k_c^{(u)}\cos ug + k_s^{(u)}\sin ug),$$

and substitute in the general expression (13) it will be found that the terms in  $r_1^2 \delta \rho$ which have the infinite values of  $\nu$  as a factor are to be omitted, and replaced by

$$r_1^2 \delta \rho = \frac{1}{2} \frac{m'ant}{a_1(1+m)} \left\{ \eta \sum p_u k_c^{(u)} - \xi \sum q_u k_s^{(u)} \right\}$$
 (20)

The two parts of  $r_1^2 \delta \rho$  thus found include all the terms of the first order with respect to the disturbing forces. But when terms of the second order are taken into account, we shall find terms in Q proceeding from secular variation in which the time appears as a factor, outside the signs sin and cos. Let us represent such of these terms as depend on any angle N by

$$Q = \frac{m'nt}{a_1} (k_c \cos N + k_s \sin N)$$

and use the symbol  $\nu_i$ , as before, to represent the ratio of the mean motion of the planet to the coefficient of t in the angle N+ig, so that if  $\mu'$  represents the coefficients of t in N we have

$$v = \frac{n}{\mu'},$$

$$v_i = \frac{n}{\mu' + in} = \frac{1}{\frac{\mu'}{n} + i},$$

we find the expression

$$\int \xi Q dt = \frac{1}{4} \frac{m' \sum p_i}{a_1 n} \left\{ (\nu_i^2 k_o - \nu_i k_s n t) \cos(N + ig) + (\nu_{-i}^2 k_o - \nu_{-i} k_s n t) \cos(N - ig) \right. \\ \left. (\nu_i^2 k_s + \nu_i k_o n t) \sin(N + ig) + (\nu_{-i}^2 k_s + \nu_{-i} k_o n t) \sin(N - ig) \right\}$$

$$\int \eta Q dt = \frac{1}{4} \frac{m' \sum q_j}{a_1 n} \left\{ (\nu_j^2 k_o - \nu_j k_s n t) \sin(N + jg) - (\nu_{-j}^2 k_o - \nu_{-j} k_s n t) \sin(N - jg) - (\nu_j^2 k_s + \nu_j k_o n t) \cos(N + jg) + (\nu_{-j}^2 k_s + \nu_{-j} k_o n t) \cos(N - jg) \right\}.$$

If we now put for brevity

$$v_i^2 k_s + v_i k_o nt = c_i,$$
  
$$v_i^2 k_o - v_i k_o nt = s_i,$$

the general value of  $r_0^2 \delta \rho$  becomes

$$\delta \rho = \frac{1}{16} \frac{m' a r_1^{-2}}{a_i (1+m)} \times \left\{ \begin{aligned} &(c_j - c_i) \cos \left(N + (i+j)g\right) + (s_i - s_j) \sin \left(N + (i+j)g\right) \\ &+ (c_i - c_{-j}) \cos \left(N + (i-j)g\right) + (s_{-j} - s_i) \sin \left(N + (i-j)g\right) \\ &+ (c_j - c_{-i}) \cos \left(N - (i-j)g\right) + (s_{-i} - s_j) \sin \left(N - (i-j)g\right) \\ &+ (c_{-i} - c_{-j}) \cos \left(N - (i+j)g\right) + (s_{-j} - s_{-i}) \sin \left(N - (i+j)g\right) \end{aligned} \right\}$$

If, as before, we transform this expression by putting

in the first line 
$$j=u-i$$
;  
in the second "  $j=i-u$ ;  
in the third "  $j=i+u$ ;  
in the fourth "  $j=i-u$ .

the value of  $r_1^2 \delta \rho$  reduces to

$$\frac{1}{8} \frac{m'a}{a_{i}(1+m)} \times \sum_{i,u}^{2} \left\{ p_{i}q_{(u-i)}(c_{(u-i)}-c_{i}) \cos(N+ug) + p_{i}q_{(u-i)}(s_{i}-s_{(u-i)}) \sin(N+ug) \right\} \\
p_{i}q_{(u+i)}(c_{(u+i)}-c_{-i}) \cos(N+ug) + p_{i}q_{(u+i)}(s_{i}-s_{(u+i)}) \sin(N+ug) \right\}$$
(21)

or, putting i - u for i in the last line,

$$\delta \rho = \frac{1}{8} \frac{m' a r_1^{-2}}{a_1 (1+m)} \times$$

$$\sum_{u,i}^{2} \left\{ p_i q_{(u-i)} - p_{(u-i)} q_i \right\} \left\{ (c_{(u-i)} - c_i) \cos (N + ug) + (s_i - s_{u-i}) \sin (N + ug) \right\};$$

to which expression is to be added, in lieu of the terms which will have infinite values of  $\nu$  as a factor.

$$\frac{1}{4} \frac{m' a r_1^{-2} n^2 t^2}{a_i (1+m)} \left\{ \eta \sum p_u k_c^{(u)} - \xi \sum q_u k_s^{(u)} \right\}$$
 (22)

 $k_c^{(u)}$  and  $k_s^{(u)}$  being the factors of  $\frac{m'}{a_1}nt\cos ug$  and  $\frac{m'}{a_1}nt\sin ug$  in the expression for Q.

The formulæ 19, 20, 21, and 22 give the complete expressions for the perturbations of the logarithm of radius vector by successively substituting in it all the terms of Q.

#### Perturbations of Longitude.

We now pass to the perturbations of longitude. In the Mécanique Céleste (Première Partie, Liv. ii. Chap. vi.), Laplace gives an equation (Y) by which the perturbations of longitude, which are of the first order, may be derived from those of the radius vector without the formation of any other derivatives of R than those which enter into Q. But the formula does not seem easily adapted to the case in which the perturbations of the second order are taken into account, we shall therefore derive all the perturbations of longitude from the second of equations (1). By integration this equation gives

$$\frac{dv}{dt} = \frac{\mu}{r^2} \left\{ \int \frac{\partial R}{\partial \mathbf{v}} dt + C \right\}$$

C being the arbitrary constant of the integral. Representing, as before, by subscript zeros the values of the co-ordinates corresponding to the ellipse to which the orbit is supposed to reduce itself when the disturbing forces vanish, we have

$$\frac{dv_0}{dt} = \frac{a^2 n \cos \psi}{r_0^2} = \frac{\mu C}{r_0^2},$$

because the constant to which the integral must reduce itself in the elliptic motion is  $\frac{a^2n\cos\psi}{\mu}$ . Subtracting the last equation from the preceding, and putting  $v-v_0=\delta v$ , we find

$$\frac{d\delta v}{dt} = \frac{\mu}{r^2} \int_{\partial V}^{\partial R} dt + \left(\frac{1}{r^2} - \frac{1}{r_0^2}\right) a^2 n \cos \psi.$$

Developing  $\frac{1}{x^2}$  to terms of the second order with respect to the disturbing force

$$\frac{1}{r^2} = \frac{1}{r_0^2} \left( 1 - 2\delta \rho + 2\delta \rho^2 - \text{etc.} \right),$$

which, being substituted in the last equation by putting

$$\mu = \frac{a^3 n^2}{1+m},$$

$$r_0^2 = a^2 r_1^2,$$

gives

$$r_1^2 \frac{d\delta v}{dt} = \frac{an^2}{1+m} (1-2\delta\rho) \int \frac{\partial R}{\partial v} dt - 2n \cos\psi (\delta\rho - \delta\rho^2), \qquad (23)$$

which is rigorous to quantities of the second order.

The most convenient mode of making the numerical computation of the second order terms by means of this equation will depend upon circumstances. If the perturbations of longitude and radius vector of both planets are already known with a sufficient degree of approximation for the computation of formula (11), it will be more convenient to form at once the complete values of all the quantities which enter into the equations (12), (13), (19) to 22), and (23), so that no steps of the process shall have to be repeated. If such perturbations are not known, they must first be computed, and it will then be necessary to begin with the perturbations of the first order, and afterward add those of the second. There is, however, one class of terms of the second order which it will be most convenient to take account of from the beginning, namely, those arising from the constant term in  $\delta \rho$  and  $\delta \rho'$ . This is effected by correcting the mean distances for an approximate value of these constants at the beginning of the computation, and then proceeding in the usual way. This is in fact what we have supposed to be done in the preceding investigation. The values of  $\delta v$ ,  $\delta v$ ,  $\delta \rho$ ,  $\delta \rho'$  in formula (11) will then contain only periodic terms.

In computing the terms of the first order we determine the value of  $\delta \rho$  from the equations (19) and (20), using the value of  $Q_0$  in (18). Then those of  $\delta v$  are obtained by integrating the equation

$$\frac{d\delta v}{dt} = \frac{an^2 r_1^{-2}}{1+m} \int \frac{\partial R_0}{\partial v} dt - 2n \cos \psi \frac{\delta \rho}{r_1^{-2}}.$$
 (24)

Having found the values of  $\delta v$  and  $\delta \rho$  for both planets, they are to be substituted in (11), to obtain  $\delta R$ ,  $\delta \frac{\partial R}{\partial v}$  and  $\delta \frac{\partial R}{\partial \rho}$ . But, rigorously,  $\delta v$  and  $\delta v'$  are not the same with  $\delta v$  and  $\delta v'$ , owing to the movement of the orbits of the planets, and the corrections for  $\delta \gamma$  are also to be added. Considering, for the present, only the perturbations of the second order, which depend on  $\delta v$ ,  $\delta v'$ ,  $\delta \rho$ , and  $\delta \rho'$ , we may use the following equation for  $\delta R$ , and similar ones for its derivatives:

$$\delta R = \frac{\partial R}{\partial \mathbf{v}} \, \delta \mathbf{v} + \frac{\partial R}{\partial \mathbf{v}'} \, \delta \mathbf{v}' + \frac{\partial R}{\partial \rho} \, \delta \rho + \frac{\partial R}{\partial \rho'} \, \delta \rho'. \tag{25}$$

Having thus found  $\delta R$ , and hence  $D_t \delta R$  by differentiation, and then  $\delta \frac{\partial R}{\partial \rho}$ , we form the quantity

 $\delta Q = 2 \int D_t \delta R dt + \delta \frac{\partial R}{\partial \rho} - \frac{1}{\mu} \frac{d^2 (r_0^2 \delta \rho^2)}{dt^2} + \frac{1}{2} \frac{\delta \rho^2}{r_0}$  (26)

which is the difference between the value of  $Q_0$  in (18) and that of Q in (12). The terms in  $\delta\rho$  arising from  $\delta Q$  are then to be computed by the formulæ (19), (20), (21), and (22), when we shall have  $\delta\rho$  accurate to quantities of the second order. Let us represent these additional terms by  $\delta^2\rho$ . Subtracting (24) multiplied by  $r_1^2$  from (23), recollecting that the  $\delta\rho$  which appears in the second term of the former is really  $\delta\rho - \delta^2\rho$ , we find, neglecting quantities of the third order,

$$r_1^2 \frac{d\delta^2 v}{dt} = an^2 \left\{ \int \delta \frac{\partial R}{\partial v} dt - 2\delta \rho \int \frac{\partial R_0}{\delta v} dt \right\} - 2n \cos \psi \left( \delta^2 \rho - \delta \rho^2 \right)$$

from which the terms of  $\delta v$  of the second order are obtained by multiplying by  $r_1^{-2}$  and integrating.

#### Motion of the Orbital Planes.

The general theory of the motion of the planes of reference, especially of the motion of the instantaneous orbit, has been so often treated that I can scarcely hope to add anything essentially new to it. I shall, however, endeavor to present the differential equations of the motion in a simple and general form, and one in which the geometrical conceptions of the problem shall be made as clear as possible.

The orbital plane of each planet being at each moment osculatory to that part of the orbit which the planet is actually describing, its only motion is one of rotation around the radius vector of the planet as an instantaneous axis. This rotation may be resolved into two others around any pair of rectangular axes fixed in the moving plane. But the rotation produced by any one planet is most simply expressed when referred to axes, one of which coincides with the common node of the two orbits. The rotation produced by each separate planet must, therefore, be first referred to its node on the moving orbit, and then the combined rotations must be resolved into two around axes assumed at pleasure. To effect this, let us suppose positive rotation around an axis to be such that an observer looking from the origin along the positive direction of the axis sees the right hand side of the plane move downwards, and the left hand side upwards. Let us also denote the first axis in the order of longitude the principal axis, or that of X, and that  $90^{\circ}$  farther advanced the secondary axis, or that of Y. Let us now put

dq, the instantaneous rotation around the axis of X;

dp, the instantaneous rotation around the axis of Y. Let us also put, relatively to any disturbing planet,

 $d\eta$ , the instantaneous rotation around the ascending node of the disturbing planet on the orbit of the disturbed one.

dk, that around the corresponding secondary axis.

Then, from the known equations for the perturbations of the inclination and node of an orbit, we find, that, if any term of the perturbative function be represented, as before, by

$$\frac{m'h}{a_1}\cos(i'\lambda'+i\lambda+j'\omega'+j\omega),$$

the differential rotations  $\eta$  and k will be given by the equations

$$\frac{d\eta}{dt} = -\frac{m'h}{a_1} \frac{an}{\cos\psi} \left\{ (i+j)\cot\gamma + (i'+j')\csc\gamma \right\} \sin N$$

$$\frac{dk}{dt} = -\frac{m'an}{a_1\cos\psi} \frac{\partial h}{\partial \gamma} \cos N.$$

As R is actually developed, the mutual inclination  $\gamma$  does not explicitly appear, but is replaced by

$$\sigma = \sin \frac{1}{2} v$$
.

Making this substitution, and putting also

$$i+i+j+j=-\iota$$

these equations become

$$\frac{d\eta}{dt} = \frac{m'an}{a_1 \cos \psi \cos \frac{1}{2}\gamma} \left\{ \frac{dh}{2\sigma} + (i+j)\sigma h \right\} \sin N$$

$$\frac{dk}{dt} = -\frac{m'an \cos \frac{1}{2}\gamma}{2a_1 \cos \psi} \frac{\partial h}{\partial \sigma} \cos N.$$
(27)

To pass to the general rotations dp and dq, let us represent by  $\theta_1$ ,  $\theta_2$ , etc., the longitudes of the ascending nodes of the several orbits of the disturbing planets on that of the disturbed planet. We shall then have

$$\frac{dq}{dt} = \sum \cos \theta_i \frac{d\eta_i}{dt} - \sum \sin \theta_i \frac{dk_i}{dt}$$

$$\frac{dp}{dt} = \sum \cos \theta_i \frac{dk_i}{dt} + \sum \sin \theta_i \frac{d\eta_i}{dt}.$$
(28)

These equations completely define the instantaneous motion of the orbital plane. They cannot, however, be rigorously integrated in their present form because p and q as integrals have no completely defined signification. To do this it is necessary to express the differential rotations dp, dq, etc., in terms of the differentials of any elements we may select to define the position of the orbital plane, and then to integrate the equations thus formed. But, for the purpose of constructing tables of the planets we may consider p, q, etc., to represent small rotations of the planes of which the powers and products may be neglected, and the integration is then quite simple.

Perturbations of the second order depending on the motion of the orbital planes.

R being a function of the five quantities of r, r', v, v', and  $\gamma$ , the motion of the orbital planes introduces terms of the second order by changing the values of v, v', and  $\gamma$ . These terms we have hitherto neglected. To investigate them let us refer the rotations of both planes as given by (28) to the node of the disturbing on the disturbed planet as the principal axis. If we represent by  $d\eta$ , dk,  $d\eta'$ , and dk' the rotations corresponding to this axis, and designate by the subscript 1, the quantities which refer to the disturbing planet whose action we are considering, and by 2, 3, etc., the other planets, the equations (28) will be replaced by these

$$\frac{d\eta}{dt} = \frac{d\eta_1}{dt} + \Sigma \cos(\theta_i - \theta_1) \frac{d\eta_i}{dt} - \Sigma \sin(\theta_i - \theta_1) \frac{dk_i}{dt},$$

$$\frac{dk}{dt} = \frac{dk_1}{dt} + \Sigma \cos(\theta_i - \theta_1) \frac{dk_i}{dt} + \Sigma \sin(\theta_i - \theta_1) \frac{d\eta_i}{dt},$$

the summation commencing with i=2.

By formulæ of the same kind we are to find the differential rotations  $d\eta'$  and dk' of the orbit of the disturbing planet, produced by the action of all the planets.

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These rotations will be around the same principal axis with the rotations  $d\eta$  and dk, but around a secondary axis in the plane of the disturbing orbit, and therefore making an angle  $\gamma$  with the secondary axis of the disturbed orbit. A geometrical construction will now show quite simply that the infinitesimal rotations  $\delta\eta$ ,  $\delta k$ ,  $\delta\eta'$ , and  $\delta k'$  will produce the following changes in v, v', and  $\gamma$ .

$$\delta v = \cot \gamma \delta k - \csc \gamma \delta k'$$

$$\delta v' = \csc \gamma \delta k - \cot \gamma \delta k'$$

$$\delta \gamma = \delta \eta' - \delta \eta$$
(29)

If we substitute these values in the general formulæ (11) the terms of the second order added to  $\delta R$  will be

$$\delta R = \left(\frac{\partial R}{\partial \mathbf{v}} \cot \gamma + \frac{\partial R}{\partial \mathbf{v}'} \csc \gamma\right) \delta k$$

$$- \left(\frac{\partial R}{\partial \mathbf{v}} \csc \gamma + \frac{\partial R}{\partial \mathbf{v}'} \cot \gamma\right) \delta k'$$

$$+ \frac{\partial R}{\partial \gamma} (\delta \eta' - \delta \eta).$$
(30)

The first two terms of this expression may be put into the form

$$\left\{ \frac{1}{2} \left( \frac{\partial R}{\partial v} + \frac{\partial R}{\partial v'} \right) (\csc \gamma + \cot \gamma) - \frac{1}{2} \left( \frac{\partial R}{\partial v} - \frac{\partial R}{\partial v'} \right) (\csc \gamma - \cot \gamma) \right\} \delta k$$

$$- \left\{ \frac{1}{2} \left( \frac{\partial R}{\partial v} + \frac{\partial R}{\partial v'} \right) (\csc \gamma + \cot \gamma) + \frac{1}{2} \left( \frac{\partial R}{\partial v} - \frac{\partial R}{\partial v'} \right) (\csc \gamma - \cot \gamma) \right\} \delta k.$$
But,

$$\cos c \gamma + \cot \gamma = \cot \frac{1}{2} \gamma = \frac{\cos \frac{1}{2} \gamma}{\sigma}.$$

$$\csc \gamma - \cot \gamma = \tan \frac{1}{2} \gamma = \frac{\sigma}{\cos \frac{1}{2} \gamma}$$

and in the general term of R, by (7)

$$\frac{\partial R}{\partial \mathbf{v}} = -\frac{m'h}{a_1}(i+j)\sin N$$

$$\frac{\partial R}{\partial \mathbf{v}'} = -\frac{m'h}{a_1}(i'+j')\sin N.$$

Making these substitutions, and putting, as before,

$$i+j+i+j'=-\iota$$

the above value of  $\delta R$  reduces to

$$\delta R = \frac{m'h}{2a_1} \left\{ \iota \cot \frac{1}{2} \gamma \left( \delta k - \delta k' \right) + \left( i + j - i' - j' \right) \tan \frac{1}{2} \gamma \left( \delta k + \delta k' \right) \right\} \sin N + \frac{m' \cos \frac{1}{2} \gamma}{2a_1} \frac{\partial h}{\partial \sigma} \left( \delta \eta' - \delta \eta \right) \cos N$$
(31)

The corresponding terms of  $\delta \frac{\partial R}{\partial v}$  and  $\delta \frac{\partial R}{\partial \rho}$ , and may be obtained in the same way

by substituting  $\frac{\partial R}{\partial \mathbf{v}}$  and  $\frac{\partial R}{\partial \rho}$  for R in (30) and continuing the corresponding sub-

stitutions of the general terms of the derivatives of R as given on page 9. The equation (31), besides being of the second order with respect to the disturb-

ing forces, is also of the second order with respect to the mutual inclinations. For  $\delta k$ ,  $\delta k'$ ,  $\delta \eta$ , and  $\delta \eta'$  are of the first order with respect to both quantities, and, whenever  $\iota$  is not zero, h is a quantity of the second order, containing  $\sigma^2$  as a factor. It is, therefore, only in exceptional cases that the terms of the second order depending on the motion of the orbital planes can become sensible.

## Reduction of the longitude in the orbit to lo gitude on the ecliptic.

The integration of (23) gives a value of  $\delta v$ , which, added to the longitude in orbit corresponding to the pure elliptic motion gives the longitude in the disturbed orbit, counted from a fixed point in the moving plane of that orbit. The position of this fixed point is completely determined by the condition that the instantaneous rotation of the plane in question around the axis perpendicular to itself is always zero, so that the motion of the point of reference is always perpendicular to the direction of the plane. But, although this instantaneous rotation is zero, the integrated rotation is not rigorously zero when we consider the terms of the second order. It follows that the value of v, the longitude in orbit, and the position of the plane of the orbit do not rigorously determine the position of the planet: we must also know how the fixed point of reference has changed its position in consequence of the motions which the plane has undergone. Let us consider the relative positions of this plane at two epochs. If the fixed point were equally distant from the common node of the two planes, the integrated rotation of the plane around its own axis would be zero. But, these distances not being equal, their difference is a correction to be applied to the longitude of the planet in its Suppose, now, that at the end of any time the inclination of the actual orbit to the primitive orbit is  $\phi$ , and the distance of its ascending node from the present position of the moving axis of x is  $\theta$ . A rotation around the line of nodes will not change the quantity sought. But, if we represent the infinitesimal rotation around an axis perpendicular to it by dr we shall have

$$\cos\theta dp - \sin\theta dq = dr,$$

dq and dk being the instantaneous rotations around the respective axes of x and  $\gamma$ . By this rotation it is easy to see that the relative distance of any two fixed points, one on each plane, from the node, will be altered by the quantity,

$$dr (\operatorname{cosec} \phi - \cot \phi) = dr \tan \frac{1}{2} \phi,$$

the relative longitude of the fixed point on the moving plane being increased by The correction to the longitude in orbit from this cause is, therefore,

$$dl = dr \tan \frac{1}{2} \phi = \tan \frac{1}{2} \phi (\cos \theta dp - \sin \theta dq).$$

Counting the integrated values of p and q in a direction perpendicular to the moving plane we have

$$\sin \theta = \frac{\tan p}{\tan \phi}$$

$$\cos \theta = \frac{\tan q}{\tan \phi}$$

which, being substituted in the expression for dl, gives

$$dl = \frac{\cos \phi}{1 + \cos \phi} (\tan q dp - \tan p dq).$$

The approximate value of the integrated correction is therefore

$$\delta l = \frac{1}{2} \int (qdp - pdq). \tag{32}$$

For every pair of periodic terms in p and q, such as

$$q = s \sin \mu t, p = s \cos \mu t,$$

 $\delta l$  will contain the secular term  $-\frac{1}{2} s^2 \mu t$ , which will be confounded with the mean motion, and, if it were not so confounded, would in few or none of the larger planets amount to a second in a thousand years. If the secular terms in p and q be

$$q = st$$
;  $p = s't$ 

El will vanish. We hence conclude that these terms are entirely unimportant in the present state of astronomy, and that, if we consider the positions of the plane of the orbit at two epochs, we may consider the points of departure in them to be equally distant from their common node.

We have therefore only to consider the motion of the inclination and node due to the change of the position of the orbit and of the ecliptic. If we put

 $\phi$ , the inclination of the orbit of the planet to the ecliptic,

 $\theta$ , the longitude of its node counted on the ecliptic,

 $\tau$ , the longitude of the same node counted from the same fixed point in the moving plane of the orbit from which v is counted,

Then, the longitude of the planet on the ecliptic, or L, will be given by the equation

$$\tan (L - \theta) = \cos \phi \tan (v - \tau),$$

or, when developed in powers of  $\phi$ ,

$$L = v + \theta - \tau + D, \tag{33}$$

where D is the reduction to the ecliptic, the value of which is

$$D = -\tan^2 \frac{1}{2} \phi \sin 2 (v - \tau) + \frac{1}{2} \tan^4 \frac{1}{2} \phi \sin 4 (v - \tau) - \text{etc.}$$

Let us refer the instantaneous rotations of the orbit and of the ecliptic to the fixed points of reference in the two planes; q being the rotation around an axis passing through the sun and the fixed point, and p that around an axis in 90° greater longitude, and the accented quantities referring to the ecliptic. We then have

$$\frac{d\phi}{dt} = \cos \tau \frac{dq}{dt} + \sin \tau \frac{dp}{dt} 
-\cos \theta \frac{dq'}{dt} - \sin \theta \frac{dp'}{dt} 
\frac{d\theta}{dt} = \csc \phi \left( -\sin \tau \frac{dq}{dt} + \cos \tau \frac{dp}{dt} \right) 
+ \cot \phi \left( \sin \theta \frac{dq'}{dt} - \cos \theta \frac{dp'}{dt} \right) 
\frac{d\tau}{dt} = \cot \phi \left( -\sin \tau \frac{dq}{dt} + \cos \tau \frac{dp}{dt} \right) 
+ \csc \phi \left( \sin \theta \frac{dq'}{dt} - \cos \theta \frac{dp'}{dt} \right)$$

If we differentiate (33) and substitute these values of  $\frac{d\theta}{dt}$  and  $\frac{d\tau}{dt}$ , we shall have

$$\frac{dL}{dt} = \frac{dv}{dt} + \frac{dD}{dt} - \tan\frac{1}{2}\phi\left(\cos\tau\frac{dp}{dt} - \sin\tau\frac{dq}{dt} + \cos\theta\frac{dp'}{dt} - \sin\theta\frac{dq'}{dt}\right)$$
(35)

If we consider only quantities of the first order with respect to the disturbing forces, we may, in integrating, suppose  $\tau$  and  $\theta$  equal and constant, and  $\phi$  constant. The integral will then be

$$L = v + D + \tan \frac{1}{2} \phi \left\{ \cos \theta \left( \delta k + \delta k' \right) - \sin \theta \left( \delta \eta + \delta \eta' \right) \right\}$$
 (36)

In the case of Uranus,  $\tan \phi$  is so small that this equation will be sufficient for a long time before and after our epoch.

In the application of the method to other planets the mode of operation must depend on the circumstances of each particular case. The differential equations (34) between  $\theta$ ,  $\tau$ , and  $\phi$  are rigorous, and their integrals may be approximated to in various ways, out of which that best applicable to the particular case must be selected.

## Expressions for the latitude.

If the position of the orbital plane and of the ecliptic were each determined by the preceding formulæ, there would be no perturbations of the latitude, the latitude itself being given rigorously by the equation

$$\sin \beta = \sin \phi \sin (v - \tau).$$

$$= \sin \phi \cos \tau \sin v - \sin \phi \sin \tau \cos v.$$

But the instantaneous values of  $\phi$  and  $\tau$ , or of  $\sin \phi \cos \tau$  and  $\sin \phi \sin \tau$ , are troublesome to tabulate; it will therefore, in practice, be found more convenient to use only their mean values, and to consider their changes from this mean as perturbations of the latitude. Representing by the sign  $\delta$  the deviations from the mean values, which are of course arbitrary, we have

$$\cos \beta \delta \beta = \cos \phi \sin (v - \tau) \delta \phi - \sin \phi \cos (v - \tau) \delta \tau.$$

Let us substitute for  $\delta \phi$  and  $\delta \tau$  their values given by the integration of (34) to

quantities of the first order, in which case  $\theta$  and  $\tau$  may be assumed equal. These values are

$$\delta \phi = \sin \tau \, \delta p + \cos \tau \, \delta q$$
$$\sin \phi \, \delta \tau = \cos \phi \, (\cos \tau \, \delta p - \sin \tau \, \delta q)$$

the terms dependent on  $\delta p'$  and  $\delta q'$  being omitted because, being purely secular, they may be included in the mean values of  $\phi$  and  $\tau$ . Substituting in the expression for  $\delta \beta$ 

 $\cos \beta \delta \beta = \cos \phi \left\{ \sin v \, \delta q - \cos v \, \delta p \right\}. \tag{37}$ 

In the case of all the larger planets both  $\cos \beta$  and  $\cos \phi$  may here be put equal to unity, when the expression for  $\delta\beta$  will become

$$\delta\beta = \sin v \, \delta q - \cos v \, \delta p. \tag{38}$$

To develop this expression in purely periodic terms we must substitute for v its value in terms of the mean longitude or mean anomaly, namely,

$$v = l + 2e \sin g + \frac{5}{4}e^2 \sin 2g + \text{etc.};$$

suppose the terms of  $\delta p$  and  $\delta q$  depending on any argument, N to be

$$\delta p = -a_s \sin N - a_c \cos N$$

$$\delta q = a_s' \sin N + a_c' \cos N$$
(39)

and put  $\pi$  for the longitude of the perihelion, so that

$$l = \pi + g$$

then, to terms of the first order with respect to the eccentricities, we have  $\delta\beta = -e(a_c\cos\pi + a_s\sin\pi)\sin N - e(a_c\cos\pi + a_c\sin\pi)\cos N$ 

$$\frac{1}{2} \left\{ (a_s + a'_c) \cos \pi + (a'_s - a_c) \sin \pi \right\} \sin (N + g) 
+ \frac{1}{2} \left\{ (a_c - a'_s) \cos \pi + (a'_c + a_s) \sin \pi \right\} \cos (N + g) 
+ \frac{1}{2} \left\{ (a_s - a'_c) \cos \pi + (a'_s + a_c) \sin \pi \right\} \sin (N - g) 
+ \frac{1}{2} \left\{ (a_c + a'_s) \cos \pi + (a'_c - a_s) \sin \pi \right\} \cos (N - g) 
+ \frac{1}{2} e \left\{ (a_s + a'_c) \cos \pi + (a'_s - a_c) \sin \pi \right\} \sin (N + 2g) 
+ \frac{1}{2} e \left\{ (a_c - a'_s) \cos \pi + (a'_c + a_s) \sin \pi \right\} \cos (N + 2g) 
+ \frac{1}{2} e \left\{ (a_s - a'_c) \cos \pi + (a'_s + a_c) \sin \pi \right\} \sin (N - 2g) 
+ \frac{1}{2} e \left\{ (a_c + a'_s) \cos \pi + (a'_c - a_s) \sin \pi \right\} \cos (N - 2g) 
+ \frac{1}{2} e \left\{ (a_c + a'_s) \cos \pi + (a'_c - a_s) \sin \pi \right\} \cos (N - 2g)$$

The point of the orbit from which  $\pi$  and v are counted is entirely arbitrary, and, in considering the action of but a single planet, it will be most convenient to count them from the common node, in which case  $\pi$  must be replaced by  $\omega$ , and  $\delta p$  and  $\delta q$  by  $\delta k$  and  $\delta \eta$ . Thus, deducing the perturbations of the latitude immediately from the formulæ (27), we shall have

$$\delta\beta = \sin v \, \delta\eta - \cos v \, \delta k.$$

#### CHAPTER II.

APPLICATION OF THE PRECEDING METHOD TO THE COMPUTATION OF THE PERTURBATIONS OF URANUS BY SATURN.

#### Data of Computation.

The elements of Uranus, adopted in this computation, were deduced from the comparison of nine normal heliocentric longitudes at intervals of 3697 days extending from 1781, December 26, to 1862, December 18, with corresponding provisional places derived from the elements given in the "Investigation of the Orbit of Neptune," with perturbations produced by Jupiter, Saturn, and Neptune. As the perturbations are to be entirely re-computed, and the elements to be re-corrected from more extended series of observations, all the details of this first approximation will be omitted. The resulting elements of Uranus are given in the following table, together with the adopted elements of Saturn, which are nearly the same as those employed in the theory of Neptune, except that the inclination and longitude of the node have been corrected to agree with observations:—

	Elements	s II. of	f Uranus.	Elemen	nts I.	of Saturn.
π	168°	16'	31"	90°	4'	0"
8	28	25	36.0	14	48	45.0
0	73	11	58	112	20	0
ф	0	46	20	2	29	39.2
e	.04	69276	3	.05	6005	0
e in seconds,		96	79.5		115	551.9
n		154	26.10		439	996.13
m			1			1
m		3	21000		5	3501.6

In computing the perturbations of the radius vector, one of the largest terms will be a constant. To avoid the necessity of computing separately the perturbations of the second order, which depend on this constant, we shall include an approximate value of it in the mean distance. This approximate value is, in the action of an outer or an inner planet,  $\delta \log a = -\frac{1}{6} m' M a^2 D_a b_{\frac{1}{6}}^{(0)}$ . In the action of an inner or an outer planet,  $\delta \log a' = +\frac{1}{6} m M (b_{\frac{1}{6}}^{(0)} + \alpha D_a b_{\frac{1}{6}}^{(0)})$ . M being the modulus of the system of logarithms.

Using the values of  $b_{i}^{(0)}$  and a  $D_{a}$   $b_{i}^{(0)}$ , which are found in different works relating to Celestial Mechanics, we find that the different planets produce the following changes in 6 log a, the units being those of the seventh place of decimals:—

		On Saturn.	On Uranus.
Action of	Venus,	+ 22	+ 22
"	Earth,	+ 24	+ 25
66	Mars,	+ 3	+ 3
"	Jupiter,	+10865	+8780
"	Saturn,		+3081
66	Uranus,	<b>—</b> 35	
46	Neptune,	_ 9	— 119
66	Sum,	+.0010870	+.0011792
$\delta \log a$		+.0001812	+.0001965

The uncorrected mean distance is deduced from the mean motion by the relation

 $a^3 = \frac{\mu(1+m)}{n^2}.$ 

We thus have

	Saturn.	Uranus.
Uncorrected mean dist. (log)	0.979496	1.282901
Action of the planets	+ 181	+ 197
Corrected log a	0.979677	1.283098

The following functions of the elements are derived from the preceding elements by well known formulæ:—

γ (mutual inclination)	1°	57' 2	4.4"
$\log \sin \frac{1}{2} \gamma = \sigma$	8	.2323	373
$\log \cos \frac{1}{2} \gamma$	9	.9999	9367
τ (long. of ascending node of Saturn on U	Tranus) 126°	44'	51"
O The state of the	41	31	40
ω' 6 - ( · · · · · · · · · · · · · · · · · ·	323	18	21
$\omega' - \omega = (\omega)$	281	46	41
$\log \sin (\omega)$	_9	.990	759
log cos (ω)	+9	.3098	888
$\sin 2(\omega)$		0.399	966
cos 2(ω)	_	0.91	667
α	(	.497	249
$\frac{1}{\alpha^2}$		4.04	438

The following functions of  $\alpha$ , necessary in computing the coefficients h, are derived from Runkle's Tables, published by the Smithsonian Institution:—

Values of anD'	6	1)
----------------	---	----

i	60	$aDab^{(i)}_{\frac{1}{4}}$	$a^2 D_a^2 b_{\frac{1}{4}}^{(i)}$	$a^3D_a^2b_b^{(0)}$	$a^4D_a^4b_4^4$	$a^{5}D_{a}^{5}b_{k}^{(0)}$
0	2.14447	0.33969	0.5878	1.081	3.44	13.6
1	0.55207	.68314	.4990	1.177	3.40	13.8
2	0.20836	.47198	.7396	1.152	3.59	13.9
3	0.08687	.28491	.7123	1.463	3.68	14.5
4	0.03793	.16270	.5632	1.596	4.30	15.1
5	0.01702	.09010	.3998	1.485	4.87	16.9
6	0.00777	.04896	.2653	1.231	4.98	19.1
7	0.00359	.02624	.1682	0.940	4.60	20.5
8	0.00168	.01392	.1022	0.675	3.91	20.4
9	-0.00079	0.00733	0.0615	0.463	3.11	18.8

# Derivatives with respect to $(\log a = n)$ of $a^n D_a^n b_a^{(n)}$ .

				-	
i	n=0	1	2	3	4
	$D_{\mathbf{v}}b^{(\mathbf{i})}$	$D_{\mathfrak{D}}(a Dab^{(l)}_{i})$	$D_{\mathbf{v}}(\mathbf{a}^2D_{\mathbf{a}}^2b_{\mathbf{b}}^{(i)})$	$D_{v}(a^{3}D_{a}^{3}b_{-}^{(i)})$	$D_{\mathbf{v}}(a^4D_a^4b_a^{(0)})$
0	0.33969	0.9275	2.257	6.68	- 27.4
1	.68314	1.1821	2.175	6.93	27.4
2	.47198	1.2116	2.631	7.05	28.3
3	.28491	0.9972	2.888	8.07	29.2
4	.16270	0.7259	2.722	9.09	32.3
5	.09010	0.4899	2.285	9.33	36.4
6	.04896	0.3143	1.762	8.67	39.0
7	.02624	0.1944	1.276	7.41	38.9
8	.01392	0.1161	0.879	5.93	36.0
9	0.00733	0.0688	0.586	4.50	31.2

## Second derivatives.

i	$D_{x}^{2}b_{x}^{(0)}$	$D_{\nu}^{2}(aDab_{\downarrow}^{(i)})$	$D_{p}^{2}(a^{2}D_{a}^{2}b_{4}^{(i)})$	$D_{v}^{2}(a^{3}D_{a}^{3}b_{4}^{(0)})$
0	0.9275	3.184	11.19	47.4
1	1.1821	3.357	11.28	48.2
2	1.2116	3.843	12.31	49.4
3	0.9972	3.885	13.85	53.4
4	0.7259	3.448	14.53	59.6
5	0.4899	2.775	13.90	64.4
6	0.3143	2.076	12.19	65.0

## Vulues of $a^{n+1}D_a^nb_{\frac{1}{4}}^{(i)}$

			A T	
i	ab 3	$a^2Dab_{\frac{3}{4}}^{(i)}$	$a^3 D_a^2 b_{\frac{3}{2}}^{(6)}$	$a^4 D_a^3 b_{\frac{3}{4}}^{(0)}$
0	1.865	2.674	8.104	30.8
1	1.267	2.844	7.77	30.8
2	0.761	2.412	7.63	29.9
3	0.433	1.790	6.92	28.7
4 .	0.240	1.224	5.73	26.8
5	0.130	0.792	4.41	23.5
6	0.070	0.493	3.20	19.6
April, 1873.				

		20,000		coproc to (to	9 00		
		i	$D_{\mathfrak{D}}(\mathfrak{a}b_{\delta}^{(i)})$	$D_{\mathfrak{v}}(\mathfrak{a}^{2}D\mathfrak{a}b_{3}^{(i)})$	$D_{\mathfrak{v}}(\mathfrak{a}^3D$	ab (0)	
			$=a_1B_1^{(i)}$	$=2a_1B_2^{(i)}$	$=6a_{1}I$		
		0	4.539	13.452	55.	1	
		1	4.111	13.46	54.	1	
		2	3.173	12.45	52.	8	
		3	2,223	10.50	49.	5	
		4	1.464	8.18	44.	0	
		5	0.922	5.99	36.	7	
		6	0.563	4.19	29.	2	
					CELLO E		
			Second	derivatives.			
		i	$a_1 D_{\mathbf{w}} B^{(i)}$	$a_1 D_{\mathcal{D}} B_1^{(i)}$	$2a_1D_{v}$	$B_{2}^{(\mathbf{I})}$	
		0	4.539	17.99	82.	0	
		1	4.111	17.57	81.	0	
	•	2	3.173	15.62	77.	7	
		3	2.223	12.72	70.	5	
		4	1.464	9.64	60.	4	
		5	0.922	6.91	48.	7	
		6	0.563	4.75	37.	6 .	
	~ 77(0)	a Tr(0)	$2a_{1}E_{2}^{(i)}$	$6a_1E_s^{(i)}$	$a_1D_{\mathfrak{D}}E^{(i)}$	$a_{\scriptscriptstyle 1}D_{\scriptscriptstyle 2}E_{\scriptscriptstyle 1}^{\scriptscriptstyle (i)}$	$2a_{1}D_{2}E_{2}^{(2)}$
6	$a_1 E^{(i)}$	$a_{_{1}}E_{_{1}}^{(i)}$	$\frac{2a_1 E_2}{13.46}$	54.1	4.111	$\frac{a_1D_0E_1}{17.57}$	81.0
0	1.267	4.111			3.856	16.80	79.8
1	1.313	3.856	12.95	54.0			
2	0.850	3.167	11.98	51.8	3.167	15.15	75.8
3	0.500	2.318	10.31	48.4	2.318	12.63	69.0
4	0.281	1.573	8.24	43.1	1.573	9.82	59.6
5	0.155	1.014	6.18	36.6	1.014	7.20	49.0

The notation  $B_n^{(l)}$  and  $E_n^{(l)}$  is that of Le Verrier in his development in the first volume of "Annales de l'Observatoire Imperial de Paris."

#### Numerical expression of R and its derivatives.

We next proceed to the computation of the coefficients h and their derivatives. As an example of the most convenient form of computation we present in full that of the coefficient of  $\frac{m'}{a_1}\cos{(i\lambda'-(i-1)\lambda-\omega)}$  in the expression of R for the action of Saturn on Uranus. In this computation I use the tables given by Le Verrier in his "Annales de l'Observatoire," tome i, pages 358-383, comparing the development with that of Professor Peirce in the Astronomical Journal, vol. i, as a control.

j=0; j=1.										
	-3	-2	-1	0	+1	2	3	4	5	6
0	+4	3	2	1	0	-1	-2	-3	-4	5
(0)×b(f)	+0.5212	+0.8334	+ 1.1041	0	-1.10414	-0.83344	-0.5212	-0.3034	-0.1702	-0.0929
(1) × a Dab (6)	-0.2849	-0.4720	- 0.6831	-0.3397	-0.68314	-0.47198	-0.2849	-0.1627	-0.0901	-0.0490
Δa <sub>1</sub> (50)(f)			-16.1775							
a <sub>1</sub> (50)(i)	+0.2363	+0.3614	-15.7565	-0.3397	-0.78728	-1.30542	-0.8061	-0.4661	-0.2603	-0.1419
(0)b(f)	-13.55	-11.25	- 5.52	0.00	0.00	+ 2.92	+ 5.73	+ 6.83	+ 6.46	Contract of
(1) ×aDa	+ 8.54	+ 7.78	+ 4.78	+0.51	0.00	+ 1.18	+ 2.56	+ 3.25	+ 3.06	
(2)×a <sup>2</sup> D <sup>2</sup> a	+ 1.43	+ 0.74	- 0.00	-0.59	- 1.00	- 2.22	- 2.85	- 2.82	- 2.40	
(3)×a <sup>3</sup> D <sup>8</sup> a	- 0.73	- 0.58	- 0.59	100	- 0.59	- 0.58	- 0.73	- 0.80	- 0.74	
Δα <sub>1</sub> (51)			+ 48.53							
a <sub>1</sub> (51)	- 4.31	- 3.31	+ 47.20	-0.62	- 1.59	+ 1.30	+ 4.71	+ 6.46	+ 6.38	
(0)×b(f)	-18.76	-13.33	- 4.42	0.00	+ 4.42	+13.33	+18.76	+19.41	+17.01	and the
(1) ×aDa	+13.10	+10.38	+ 4.10	-0.68	- 1.37	+ 2.83	+ 6.27	+ 7.48	+ 7.02	Sur to
(2)×a <sup>2</sup> D <sup>2</sup> a	+ 1.43	0.00	- 1.00	-2.35	- 3.00	- 5.92	<b>— 7.13</b>	- 6.76	- 5.60	
(3)×a³D³a	- 1.46	- 1.15	- 1.18	-1.08	- 1.18	- 1.15	- 1.46	- 1.60	- 1.48	O THE P
∆a <sub>1</sub> (52)			+ 32.36							
a <sub>1</sub> (52)	- 5.69	- 4.10	+ 29.86	-4.11	- 1.13	+ 9.09	+16.44	+18.53	+16.95	
(0)×aE₁(f)	-3.00	- 3.40	_ 2.63	0.00	+ 2.63	+ 3.40	+ 3.00	+ 2.25	+ 1.55	
$(1) \times a_1 E_1(i)$	+2.32	+ 3.17	+ 3.86	+4.11	+ 3.86	+ 3.17	+ 2.32	+ 1.57	+ 1.01	
Δa <sub>1</sub> (60)	i		+ 16.18							
a <sub>1</sub> (60)	-0.68	- 0.23	+ 17.41	+4.11	+ 6.49	+ 6.57	+ 5.32	+ 3.82	+ 2.56	
½ e ×(50)	+6.611	+10.12	-441.22	-9.51	-50.049	-36.556	-22.573	-13.05	- 7.28	-3.97
½ e <sup>3</sup> ×(51)	-0.09	- 0.07	+ 1.04	-0.01	- 0.035	+ 0.028	+ 0.103	+ 0.14	+ 0.14	
½ ee <sup>12</sup> ×(52)	-0.08	- 0.06	+ 0.45	-0.06	- 0.017	+ 0.138	+ 0.248	+ 0.28	+ 0.26	
½ ce2×(60)	-0.05	- 0.02	+ 0.14	+0.03	+ 0.051	+ 0.052	+ 0.043	+ 0.03	+ 0.02	
h .	+6.39	+ 9.97	-439.59	<b>—9 55</b>	-50.050	-36.338	—22 179	-12.60	<b>— 6.86</b>	-3.60

The derivatives of h with respect to  $(\log a = n)$  are computed in precisely the same way by simply substituting for  $b_{\downarrow}^{(i)}$ ,  $aDab_{\downarrow}^{(i)}$ , etc., their derivatives with respect to n as given in the above table of constants.

The quantities  $\Delta a_1(50)^{(i)}$ , etc., which appear in the third series of terms above express that part of the perturbations of Uranus caused by the action of Saturn

<sup>1</sup> In units of the third place of decimals.

on the sun. They are each of the form  $N \times \alpha^{-2}$ , N being a numerical coefficient given by Le Verrier under the coefficient for each term. The derivative of this expression with respect to p is  $-2N \times \alpha^{-2}$ , so that for the corresponding terms in  $D_{p}h$  and  $D_{p}^{2}h$  we have

$$\Delta D_v h = -2\Delta h$$
 $\Delta D_v^2 h = +4\Delta h$ 

The values of h and its derivatives, corresponding to any one argument i' and i, are to be combined into two terms depending the one on the cosine, the other on the sine of the argument. Let us represent by g the mean anomaly of Uranus, and let us put l' for the mean longitude of Saturn counted from the perihelion of Uranus, or, more exactly, for the arc  $\lambda'$ — $\omega$ . Put also

$$N = ig + il',$$

$$i + i' + j = j'',$$

$$P = j\omega + j'\omega',$$

$$P' = j''\omega + j'\omega'.$$

Then, for each value of N there will be several values of P corresponding to different powers and products of the eccentricities and inclinations in h. Distinguishing these values and the corresponding values of h by subscript numerals, we shall have a series of terms of R of the following form—

$$R = rac{m}{a_1} \left\{ egin{array}{l} h_1 \cos{(N+P'_1)} \ + h_2 \cos{(N+P'_2)} \ + h_3 \cos{(N+P'_3)} \ + ext{ etc.} \end{array} 
ight\}$$

and by putting

$$h_c = h_1 \cos P'_1 + h_2 \cos P'_2 + h_3 \cos P'_3 + \text{etc.}$$

$$h_s = -h_1 \sin P'_1 - h_2 \sin P'_2 - h_3 \sin P'_3 - \text{etc.}$$
(41)

The above terms may be condensed into

$$R = \frac{m}{a_1} h_c \cos N + \frac{m}{a_1} h_s \sin N,$$

which are of the form supposed in the preceding theory.

In order that the derivative of R, with respect to the true longitude of Uranus, may be expressed in the form

$$\frac{\partial R}{\partial \mathbf{v}} = \frac{m}{a_1} v_s \sin N + \frac{m}{a_1} v_c \cos N$$

we must, by (7), put

$$v_s = -(i+j_1) h_1 \cos P'_1 - (i+j_2) h_2 \cos P'_2 - \text{etc.}$$

$$v_c = -(i+j_1) h_1 \sin P'_1 - (i+j_2) h_2 \sin P'_2 - \text{etc.}$$
(42)

 $j_1$ ,  $j_2$ , representing the several values of j in the different terms which correspond to one and the same set of values of i and i'.

To obtain the derivative with respect to  $\gamma$  we notice that all the appreciable terms in the different values of  $\hbar$ , which depend upon the mutual inclination, are of the form

$$h = \sigma^2 A$$
,

where  $\sigma = \sin \frac{1}{2} \gamma$ . These equations give

$$\frac{\partial h}{\partial \gamma} = \frac{\partial h}{\partial \sigma} \frac{\partial \sigma}{\partial \gamma} = A\sigma \cos \frac{1}{2} \gamma = \frac{1}{2} A \sin \gamma.$$

Consequently

$$\frac{\partial R}{\partial \gamma} = \frac{1}{2} A \sin \gamma \cos (N + P').$$

and the various terms depending on the same argument (i', i) may be condensed into two, exactly as in the case of R itself.

The different co-efficients h and  $D_{\varepsilon}h$ , computed in the way already described, are given in extenso in the following table. At the top of each individual column is given the value of P, or of  $j\omega + j'\omega'$ , corresponding to the values of h below, and immediately under P is given its modified value, or P', to be used in condensing the terms, putting for brevity

$$(\omega) = \omega - \omega'$$
.

P and P' are therefore regarded as constant angles the numerical values of the sines and cosines of which may be obtained from the values of  $\omega$  and  $\omega'$  already given.

The condensed  $h_c$  and  $h_s$  are given in the two right hand columns. All the numbers are given in units of the third place of decimals.

VALUES OF h.										
P P'	=0		ω' — ω (ω)							
i i' -4,+4 -3, 3 -2, 2 -1, 1	h		$ \begin{array}{c} h \\ + 0.62 \\ + 0.82 \\ + 0.88 \\ + 0.53 \end{array} $		h	,		h,		
0, 0 +1,-1 2,-2 3,-3 4,-4		1.36	-0.4975 $-0.83$ $-9.63$ $+1.62$ $+1.54$		$\begin{array}{c} +\ 1072.80 \\ -\ 3481.42 \\ +\ 204.14 \\ +\ 84.77 \\ +\ 36.24 \end{array}$		+	$ \begin{array}{r} -1.83 \\ -10.29 \\ +0.79 \\ +0.90 \end{array} $		
5,—5 P P'	$+\frac{15}{0}$	-ω' -(ω)	$\begin{array}{c c} +1.2 \\ \hline & \omega - 2\omega' \\ & -2(\omega) \end{array}$	ω' — 2ω + (ω)	+ 1	5.81 ω +2ω	+	0.81		
i i' -3,+4 -2, 3 -1, 2 0, 1 +1, 0 2,-1 3,-2 4,-3 5,-4 6,-5	$\begin{array}{c} h \\ -2.31 \\ -3.42 \\ -3.54 \\ +287.30 \\ +58.38 \\ -39.760 \\ +35.13 \\ +20.39 \\ +11.25 \\ +6.00 \\ \end{array}$	h + 6.39 + 9.97 -439.59 - 9.55 - 50.05 - 36.338 - 22.179 - 12.60 - 6.86 - 3.6	h 0 -0.95 0 +0.13 -0.02 -0.074 -0.105 -0.11	h 0 0 00205071313 + .17 + .23 + .22	h 0 0 03 04 03 016	h 0 +.02 +.02 +.09 0 0 0	$\begin{array}{c} h_e \\ -1.01 \\ -0.51 \\ -93.30 \\ +285.20 \\ +48.15 \\ -47.138 \\ +30.63 \\ +17.96 \\ +9.98 \\ +5.38 \end{array}$	$\begin{array}{c} h_{\bullet} \\ -6.26 \\ -9.40 \\ +430.35 \\ +9.19 \\ +48.96 \\ +35.531 \\ +21.44 \\ +12.55 \\ +7.00 \\ +3.78 \end{array}$		

VALUES OF h.									
P P'	$-\frac{2\omega}{0}$	— ω' — ω — (ω)	$-2\omega'$ $-2(\omega)$	$0 + 2\omega$					
i i'1, 3 0, 2 +1, 1 2, 0 3,-1 4,-2 5,-3 6,-4 7,-5	h $+0.04$ $+0.06$ $-0.74$ $+3.09$ $+1.268$ $+4.16$ $+3.13$ $+2.11$ $+1.35$	$\begin{array}{c c} h \\ -0.27 \\ +31.65 \\ -0.83 \\ -5.19 \\ -6.290 \\ -5.458 \\ -4.03 \\ -2.74 \\ -1.76 \end{array}$	$\begin{array}{c} h \\ -42.24 \\ -0.04 \\ -1.08 \\ +1.89 \\ +2.082 \\ +1.767 \\ +1.29 \\ +0.87 \\ +0.55 \end{array}$	$\begin{array}{c} h \\ +0.11 \\ +0.18 \\ -0.91 \\ +0.18 \\ +0.111 \\ +0.061 \\ +0.04 \\ +0.02 \\ +0.01 \\ \end{array}$	$\begin{array}{c} h_c \\ +38.72 \\ +6.58 \\ -0.03 \\ +0.32 \\ -1.912 \\ +1.44 \\ +1.13 \\ +0.75 \\ +0.49 \end{array}$	$h_s$ $+17.03$ $-31.15$ $+2.15$ $+4.14$ $+5.216$ $+4.576$ $+3.39$ $+2.31$ $+1.49$			
P P'	3ω 0		$ \begin{array}{c cccc} 2\omega' - \omega & -3 \\ -2(\omega) & -3 \end{array} $		- India				
i i' +1,+2 2, 1 3, 0 4,-1 5,-2 6,-3 7,-4 8,-5	h 0 +.01 +.18 +.222 +.424 +.398 +.327 +.24	46 760 847 773 627	$\begin{array}{c cccc} h & & h \\ 0 & &1 \\ +.03 & &0 \\ +.34 & &0 \\ +.520 & &1 \\ +.558 & &1 \\ +.498 & &1 \\ +.395 & &0 \\ +.29 & &0 \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c c} 0 &15 \\ 9 &325 \\ 1 &176 \\ 4 &145 \end{array}$	$h_{\bullet}$ $+.06$ $+.04$ $+.213$ $+.416$ $+.490$ $+.460$ $+.379$ $+.289$			
$\begin{array}{c c} A \\ P' \\ \hline i & i' \\ 4, & 0 \\ 5, -1 \\ 6, -2 \\ 7, -3 \\ 8, -4 \\ 9, -5 \\ \end{array}$	$ \begin{array}{c c} -4\omega & -6 \\ \hline h & 0 \\ +.02 \\ +.039 \\ +.043 \\ +.042 \\ +.035 \end{array} $	$ \begin{array}{c cccc}(\omega) & & & & & & & & $	-2(a) -3	$ \begin{array}{c cccc} 04 & +.01 \\ 047 & +.008 \\ 048 & +.008 \\ 044 & +.007 \end{array} $	$h_s$ $04$ $03$ $045$ $049$ $044$ $037$	$h_c$ 0 +.003 +.028 +.034 +.032 +.029			

	Values of $D_{\mathbf{p}}h$ .									
P P'	0	ω' — ω (ω)								
$ \begin{vmatrix} i & i' \\ -4, +4 \\ -3, & 3 \\ -2, & 2 \\ -1, & 1 \end{vmatrix} $	$D_{m p}h$ .	$\begin{array}{c} D_{v}h \\ + 3.18 \\ + 3.24 \\ + 2.39 \\ + 0.40 \end{array}$	$D_{m{v}}h_{m{c}}$	$D_{\mathfrak{v}}h_{\mathfrak{s}}$						
$0, 0 \\ +1, -1$	$+171.93 \\ +8749.59$	$\begin{array}{ccc} - & 2.075 \\ - & 2.69 \end{array}$	$+\   171.51 \\ +\   8749.12$	_ 3.02						
2,—2 3,—3 4,—4 5,—5	$\begin{array}{c} + 467.72 \\ + 277.00 \\ + 153.87 \\ + 82.12 \end{array}$	$ \begin{array}{r}                                     $	$ \begin{array}{r} + 472.46 \\ + 278.25 \\ + 155.46 \\ + 83.54 \end{array} $	$ \begin{array}{r} + 18.05 \\ - 0.36 \\ + 1.41 \\ + 1.80 \end{array} $						

	Values of $D_{0}h$ .									
P P'  i i' -3,+4 -2, 3 -1, 2 -0, 1 1, 0 2,-1 3,-2 4,-3 5,-4 6,-5	$\begin{array}{c c} -\omega \\ 0 \\ \hline D_{vh} \\ -9.28 \\ -9.74 \\ -4.63 \\ -556.40 \\ +30.16 \\ +265.17 \\ +83.10 \\ +68.34 \\ +49.04 \\ +32.1 \\ \hline \end{array}$	$\begin{array}{c} -\omega' \\ -(\omega) \\ \hline D_0 h \\ + 19.4 \\ + 18.5 \\ + 907.62 \\ - 26.17 \\ - 71.56 \\ - 86.47 \\ - 74.60 \\ - 54.9 \\ - 36.9 \\ - 23.2 \\ \end{array}$	$\begin{array}{c} \omega-2\omega\\-2(\omega)\\\hline D_0h\\0\\+2.05\\+.05\\10\\+.04\\19\\42\\55\\58\\53\\\end{array}$	$\begin{array}{c} \omega'-2\omega\\ +(\omega)\\ \hline D_0h\\ 0\\06\\08\\09\\19\\26\\ +.63\\ +.29\\ +.68\\ +.90\\ \end{array}$	$\begin{array}{c c} +\omega \\ \omega +\omega ' \\ \hline D_v h \\ 0 \\12 \\13 \\14 \\11 \\07 \\04 \\02 \\01 \\ 0 \\ \end{array}$	$\begin{array}{c} \omega \\ 2\omega \\ \hline D_{\overline{\nu}h} \\ 0 \\ +.08 \\ +.07 \\12 \\ +.02 \\ 0 \\ 0 \\ 0 \\ 0 \\ \end{array}$	$\begin{array}{c} D_{v}h_{e} \\ -5.32 \\ -7.97 \\ +180.44 \\ -561.82 \\ +15.37 \\ +247.58 \\ +68.34 \\ +57.70 \\ +42.19 \\ +28.1 \end{array}$	$\begin{array}{c} D_{6}h_{s}\\ -19.00\\ -17.43\\ -888.65\\ +25.60\\ +69.86\\ +84.30\\ +73.49\\ +53.9\\ +36.7\\ +23.4\\ \end{array}$		
$\begin{array}{c} P \\ P' \\ \hline \\ i  i' \\ -1, +3 \\ 0,  2 \\ +1,  1 \\ 2,  0 \\ 3,  1 \\ 4, -2 \\ 5, -3 \\ 6, -4 \\ 7, -5 \\ \end{array}$	$\begin{array}{c c} -2\omega \\ 0 \\ \hline \\ D_{vh} \\ +0.16 \\ +0.32 \\ +3.27 \\ +2.56 \\ +13.745 \\ +10.25 \\ +10.76 \\ +9.39 \\ +7.3 \\ \end{array}$	$\begin{array}{c c} -\omega & -\omega $	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		$\begin{array}{c} 0 \\ +2\omega \\ \hline D_{v}h \\ +0.47 \\ +0.60 \\ +3.02 \\ +0.60 \\ +0.463 \\ +0.32 \\ +0.21 \\ +0.13 \\ +0.09 \\ \end{array}$	3	$D_vh_e$ $-78.76$ $-12.92$ $-1.22$ $-3.74$ $+3.933$ $-0.77$ $+0.69$ $+1.22$ $+1.2$	$\begin{array}{c} D_{\text{p}h},\\ -34.19\\ +62.54\\ -2.26\\ +6.00\\ +12.153\\ +15.07\\ +14.68\\ +12.4\\ +9.6\end{array}$		
$\begin{array}{c c} P \\ P' \\ \hline i & i' \\ +1, +2 \\ 2, & 1 \\ 3, & 0 \\ 4, -1 \\ 5, -2 \\ 6, -3 \\ 7, -4 \\ 8, -5 \\ \end{array}$	$\begin{array}{c} -3\omega \\ 0 \\ \hline \\ Dvh \\ +0.03 \\ +0.12 \\ +0.21 \\ +0.89 \\ +1.08 \\ +1.40 \\ +1.46 \\ +1.32 \\ \end{array}$	$\begin{array}{c} -2\omega - \omega' \\ -(\omega) \\ \hline D_{v}h \\ +0.18 \\ -0.26 \\ -0.89 \\ -2.02 \\ -3.00 \\ -3.47 \\ -3.44 \\ -3.00 \\ \end{array}$	$\begin{array}{c} -\omega - 2\omega' \\ -2(\omega) \\ \hline D_{ph} \\ +0.05 \\ +0.33 \\ +0.98 \\ +1.89 \\ +2.53 \\ +2.73 \\ +2.60 \\ +2.20 \\ \end{array}$	$\begin{array}{c} -3\omega' \\ -3(\omega) \\ \hline D_{vh} \\ +0.22 \\ -0.09 \\ -0.31 \\ -0.54 \\ -0.67 \\ -0.69 \\ -0.62 \\ -0.51 \\ \end{array}$		$\begin{array}{c} -\omega \\ +2\omega \\ \hline D_{ph} \\ +.08 \\ +.17 \\ +.13 \\ +.11 \\ +.09 \\ +.06 \\ +.04 \\ \end{array}$	$\begin{array}{c} D_v h_o \\ -0.31 \\ -0.08 \\ -0.59 \\ -0.84 \\ -1.38 \\ -1.33 \\ -1.20 \\ -0.99 \end{array}$	$D_{p}h_{s}$ $-0.17$ $-0.09$ $+0.13$ $+0.69$ $+1.30$ $+1.68$ $+1.78$ $+1.62$		
P P'  i i' 4, 0 5,—1 6,—2 7,—3 8,—4 9,—5	$\begin{array}{ c c c }\hline -4\omega \\ 0\\\hline D_{n}h\\ +.02\\ +.05\\ +.10\\ +.15\\ +.18\\ +.19\\\hline\end{array}$	$ \begin{array}{c} -3\omega - \omega' \\ -(\omega) \\ Dvh \\09 \\22 \\38 \\52 \\59 \\59 \end{array} $	$ \begin{array}{r} -2\omega - 2\omega' \\ -2(\omega) \end{array} $ $ \begin{array}{r} D_{0}h \\ +.13 \\ +.30 \\ +.48 \\ +.62 \\ +.66 \\ +.65 \end{array} $	$ \begin{array}{r} -\omega - 3 \\ -3(\omega) \\ D_0 h \\ -08 \\ -18 \\ -26 \\ -32 \\ -33 \\ -31 \end{array} $	D + + + + + + + + + + + + + + + + + + +	4ω' 4(ω) 2πh .02 .04 .05 .06 .06 .05	$\begin{array}{c} D_{v}h_{e} \\06 \\14 \\24 \\30 \\32 \\31 \end{array}$	$\begin{array}{c} D_{v}h_{*}\\01\\02\\ +.01\\ +.04\\ +.09\\ +.11 \end{array}$		

The values of  $D_*h$ , needed in computing the perturbations of the second order with respect to the masses being obtained in the same way, by the simple substitution of the second derivatives of the functions  $b_*aDab$ , etc., for those functions themselves in the expressions for h, it is not necessary to present the details of the computation.

After obtaining h and its derivatives, it will be found convenient to change the arrangement of the terms. Hitherto we have kept in one series those in which the sum of the indices are a constant. Now, we shall put together all those in which

the index of the disturbing planet has the same value, arranging the individual terms of each series according to the index of the disturbed planet. Thus, the index of the product of any term, as  $h \cos N$ , by any multiple of the mean anomaly of the disturbed planet, as jy, will be found in the same series with that of N itself, and j lines above and below.

The next process will be the formations of the required functions of the mean anomaly of Uranus,  $\frac{dv}{dt}$ ,  $\frac{d\rho}{dt}$ ,  $\frac{a^2}{r^2}$ , log r. Their values are as follows:—

Considering only those terms which are of the first order, the value of  $D_l R$  may be found in two ways, the agreement of which will afford a check upon the entire development of the perturbative function, and upon the computations of R and  $\frac{\partial R}{\partial v}$ . These are (1) by direct differentiation, with respect to the time as contained in the mean anomaly of a single planet, whereby each term in R of the form

$$R = \frac{m}{a_1} h \cos N$$

will produce in  $D'_{\iota}R$  the term

$$D_t'R = -\frac{m}{a_t} inh \sin N.$$

and (2) by forming the expression

$$D_{t}R = \frac{\partial R}{\partial \mathbf{v}} \frac{dv_{0}}{dt} + \frac{\partial R}{\partial \rho} \frac{d\rho_{0}}{dt}.$$

As several "mechanical multiplications," like those indicated in this last expression, are to be performed, the following example of the form of computation is presented. It exhibits the formation of the product of those terms of  $\frac{\partial R}{\partial \mathbf{v}}$  in which i = -1 by  $\frac{d\mathbf{v}_0}{dt}$ .

The multipliers on the left are each one-half the coefficient cos jg in the expression for  $\frac{dv_0}{dt}$ , and each product is placed in the two columns corresponding respectively to N+jg and N-jg.

All the derivations of  $R_0$  necessary in the computation of the perturbations of the first order are given in the following tables. First we have the values of  $D_t R$  obtained by direct differentiation, as indicated in the preceding formulæ. Next we have  $\frac{\partial R}{\partial v}$  and  $\frac{\partial R}{\partial \rho}$ , obtained by the formulæ (7) and (42). The products  $\frac{\partial R}{\partial v}$  by  $\frac{\partial v}{\partial t}$  and of  $\frac{\partial R}{\partial \rho}$  by  $\frac{\partial \rho}{\partial t}$ , being formed in the simple way just pointed out, and with the values of the component factors just given, their sum is next shown. This sum should agree accurately with  $D_t R$ . The discrepancies are shown in the next two columns. The only apparently large discrepancy is found in the argument  $\frac{\partial R}{\partial v}$ , so far as they depend on this argument. As the entire term does not amount to 0".01, I have not sought to correct it.

The great value of this check arises from the fact that it gives a complete control of the correctness of the development of the perturbative function, ab initio, since the two valves of  $D_t$  are derived from different terms of that development. It also controls all the computations except that of  $\frac{\partial R}{\partial \rho}$ . This quantity being multiplied by quantities of the order of the eccentricities in the second value of  $D_t$ , an error in its value will produce a discrepancy of only  $\frac{1}{40}$  its own amount in  $D_t$ , and may therefore be overlooked. The derivative in question must therefore be checked by a complete duplicate computation.

In the column next following are given the integrating factors  $\nu$ , for which the expression is

$$v = \frac{n}{i'n' + in} = \frac{1}{i + i' \frac{n'}{n}}.$$

For each value of i the values of v are therefore the reciprocals of a series of numbers in arithmetical progression, the common difference being unity.

	$D_t'R =$	$=\frac{m'}{a_1} n \times$	$\frac{\partial^R}{\partial \mathbf{v}} = 0$	$\frac{m'}{a_1}$ ×	$\frac{\partial R}{\partial \vec{\rho}} = \frac{m'}{a_1} \times$		
g l'	sin	cos	sin	cos	cos	sin	
0, 0	0 48.15	0 + 48.96	+ 10.20	+ 0.487 + 49.07	<b>—</b> 63.52	—118.82	
2, 3, 4,	$\begin{array}{c cccc} - & 0.64 \\ + & 0.45 \\ + & 0.16 \end{array}$	+ 8.28 + 0.64	$\begin{array}{c c} + & 4.48 \\ + & 0.50 \\ + & 0.06 \end{array}$	+ 3.20 - 0.08 - 0.06	$\begin{array}{cccc} + & 3.42 \\ + & 0.74 \\ + & 0.10 \end{array}$	$ \begin{array}{rrrr}  - & 10.14 \\  + & 0.34 \\  + & 0.01 \end{array} $	
2,1 1, 0,	0 - 0.03	$\begin{array}{c c} + & 0.08 \\ + & 2.15 \\ 0 \end{array}$	$\begin{array}{c c} + & 0.02 \\ + & 1.63 \\ - & 287.42 \end{array}$	$\begin{array}{c c} - & 0.04 \\ + & 1.34 \\ - & 0.10 \end{array}$	+ 0.08  + 1.25  + 276.62	$ \begin{array}{c c} - & 0.05 \\ - & 0.11 \\ + & 34.79 \end{array} $	
1, 2,	$+3481.42 \\ + 94.28$	-1.33 + 71.06	+3481.14 + 54.42	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	-5267.70 $-200.44$	+ 4.35 —119.83	
3, 4, 5,	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	+ 15.65  + 1.66  + 0.15	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c c} + & 9.490 \\ + & 0.42 \\ & 0 \end{array}$	$\begin{array}{cccc} - & 2.02 \\ + & 1.16 \\ + & 0.17 \end{array}$	- 17.37 - 1.11 - 0.01	
—1,—2 0,	+ 0.17	+ 0.06	+ 0.21 - 6.58	- 0.16 + 30.99	+ 0.14 + 6.34	- 0.11 + 31.39	
1, 2, 3,	+ 93.30 - 408.28 - 91.89	-430.35 $-20.58$ $+64.32$	+ 96.81 $- 410.42$ $- 57.01$	-430.37 - 12.01 - 64.98	$ \begin{array}{rrr}  & - & 87.14 \\  & - & 676.60 \\  & - & 98.97 \end{array} $	-458.30 - 7.76 - 94.93	
4, 5, 6,	$ \begin{array}{rrr}  & 5.76 \\  + & 0.88 \\  + & 0.27 \end{array} $	$+ 18.30  + \cdot 2.45  + 0.17$	$\begin{array}{cccc} + & 1.45 \\ + & 1.30 \\ + & 0.20 \end{array}$	+ 12.96  + 1.04  - 0.02	$ \begin{array}{rrr}  & 0.67 \\  + & 1.56 \\  + & 0.28 \end{array} $	- 19.65 - 1.79 - 0.04	
1,—3 2, •	-38.72 + 1.02	-17.03 + 18.80	<ul><li>38.75</li><li>5.31</li></ul>	-17.29 + 19.14	+ 40.04 + 8.48	— 17.16 — 26.83	
3, 4, 5,	$\begin{array}{rrrr} & - & 254.31 \\ - & & 71.84 \\ - & & 5.65 \end{array}$	+ 2.37  + 50.20  + 16.95	<ul><li>254.15</li><li>51.49</li><li>0.23</li></ul>	$ \begin{array}{rrr}  - & 0.02 \\  + & 49.90 \\  + & 13.0 \end{array} $	- 363.02 - 75.66 - 1.82	-0.43 $-66.45$ $-18.07$	
6, 7,	+ 0.87 + 0.34	+ 2.76 + 0.24	$+ 1.29 \\ + 0.27$	+ 1.5 0	+ 1.48 + 0.35	- 2.14 - 0.07	
3,—4 4, 5,	+ 3.03 $-$ 144.96 $-$ 49.90	+ 18.78  + 3.60  + 35.00	+ 1.34 - 144.78 - 38.64	+ 18.78  + 1.5  + 34.58	+ 6.33 - 191.70 - 52.17	- 25.26 - 2.31 - 43.7	
6, 7, 8,	$ \begin{array}{rrrr}  & 4.50 \\  & + & 0.75 \\  & + & 0.35 \end{array} $	+ 13.86  + 2.65  + 0.26	$ \begin{array}{cccc}  & - & 0.9 \\  & + & 1.1 \\  & + & 0.3 \end{array} $	+ 11.2  + 1.6  + 0.1	$ \begin{array}{rrrr}  & - & 1.97 \\  & + & 1.31 \\  & + & 0.36 \end{array} $	- 14.7 - 2.2 - 0.1	
5,—5 6,	<ul><li>79.05</li><li>32.3</li></ul>	+ 4.05 + 22.7	- 78.9 - 26.3	$+ 2.4 \\ + 22.3$	<ul><li>99.3</li><li>33.5</li></ul>	— 2.1 — 27.2	
7, 8, 9,	$ \begin{array}{rrrr}  & 3.4 \\  & + & 0.7 \\  & + & 0.3 \end{array} $	$+ 10.4 \\ + 2.3 \\ + 0.3$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c cccc} + & 8.7 \\ + & 1.5 \\ + & 0.1 \end{array}$	- 1.7 + 1.1 + 0.3	- 11.1 - 1.0 + 0.1	

	$ \frac{\partial R}{\partial \mathbf{v}} \frac{d\mathbf{v}_{0}}{dt} + \frac{\partial R}{\partial \rho} \frac{d\rho_{0}}{dt} \\ = \frac{m'}{a_{1}} n \times $		Discre	epancy.		k.	k <sub>a</sub>
g l'	sin	cos	sin	cos			
0, 0	0	- 0.01	0	01	Market State of	-1244.31	
1,	- 48.05	+ 48.92	+.10	04	+1.0	+ 32.78	- 20.90
2,	- 0.63	+ 8.27	+.01	01	+0.5	+ 4.06	- 1.86
3,	+ 0.45	+ 0.65	0	+.01	+1/3	+ 0.44	+ 0.08
4,	+ 0.11	- 0.03	05	03	+0.25		
_2,_1	_ 0.03	+ 0.02	03	06	-0.206098	+ 0.08	- 0.08
_1,	- 0.05	+ 2.16	02	+.01	-0.259601	+ 1.23	- 1.23
0,	- 0.06	+ 0.09	06	+.09	-0.350623	+ 276.62	+ 34.79
+1	+3481.41	_ 1.33	01	- 0	-0.539942	-1508.18	+ 5.78
2,	+ 94.20	+ 71.06	08	0	-1.173630	+ 20.85	-286.59
3,	+ 5.78	+ 15.63	+.04	02	+6.75940	- 79.56	+194.17
4,	+ 1.27	+ 1.66	03	0	+0.871126	- 1.10	+ 1.79
5,	+ 0.14	+ 0.11	01	04	+0.4656	+ 0.03	+ 0.13
_1,_2	+ 0.16	+ 0.10	01	+.04	-0.149162	+ 0.19	- 0.13
0,	+ 0.01	+ 0.07	+.01	+.07	-0.175312	+ 6.34	+ 31.39
+1,	+ 93.24	-430.37	06	02	-0.212580	- 47.47	-275.33
2,	- 408.28	_ 20.60	0	02	-0.269971	- 897.05	+ 3.35
3,	_ 91.90	+ 64.33	01	+.01	-0.369806	- 166.93	-142.50
4,	- 5.77	+ 18.17	01	13	-0.586813	- 7.44	- 41.13
5,	+ 0.91	+ 2.45	+.03	0	-1.42022	+ 4.05	- 8.75
6,	+ 0.29	+ 0.15	+.02	02	+3.3797	- 1.53	+ 1.09
1,-3	_ 38.78	- 17.03	06	0	-0.132342	+ 29.78	- 12.65
2,	+ 1.02	+ 18.68	0	—12	-0.152528	+ 8.79	- 32.56
3,	- 254.29	+ 2.37	+.02	0	-0.179981	- 454.55	- 1.28
4,	- 71.88	+ 50.13	04	07	-0.219482	107.20	— 88.50
5,	- 5.69	+ 17.01	04	+.06	-0.281202	- 5.00	- 27.61
6,	+ 0.91	+ 2.73	+.04	03	-0.391210	+ 2.15	- 4.30
7,	+ 0.35	+ 0.19	+.01	05	-0.6426	+ 0.79	- 0.38
3,—4	+ 3.10	+ 18.78	+.07	0	+0.11893	+ 7.05	- 29.73
4,	- 145.0	+ 3.51	04	09	-0.13500	230.83	- 3.28
5,	- 49.9	+ 34.85	0	15	-0.15605	- 67.74	- 54.60
6,	- 4.7	+ 13.95	20	+.09	-0.18490	- 3.63	- 19.80
7,	+ 0.8	+ 2.62	+.05	03	-0.22685	+ 1.65	- 3.36
8,	+ 0.3	+ 0.2	05	06	-0.2934	+ 0.57	- 0.27
5,—5	- 79.3	+ 2.7	25	-1.35	-0.1080	116.4	- 3.5
6,	- 32.4	+ 22.7	10	0	-0.1211	_ 41.3	_ 32.7
7,	- 3.5	+ 10.5	10	+.10	-0.1377	- 2.6	— 13.9
8,	+ 0.8	+ 2.3	+.10	0	-0.1597	+ 1.3	- 2.6
9,	+ 0.3	+ 0.2	0	10	-0.1901	+ 0.5	- 0.2
					9 (6)		

The values of  $\frac{a_1}{m} \int D'_t R_0 dt$  are formed from  $\frac{a_1}{m'n} D'_t R$  by simple multiplication by  $\nu$ , and proper changes of sign. The values of  $k_c$  and  $k_s$  are then formed by adding the terms of  $2 \frac{a_1}{m'} \int D'_t R_0 dt$  to the corresponding terms of  $\frac{a_1}{m'} \frac{\partial R}{\partial \rho}$ .

Perturbations of radius vector.

Let us now resume equation (19), and put for brevity

$$M = \frac{m'a}{a_1(1+m)}. (44)$$

If we give to u the successive values 0, +1, -1, +2, -2, +3, -3, we have

$$r_{1}^{2}\delta\rho = M \times \begin{cases} \frac{1}{4} \sum_{i} p_{i}q_{i} (\nu_{i} - \nu_{-i}) \left\{ k_{c} \cos N + k_{s} \sin N \right\} \\ + \frac{1}{8} \sum_{i} (p_{i}q_{(i-1)} + p_{(i-1)}q_{i}) (\nu_{i} - \nu_{(1-i)}) \left\{ k_{c} \cos (N + g) + k_{s} \sin(N + g) \right\} \\ + \frac{1}{8} \sum_{i} (p_{i}q_{(i+1)} + p_{(i+1)}q_{i}) (\nu_{i} - \nu_{-(i+1)}) \left\{ k_{c} \cos (N - g) + k_{s} \sin(N - g) \right\} \\ + \frac{1}{8} \sum_{i} (p_{i}q_{(i-2)} - p_{(i-2)}q_{i}) (\nu_{i} - \nu_{(2-i)}) \left\{ k_{c} \cos (N + 2g) + k_{s} \sin(N + 2g) \right\} \\ + \text{etc.} \qquad \text{etc.} \qquad \text{etc.} \end{cases}$$

the finite integral being taken with respect to all values of i from  $-\infty$  to  $+\infty$ , and the terms in which the angles  $N\pm ug$  vanish being omitted. Proceeding farther to expand with respect to i, if we collect similar terms we shall find the individual terms in  $r^2\delta\rho$  to be as follows:

$$\begin{split} r_1^2 \delta \rho &= \frac{1}{2} \, M \, \left\{ \begin{array}{c} p_1 q_1 \, (\nu_1 - \nu_{-1}) \\ + p_2 q_2 \, (\nu_2 - \nu_{-2}) \end{array} \right. \, \left. \right\} \, \left\{ k_c \cos N + k_s \sin N \right\} \\ &+ \frac{1}{4} \, M \, \left\{ \begin{array}{c} p_0 q_1 \, (\nu_1 - \nu_0) \\ + (p_1 q_2 + p_2 q_1) \, (\nu_2 - \nu_{-1}) \\ + (p_2 q_3 + p_3 q_2) \, (\nu_3 - \nu_{-2}) \\ + \text{etc.} \end{array} \right. \, \left\{ k_c \cos \left( N + g \right) + k_s \sin \left( N + g \right) \right\} \\ &+ \frac{1}{4} \, M \, \left\{ \begin{array}{c} p_0 q_1 \, \left( \nu_0 - \nu_{-1} \right) \\ + \left( p_1 q_2 + p_2 q_1 \right) \, \left( \nu_1 - \nu_{-2} \right) \\ + \left( p_2 q_3 + p_3 q_2 \right) \, \left( \nu_2 - \nu_{-3} \right) \\ + \text{etc.} \end{array} \right. \, \left\{ k_c \cos \left( N - g \right) + k_s \sin \left( N - g \right) \right\} \\ &+ \frac{1}{4} \, M \, \left\{ \begin{array}{c} p_0 q_2 \, \left( \nu_2 - \nu_0 \right) \\ + \left( p_1 q_3 + p_3 q_1 \right) \, \left( \nu_3 - \nu_{-1} \right) \\ + \text{etc.} \end{array} \right. \, \left\{ k_c \cos \left( N + 2g \right) + k_s \sin \left( N + 2g \right) \right\} \\ &+ \frac{1}{4} \, M \, \left\{ \begin{array}{c} p_0 q_2 \, \left( \nu_0 - \nu_{-2} \right) \\ + \text{etc.} \end{array} \right. \, \left\{ k_c \cos \left( N - 2g \right) + k_s \sin \left( N - 2g \right) \right\} \\ &+ \frac{1}{4} \, M \, \left\{ \begin{array}{c} p_0 q_2 \, \left( \nu_0 - \nu_{-2} \right) \\ + \text{etc.} \end{array} \right. \, \left\{ k_c \cos \left( N - 2g \right) + k_s \sin \left( N - 2g \right) \right\} \\ &+ \frac{1}{4} \, M \, \left\{ \begin{array}{c} p_0 q_3 \, \left( \nu_3 - \nu_0 \right) \\ + \left( p_1 q_4 + p_3 q_1 \right) \, \left( \nu_4 - \nu_{-1} \right) \\ + \left( p_1 q_2 - p_2 q_1 \right) \, \left( \nu_2 - \nu_1 \right) \\ + \left( p_1 q_2 - p_2 q_1 \right) \, \left( \nu_2 - \nu_1 \right) \\ + \left( p_1 q_2 - p_2 q_1 \right) \, \left( \nu_2 - \nu_1 \right) \\ + \left( p_1 q_2 - p_2 q_1 \right) \, \left( \nu_2 - \nu_1 \right) \\ + \left( p_1 q_2 - p_2 q_1 \right) \, \left( \nu_2 - \nu_1 \right) \\ + \left( p_1 q_2 - p_2 q_1 \right) \, \left( \nu_2 - \nu_1 \right) \\ + \left( p_1 q_2 - p_2 q_1 \right) \, \left( \nu_2 - \nu_1 \right) \\ + \left( p_1 q_2 - p_2 q_1 \right) \, \left( \nu_2 - \nu_1 \right) \\ + \left( p_1 q_2 - p_2 q_1 \right) \, \left( \nu_2 - \nu_1 \right) \\ + \left( p_1 q_2 - p_2 q_1 \right) \, \left( \nu_2 - \nu_1 \right) \\ + \left( p_1 q_2 - p_2 q_1 \right) \, \left( \nu_2 - \nu_1 \right) \\ + \left( p_1 q_2 - p_2 q_1 \right) \, \left( \nu_2 - \nu_1 \right) \\ + \left( p_1 q_2 - p_2 q_1 \right) \, \left( \nu_2 - \nu_1 \right) \\ + \left( p_1 q_2 - p_2 q_1 \right) \, \left( \nu_2 - \nu_1 \right) \\ + \left( p_1 q_2 - p_2 q_1 \right) \, \left( \nu_2 - \nu_1 \right) \\ + \left( p_1 q_2 - p_2 q_1 \right) \, \left( \nu_2 - \nu_1 \right) \\ + \left( p_1 q_2 - p_2 q_1 \right) \, \left( \nu_1 - \nu_2 \right) \\ + \left( p_1 q_2 - p_2 q_1 \right) \, \left( \nu_2 - \nu_1 \right) \\ + \left( p_1 q_2 - p_2 q_1 \right) \, \left( \nu_1 - \nu_2 \right) \\ + \left( p_1 q_2 - p_2 q_1 \right) \, \left( \nu_1 - \nu_2 \right) \\ + \left( p_1 q_2 - p_2 q_1 \right) \, \left( \nu_1 - \nu_2 \right) \\ + \left( p_1 q_2 - p_2 q_1 \right$$

$$+ \frac{1}{4} M \begin{cases} p_0 q_3 & (\nu_0 - \nu_{-3}) \\ + (p_1 q_4 + p_4 q_1) & (\nu_2 - \nu_{-4}) \\ + (p_1 q_2 - p_2 q_1) & (\nu_{-1} - \nu_{-2}) \\ + \text{ etc.} \end{cases} \begin{cases} k_c \cos(N - 3g) + k_s \sin(N - 3g) \end{cases}$$

A law of the factors of  $k_c \cos(N + ug) + k_s \sin(N + ug)$  which will be noticed in the above expression, is this: Representing this factor by  $K_u$ , we have

$$K_u^i = K_u^{(i+u)},$$

the index i representing the coefficient of g in N, so that only half the values of K need be separately computed.

As the computation of  $r_1^2 \delta \rho$  from these formulæ can be arranged in such a way as to be very simple, the computation of the terms in which the index i' is -1 is here presented quite fully. The logarithms only are omitted, being used only in the cases in which they are more convenient than a table of products. In practice I find it convenient to write them in red ink immediately under the numbers which they represent.

First, to find M, it will be noticed that in the expression  $\frac{m'a}{a_1(1+m)}$ , the a in the numerator represents the mean distance of the disturbed planet, as deduced from the observed mean motion by the equation  $a^3n^2 = \mu(1+m)$  while  $a_1$  represents the mean motion of the outer planet. When the outer planet is the disturbed one, the ratio  $\frac{a}{a_1}$  would be unity, but that, to avoid a large class of second order terms,  $a_1$  has been corrected for perturbations in the beginning (p. 32). In the case of Uranus disturbed by Saturn, we have in consequence

$$\log \frac{a}{a_1} = 9.999803.$$

Whence

$$M = 285.44$$

in units of the sixth place of decimals.

Computing the values of  $p_i$  and  $q_i$  from (16) we find, for Uranus,

$$\begin{array}{lll} \frac{1}{2} \, M & p_1 q_1 & = + \ 142.56 \\ \frac{1}{2} \, M & p_2 q_2 & = + \ 0.0784 \\ \frac{1}{4} \, M & p_0 q_1 & = - \ 10.044 \\ \frac{1}{4} \, M (p_1 q_2 + p_2 q_1) = + & 3.3433 \\ \frac{1}{4} \, M (p_2 q_3 + p_3 q_2) = + & 0.0028 \\ \frac{1}{4} \, M & p_0 q_2 & = - & 0.2358 \\ \frac{1}{4} \, M (p_1 q_3 + p_3 q_1) = + & 0.118 \\ \frac{1}{4} \, M & p_0 q_2 & = - & 0.008 \\ \frac{1}{4} \, M (p_1 q_4 + p_4 q_1) = + & 0.005 \\ \frac{1}{4} \, M (p_1 q_2 - p_2 q_1) - + & 0.003 \end{array} \right]$$

In the computation the first three lines are copied from previous pages.

	811-				<i>i</i> ' = -	1				
i	-4	_3	-2	-1	0	+1	2	3	4	5
ν	-0.1459	-0.1709	-0.20610	-0.25960	-0.35062	-0.53994	-1.17363	+6.75940	+0.87113	+0.4656
		kc ks	+0.08 -0.08	$^{+1.23}_{-1.23}$	$+276.62 \\ +34.79$	-1508.18 +5.79	$^{+20.85}_{-286.59}$	$-79.56 \\ +194.17$	$-1.10 \\ +1.79$	$^{+0.03}_{+0.13}$
	+142.56 + 0.0784 - 10.044 + 3.3433 + 0.0028	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	0887 2047 0535 1797	14452 3690 0910 3338	28034 9675 1893 9140	$ \begin{array}{r}82301 \\ +7.0190 \\63368 \\ +7.1100 \end{array} $	+7.29934 +1.2218 +7.9330 +1.4110	+2.04476 +1.0055 -5.8883 +1.6392	-6.2938 +1.4913 -0.4056 -6.4417	-0.5535 -6.5186
	$\begin{array}{c} + & 0.0028 \\ - & 0.2358 \\ + & 0.118 \end{array}$	v <sub>3</sub> v <sub>-2</sub> v <sub>3</sub> v <sub>-1</sub>	39 144 369	-1.00 $280$ $968$	+6.96 823 +7.019	+1.13 $+7.299$ $+1.222$	+0.82 $+2.045$ $+1.005$	+0.86 $-6.294$ $+1.490$	+1.41	
	$\begin{array}{l} - & 0.008 \\ + & 0.005 \\ + & 0.0003 \end{array}$	ν <sub>3</sub> ν <sub>0</sub> ν <sub>4</sub> ν <sub>-1</sub> ν <sub>3</sub> ν <sub>-1</sub>	33 -1.00 09	$ \begin{array}{r}91 \\ +6.97 \\19 \end{array} $		+1.41 $+0.82$ $+7.93$	+1.64 +0.86 -5.89			
	142.56 0.0784	$\begin{array}{c} \times (\nu_2 - \nu_{-1}) \\ \times (\nu_3 - \nu_{-2}) \\ K_0 \end{array}$	-12.35 $-0.02$ $-12.37$	-20.60 - 0.03 -20.63	-39.965 - 0.075 -40.040	-117.327 +0.550 -116.777	$+1040.59 \\ +0.10 \\ +1040.69$	+291.49 +0.08 +291.57	$ \begin{array}{r} -897.2 \\ +0.1 \\ -897.1 \end{array} $	-78.8 - 0 5 -79.3
	- 10.044 + 3.3433 + 0.0028	$\begin{array}{c} \times (\nu_1 - \nu_0) \\ \times (\nu_2 - \nu_{-1}) \\ \times (\nu_3 - \nu_{-2}) \end{array}$	+0.532 -0.601 -0.001	+0.914 $-1.126$ $-0.003$	+1.901 $-3.056$ $+0.020$	+6.364 $+23.770$ $+0.003$	$   \begin{array}{r}     -79.68 \\     + 4.72 \\     0   \end{array} $	+59.14 + 5.48 0	$\begin{array}{c} +4.1 \\ -21.5 \\ 0 \end{array}$	
		$K_1 \atop K_{-4}$		$-0.20 \\ -0.07$	$-1.135 \\ -0.205$	+30.137 $-1.135$	$-74.96 \\ +30.14$	$\begin{array}{r} +64.62 \\ -74.96 \end{array}$	$-17.4 \\ +64.6$	
	2358 + .118	$\begin{array}{c} \times ({\scriptstyle \nu_2 - \nu_0}) \\ \times ({\scriptstyle \nu_3 - \nu_{-1}}) \\ K_{\scriptstyle 2} \\ K_{\scriptstyle -2} \end{array}$	+0.034 -0.043	+0.066 -0.114	+0.194 $+0.828$ $+1.022$ $-0.009$	$ \begin{array}{r} -1.721 \\ +0.144 \\ -1.577 \\ -0.048 \end{array} $	$ \begin{array}{r} -0.48 \\ +0.12 \\ -0.36 \\ +1.02 \end{array} $	+ 1.48 + 0.18 + 1.66 + 1.58		
	008 + .005	$\begin{array}{c} \times (\nu_1 - \nu_0) \\ \times (\nu_4 - \nu_1) \\ K_3 \\ K_{-3} \end{array}$	+ .003 005	+ .007 + .035		011 +.004 007 002	013 +.004 009 +.042			
		$K_0$ $k_c$ $K_1$ $k_c$ $K_1$ $k_c$ $K_1$ $k_c$ $K_2$ $k_c$ $K_3$ $k_c$ $K_4$ $k_c$ $K_5$ $k_c$ $K_6$ $k_7$ $k_c$ $K_7$ $k_0$ $K_8$ $k_0$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{r} -26 \\ 0 \\ -56 \\ 0 \\ +72 \\ 0 \\ +1 \\ -9 \\ 0 \\ -438 \\ 0 \\ +485 \\ -3 \\ +34 \end{array} $	$\begin{array}{c} -11076 \\ 0 \\ +1712 \\ 0 \\ +21 \\ 0 \\ 0 \\ -9343 \\ 0 \\ +8283 \\ 0 \\ -48 \\ -4 \\ -1112 \end{array}$	$\begin{array}{c} -\\ +\\ 176117\\ -314\\ +628\\ 0\\ +126\\ 0\\ 0\\ +176557\\ -438\\ -821\\ 0\\ -62\\ -1\\ +175235\\ \end{array}$	+21698 -45452 +5964 + 282 0 0 -17508 +8283 -1053 -26 -11 0 -10315	$\begin{array}{c} -23197 \\ -1563 \\ -71 \\ +2378 \\ 0 \\ 0 \\ 0 \\ -22453 \\ -821 \\ -195 \\ +485 \\ 0 \\ -2 \\ -22986 \end{array}$	+991 -5142 0 -8 0 +8 0 -4151 -1053 -5 -48 0 +30 -5227	$\begin{array}{c} -2\\ +19\\ 0\\ -132\\ 0\\ 0\\ -115\\ -195\\ -62\\ 0\\ -3\\ -375\\ \end{array}$
		$K_0$ $k_s$ $K_1$ $k_s$ $K_{-1}$ $k_s$ $K_{-1}$ $k_s$ $K_{-2}$ $k_s$ $K_{-2}$ $k_s$ $K_{-3}$ $k_s$ $r_1^2$ $\delta_P$ (sin) $\times .046915$ $\times .002751$ $\times .000168$ $\cos \phi \delta_P$ (sin)	+ 1 0 0 0 0 0 0 + 1 { 0 0 0 - 5 - 5 - 9	+ 26	-1393 0 -6 0 -293 0 -1692 0 -453 0 -860 + 13 -2992	$\begin{array}{c} -676 \\ -39 \\ -8637 \\ 0 \\ -306 \\ 0 \\ -9658 \\ -79 \\ -14666 \\ 0 \\ +215 \\ +2 \\ -24186 \end{array}$	-298254 +175 -14556 +36 -10 -312600 -453 +3669 -5 +30 0 -309359	-14666 +518 -27 0 0	-1606 +12548 -2 +104 0 0 +11044 +3669 +13 -860 0 -2 +13864	-10 -30 0 +322 0 -1 +281 +518 0 +215 0 -3 +961

In forming the next ten lines, it will be noticed that the value of  $v_u$  corresponding to any vertical column is found u columns to the right. It is therefore necessary to extend the line v two columns at each end. The extension on the right is, however, omitted for want of space. In performing the subtractions it will be convenient to copy the v's again on the lower edge of a horizontal strip of paper, and, in forming the differences  $v_u-v_u$  to lay the strip above the line of v's, and u-u columns to the right.

On the left of each line of differences is written the factor by which that line is to be multiplied.

The mode of formation of the K's is evident from the formula.

It will be seen that the same computation which gives  $K_u$  gives also  $K_{-u}$ , only the latter belongs u columns to the right.

Each  $k_e$  and  $k_s$  is multiplied in succession by all the K's which lie below it in the same column, but the product by  $K_u$  is to be written u columns to the right, and that by  $K_{-u}$  u columns to the left. The sum of the products in any one column-gives the coefficient of  $\frac{\cos}{\sin}$  (ig + il) in the development of  $r_1^2 \delta \rho$ .

This quantity being multiplied by  $\frac{dv_0}{ndt} = \frac{a^2 \cos \psi}{r_0^2}$  we have  $\cos \psi \delta \rho$ , which only needs to be multiplied by  $\sec \psi = 1.001103$  to give  $\delta \rho$ . The units of  $r_1^2 \delta \rho$  and  $\delta \rho$  correspond to the ninth place of decimals.

All the periodic terms are to be treated in this manner, all the series of values of  $k_e$  and  $k_s$ , including the constant term, being subjected to the same process. But, when i' and i are both zero,  $\nu$  will be infinite. Here we simply omit the  $\nu$ , treating it as if it were zero. We thus obtain the complete value of the terms with constant coefficients in  $r_1^2 \delta \rho$  and  $\delta \rho$  which are given in the following table. The terms multiplied by the time are still to be computed. They are derived from (20), which may be put in the form

$$r_1^2 \delta \rho = \frac{1}{2} M \{ \eta \sum p_u k_c^{(u)} - \xi \sum q_u k_s^{(u)} \} nt.$$

This expression is computed thus:

We have now

$$\begin{split} \Sigma p_u k_s^{(u)} &= +208.02; & \frac{1}{2} M \Sigma p_u k_s^{(u)} = +29689 \\ -\Sigma q_u k_s^{(u)} &= +20.93; & \frac{1}{2} M \Sigma q_u k_s^{(u)} = +2988 \\ r_1^2 \delta \rho &= -210 \ nt \\ &+ 2986 \ nt \cos \ g + 29681 \ nt \sin \ g \\ &+ 70 \ nt \cos 2g + 697 \ nt \sin 2g \\ &+ 2 \ nt \cos 3g + 24 \ nt \sin 3g, \end{split}$$

in units of the ninth place of decimals. The value of  $\cos \psi \delta \rho$  is obtained from them by multiplying by  $r_1^{-2}$ , exactly as in the case of the constant terms.

	374	$r_1$	δρ	cos	ψδρ	$\log M_{\nu}$	V <sub>c</sub>	v.
١						20.		
1	g l'	cos	sin	cos	sin			
ı	0, 0	—210 nt		-70 nt			+139n't	
I	1,	+2986 nt	+29681 nt	+2978 nt	+29633 nt			
ı	2,	+70 nt	+697 nt	+209  nt	+2084 nt			
١	3,	+2 nt	+24 nt	+14 nt	+139 nt			
ł	0, 0	355045		354347		oc	0	Mar E
1	1,	+14875	1503	-18411	-1496	2.45551	-2912	+14206
ı	2,	-283	+49	-1536	-21	2.25448	-639	+457
	3.	20	- 1	—112	_ 2	1.97839	-46	—8
	_2,_1	<u> </u>	+ 1	+ 3	— 9	1.7696	+ 1	+2
	-1,	<del>-1</del> 0	+ 8	+34	151	1.8698	+12	<del>99</del>
	0,	-9343 $+176557$	-1692 9658	-1112 $+175235$	—2992 —24186	2.00035 $2.18786$	-2876 +536512	$+10 \\ +160$
I	+1, 2,	<del>-17508</del>	-9658 -312600	<del>-113235</del> <del>-10315</del>	-24186 -309359	2.52504	+350312 $+1823$	<del></del>
ı	3,	-22453	-312000 $+78204$	-22986	+64029	3.28542	—13482	+18310
١	4,	<u>-4151</u>	+11044	_5227	+13864	2.39559	-293	+104
١	5,	<b>—115</b>	+281	<del>-373</del>	+961	2.1235	—13	0
ı	_1,-2	_ 1	+ 1	+ 1	_ 2	1.6292	+ 9	+7
ı	0,	56	-276	+32	-100	1.6993	-329	-1551
ł	+1,	+710	+3723	+1675	+3728	1.78303	+5874	+26114
1	2,	+20180	—13	+20583	+484	1.88683	-31660	+926
ı	3,	+7797	+6512	+8824	+6796	2.02348	-6019	-6860
ı	4,	+1534	+6202	+2054	+6230	2.22401	+243	-2172
ı	5,	+2071	<b>—</b> 5954	+2134	-5610	2.60786	+527	-421
ı	6,	653	+755	<b>—</b> 550	+494	2.98438	—190	20
	1,3	<b>—151</b>	+64	-137	+75	1.5772	-1464	+653
ı	2,	52	+221	+149	+229	1.63886	+231	-833
ı	3,	+4348	+15	+4420	+88	1.71074	-13050	+1
	4,	+1564	+1280	+1774	+1314	1.79691	-3225	-3126
	5, 6	+133 111	+685	+214 109	$+756 \\ +272$	1.9045 2.0479	—18 +144	—1943 —163
	6, 7,	—111 —163	+232 +87	—109 —168	$+212 \\ +100$	2.2634	+50	—105 —7
	3,—4	—28			+122	1.5408	+181	-638
	3,—4 4,	$-28 \\ +1223$	$+121 \\ +17$	$+31 \\ +1245$	$+122 \\ +41$	1.5408	<del></del>	—058 —58
	5,	+1225	+389	+545	+400	1.6488		<u>—1540</u>
	6,	+38	+201	+63	+221	1.7225	<b>—</b> 50	-590
	7,	-25	+53	23	+63	1.8012	+70	100
	8,	<b>—1</b> 5	+ 7	-16	+ 9	1.9229	E-Marie	-
	5,—5	+392	+12	+400	+18	1.4889	-2432	-74
	6,	+175	+138	+194	+142	1.5385	908	<b>—760</b>
	7,	+14	+77	+22	+84	1.5946	-40	-340
	8,	-10	+20	_ 9	+24	1.6589	+40	-70
	9,	<b>—</b> 5	+ 3	_ 5	+ 4	1.7345		
1		N			1			

#### Perturbations of Longitude.

The perturbations of the longitude are now to be computed by formulæ (24). To do this in the most simple way we remark that the numbers given on page 42, under the heading  $\frac{\partial R}{\partial \mathbf{v}}$ , are those represented in formula (42) by  $v_s$  and  $v_e$ . If we put

$$nt = t$$

equation (24) may be put into the form

$$\frac{d\delta v}{dt}$$
, =  $r_1^{-2}$   $\left\{ \frac{a}{1+m} \int \frac{\partial R}{\partial v} dt - 2\cos\psi \delta \rho \right\}$ ;

but we have from (42)

$$\int \frac{\partial R}{\partial v} dt = \sum \left( \frac{m'\nu}{a_1} v_c \sin N - \frac{m'\nu}{a_1} v_s \cos N \right).$$

If now we represent the numerical values of  $\cos 4\delta \rho$ , already found, by

$$\Sigma (\rho_s \sin N + \rho_c \cos N),$$

and if we substitute these expressions in the above value of  $\frac{d \hat{v}}{dt}$ , the latter will become

$$\frac{d \delta v}{d t'} = r_1^{-2} \Sigma \left\{ (\mathbf{v}_s - 2\rho_s) \sin N + (\mathbf{v}_s - 2\rho_s) \cos N \right\},$$

where we put for brevity

The numerical expression for  $r_1^{-2}$  is given on page 40, and by multiplying the quantities within brackets by this expression, after the manner explained on pages 40 and 41, we form the terms of  $\frac{d\delta v}{dt}$ . Multiplying each of these terms by its corresponding value of v, changing  $\cos$  to  $\sin$  and  $\sin$  to  $\cos$ , we have the coefficients in the expressions for  $\delta v$  given on page 50.

As previously mentioned, before commencing the above computation, I had computed all the perturbations of Uranus by the method of "perturbations of the elements," using the formulæ developed in my Investigation of the Orbit of Neptune. The two results are here placed side by side, for the purpose of comparison. The discrepancies in the various coefficients, expressed in thousandths of a second, are shown in the sixth and seventh columns.

It will be seen that the largest discrepancies, and indeed the only ones (with a single exception) exceeding one-tenth of a second, occur in the coefficients of the terms 2j-l aug 3g-l. Here the errors are almost certainly in the computation from perturbations of the elements. Owing to the long period of the term 3g-l they would not become sensible in the course of any one century.

PERTURBATIONS OF THE LONGITUDE OF URANUS PRODUCED BY THE ACTION OF SATURN, AND DEPENDING ON THE FIRST POWER OF THE DISTURBING FORCES.

1	100	ושע	PENDING ON TH	E FIRST POWER	OF THE DISTU	IBING F	INCES.		
			p. preceding	From pert.		Discr	epancy.	0.4349	294 δρ
	g, l'	sin "	cos	sin "	cos	sin "	cos "	cos	sin
ı	0, 0		+ 10.9690t		+10.9645t		.0045t		
ı	1,	1.230 nt	+ 12.231 nt	_1.228 nt	+12.271 nt	.002 nt	.040 nt	+13 nt	+128nt
1	2,	0.072 nt	+ 0.717 nt	-0.072 nt	+ 0.720 nt	0	.003 nt	+1 nt	+9nt
١	3,	0.004 nt	+ 0.043 nt	-0.004 nt	+ 0.043 nt	0	0	0	0
1	0, 0							1541	
ı	1,	+ 8.545	_ 4.735	+ 2.844	+ 1.013			80	6
ı	2,	+ 0.461	0.169	+ 0.133	+ 0.166			7	0
	3,	+ 0.028	- 0.005	+ 0.013	+ 0.014			0	0
	1,1	+ 0.036	+ 0.039	+ 0.032	+ 0.005	4	34	0	_ 1
	0,	+ 1.282	+ 0.718	+ 1.280	+ 0.719	2	1	_ 5	13
	1,	_20.817	+ 8.522	20.873	+ 8.595	56	73	+761	106
	2,	11.890	+143.463	. — 11.093	+143.465	797	2	45	<b>—1</b> 351
ı	3,	+ 49.30	+115.86	+ 49.62	+116.08	320	220	103	+ 280
ı	4,	+ 2.133	+ 5.616	+ 2.195	+ 5.621	62	5	24	+ 61
1	5,	+ 0.126	+ 0.329	+ 0.109	+ 0.331	17	2	_ 2	+ 4
ı	0,—2	+ 0.017	_ 0.017	+ 0.025	0.033	8	16	0	0
ı	1,	+ 0.042	+ 0.814	+ 0.034	+ 0.818	8	4	+ 7	+ 16
	2,	+ 4.110	- 0.009	+ 4.103	- 0.012	7	3	+ 89	+ 2
1	3,	+ 2.079	- 1.607	+ 2.106	1 676	27	69	+ 38	+ 30
-	4,	+ 0.648	- 1.830	+ 0.643	- 1.902	5	72	+ 9	+ 27
1	5,	+ 1.163	+ 2.956	+ 1.274	+ 2.991	111	35	+ 9	24
ı	6,	+ 0.503	+ 0.378	+ 0.556	+ 0.445	53	67	_ 2	+ 2
ł	1,—3	+ 0.034	+ 0.012	+ 0.036	+ 0.015	2	3	0	0
1	2,	+ 0.037	- 0.041	+ 0.014	0.050	23	9	+ 1	+ 1
1	3,	+ 0.824	- 0.019	+ 0.812	0.017	12	2	+ 19	0
	4,	+ 0.355	- 0.267	+ 0.351	- 0.263	4	4	+ 8	+ 6
	5,	+ 0.047	- 0.165	+ 0.039	- 0.191	8	26	+ 1	+ 3
	6,	- 0.026	- 0.063	- 0.028	- 0.066	2	3	0	+ 1
	7,	- 0.053	- 0.032	- 0.053	- 0.018	0	14	- 1	0
	3,—4	+ 0.006	- 0.022	0.005	0.023	11	1	0	+ 1
	4,	+ 0.228	- 0.008	+ 0.221	+ 0.002	7	10	+ 5	0
	5,	+ 0.103	- 0.077	+ 0.084	- 0.075	19	2	+ 2	+ 2
	6,	+ 0.013	- 0.044	+ 0.013	0.057	0	13	0	+ 1
	7,	- 0.005	- 0.013	- 0.001	- 0.015	4	2	0	0
	8,	- 0.003	- 0.002	0	+ 0.002	3	4	0	0
	5,—5	+ 0.074	- 0.003	+ 0.071	0	3	3	+ 2	0
	6,	+ 0.038	0.027	+ 0.023	0.026	15	1	+ 1	+ 1
	7,	+ 0.005	0.016	+ 0.005	- 0.025	0	9_	0	0
	8,	- 0.002	- 0.004	0	0.003	2	1	0	0
ļ			l .					1	

## Perturbations of Latitude.

These are computed from the formulæ (27) and (40), no reductions being made from  $\delta k$  and  $\delta \eta$  to  $\delta p$  and  $\delta q$ , but the perturbations of the latitude being computed directly from the former by (40). We have only to represent the expressions for  $\delta k$  and  $\delta \eta$  by

$$\delta k = -\sum a_c \cos N - \sum a_s \sin N$$
  
$$\delta r_i = \sum a_c \cos N + \sum a_s \sin N$$

and substitute  $\omega$  for  $\pi$  in the equations (40) from which  $\delta\beta$  is computed.

The principal steps of the computation are shown quite fully in the following table. The values of

$$\frac{\partial h}{\partial \gamma} = \frac{1}{2} \cos \frac{1}{2} \gamma \frac{\partial h}{\partial \sigma}$$

are first formed from those terms of h, on pages 37 and 38, which contain  $\sigma$  as a coefficient. Then, having for each original term of R

$$\frac{\partial R}{\partial \gamma} = \frac{m'}{a_1} \frac{\partial h}{\partial \gamma} \cos N$$

all the terms which have the same coefficients of  $\lambda$  and  $\lambda'$  in N are combined into two depending on g and l' as shown in the case of R on page 36. The coefficients of these terms, in units of the third place of decimals, are given in the columns headed  $\frac{\partial R}{\partial \gamma}$ .

The value of  $\frac{i\hbar}{2\sigma}$  sin N being formed for each term of R, all the terms depending on the same multiples of  $\lambda$  and  $\lambda'$  are combined into two, of which the coefficients are given under the proper heading. The terms of  $(i+j)\,\sigma h$  sin N being formed in like manner, we have, by adding the last two expressions, all the quantities which enter into the formulæ (27). To integrate these equations thus forming the numerical values of  $\delta k$  and  $\delta \eta$  we have only to multiply each term in the second, third, eighth, and ninth columns of the table by the corresponding values of  $\frac{m'a\nu}{a_1\cos\psi}$ , for which we may use the value of  $\frac{M\nu}{\sin 1''}$  already given.

The quantities given in the four columns under  $\delta k$  and  $-\delta \eta$  show the values of  $-a_s$ ,  $-a_c$ ,  $-a'_c$ ,  $-a'_s$ , corresponding to each argument. From these the terms of  $\delta \beta$  are formed by equation (40) with the modification mentioned above.

			PER	rurbat	ions o	F THE L	ATITUI	E PROD	UCED B	y Satu	RN.			
g l'	$\frac{\partial^R}{\partial r} =$	$\frac{m'}{a_1} \times$	$\Sigma \frac{ih}{2\sigma}$	sin N	Σ (i+j)	σh sin N	$\frac{dn}{dt}$	Mn ×	8	ìk .		<b>—</b> δη	δ	β
i i'	cos	sin	sin	cos	sin	cos	sin	cos	sin //	eos //	cos	sin //	sin //	cos
0, 0	_10.82	0	0	0	0	+0.008	0.00	+ .008						+0.192
1,				-		+0.84								
2,	1					+0.05								
3,	+ 1.31	- 1.71	+1.31	+ 1.71	+ 0.01	0.00	+ 1.32	+ 1.71	-0.026	-0.033	+0.026	-0.033	-0.008	+0.003
-2,-1	+ 1.0	+ 0.1	_1.0	0.1	0.00	0.00	_ 1.0	_ 0.1	+0.012	_0.001	+0.012	-0.001	0.000	0.000
_1,						+0.02								
0,						0.00								
+1,	+46.67		0.00			-0.02					-14			
2,	1.84	_ 2.86	_0.99	_ 0.20	+ 0.93	+1.22	- 0.06	+ 1.02	_0.127	+0.197	+0.004	+0.070	+2.218	+1.920
3,	+ 0.90	<b>—</b> 6.98	+0.78	+ 6.44	+ 0.12	+0.16	+ 0.90	+ 6.60	-0.358	-2 781	+0.358	-2.630	+0.091	-0.071
4,	+ 1.09	- 1.38	+1.09	+ 1.38	+ 0.02	+0.01	+ 1.11	+ 1.39	-0.056	-0.071	+0.057	-0.071	-0.048	+0.056
1 0	+ 7.6	1.5	<b>—</b> 7.6	1 7 5	. 0.00	0.00	7.0	1.75	Looge	L0.010	10.00	1.0.012	T0 003	1.0.004
	+ 1.3					+0.53					+ 4			
0,						<b>—7.35</b>								
+1, 2,	-14.51		0.00			_0.21								
						+1.11								
4,						+0.22								
5,						+0.02								
,	0.00	0.00	1 0.00	1 (100)	7 0.02	0.02	7 0.02	7- 1.01	10.001	70.000	0.000	1 0.001		
2,-3	- 1.17	+ 0.86	+1.22	+ 0.97	+ 0.09	+0.33	+ 1.31	+ 1.30	-0.010					
3,	- 8.54		0.00	-15	<b>— 4.34</b>		<b>— 4.</b> 34					0	1/100	
4,						+0.85								_
				100		+0.22	1/2				CALCO			
6,	+ 0.55	- 0.66	+0.55	+ 0.66	+ 0.02	+0.02	+ 0.57	+ 0.68	+0.013	+0.015	0.013	+0.016	+0.004	<u>0.001</u>
3,-4	- 0.72	+ 0.47	+0.82	+ 0.78	+ 0.09	+0.32	+ 0.91	+ 1.10	-0.005	-0.003	-0.006	+0.008	+0.022	<b>0.02</b> 0
. 4,	<b> 4.</b> 80		0.00			-0.02								
5,	_ 1.41	- 1.09	-0.01			+0.59	1000				-			
6,	+ 0.12	- 1.3	+0.12	+ 1.0	- 0.02	+0.19	+ 0.10	+ 1.2	+0.001	+0.014	-0.001	+0.013	+0.004	+0.002
5,—5	<b> 2.64</b>	0	0	0	- 1.35	+0.04	<b>— 1.</b> 35	+ 0.04	-0.017	0	+0.008	0		
					Secul	ar terms	$\begin{cases} \delta k = - \\ \delta \beta = - \end{cases}$	- 4".77 - 4".77	T T cos v.					

#### CHAPTER III.

#### PERTURBATIONS PRODUCED BY NEPTUNE AND JUPITER.

THE perturbations of Uranus by Neptune were originally computed with elements of both planets quite different from those finally adopted. But the last computations, on which the concluded values of the perturbations depend, were made with the concluded elements of Neptune found in my investigation of the orbit of that planet. They are as follows:

	0	,	"	
π,	43	17	30	
θ,	130	7	33	
ε,	335	5	39	
φ,	1	47	1	.6
n,		7	864	.935
е,	0.0	00849	962	
$\log a$ ,	1.4	1781	41	
Mass,		1700	0	

Hence follow the following functions of the elements of Neptune and Uranus:

```
\alpha = 0.638195
\omega = 12^{\circ} 44' 58''
\omega' = 247 45 20
\gamma = 1 30 29.6
\sigma = \sin \frac{1}{2} \gamma = 0.013161
M = 37.522 (in units of 6th place of decimals).
```

From these values of the elements are obtained the following values of the various terms in the development of the perturbative function, and of  $\nu$ . As the developments have been formed on the same principle as in the case of Saturn, it is deemed unnecessary to give the details of the process. It is only necessary to remark that the indices i' and i are the coefficients of l' and g respectively, the mean longitude of Neptune, or l', being counted from the perihelion of Uranus.

<sup>&</sup>lt;sup>1</sup> Smithsonian Contributions to Knowledge, Vol. XV.

				Action of	NEPTUNE	de .	3, 14		
	R =	$\frac{m'}{a_1}$ ×	$\frac{\partial R}{\partial v} =$	$\frac{m'}{a_1}$ ×	$\frac{\partial R}{\partial \rho} =$	$\frac{m'}{a_1} \times$	Q=-	$\frac{m'}{a_1}$ ×	ν
i' i 0, 0 + 1 + 2 + 3	$ \begin{array}{c c} h_c \\ +1135.63 \\ -18.07 \\ +0.41 \\ 0 \end{array} $	$\begin{vmatrix} h_8 \\ 0 \\ -1.25 \\ -0.03 \\ 0 \end{vmatrix}$	$\begin{array}{ c c c c c }\hline v_8 & & & \\ 0 & & & \\ + & 1.01 & & \\ \hline - & 0.6 & & \\ 0 & & & \\ \end{array}$	$ \begin{vmatrix} v_c \\ + 0.202 \\ - 1.23 \\ - 0.1 \\ 0 \end{vmatrix} $	$ \begin{array}{c} \cos \\ +368.26 \\ -64.80 \\ +2.98 \\ 0 \end{array} $	$\begin{vmatrix} \sin & 0 \\ -5.89 \\ +0.12 \\ 0 \end{vmatrix}$	$k_c$ +368.26 -100.94 + 3.82	$\begin{vmatrix} k_{\theta} \\ 0 \\ -8.39 \\ +0.06 \\ 0 \end{vmatrix}$	+ 1.0 + 0.5 + 0.33333
1,— 3 — 2 — 1 0 + 1 + 2	$\begin{array}{c} + & 0.21 \\ - & 5.21 \\ + & 134.19 \\ - & 25.45 \\ + & 1.12 \\ - & 0.05 \end{array}$	$ \begin{array}{r} -0.01 \\ -0.62 \\ +0.30 \\ -10.43 \\ +1.19 \\ +0.01 \end{array} $	$\begin{array}{c} + & 0.7 \\ - & 4.90 \\ + 133.98 \\ - & 18.06 \\ + & 0.5 \\ + & 0.02 \end{array}$	$ \begin{array}{r} -0.2 \\ +1.27 \\ -0.08 \\ +0.02 \\ -0.1 \\ +0.02 \end{array} $	$\begin{array}{r} + & 1.6 \\ - & 29.5 \\ +509.94 \\ - & 84.57 \\ + & 5.83 \\ - & 0.24 \end{array}$	$\begin{array}{c} + 0.2 \\ + 0.6 \\ + 0.77 \\ -11.47 \\ + 0.82 \\ 0 \end{array}$	$\begin{array}{r} + 2.1 \\ - 43.5 \\ + 1057.49 \\ - 84.57 \\ + 7.31 \\ - 0.32 \end{array}$	+ 0.1 - 1.1 + 1.99 - 11.47 + 1.07 + 0.02	$\begin{array}{c} -0.40158 \\ -0.67107 \\ -2.04023 \\ +1.96137 \\ +0.66232 \\ +0.39843 \end{array}$
2,— 4 — 3 — 2 — 1 0 + 1	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{r} -0.03 \\ -1.01 \\ +0.36 \\ -3.180 \\ +0.46 \\ -0.01 \end{array} $	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{r} 0 \\ + 3.1 \\ - 0.75 \\ + 3.203 \\ - 0.4 \\ + 0.02 \end{array} $	$\begin{array}{c} + 2.5 \\ + 18.7 \\ + 9 7.82 \\ -171.79 \\ + 12.24 \\ - 0.51 \end{array}$	$\begin{array}{r} + 0.1 \\ - 2.4 \\ + 1.25 \\ -13.13 \\ + 1.84 \\ - 0.08 \end{array}$	$\begin{array}{r} + 4.8 \\ + 59.7 \\ +2491.69 \\ +5931.21 \\ + 12.24 \\ - 0.60 \end{array}$	$\begin{array}{c} 0 \\ -5.5 \\ +2.72 \\ +309.82 \\ +1.84 \\ -0.09 \end{array}$	$\begin{array}{c} -0.33554 \\ -0.50497 \\ -1.02009 \\ +50.7820 \\ +0.98069 \\ +0.49512 \end{array}$
3,— 5 — 4 — 3 — 2 — 1	$\begin{array}{r} + & 0.83 \\ + & 12.09 \\ + & 200.37 \\ - & 52.33 \\ + & 5.05 \\ - & 0.24 \end{array}$	- 0.04 - 0.96 - 0.04 - 9.88 + 1.56 - 0.07	$\begin{array}{c} + 27 \\ + 36.9 \\ + 601.13 \\ - 150.02 \\ + 13.8 \\ - 0.58 \end{array}$	$     \begin{array}{r}       + 0.2 \\       + 3.8 \\       - 0.42 \\       + 19.81 \\       - 3.1 \\       + 0.15     \end{array} $	$\begin{array}{r} + 3.0 \\ + 34.5 \\ +717.94 \\ -190.33 \\ + 20.12 \\ - 1.11 \end{array}$	$\begin{array}{r} -0.1 \\ -3.6 \\ +0.81 \\ -27.51 \\ +4.65 \\ -0.30 \end{array}$	$\begin{array}{r} + 5.5 \\ + 73.6 \\ +1535.51 \\ -635.23 \\ + 1.0 \\ - 1.11 \end{array}$	$\begin{array}{c} - & 0.2 \\ - & 6.7 \\ + & 0.65 \\ -111.69 \\ - & 1.2 \\ - & 0.30 \end{array}$	- 0.28814 - 0.40478 - 0.68006 - 2.12559 + 1.88844 + 0.65378
4,— 6 — 5 — 4 — 3 — 2 — 1	$\begin{array}{r} + & 0.75 \\ + & 9.47 \\ + & 111.16 \\ - & 38.58 \\ + & 5.205 \\ - & 0.36 \end{array}$	$\begin{array}{c} -0.07 \\ -0.79 \\ -0.12 \\ -7.43 \\ +1.896 \\ -0.17 \end{array}$	+ 3.2 + 38.3 +444.7 -149.10 + 19.54 - 1.28	$\begin{array}{c} + 0.3 \\ + 4.0 \\ - 0.18 \\ + 22.37 \\ - 5.50 \\ + 1.49 \end{array}$	$   \begin{array}{r}     + 3.4 \\     + 38.5 \\     +512.22 \\     -178.15 \\     + 25.30 \\     - 1.90   \end{array} $	$\begin{array}{c} -0.2 \\ -3.9 \\ +0.35 \\ -27.95 \\ +7.19 \\ -0.70 \end{array}$	+5.7 $+70.4$ $+965.7$ $-419.12$ $-503.3$ $-1.21$	$\begin{array}{c} - & 0.4 \\ - & 6.6 \\ - & 0.1 \\ - & 74.36 \\ -185.4 \\ - & 0.37 \end{array}$	$\begin{array}{r} -0.25249 \\ -0.33777 \\ -0.51004 \\ -1.04100 \\ +25.3910 \\ +0.96210 \end{array}$
5,— 7 — 6 — 5 — 4 — 3 — 2 — 1	+ 0.65 + 6.97 + 63.03 - 27.43 + 4.84 - 0.45 + 0.03	$\begin{array}{c} -0.07 \\ -0.59 \\ -0.16 \\ -5.32 \\ +1.81 \\ -0.24 \\ +0.02 \end{array}$	+ 3.5 + 35.1 +315.3 -133.4 + 23.0 - 2.09 + 0.12	$\begin{array}{c} + 0.4 \\ + 3.4 \\ + 0.1 \\ + 21.4 \\ - 7.0 \\ + 0.90 \\ - 0.06 \end{array}$	$\begin{array}{c} + & 3.5 \\ + & 36.7 \\ + & 354.8 \\ - & 153.6 \\ + & 27.82 \\ - & 2.77 \\ + & 0.18 \end{array}$	$\begin{array}{r} -0.3 \\ -3.4 \\ -0.1 \\ -25.3 \\ +8.57 \\ -1.14 \\ +0.09 \end{array}$	$\begin{array}{c} + 5.5 \\ + 60.9 \\ + 612.0 \\ -304.8 \\ + 92.2 \\ + 0.48 \\ + 0.15 \end{array}$	- 0.5 - 5.5 - 0.7 - 54.6 + 32.7 + 0.57 + 0.07	$\begin{array}{c} -0.22468 \\ -0.28984 \\ -0.40804 \\ -0.68929 \\ -2.21843 \\ +1.82073 \\ +0.6455 \end{array}$
6,— 7 — 6 — 5 — 4 — 3 — 2	+ 4.93 + 36.16 - 19.04 + 4.14 - 0.490 + 0.036	$\begin{array}{c} -0.41 \\ -0.17 \\ -3.74 \\ +1.59 \\ -0.271 \\ +0.026 \end{array}$	+ 29 8 +217.1 -111.6 + 23.9 - 2.79 + 0.20	$   \begin{array}{r}     + 2.7 \\     + 0.4 \\     + 18.8 \\     \hline     - 7.8 \\     + 1.30 \\     \hline     - 0.12   \end{array} $	$\begin{array}{r} + 31.5 \\ +239.9 \\ -125.7 \\ + 27.76 \\ - 3.42 \\ + 0.28 \end{array}$	$\begin{array}{r} -2.9 \\ -0.4 \\ -21.4 \\ +9.06 \\ -1.55 \\ +0.16 \end{array}$	$   \begin{array}{r}     + 49.0 \\     +387.4 \\     -223.8 \\     + 63.0 \\     + 46.40 \\     + 0.14   \end{array} $	$\begin{array}{r} -4.4 \\ -1.1 \\ -40.6 \\ +22.6 \\ +26.01 \\ +0.06 \end{array}$	$\begin{array}{l} -0.2538 \\ -0.3400 \\ -0.5152 \\ -1.0628 \\ +16.9273 \\ +0.9443 \end{array}$
7,— 8 — 7 — 6 — 5 — 4 — 3	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} -0.28 \\ -0.16 \\ -2.54 \\ +1.31 \\ -0.276 \\ +0.034 \end{array}$	+24.0 $+146.4$ $-89.2$ $+23.0$ $-3.25$ $+0.28$	$\begin{array}{c} + 2.1 \\ + 0.4 \\ +15.4 \\ - 7.7 \\ + 1.61 \\ - 0.19 \end{array}$	$\begin{array}{c} + 25.5 \\ + 160 0 \\ - 98.9 \\ + 26.0 \\ - 3.79 \\ + 0.37 \end{array}$	$\begin{array}{c} -2.5 \\ -0.6 \\ -17.2 \\ +8.8 \\ -1.87 \\ +0.24 \end{array}$	$ \begin{array}{r} + 37.8 \\ + 245.3 \\ - 163.1 \\ + 49.8 \\ - 12.83 \\ - 0.09 \end{array} $	$ \begin{array}{r} -3.5 \\ -1.3 \\ -29.8 \\ +18.0 \\ -6.99 \\ -0.12 \end{array} $	$\begin{array}{c} -0.2257 \\ -0.2914 \\ -0.4113 \\ -0.6988 \\ -2.3198 \\ +1.7577 \end{array}$
8,— 9 — 8 — 7 — 6 — 5 — 4	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{r} -0.20 \\ -0.13 \\ -1.71 \\ +1.05 \\ -0.26 \\ +0.039 \end{array} $	+ 18.8 + 96.6 - 68.9 + 21.0 - 3.5 + 0.37	$\begin{array}{c} + 1.6 \\ + 0.3 \\ + 12.1 \\ - 7.1 \\ + 1.8 \\ - 0.26 \end{array}$	$\begin{array}{c} + 19.5 \\ + 105.0 \\ - 75.5 \\ + 23.2 \\ - 3.90 \\ + 0.45 \end{array}$	$\begin{array}{r} -2.1 \\ -0.7 \\ -13.1 \\ +8.1 \\ -1.99 \\ +0.31 \end{array}$	$\begin{array}{c} + 28.1 \\ + 154.8 \\ - 117.7 \\ + 40.0 \\ - 8.8 \\ - 4.50 \end{array}$	The latest and the la	- 0.2032 - 0.2550 - 0.3423 - 0.5205 - 1.0855 +12.6955
9,— 9 — 8 — 7 — 6 — 5	$ \begin{array}{cccc} + & 7.0 \\ - & 5.9 \\ + & 2.07 \\ - & 0.39 \\ + & 0.050 \\ + & 4.1 \end{array} $	$ \begin{array}{c} -0.1 \\ -1.13 \\ +0.81 \\ -0.25 \\ +0.042 \\ -0.1 \end{array} $	$ \begin{array}{c cccc} + & 63.4 \\ - & 51.9 \\ + & 18.1 \\ - & 3.4 \\ + & 0.43 \end{array} $ $ + & 43. $	$ \begin{array}{c cccc} + & 0.1 \\ + & 9.1 \\ - & 6.4 \\ + & 1.9 \\ - & 0.32 \end{array} $	$ \begin{array}{c} + 68.2 \\ - 56 3 \\ + 19.8 \\ - 3.78 \\ + 0.51 \\ + 44.3 \end{array} $	$ \begin{array}{c c} -0.6 \\ -9.9 \\ +7.0 \\ -2.02 \\ +0.36 \\ -0.5 \end{array} $	$\begin{array}{c c} + & 31.8 \\ - & 7.1 \\ + & 1.72 \end{array}$	$ \begin{array}{c c} - & 15.2 \\ + & 11.7 \\ - & 4.1 \\ + & 1.38 \end{array} $	- 0.2267 - 0.2931 - 0.4147 - 0.7085 - 2.4308 - 0.2040
- 9 - 8 - 7 - 6	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	- 0.8 + 0.6 - 0.2 + 0.04	-40. + 14.7	$\begin{array}{c c} + 6. \\ - 5.6 \\ + 1.9 \\ - 0.37 \end{array}$	$\begin{array}{c c} - 42.0 \\ + 16.1 \\ - 3.5 \end{array}$	$ \begin{array}{c c} -7.0 \\ +6.0 \\ -1.9 \\ +0.40 \end{array} $	- 60. + 25.1 - 5.8	$\begin{array}{c c} - 11. \\ + 9.3 \\ - 3.4 \end{array}$	- 0.2563 - 0.3446 - 0.5259 - 1.1092

## The term of Long Period.

From the expressions for the perturbations of Uranus, subsequently given, it will be seen that several of the terms have very large coefficients, that of  $\sin(2l'-g)$  being nearly an entire degree. The magnitude of most of the terms in which i' is even arises from the near approach to commensurability in the mean motions of the two planets. Twice the mean annual motion of Neptune exceeds that of Uranus by only 303".8. The elements of the orbits of both planets will therefore, in consequence of their mutual action, be affected with a slow oscillation, having a period of about 4266 years. The employment of these large terms and the great inconveniences to which they will give rise, especially in the corrections of the elements of Uranus, may be avoided by the device employed in the theory of Neptune. The following are the essential features of this method:

First, all the perturbations arising from that portion of the perturbative function in which the coefficient of the time is 2n'-n or its multiples are considered and developed as perturbations of the elements.

Secondly, the arbitrary constants to be added to the integrals of these perturbations are so taken that the perturbations shall vanish at the epoch 1850.0.

In other words, the perturbations in question will be treated as producing secular variations of the elements of the orbit, only, instead of being developed in powers of the time, these variations will be retained in their rigorous form.

The formulæ for the computations of the perturbations in question, are as follows:

Let

$$\frac{m'}{a_1} h \cos (i'l' + il + j\omega' + j\omega) = \frac{m'}{a_1} \cos N$$

be any term of the perturbative function, h being a function of  $\alpha$ , e, and  $\sigma$ .

$$\sin \psi = e$$

$$g = \cos \psi \tan \frac{1}{2} \psi$$

$$\iota = -(i' + i + j' + j)$$

$$\nu = \frac{n}{i'n' + in'}$$

For each such term, compute

$$A = 2ih$$

$$L = -3ivh - 2\frac{\partial h}{\partial p} + \frac{\partial h}{\partial e}$$

$$eW = \cos\psi \frac{\partial h}{\partial e}$$

$$E = -h(ig + j\cot\psi)$$

$$T = \frac{1}{2}\frac{\partial h}{\partial \sigma}$$

$$I = \frac{1}{2}\iota\frac{h}{\sigma} + (i+j)\sigma h.$$

The corresponding perturbations of the elements may then be put into the form

$$\delta \log a = M_{\nu}A \cos N + \delta n_0,$$
 $\delta l = M_{\nu}L \sin N + \delta l_0,$ 
 $e \delta \pi = M_{\nu}eW \sin N + e \delta \pi_0,$ 
 $\delta e = M_{\nu}E \cos N + \delta e_0,$ 
 $\delta \gamma = M_{\nu}I \cos N + \delta \gamma_0,$ 
 $\tan \gamma \delta \tau = M_{\nu}T \sin N + \tan \gamma \delta \tau_0.$ 

Here,  $\delta n_0$ ,  $\delta l_0$ , etc., are arbitrary constants so taken that  $\delta \log a$ ,  $\delta l$ , etc., shall vanish at the fundamental epoch.

All the terms depending on the same values of i and i are to be combined into a single one. And it will save labor to make this combination at as early a stage as possible in the computation; that is, to multiply the various values of h,  $\frac{\partial h}{\partial v}$ ,  $\frac{\partial h}{\partial e}$ ,  $\frac{\partial h}{\partial \sigma}$ , and E by the sines and cosines of  $j'\omega' + j\omega$ , and afterward proceed

with the sums of the products according to the proper modification of the formulæ.

Thus are obtained the following long period perturbations of the elements of Uranus:

$$\delta l = -3474.32 \sin(2l' - g) + 180.10 \cos(2l' - g) + 146.72 \sin(4l' - 2g) - 54.10 \cos(4l' - 2g) - 8.97 \sin(6l' - 3g) + 5.03 \cos(6l' - 3g) + 0.64 \sin(8l' - 4g) - 0.53 \cos(8l' - 4g) + \cos \tan = 3320''.18.$$

$$e\delta \pi = -484.96 \sin(2l' - g) + 0.73 \cos(2l' - g) + 38.06 \sin(4l' - 2g) - 7.06 \cos(4l' - 2g) - 3.61 \sin(6l' - 3g) + 1.38 \cos(6l' - 3g) + 0.33 \sin(8l' - 4g) - 0.15 \cos(8l' - 4g) + \cos \tan = 465''.23.$$

$$= -484.21 \cos(2l' - g) - 0.29 \sin(2l' - g) + 38.21 \cos(4l' - 2g) + 7.16 \sin(4l' - 2g) - 3.61 \cos(6l' - 3g) - 1.40 \sin(6l' - 3g) + 0.33 \cos(8l' - 4g) + 0.15 \sin(8l' - 4g) - \cos \tan = 158''.59.$$

$$\delta n = +2277 \cos(2l' - g) + 120 \sin(2l' - g) - 198 \cos(4l' - 2g) - 78 \sin(4l' - 2g) + 18 \cos(6l' - 3g) + 7 \sin(6l' - 3g) + \cos (6l' - 3g) + 18 \cos(6l' - 3g) + 7 \sin(6l' - 3g) + \cos (6l' - 3g) +$$

The variations of the elements which fix the position of the plane of the orbit are here omitted, because their nature is such that it is indifferent in which form they are developed.

These expressions are reduced to perturbations of the co-ordinates by the follow-

ing formulæ. Express the usual developments of the longitude and logarithm of radius vector in the form

 $v = l + \sum V_i \sin ig;$  $\rho = p + \sum R_i \cos ig.$ 

Put also

$$\begin{split} V_{i} &= \frac{\partial V_{i}}{\partial e} \\ V_{i}' &= \frac{i}{e} V_{i} \\ R_{i}' &= \frac{\partial R_{i}}{\partial e} \\ R_{i}'' &= -\frac{i}{e} R_{i}. \end{split}$$

Express any set of corresponding terms of the preceding perturbations in the form

$$\ell l = L_s \sin N + L_c \cos N;$$
 $e^{\xi}l - e\delta\pi = F_s \sin N + F_c \cos N;$ 
 $\delta e = E_c \cos N + E_s \sin N;$ 
 $\delta p = A_s \cos N + A_s \sin N.$ 

We shall then have

$$2\delta v = \sum (V''_{i}F_{s} + V'_{i}E_{c})\sin(N + ig) + \sum (V''_{i}F_{s} - V'_{i}E_{c})\sin(N - ig) + \sum (V''_{i}F_{c} - V'_{i}E_{s})\cos(N + ig) + \sum (V''_{i}F_{c} + V'_{i}E_{s})\cos(N - ig) + 2\delta l$$

$$2\delta\rho = \sum (R'_{i}E_{o} - R''_{i}F_{s})\cos(N + ig) + \sum (R'_{i}E_{o} + R''_{i}F_{s})\cos(N - ig) + \sum (R'_{i}E_{s} + R''_{i}F_{o})\sin(N + ig) + \sum (R'_{i}E_{s} - R''_{i}F_{o})\sin(N - ig) + 2\delta\rho$$

The numerical values of V, V, R', and R" are as follows:

$$\begin{array}{llll} V_1 = & 1.99835 & V''_1 = & 1.99945 \\ V_2 = & 0.11713 & V''_2 = & 0.11722 \\ V_3 = & 0.00714 & V''_3 = & 0.00714 \\ V_4 = & 0.00044 & V''_4 = & 0.00044 \\ R'_0 = & + 0.02348 & & & & \\ R'_1 = & -0.99753 & R''_1 = & +0.99917 \\ R_2 = & -0.07020 & R''_2 = & +0.07030 \\ R'_3 = & -0.00466 & R''_3 = & +0.00467 \end{array}$$

The final results of the entire computations are given in the following table: In the columns  $\delta v_1$ , we have the complete perturbations of the longitude computed by the direct method from the values of  $\frac{\partial R}{\partial v}$ ,  $\frac{\partial R}{\partial \rho}$ , Q, etc., already given. Next we have, under the caption  $\delta v_2$ , the perturbations of the true longitude deduced from the long period perturbations of the elements, as set forth in the last paragraph, omitting the constants added to the perturbations. Under  $\delta v_3$  we have the 8 April, 1873.

perturbations of the longitude deduced from all the remaining terms of the perturbations of the elements. The sum of the columns  $\delta v_2$  and  $\delta v_3$  shows the entire perturbations computed by the method of variation of elements. Thus, in  $\delta v_1$  and  $\delta v_2 + \delta v_3$  we have two complete sets of perturbations computed by methods entirely independent. The differences of the results, expressed in thousandths of a second, are given in the last two columns of the table.

This comparison gives rise to remarks similar to those suggested by the perturbations of Saturn computed by the same methods. The only terms in which the difference of results amounts to as much as one-tenth of a second are those of very long period, and those very nearly the period of Uranus, where a more accurate value is not at present of great importance, because the error will be compensated by the corrections of the element during several centuries.

	PERTUR	BATIONS OF TH	E Longitude	of Uranus	PRODUCED H	BY NEPTUNI	c.	
	δ	$v_{\mathbf{i}}$		$\delta v_2$	δ	v <sub>3</sub>	Discre	epaney.
ľ g	sin "	cos	sin	cos	sin	cos	sin	cos
0, 0 1 2	065 nt 004 nt	-0.4262 t -1.181 nt -0.069 nt						
0, 0 -1 -2 -3	$ \begin{array}{cccc} + & 0.697 \\ + & 0.046 \\ + & 0.003 \end{array} $	- 0.088 - 0.005						
1,—3 —2 —1 0 —1 .—2	$\begin{array}{cccc} + & 0.147 \\ + & 2.509 \\ + & 39.658 \\ + & 4.257 \\ + & 0.280 \\ + & 0.017 \end{array}$	- 0.001 - 0.019 - 0.080 - 0.511 - 0.032 - 0.002			$\begin{array}{c} + 0.146 \\ + 2.509 \\ + 39.673 \\ + 4 249 \\ + 0.275 \end{array}$	-0.002 -0.010 -0.081 -0.478 -0.032	1 0 15 8 5	1 9 1 33 0
2,—4 —3 —2 —1 0 —1	$\begin{array}{r} + & 2.978 \\ + & 49.015 \\ + & 840.93 \\ - & 3475.4 \\ - & 162.07 \\ - & 9.447 \end{array}$	$\begin{array}{c} + & 0.027 \\ + & 0.413 \\ + & 7.388 \\ + & 180.36 \\ + & 8.01 \\ + & 0.468 \end{array}$	$\begin{array}{r} + & 2.89 \\ + & 47.22 \\ + & 805.64 \\ - & 3474.32 \\ - & 161.96 \\ - & 9.50 \end{array}$	+ '0.03 + 0.44 + 7.43 +180.10 + 8.01 + 0.47	+ 0.098 + 1.797 +35.355 - 0.700 - 0.067	$\begin{array}{c} -0.002 \\ -0.021 \\ -0.028 \\ +0.095 \\ +0.015 \end{array}$	10 2 65 380 43	1 6 14 165 15
3,—5 —4 —3 —2 —1 0	- 0.076 - 1.162 - 17.286 - 22.085 - 0.673 - 0.037	$\begin{array}{c} 0.000 \\ 0.000 \\ + 0.228 \\ + 4.037 \\ + 0.082 \\ + 0.006 \end{array}$			$\begin{array}{c} -0.077 \\ -1.153 \\ -17.285 \\ -22.077 \\ -0.682 \end{array}$	$\begin{array}{c} -0.003 \\ -0.011 \\ +0.229 \\ +4.020 \\ +0.079 \end{array}$	1 9 1 8 9	3 11 1 17 3
4,—6 —5 —4 —3 —2 —1	$\begin{array}{c} - & 0.036 \\ - & 0.558 \\ - & 7.968 \\ - & 75.00 \\ + & 146.78 \\ + & 6.960 \end{array}$	$\begin{array}{c} + & 0.002 \\ + & 0.037 \\ + & 0.750 \\ + & 12.832 \\ - & 54.218 \\ - & 2.579 \end{array}$	$\begin{array}{c} -0.015 \\ -0.25 \\ -4.08 \\ -69.55 \\ +146.72 \\ +6.81 \end{array}$	$\begin{array}{c} +\ 0.002 \\ +\ 0.04 \\ +\ 0.68 \\ +11.67 \\ -54.10 \\ -\ 2.63 \end{array}$	- 0.027 - 0.315 - 3.908 - 5.733 + 0.126	$\begin{array}{c} -0.003 \\ -0.007 \\ +0.059 \\ +1.067 \\ -0.079 \end{array}$	6 7 20 283 66	3 4 11 95 39

		PERTURBAT	TIONS OF THE	Longitude	_Continued	l.	State	
	8	v <sub>1</sub> -	δι	v <sub>2</sub>	80	's	Discrep	pancy.
l' g 5,— 7	sin //0.009	0,000	sin	cos	sin 0.015		sin 6	cos
$     \begin{array}{r}       -6 \\       -5 \\       -4 \\       -3 \\       -2 \\       -1     \end{array} $	$     \begin{array}{r}       -0.103 \\       -0.986 \\       +3.366 \\       +3.210 \\       +0.077 \\       +0.005     \end{array} $	+0.006 -0.042 -0.670 -1.169 -0.017 -0.001			-0.113 $-0.994$ $+3.370$ $+3.227$ $+0.075$	-0.004 -0.042 -0.662 -1.186 -0.002	10 8 4 17 2	10 0 8 17 15
6,— 7 — 6 — 5 — 4 — 3 — 2	$\begin{array}{c} -0.050 \\ -0.387 \\ +1.261 \\ +7.781 \\ -9.025 \\ -0.437 \end{array}$	$\begin{array}{c} -0.004 \\ -0.020 \\ -0.320 \\ -2.825 \\ +5.073 \\ +0.246 \end{array}$	$0.00 \\ +0.02 \\ +0.40 \\ +6.80 \\ -8.97 \\ -0.42$	0.00 $-0.01$ $-0.14$ $-2.54$ $+5.03$ $+0.26$	-0.054 $-0.423$ $+0.855$ $+0.857$ $+0.017$	-0.002 -0.013 -0.169 -0.318 -0.022	4 16 6 124 72	2 3 11 33 65
7,— 8 — 7 — 6 — 5 — 4 — 3	$\begin{array}{c} -0.027 \\ -0.186 \\ +0.272 \\ -0.571 \\ -0.459 \\ -0.010 \end{array}$	-0.002 -0.003 -0.046 +0.217 +0.250 +0.005	::::	::::	-0.189 $+0.260$ $-0.538$ $-0.419$	$\begin{array}{c} -0.009 \\ -0.047 \\ +0.202 \\ +0.255 \end{array}$	3 12 33 40	6 1 15 5
8,— 9 — 8 — 7 — 6 — 5 — 4	$\begin{array}{c} -0.013 \\ -0.084 \\ +0.125 \\ -0.194 \\ -0.839 \\ +0.647 \end{array}$	$\begin{array}{c} 0.000 \\ -0.002 \\ -0.022 \\ +0.082 \\ +0.463 \\ -0.501 \end{array}$	-0.038 -0.66 +0.64	+0.017 +0.30 -0.53	$ \begin{array}{r} -0.093 \\ +0.115 \\ -0.145 \\ -0.110 \end{array} $	$\begin{array}{c} -0.007 \\ -0.024 \\ +0.055 \\ +0.067 \end{array}$	9 10 11 69	5 2 10 96
9,— 9 — 8 — 7 — 6 — 5	+0.063 $-0.055$ $+0.080$	-0.001 -0.011 +0.020 -0.049 -0.050		::::	$\begin{array}{r} -0.048 \\ +0.002 \\ -0.059 \\ +0.083 \end{array}$	$\begin{array}{c} -0.005 \\ -0.011 \\ +0.025 \\ -0.054 \end{array}$	8 61 4 3	4 0 5 5
10—10 — 9 — 8 — 7 — 6	+0.035 $-0.027$ $+0.026$	0.000 0.005 0.010 0.017 0.079			0.025	-0.005	5	5

The perturbations of the logarithms of the radius vector are given in a form similar to those of the longitude. Under  $\delta\rho_1$  we have the complete perturbation. Under  $\delta\rho_2$  the effect of the perturbations of long period. But under  $\delta\rho_3$  we have only the difference between  $\delta\rho_1$  and  $\delta\rho_2$ , it being deemed unnecessary to present in full the perturbations of the radius vector as computed by the other method.  $\delta\rho_1$  being employed in computing  $\delta v_1$  may, in fact, be regarded as completely checked by its affording a correct value of the latter.

In the last two columns  $\delta \rho_3$  is reduced to common logarithms by multiplying the coefficients by the modulus 0.434294.

PERTURBATIONS OF THE LOGARITHM OF THE RADIUS VECTOR OF URANUS PRODUCED BY NEPTUNE.

					ī		1	
ľ g	δ	91	δ	02	δρ	93	М	δρ
0, 0 —1 —2	cos +138	sin	cos	sin 	cos	sin	cos + 60	sin 0
1,—3 —2 —1 0 +1	$ \begin{array}{r} + 4 \\ + 68 \\ + 523 \\ - 68 \\ - 8 \end{array} $	$\begin{array}{c} 0 \\ 0 \\ +1 \\ -6 \\ -1 \end{array}$					$\begin{array}{c c} + & 2 \\ + & 30 \\ + & 227 \\ - & 30 \\ - & 3 \end{array}$	0 0 0 - 3 0
2,—4 —3 —2 —1 0	+94 $+1416$ $+20025$ $+1663$ $+3912$	-1 $-12$ $-179$ $+116$ $+194$	+92 $+1374$ $+19490$ $+1726$ $+3927$	$ \begin{array}{r} -1 \\ -12 \\ -180 \\ +120 \\ +194 \end{array} $	$ \begin{array}{r} + 2 \\ + 42 \\ +535 \\ - 63 \\ - 15 \end{array} $	$\begin{array}{c} 0 \\ 0 \\ + 1 \\ - 4 \\ 0 \end{array}$	$\begin{array}{c c} + & 1 \\ + & 18 \\ + & 232 \\ - & 27 \\ - & 7 \end{array}$	$\begin{array}{c} 0 \\ 0 \\ 0 \\ -2 \\ 0 \end{array}$
3,—5 —4 —3 —2 —1	$ \begin{array}{r} -3 \\ -38 \\ -527 \\ -284 \\ +16 \end{array} $	$\begin{array}{c} 0 \\ 0 \\ -6 \\ -54 \\ +2 \end{array}$					$\begin{array}{c c} -1 \\ -17 \\ -229 \\ -124 \\ +7 \end{array}$	$ \begin{array}{c} 0 \\ 0 \\ -3 \\ -23 \\ +1 \end{array} $
4,—6 —5 —4 —3 —2 —1	1 19 254 1759 143 167	0 1 22 300 61 62	— 8 — 118 —1681 — 154 — 165	 — 20 —282 —*70 — 64	$ \begin{array}{c c} -11 \\ -136 \\ -78 \\ +11 \\ -2 \end{array} $	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	- 5 - 59 - 34 + 5 - 1	0 1 8 +- 4 +- 1
5,—6 —5 —4 —3	$ \begin{array}{c}  - & 4 \\  - & 40 \\  + 103 \\  + & 39 \end{array} $	$0 \\ + 1 \\ +20 \\ +15$		: 	: :	::::	- 2 - 17 + 45 + 17	0 0 + 9 + 6
6,—7 —6 —5 —4 —3	$ \begin{array}{rrr}     - 2 \\     - 17 \\     + 42 \\     + 180 \\     + 13 \end{array} $	$ \begin{array}{c} 0 \\ +1 \\ +10 \\ +65 \\ +8 \end{array} $	$\begin{array}{c} \cdots \\ + 10 \\ + 164 \\ + 14 \end{array}$	 + 4 + 61 + 5	$ \begin{array}{rrr}     & - & 2 \\     & - & 17 \\     & + & 32 \\     & + & 16 \\     & - & 1 \end{array} $	$   \begin{array}{c}     0 \\     + 1 \\     + 6 \\     + 4 \\     + 3   \end{array} $	$ \begin{array}{c c} - & 1 \\ - & 7 \\ + & 14 \\ + & 7 \\ 0 \end{array} $	0 0 + 3 + 2 + 1
7,—7 —6 —5 —4	$     \begin{array}{r}       -8 \\       +11 \\       -17 \\       -5     \end{array} $	$\begin{array}{c} 0 \\ + 2 \\ - 7 \\ - 3 \end{array}$		 :: 			$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 0 \\ + 1 \\ - 3 \\ - 1 \end{array}$
8,—8 —7 —6 —5	- 4 + 5 - 7 -19	$\begin{array}{c} 0 \\ +1 \\ -3 \\ -11 \end{array}$					- 2 + 2 - 3 - 8	0 0 1 5
9,—9 —8 —7 —6	$ \begin{array}{c} -2 \\ +3 \\ -2 \\ +2 \end{array} $	$\begin{array}{c} 0 \\ 0 \\ -1 \\ +2 \end{array}$	••••	••••	••••		- 1 + 1 - 1 + 1	0 0 0 + 1

			Ры	RTURB	ATIONS	OF T	HE LAT	ITUDE	PRODUCE	D BY NEI	TUNE,			
	$\frac{\partial R}{\partial \gamma} =$	$\frac{m'}{a_1}$ ×	2 1h 8	in N	z (i+ × h s		$\frac{d\eta}{dt} = n$	n'an×	8/	૯	ðı	7	8,	3
i' i	_21.65	sin 0	sin 0	0	sin 0	0.00					sin '' 0 +.080	012		
.)	+14.58 - 1.16	-9.39 $+7.0$ $-9.65$	+19.32 $-14.7$ $+1.04$	+9.39 $+7.0$ $-2.40$	0 -0.07	0 0 +0.02	+19.31 $-14.7$ $+3.97$	+9.39 $+7.0$ $-2.4$	+0.045 -0.006	+0.021 $-0.036$ $-0.022$ $+0.014$	$ \begin{array}{c c} +0.030 \\ -0.073 \end{array} $ $ \begin{array}{c c} -0.045 \\ +0.020 \end{array} $	-0.012 $+0.036$ $-0.022$ $+0.012$	+.007 +.201	002 002
$-1 \\ 0 \\ +1$	$ \begin{array}{r} -34.26 \\ + 3.74 \\ + 15.77 \end{array} $	0 + 2.32 - 7.87	$-\frac{0}{2.80}$	$0 \\ -1.48 \\ +7.75$	$^{+1.76}_{-0.24}$	0 0	+1.76 $-3.04$ $+16.25$ $-10.6$	-1.48 + 7.75	-0.057	0 + 0.035 - 0.040 $-0.013$	+0.028 +0.046 -0.083 -0.027	$ \begin{array}{c} 0 \\ -0.022 \\ +0.040 \end{array} $ $ \begin{array}{c} -0.013 \end{array} $		+.084 +.007
-3 $-2$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$													
-4 -3 -2 -1	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$													+.041  +.074 026
$ \begin{bmatrix} 4, -5 \\ -4 \\ -17.4 \\ 3 \\ +6.34 \\ +1.34 \\ -2 \\ +9.42 \\ -5.37 \\ +10.57 \\ +5.04 \\ +0.25 \\ -1 \\ -1.72 \\ +0.32 \\ -1.72 \\ -0.32 \\ -0.02$										+0.004 0 -0.011 [-1.056] +0.002	$\begin{array}{c c} +0.008 \\ +0.023 \\ -0.020 \\ \hline [-2.127] \\ +0.013 \end{array}$	+0.004 0 -0.001 [+0.977] -0.002	008 +.048 047	+.006
-5 -4 -3	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$												$0 \\028 \\ +.001$	
6,—6 —5 —4 —3	+ 4.63	_9 70	1 5 15	1 2 45	1.0.31	+0.24	1 4 5.46	+0.28 +2.35	+0.033	$0 \\ -0.003 \\ +0.022 \\ [+0.041]$	+0.007 -0.006 +0.045 [+0.195]	0 -0.001 -0.019 [-0.038]	028 010	0
- 5	- 5.6 + 3.63 + 2.49 - 1.19	9 00	3 52	1 68	0.30	-0.10	-3.82	+1:08	$\begin{array}{c} -0.012 \\ +0.012 \\ +0.013 \\ -0.021 \end{array}$	$ \begin{array}{c c} 0 \\ -0.002 \\ +0.011 \\ -0.005 \end{array} $	$ \begin{array}{r} +0.004 \\ -0.004 \\ +0.020 \\ -0.022 \end{array} $	0 -0.001 -0.008 +0.004	+.014	-,004 0
8,—8 —7 —6 —5	+ 2.76	+0.50	1 2.38	0	+0.27	+0.16 $-0.09$	+1.3 $-0.91$ $+2.65$ $-0.97$	$+0.16 \\ +1.05$	-0.008 +0.007 +0.006 -0.008	0 -0.002 +0.006 -0.002	+0.003 +0.002 +0.011 -0.008	0 0 -0.004 +0.002		
		2				Secula	r term,	≥k = - ≥β = -	1".25 T	cos ▼				

The terms  $\delta k$  and  $\delta \eta$ , which are inclosed in brackets, are of very long period, and are therefore omitted in forming the values of  $\delta \beta$  in the last two columns

## Perturbations produced by Jupiter.

The series in which these perturbations are expressed converge so rapidly that I deem it unnecessary to present the details of the computation. They have been computed by both methods, and the separate and independent results are given in the following table, where  $\delta v_1$  represents the perturbations computed by the method developed in Chapter I, and  $\delta v_2$  those computed by the method of variation of elements.

The apparently large discrepancy between the coefficients multiplied by the time arises from the circumstances that in the form of development the mean motion, and hence the mean anomaly, appears affected by the perturbation 31".2t. Accordingly when we enter the table which gives the true longitude in terms of the mean anomaly in the form

$$v = l + 2e \sin(l - \pi) + \text{etc.},$$

we may consider this quantity 31".2t as a secular variation of  $l-\pi$  producing in v the term

$$\delta v = 62^{\circ}.4et\cos(7-\pi).$$

In  $\partial v_1$  this term is left in its primitive form, while in  $\delta v_2$  the value of l is supposed to include this term, and the secular terms are only those which arise from the secular variation of the eccentricity and perihelion.

It is also to be remarked that the terms which are independent of the mean longitude of Jupiter, or those in which i'=0, are not comparable, as they correspond to slightly different elliptic elements in the two theories.

$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$			P	ERTURBATIO:	s of Uranu	в ву Ји	PITER.			
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			8v,	8	IV <sub>2</sub>	Diff.	cos 48p	Map		
1.3 - 0.032 - 0.034 - 0.025 - 0.025 7 9	0, 0 1 2 3 0, 0 1 2 3 -1,-1 0 1 2 3 0,-2 1 2 3	sin  "  - 0.160nt  - 0.010nt  +25.657  + 1.397  + 0.072  + 0.027  + 1.269  -53.064  - 3.495  - 0.148  2 - 0.027  + 1.182  + 0.277  + 0.074  + 0.015	cos  " +31.2116t +37.585nt + 2.207nt + 0.135nt  - 1.859 - 0.087 - 0.005 + 0.009 + 0.002 - 0.004 - 0.092 - 0.047 - 0.011 + 0.515 + 0.036 - 0.005 - 0.003	sin  "  - 0.1622nt - 0.0095nt - 0.0006nt - 1.346 - 0.030 + 0.017 + 1.232 - 53.084 - 3.565 - 0.164 - 0.031 + 1.176 + 0.263 + 0.083 + 0.014		sin cos  2 0 0 0 10 237 1 20 270 10 16 3 4 3 6 0 14 1 9 3 1 0	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		

		PERTURB.	ATIONS OF THE	LATITUDE.		
g l'	ð	è	ð	η	ð	3
i i'	sin	cos	cos	sin	cos	sin
0 0 1 2 3 3 -2-1 -1 0 1 2 -3-2 0 1 2	$\begin{array}{c} 0.071 \\ -0.012 \\ -0.003 \\ -0.006 \\ -0.297 \\ -0.161 \\ +2.611 \\ +0.070 \\ +0.055 \\ +0.002 \\ -0.110 \\ -0.014 \\ \end{array}$	$\begin{array}{c}\\ -0.041\\ -0.075\\ -0.012\\ \\ +0.042\\ +1.949\\ -0.191\\ 0\\ +0.021\\ -0.088\\ -0.011\\ -0.050\\ 0\\ \end{array}$	+0.030 -0.012 -0.003 +0.006 +0.297 -0.189 +2.628 +0.066 -0.055 -0.002 -0.109 -0.011	+0.036 +0.075 +0.012 +0.042 +1.949 -0.190 0 -0.002 -0.002 -0.011 +0.046	+.060 010 002 +.005 +.001 494 024 +.002 +.010 +.017 009 002	
		Secular ter	$   \sum_{ms} \begin{cases} \delta k = 0 \\ \delta \beta = 0 \end{cases} $	" 1.14 T 1.14 T cos v		•

### CHAPTER IV.

TERMS OF THE SECOND ORDER PRODUCED BY THE ACTION OF SATURN.

Preliminary Investigation of the Orbit of Saturn.

For the accurate determination of the perturbations of a planet it is essential that the functions of the time which are substituted for the co-ordinates of each planet in the expression of the disturbing forces should approximately represent the true places of the planet. The difference between the true place and that implicitly assumed in the investigation should be so small and of such a character that, when multiplied by the mass of the disturbing planet, and by the factors introduced by the process of integration, the result shall be insensible. If one of these factors is so large as to make a perturbation of an order of magnitude approximating that of the inequality which gives rise to it, it will represent an inequality of very long period in the elements, which, though apparently sensible, may be neglected for a great length of time.

The perturbations hitherto found have been computed on the hypothesis that the disturbing action of Saturn on Uranus is the same as if both planets moved in the elliptic orbits corresponding to the adopted elements. We have given formulæ for the computation of the corrected perturbations when, to the co-ordinates of the two planets corresponding to the adopted ellipse, we add corrections represented by  $\delta v$ ,  $\delta v$ ,  $\delta \rho$ , etc. These corrections are now to be taken of such magnitude that when thus added they shall very nearly represent the actual motions of the planets.

Generally, it is considered sufficient to take for these corrections the perturbations of the first order. But this presupposes that the elliptic elements are nearly correct, which does not hold true in the case of the old elements of the outer planets. Bouvard's Tables of Saturn, the elements of which have been adopted, are subject to recurring errors amounting to 30" or more. Moreover, when we substitute the new and more accurate perturbations for the old and imperfect ones adopted in the tables, the chances are that the errors will be increased. Desiring that the theory shall be as far as possible free from doubt, we begin with a preliminary investigation of the orbit of Saturn, the design of which will be to give the co-ordinates of that body in terms of the time with sufficient certainty and accuracy to serve for computing the perturbations both of Jupiter and Uranus. As usual, the first step in this investigation will be the determinations of the perturbations of the planet.

#### General Perturbations of Saturn.

The perturbations produced by Jupiter will be taken from the exhaustive prize memoir of Hansen.<sup>1</sup> As the perturbations required are those of the co-ordinates, it will be necessary to transform those of Hansen into the usual form. Hansen gives the true anomaly v in the form

$$v = g + n\xi z + e_1 \sin(g + n\xi z) + e_2 \sin 2(g + n\xi z) + \text{etc.},$$

 $e_1$ ,  $e_2$ , etc., being the coefficients of the multiples of the mean anomaly in the usual development of the elliptic true anomaly. Whence, neglecting the second power of  $n^s z$ ,

$$\delta v = n z (1 + e_1 \cos g + 2e_2 \cos 2g + \text{etc.}).$$

To make the development sufficiently rigorous it is only necessary to increase g by  $\frac{1}{2}n\delta z$  in this expression. In the same way, we have for the perturbations of  $\log r$ ,

$$\delta \rho = \delta \rho_0 + n \ell z (e^{(1)} \sin g + e^{(2)} \sin 2g + \text{etc.})$$

 $\delta \rho_0$  being Hansen's perturbation, and  $e^{(i)}$  the negative coefficient of  $\cos ig$  in the development of the elliptic  $\log r$ .

Hansen having adopted  $\frac{1}{1070.5}$  as the mass of Jupiter, it will be necessary to multiply his perturbations by 1.0216 to reduce them to Bessel's mass. Thus the perturbations by Jupiter hereafter given have been obtained.

The perturbations by Uranus and Neptune have been computed by the preceding general method, and are given in the following table. In the table l' is the mean longitude of the disturbing planet, Uranus or Neptune, counted from the perihelion of Saturn.  $\delta \rho$  is the perturbation of the Naperian logarithm, in units of the seventh place of decimals.

GENE	RAL PERTU	RBATIONS			IN ORBIT A		OGARITH	A OF THE R	ADIUS
	Ac	tion of Uran	nus.		E DE LOS	Act	ion of Nept	une.	
		80	8	ip .		δυ δρ			p
1, 0 -1 2, 0 -1 -2 3, 0 -1 -2 -3 4,-1 -2 -3 -4	sin  '' + 0.88 + 8.60 - 0.42 - 8.49 -13.39 + 0.06 - 2.9 -10.61 - 2.05 + 0.06 - 0.62 + 0.30 - 0.26	$\begin{array}{c} + 0.21 \\ - 0.17 \\ - 2.53 \\ - 0.25 \\ + 1.62 \\ + 28.1 \\ - 20.88 \\ - 1.47 \end{array}$	$\begin{array}{c} + 10.8 \\ -247. \\ - 67.5 \\ - 0.1 \\ - 10.5 \\ + 10.5 \end{array}$	sin + 7.9 - 3.5 - 3.7 +21.4 + 6.6 +39.1 +33.0 +487. +42.8 + 0.6 -12.5 -23.4 - 0.8	# g 1,-0 -1 2, 0 -1 -2 3,-1 -2 -3	sin '' +0.23 +1.93 +0.44 -1.11 -1.27 +0.02 +0.10 -0.10	cos '' -0.05 0.00 +0.02 +0.02 -0.00 -0.03 -0.04 0.00	cos  - 2.2 +39.9 - 3.0 -18.5 -41.1 + 0.2 + 3.2 - 3.9	sin  -0.2 0.0 +0.1 -0.4 0.0 +0.4 +1.3 0.0

<sup>&</sup>lt;sup>1</sup> Untersuchungen über die gegenseitigen Störungen des Jupiters und Saturns. Von P. A. Hansen. Berlin, 1831.

<sup>9</sup> April, 1873.

I have submitted these perturbations to such duplicate computations and other checks as lead me to believe that none of the terms can be in error by more than a small fraction of a second, but, as they are not intended to form the basis of a definitive theory of Saturn, I do not vouch for their absolute precision.

In this provisional correction of the orbit of Saturn only heliocentric longitudes have been employed. These were derived for a series of dates from Airy's reduction of the Greenwich observations, the modern Greenwich observations, and the Washington observations.

For these dates the value of  $n \ell z$  for Saturn was computed from the formulæ found on pages 189 and 190 of the work of Hansen, already quoted, omitting all terms less than 1", and including only tenths of seconds in the results. The dates, the resulting values of  $n \ell z$ , of the factor  $e_1 \cos (g + \frac{1}{2}n \ell z) + 2e_2 \cos 2(g + \frac{1}{2}n \ell z)$ , and of the concluded  $\ell v$  are as follows. The formulæ for  $\ell v$  is

Date Gr. Mean Noon.	$n\delta z$	Factor.	80
	n		"
1751 May 31	-1947.7	0930	-1792.7
1757 Aug. 7	-2134.2	0652	-2038.2
1758 Aug. 27	-2212.5	0474	-2153.2
1761 Oct. 6	-2546.2	+.0244	-2664.5
1763 Nov. 1	-2880.3	+.0729	-3157.1
1765 Nov. 23	-3095.1	+.1082	-3504.0
1773 Feb. 26	-3342.0	+.0419	-3557.2
1780 May 24	-2858.2	0956	-2640.7
1794 Nov. 16	-3321.1	+.1017	_3737.9
1802 Feb. 23	-3184.7	+.0529	-3425.5
1823 Nov. 13	-2716.3	+.0944	-3036.8
1831 Feb. 18	-3378.5	+.0639	-3671.7
1838 May 19	-2976.7	0866	-2777.9
1845 Aug. 17	-2342.7	0721	-2220.9
1852 Nov. 15	-2847.0	+.0863	-3159.3
1860 Feb. 14	-3161.4	+.0740	-3468.3
1867 May 15	-2373.1	0812	-2227.6

The perturbations by Uranus and Neptune were computed from the values of their terms just given. The principal terms, the sum of which make up the heliocentric longitude resulting from the adopted elements, are shown in the first of the following tables.

In the next table we have after the date the heliocentric longitude from Bouvard's Tables, as deduced from the longitudes given in Airy's reductions of the Greenwich Observations, from the Astronomisches Jahrbuch for 1831, and from the Nautical Almanac. Then follow the corrections, roughly deduced from observations made near the opposition. Adding these columns, we have the longitude

from observation. To the right of these are the equations of condition for the correction of the elements.

Long. of	Mean	Equation of	Perturb	ations by	y	Red. to	Nuta-	True
Perihelion.	anomaly.	centre.	Jupiter.	Uranus.	Nep- tune.	Ecliptic.	tion.	longitude.
88 41 27.5 88 46 41.2 88 47 31.4 88 50 7.6 88 51 51 6 88 53 35.1 88 59 39.6 89 5 43.4 89 17 50.7 89 23 55.7 89 42 7.0 89 48 11.9 89 54 16.1 90 0 20.4 90 6 24.6 90 12 28.7	o / " 159 55 50.1 236 13 7.1 248 25 53.1 286 26 29.8 311 44 13.6 336 55 56.1 65 40 2.3 154 8 4.8 331 6 10.4 59 56 17.9 325 22 26.0 54 10 33.1 142 44 37.0 231 18 40.9 319 52 44.8 48 26 48.7	0 / // +2 3 56.6 -5 7 38.1 -5 48 30.4 -6 16 1.3 -5 0 58.2 -2 41 10.6 +6 0 35.9 +2 37 57.7 -3 18 5.2 +5 44 46.6 -3 51 58.0 +5 25 2.6 +3 40 38.1 -4 47 36.6 -4 21 53.0 +5 1 46.4	-57 5.5 -50 36.8 -61 11.7 -46 17.9 -37 0.9	"45.7" -45.7" -36.6 -35.2 -3.3 +11.9 +19.2 -32.9 -53.8 + 9.6 -18.6 -27.9 +13.3 -35.5 +4.7 +30.3	"-2.7 +1.0 +1.7 +2.9 +2.4 +1.9 -0.8 -1.7 +3.5 +2.5 -3.0 +2.5 +2.1 +0.9 -0.9 -3.4	/ // +1 36.9 -1 20.5 -1 35.8 -0 43.5 +0 43.3 +1 36.6 -1 37.1 +1 37.5 +1 30.9 -1 37.3 +1 21.6 -1 33.2 +1 29.7 -1 11.8 +1 8.8 -1 25.1	" +15.8 -11.8 -15.0 -14.1 - 4.9 + 6.7 + 4.8 -14.5 -14.1 + 1.4 - 14.7 - 7.4 - 4.3 +14.8 -18.4 +14.1	250 12 25.8 319 16 4.1 330 46 36.6 8 15 13.5 34 43 22.6 62 12 1.0 159 38 54.6 245 8 13.2 56 5 7.9 154 6 2.7 50 23 3.6 148 21 11.1 235 34 37.4 315 52 52.2 44 45 31.3 142 42 31.4
90 18 32.8	137 0 52.6	+4 9 31.2		8.2	+1.3	+1 21.6	- 4.1	230 52 59.7
Date.	Tabul: longitu		Long. from observation.		Equ	UATIONS OF	CONDIT	ION.
1751 May 1757 Aug. 1758 Aug. 1761 Oct. 1763 Nov. 1765 Nov. 1773 Feb. 1780 May 1794 Nov. 1802 Feb. 1823 Nov. 1831 Feb. 1838 May 1845 Aug. 1852 Nov. 1860 Feb. 1867 May	27 319 17 27 330 47 3 6 8 15 1 1 34 43 4 23 62 12 2 26 159 40 24 245 9 1 16 56 5 3 23 154 7 13 50 23 3 18 148 22 3 19 235 36 1 17 315 53 4 14 44 6 14 142 44 1	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	250 13 29.5 319 16 50.5 330 47 23.6 8 15 14.0 34 43 57.6 62 12 41.1 159 40 22.6 245 9 25.4 56 5 53.5 154 7 13.5 50 23 55.8 148 22 41.5 235 36 14.6 315 53 57.9 44 46 21.3 142 44 2.5 230 54 52.9	46.4 47.0 0.5 35.0 40.1 88.0 72.2 45.6 70.8 52.2 90.4 97.2 65.7 50.0 91.1	0. 0. 1. 1. 1. 0. 1. 1. 1. 0. 0.	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	5n + 0.60 $-1.53$ $-1.76$ $-1.99$ $-1.63$ $-0.88$ $+1.93$ $+0.76$ $-1.08$ $+1.85$ $-1.27$ $+1.75$ $+1.63$ $-1.43$ $+1.63$ $+1.23$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$

A normal equation for  $\delta_{\varepsilon}$  is obtained by taking the sum of all the equations. That for  $\delta n$  is formed by subtracting the sum of the first seven from the sum of the last seven, and those for  $\delta e$  and  $e\delta_{\omega}$  by taking the sum of the equations in which the coefficients of  $\delta e$  or  $e\delta_{\omega}$  are greater than unity, after changing the signs of the equations in which they are negative. The normals thus obtained are

These equations give

$$\delta \varepsilon = +64.8 \text{ (Epoch, 1800.)}$$
 $\delta n = +0.268$ 
 $\delta e = +12.6$ 
 $e \delta \omega = +8.2$ 

—Substituting these values in the seventeen equations of condition we have the following residuals, or excesses of theoretical over observed longitudes:

These residuals are much larger than they should be, and I scarcely know to what cause to attribute their magnitude. The results are however amply reliable for the purposes of the investigation, and lead to the following elements of Saturn:

$$\pi$$
,  $90 \ 6 \ 26$   
 $\varepsilon$ ,  $14 \ 50 \ 3.2$   
 $\theta$ ,  $112 \ 20 \ 0$   
 $\varphi$ ,  $2 \ 29 \ 39.2$   
 $n$ ,  $43996.395$   
 $e$ ,  $.0560660$   
 $\log (a + \delta a)$ ,  $0.979676$   
Epoch,  $1850$ , Jan. 0, Greenwich mean noon.

It will be seen that the adopted position of the plane of Saturn's orbit is retained. It was corrected from observations before the perturbations were finally computed.

Of the above corrections, those of the epoch and mean motion need not be taken account of in the corrections of the co-ordinates, since the mean longitude remains in the formulæ as an arbitrary quantity to the end. The effect of the correction of the mean distance is insensible. The corrections of eccentricity and perihelion are therefore alone to be retained. They are allowed for by adding to  $\delta v$  and  $\delta \rho$  the terms

$$\begin{array}{ll} \delta v = & 2 \delta e \sin g - e \delta \omega \cos g \\ = & + 25''.2 \sin g - 16''.4 \cos g; \\ \delta \rho = & - \delta e \cos g - e \delta \omega \sin g \\ = & - 12''.6 \cos g - 8''.2 \cos g. \end{array}$$

Perturbations of Saturn and Uranus.

The following expressions include, with these corrections, all the perturbations of Saturn and Uranus which can produce any appreciable perturbations of the second order in their mutual action. In these expressions the initial letter of each planet is put for its mean longitude counted from the perihelion of Uranus.

PERTURBATIONS OF SATURN.							
Argument.	8	v'	δ	<i>'</i>			
$\begin{array}{c} S \\ S \\ S \\ - J \\ 2S - J \\ 3S - J \\ 2S - 2J \\ 3S - 2J \\ 4S - 2J \\ 5S - 2J \\ 6S - 2J \\ U - S \\ 2U - S \\ 2U - S \\ 3U - S \\ 3U - S \\ 3U - S \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		cos  "  - 2.7 - 0.80t +176.7 -115.8 + 12.3 + 29.5 - 15.4 + 11.4 - 58.8 - 58.1 + 3.0 + 0.1 - 8.0 + 0.1 + 8.8	sin  " + 9.0 - 0.74t - 15.9 - 9.1 - 16.6 - 1.1 - 12.3 +403.0 - 34.4 + 56.9 - 0.1 + 1.4 + 0.1 - 0.7 + 7.0			
	PERT	URBATIONS OF URAN	ius.				
Argument.	8	ט	8	ip			
U - S $2U - S$ $3U - S$ $2U - 2S$ $3U - 2S$ $4U - 2S$ $5U - 2S$	sin " - 0.11t -20.8 -11.9 +49.3 + 4.1 + 2.1 + 0.6 + 1.2	$\begin{array}{c} \cos \\ "\\ + 0.05t \\ + 36.0 \\ - 2.0 \\ - 4.7 \\ + 4.2 \\ + 1.8 \\ + 0.4 \\ + 0.4 \end{array}$	sin " - 0.14t - 4.9 -63.8 +13.2 + 0.1 + 1.4 + 1.3 - 1.2				

Let us now resume the equation

$$\delta Q = 2 \int D_t \delta R dt + \delta \frac{\partial R}{\partial \rho} - \frac{1}{\mu} D_t^2 \left( r_0^2 \delta \rho^2 \right) + \frac{1}{2} \frac{\delta \rho^2}{r_0}.$$

Beginning with the last two terms of this expression, it may be shown at the outset that they are quite insensible. The effect of the constant terms in  $\delta \rho$  and  $\delta \rho'$  has already been included by correcting the logarithm of the mean distance by their amount; they are therefore omitted. The largest remaining term is 64", the square of which is only 0".02. In the product  $r_1^2 \delta \rho^2$  the largest terms are

$$+0.014$$
 $-0.013 \sin g$ 
 $-0.011 \sin (3g - 2l')$ 
 $-0.011 \cos (4g - 2l')$ 

which may be entirely neglected.

We shall therefore only consider in  $\delta Q$  the terms

$$2\int D_t \delta R dt + \delta \frac{\partial R}{\partial \rho}$$

As already remarked, R is rigorously a function only of V,  $\rho$ , and  $\rho'$ , V being the angle made by the radii vectores of the two planets. But, in the analytical development of R, the quantity V is considered as a function of V, V', and  $\gamma$ , so that we have

$$R = f(\rho, \rho', \mathbf{v}, \mathbf{v}', \gamma).$$

In the previous computation of the perturbations of Uranus, we have supposed R to be a function of  $\rho_0$ ,  $\rho'_0$ , etc. The corrections to R and its derivatives with respect to  $\nu$  and  $\nu$  are now given by the equations (11), with the modifications shown on pages 24 to 27. The derivatives of  $R_0$  which enter into these equations are formed as follows: If, in the value of R produced by the action of Saturn on Uranus, we consider any term of the form

 $\frac{m'h}{a_1}\cos N$ 

where

$$N = i\lambda + i'\lambda' + j\omega + j'\omega'$$

the accented quantities always referring to Saturn, but  $a_1$  being the corrected mean distance of Uranus, then we shall have the following terms in the derivatives of R.

$$\frac{\partial R}{\partial \mathbf{v}} = -\frac{m'h}{a_1} (i+j) \sin N$$

$$\frac{\partial R}{\partial \mathbf{v}'} = -\frac{m'h}{a_1} (i'+j') \sin N$$

$$\frac{\partial R}{\partial \rho} = -\frac{m'}{a_1} \left( h + \frac{\partial h}{\partial \rho} \right) \cos N$$

$$\frac{\partial R}{\partial \rho'} = \frac{m'}{a_1} \frac{\partial h}{\partial \rho} \cos N$$

$$\frac{\partial^2 R}{\partial \mathbf{v}^2} = -\frac{m'h}{a_1} (i+j)^2 \cos N$$

$$\frac{\partial^{2}R}{\partial v \partial v'} = -\frac{m'h}{a_{1}} (i+j) (i'+j') \cos N$$

$$\frac{\partial^{2}R}{\partial v \partial \rho} = \frac{m'}{a_{1}} \left(h + \frac{\partial h}{\partial n}\right) (i+j) \sin N$$

$$= -\frac{\partial R}{\partial v} - \frac{\partial^{2}R}{\partial v \partial \rho'}$$

$$\frac{\partial^{2}R}{\partial v \partial \rho'} = -\frac{m'}{a_{1}} \frac{\partial h}{\partial n} (i+j) \sin N$$

$$\frac{\partial^{2}R}{\partial \rho \partial v'} = \frac{m'}{a_{1}} \left(h + \frac{\partial h}{\partial n}\right) (i'+j') \sin N$$

$$\frac{\partial^{2}R}{\partial \rho^{2}} = \frac{m'}{a_{1}} \left(h + 2 \frac{\partial h}{\partial n} + \frac{\partial^{2}h}{\partial n^{2}}\right) \cos N$$

$$= -\frac{\partial R}{\partial \rho} - \frac{\partial^{2}R}{\partial \rho \partial \rho'}$$

$$\frac{\partial^{2}R}{\partial \rho \partial \rho'} = -\frac{m'}{a_{1}} \left(\frac{\partial h}{\partial n} + \frac{\partial^{2}h}{\partial n^{2}}\right) \cos N$$

All the numerical data necessary for the computation of these derivatives have been given in Chapter II. Combining the terms having the same argument, we find the following values, omitting those given in Chapter II, and those which are derived from the others by mere addition. The terms of  $\frac{\partial^2 R}{\partial v^2}$  are also omitted, because they are sensibly the same with those of  $\frac{\partial^2 R}{\partial v \partial v'}$ , changing the algebraic sign.

	$\frac{a_1}{m'}$	$\frac{\partial R}{\partial \mathbf{v'}}$	$\frac{a_1}{m'}$	$\frac{\partial^2 R}{\partial \mathbf{v} \partial \mathbf{v}'}$	$\frac{a_1}{m'} \frac{\partial^2 R}{\partial \rho \partial v'}$	
g l'	sin	cos	sin	cos	sin	cos
0,—1 —2	$+0.2874 \\ +0.0066$		+0.0310	$^{+0.2872}_{+0.0067}$	$+0.2691 \\ +0.0060$	0.0322
1, 0 —1 —2	-0.0102 -3.4811 -0.0968	-0.0491 $-0.0010$ $+0.4304$	+0.0490 $-0.0021$ $-0.4304$	-0.0101 -3.4810 -0.1039	+0.0249 $-5.2684$ $-0.0792$	+0.1194 $0$ $+0.4583$
_3 2, 0	+0.0388 -0.0045	+0.0173	-0.0179 $+0.0021$	+0.0389 -0.0080	+0.0398 +0.0155	+0.0163
-1 -2 -3	$-0.0544 \\ +0.4104 \\ -0.0053$	$ \begin{array}{r} -0.0712 \\ +0.0120 \\ -0.0191 \end{array} $	+0.1426 $-0.0171$ $+0.0390$	$ \begin{array}{r} -0.0689 \\ +0.8233 \\ -0.0226 \end{array} $	-0.1760 $-1.3515$ $+0.0288$	$+0.2403 \\ +0.0014 \\ +0.0547$
3,—1 —2 —3	$-0.0070 \\ +0.0570 \\ +0.2542$	-0.0093 -0.0650 0	$+0.0171 \\ +0.1957 \\ -0.0065$	$-0.0210 \\ +0.1013 \\ +0.7624$	+0.0197 $-0.1791$ $-1.0884$	+0.0304 +0.2840 -0.0071
4,—2 —3 —4	-0.0014 +0.0515 +0.1448	-0.0130 -0.0499 -0.0015	+0.0368  +0.1987  -0.0016	$-0.0193 \\ +0.1450 \\ +0.5789$	+0.0213 $-0.2144$ $-0.7644$	$   \begin{array}{r}     +0.0547 \\     +0.2647 \\     -0.0005   \end{array} $

	$\frac{a_1}{m'} \frac{\partial R}{\partial  ho'}$		$\frac{a_1}{m'}$ $\frac{\dot{a}_2}{\dot{c}}$		$rac{a_{_1}}{m'} rac{\partial^2 R}{\partial  ho \partial  ho'}$	
g' l	sin	cos	sin	cos	sin	cos
0, 0 —1	_0.026	$^{+0.172}_{-0.562}$	+0.556	$^{+0.002}_{0}$	+0.113	0.645 0.610
1, 0 -1 -2	$ \begin{array}{c c} +0.070 \\ -0.003 \\ +0.889 \end{array} $	$+0.015 \\ +8.749 \\ +0.180$	$ \begin{array}{c c} +0.015 \\ -8.750 \\ -0.176 \end{array} $	$^{+0.070}_{-0.001}_{+0.889}$	$\begin{array}{c c} -0.227 \\ +0.011 \\ +0.912 \end{array}$	$ \begin{array}{c c} -0.079 \\ +6.189 \\ +0.190 \end{array} $
2,—1 —2	+0.084 +0.018	$+0.248 \\ +0.472$	-0.230 -0.941	$^{+0.169}_{+0.013}$	-0.322 $-0.006$	$^{+0.020}_{-1.685}$
3,—1 —2 —3	$+0.012 \\ +0.073 \\ 0$	$+0.004 \\ +0.068 \\ +0.278$	$ \begin{array}{c c} +0.013 \\ -0.122 \\ -0.834 \end{array} $	+0.021 $+0.219$ $-0.007$	-0.049 $-0.344$ $+0.010$	+0.028 $-0.244$ $-1.260$
4, <u></u> 2 4	$+0.015 \\ +0.001$	$-0.001 \\ +0.155$	$+0.020 \\ -0.619$	+0.042	$-0.071 \\ +0.001$	+0.019 $-0.854$

The derivations with respect to  $\gamma$  and the node have been omitted because they are quite insensible. The terms of  $\delta R$  depending on these derivatives are given by equation (31). In the case of Uranus disturbed by Saturn the largest values of the coefficients

$$\frac{1}{2}i\hbar\cot\frac{1}{2}\gamma$$
;  $\frac{1}{2}\hbar\tan\frac{1}{2}\gamma$ ,  $\frac{1}{2}\frac{\partial h}{\partial \sigma}$ 

are only about .05, while the largest coefficients in  $\delta k$ ,  $\delta k'$ , and  $\delta \gamma$  are less than 10". Hence the largest terms in (31) will be of the order of magnitude 0".5 multiplied by the mass of Saturn, and may therefore be omitted entirely. Omitting them the values of  $\delta R$ ,  $\delta \frac{\partial R}{\partial \mathbf{v}}$  and  $\delta \frac{\partial R}{\partial \rho}$  become

$$\delta R = \frac{\partial R}{\partial \mathbf{v}} \, \delta \mathbf{v} + \frac{\partial R}{\partial \mathbf{v}'} \, \delta \mathbf{v}' + \frac{\partial R}{\partial \rho} \, \delta \rho + \frac{\partial R}{\partial \rho'} \, \delta \rho'$$

$$\delta \frac{\partial R}{\partial \mathbf{v}} = \frac{\partial^2 R}{\partial \mathbf{v}^2} \, \delta \mathbf{v} + \frac{\partial^2 R}{\partial \mathbf{v} \partial \mathbf{v}'} \, \delta \mathbf{v}' + \frac{\partial^2 R}{\partial \mathbf{v} \partial \rho} \, \delta \rho + \frac{\partial^2 R}{\partial \mathbf{v} \partial \rho'} \delta \rho$$

$$\delta \frac{\partial R}{\partial \rho} = \frac{\partial^2 R}{\partial \mathbf{v} \partial \rho} \, \delta \mathbf{v} + \frac{\partial^2 R}{\partial \mathbf{v}' \partial \rho} \, \delta \mathbf{v}' + \frac{\partial^2 R}{\partial \rho^2} \, \delta \rho + \frac{\partial^2 R}{\partial \rho \partial \rho'} \delta \rho'$$

All the separate factors from which the second members of these equations are formed have already been given. Forming their products in the way described in Chapter II, we have the result given in the following tables.

The expressions for  $\delta R$  are arranged so that the value of  $D'_t \delta R$  can be obtained from them by direct differentiation. This is done by distinguishing the time introduced into R by the co-ordinates of Uranus from that introduced by the co-ordinates of Saturn.

1						
	$\frac{2a_1}{m'} \left\{ \frac{\partial R}{\partial \mathbf{v}'} \delta \mathbf{v} \right\}$	$\partial' + \frac{\partial R}{\partial \rho'} \delta \rho' $		$\frac{2a_1}{m'}\left\{\frac{\partial R}{\partial \mathbf{v}'}\right\}$	$\delta v' + \frac{\partial R}{\partial \rho'} \delta \rho' $	
US	cos	sin	U S J	0,10		
1, 0 2, 0	$ \begin{array}{c c}  & 1.40t \\  & + 0.06t \\  & - 0.24t \end{array} $	-1.33t $-0.28t$ $+0.20t$	+1, 3—2 +2, +3, +4,	+375 -990 - 73 + 23	+7336 -558 -261 -42	2000
1,—1 2,—1 3,—1 0,—2	$ \begin{array}{c c} + 0.03t \\ - 1.05t \\ + 0.02t \\ + 0.93t \end{array} $	+ 0.04t - 0.95t - 0.30t - 0.83t	0, -2 1, 2, 3,	$ \begin{array}{r} -647 \\ +7737 \\ +153 \\ +24 \end{array} $	-319 +5616 -103 - 26	0.0
1,—2 2,—2 3,—2 1,—3	$ \begin{array}{c c} -12.69t \\ -0.24t \\ -0.63t \end{array} $ $ -1.60t$	+11.60t + 0.30t - 0.59t - 1.14t	4, -2, 5-2 -1, 0,	$ \begin{array}{r}                                     $	$\begin{array}{c c}  & & & & & & & & & & & \\  & + & 60 & & & & & & \\  & + & 739 & & & & & & \\  & - & 76 & & & & & & & \\ \end{array}$	1 1
2,—3 3,—3 4,—3	$\begin{array}{c} + \ 0.25t \\ + \ 0.08t \\ - \ 0.36t \end{array}$	- 0.29t + 0.02t - 0.34t	1, 2, —4, 6—2	+61 $-20$ $+27.5$	$+719 \\ +6 \\ -3.9$	30. 30. 10.00
3,—4 4,—4 <i>U U' S</i>	+ 0.19t + 0.15t	- 0.17t	-3, -2, -1, 0,	+94.1 $+66$ $-8823$ $+699$	$   \begin{array}{r}     + 24.4 \\     +243 \\     -6114 \\     +522   \end{array} $	1
1, 0 0 1, 0—1 1, 0—2 1, 0—3 1,+1—1	+ 38" + 2 -112 + 14 + 56	$   \begin{array}{r}     + 4'' \\     + 6 \\     -153 \\     - 18 \\     - 2   \end{array} $	-4, 7-2 -3, -2, -1,	+ 70 +299 +937 -1978	- 2 +147 +706 +1117	
$ \begin{array}{c} 1,-1+1\\ 1,+2-1\\ 1,-2+1\\ 1,+2-2\\ 1,-2+2 \end{array} $	+ 3 - 1 -117 - 23	$     \begin{array}{r}       0 \\       + 43 \\       + 19 \\       + 2 \\       0     \end{array} $		$\frac{2a_1}{m'} \left\{ \frac{\partial R}{\partial \mathbf{v}}  \delta \mathbf{v} \right.$	$+rac{\partial R}{\partial  ho}\delta_{ ho}\Big\}$	
1,+3—1 1,—3+1 1,+3—2 1,—3+2	$ \begin{array}{c} -28 \\ +30 \\ +140 \\ +14 \end{array} $	$+88 \\ +100 \\ +112 \\ -10$	U S' S 2,—1—1	cos ,,	sin " — 3	Fact. nt " -0.852
U S J 0, 1—1 1,	+246 2469	— 1 — 50	3, 4,	+ 59 -139	+801 +353	$+0.148 \\ +1.448$
2, 3,	- <sup>22</sup> + <sup>3</sup>	+ 4 + 6	3,—1—2 4, 5,	$ \begin{array}{c} -122 \\ -60 \\ +24 \end{array} $	+ 26 - 29 - 60	+0.148 $+1.148$ $+2.148$
-2, 2—1 -1, 0, 1, 2,	$   \begin{array}{r}     + 42 \\     +1638 \\     -136 \\     - 89 \\     + 2   \end{array} $	$ \begin{array}{r} -16 \\ -88 \\ +12 \\ -89 \\ +4 \end{array} $	-0,-1+1 +1, 2, 3,	-250 - 4 +197 - 15	$0 \\ -170 \\ -450 \\ +38$	-2.852 $-1.852$ $-0.852$ $+0.148$
-3, 3—1 -2, -1, 0,	+ 6 + 66 +478	$ \begin{array}{r}  - 8 \\  + 24 \\  -280 \end{array} $	-1,-1+2 0, 1,	- 8 - 11 - 80	+ 19 +134 + 33	-3.852 -2.852 -1.852
-3, 4—1 -2, -1,	+9 $-221$ $+297$	+ 28 - 5 -286	1,—1 0 2, 3,	- 90 + 6 + 12	$+12 \\ +158 \\ -32$	-1.852 $-0.852$ $+0.148$
10 May,	1873.			in its recommend	to out or man and	17

	$2rac{a_1}{m'n}$	8 <i>D'</i> <sub>6</sub> R	$2\frac{a_1}{m'}$	$\partial \frac{\partial R}{\partial \mathbf{v}}$	$2\frac{a_1}{m'}$	$\delta \frac{\partial R}{\partial  ho}$
U S 0, 0 1, 0 2, 0	sin  " + 1.40t - 0.12t	cos  — 1.33t — 0.56t	$\sin \frac{''}{0} \\ + \frac{1.40t}{-0.27t}$	$\cos \frac{''}{0} \\ -1.35t \\ -0.43t$	$\cos \\ + 0.14t \\ + 3.54t \\ - 0.34t$	sin  " + 3.21t + 0.90t
0,—1 1, 2, 3,	$\begin{array}{c} 0 \\ -0.03t \\ +2.10t \\ -0.06t \end{array}$	$\begin{array}{c} 0 \\ + 0.04t \\ - 1.90t \\ - 0.90t \end{array}$	$\begin{array}{c} -0.04t \\ -0.06t \\ +2.10t \\ -0.19t \end{array}$	$\begin{array}{l} -\ 0.06t \\ +\ 0.03t \\ -\ 1.89t \\ -\ 0.73t \end{array}$	$\begin{array}{l} + \ 1.06t \\ + \ 0.07t \\ + \ 3.54t \\ - \ 0.19t \end{array}$	$ \begin{array}{r} -1.02t \\ -0.12t \\ +3.22t \\ +1.18t \end{array} $
0,—2 1, 2, 3,	$0 \\ +12.69t \\ +0.48t \\ +1.89t$	$\begin{array}{c} 0 \\ +11.60t \\ +0.60t \\ -1.77t \end{array}$	$\begin{array}{l} -0.91t \\ +12.69t \\ +0.21t \\ +1.89t \end{array}$	$\begin{array}{c} -0.83t \\ +11.62t \\ +0.37t \\ -1.75t \end{array}$	$\begin{array}{c} +\ 0.84t \\ -13.52t \\ -\ 0.42t \\ +\ 2.78t \end{array}$	$\begin{array}{l} -0.94t \\ +12.34t \\ +0.14t \\ +2.52t \end{array}$
1,3 2, 3, 4,	$\begin{array}{c c} + 1.60t \\ - 0.50t \\ - 0.24t \\ + 1.44t \end{array}$	$\begin{array}{c} -1.14t \\ -0.58t \\ +0.06t \\ -1.36t \end{array}$	$\begin{array}{c} + \ 1.61t \\ - \ 0.53t \\ - \ 0.19t \\ + \ 1.43t \end{array}$	$ \begin{array}{r} -1.11t \\ -0.56t \\ +0.07t \\ -1.32t \end{array} $	$\begin{array}{l} -1.64t \\ -0.83t \\ -0.25t \\ +1.93t \end{array}$	$\begin{array}{l} -1.21t \\ +0.75t \\ -0.10t \\ +1.76t \end{array}$
3,—4 4,	$-0.57t \\ -0.60t$	$-0.51t \\ 0$	$-0.55t \\ -0.52t$	-0.53t + 0.10t	$-0.74t \\ -0.73t$	$\begin{array}{c} + \ 0.68t \\ - \ 0.10t \end{array}$
0, 0 1, 0 2, 3,	$ \begin{array}{r} -45 \\ +168 \\ +2 \end{array} $	+319 +383 + 5	+ 9 +199	+ 5 +160 +449	-192 $-49$ $+278$	709 591
-1,-1 0, 1, 2, 3, 4,	+148 + 27 - 139 - 21 - 4 + 28	$ \begin{array}{r} -61 \\ -381 \\ -70 \\ -36 \\ +38 \\ +88 \end{array} $	$   \begin{array}{c}     +70 \\     -16 \\     -4 \\     +3 \\     +1 \\     -8   \end{array} $	$ \begin{array}{rrrr}  & -71 \\  & -247 \\  & -32 \\  & -12 \\  & -1 \\  & +4 \end{array} $	$ \begin{array}{c} + 18 \\ - 49 \\ + 103 \\ + 1 \\ - 10 \\ - 19 \end{array} $	+125 $+347$ $+47$ $-215$ $+38$ $-9$
1,—2 2, 3, 4, 5,—2	$ \begin{array}{c c} +87 \\ -88 \\ +108 \\ +20 \\ \cdots \end{array} $	—153 — 7 +121 +517	$ \begin{array}{c} -14 \\ +145 \\ -60 \\ +141 \\ -18 \end{array} $	-119 $-13$ $+796$ $+352$ $+14$	$ \begin{array}{r} -10 \\ +84 \\ +83 \\ -262 \\ -45 \end{array} $	$+251 \\ + 7 \\ +816 \\ +617 \\ + 2$
3,—3 4, 5,	$   \begin{array}{r}     + 18 \\     + 69 \\     - 52   \end{array} $	+ 4 33 128	+208 + 82 49	+ 16 $- 67$ $- 130$	+ 17 - 35 - 92	+ 34 + 44 +181
4,—4 5, 6,			+ 55 + 8 - 42	— 1 —104 —103	+110 + 12 - 61	+ 8 + 52 +148

	$2\frac{a_i}{m'n}\delta D'_iR$		$2rac{a_i}{m'}$	$\delta \frac{\partial R}{\partial \mathbf{v}}$	$2\frac{a_1}{m'}$	$\delta \frac{\partial R}{\partial \rho}$
$U S \dot{J}$	sin "	cos	sin "	cos	cos	sin "
0, 1—1 1, 2, 3,	$ \begin{array}{c} 0 \\ +2469 \\ +44 \\ -9 \end{array} $	$ \begin{array}{c c}  & 0 \\  & -50 \\  & +8 \\  & +18 \end{array} $	-185 +2477 - 7 - 6	+ 2 - 50 + 13 + 16	- 84 2947 176 17	+ 13 - 69 - 17 - 20
-2, 2—1 -1, 0, +1, +2,	$^{+\ 84}_{+1638}$ $^{0}_{+\ 89}$ $^{-\ 4}$	$   \begin{array}{r}     + 32 \\     + 88 \\     0 \\     - 89 \\     + 8   \end{array} $	$\begin{array}{c} + 42 \\ +1642 \\ -114 \\ + 83 \\ - 1 \end{array}$	+ 29 + 88 - 2 - 89 + 8	$   \begin{array}{r}     + 9 \\     +1231 \\     + 41 \\     -196 \\     - 11   \end{array} $	$   \begin{array}{r}     + 49 \\     -143 \\     + 11 \\     - 62 \\     - 18   \end{array} $
-3, 3-1 -2, -1, 0,	+ 18 +132 +478 0	+ 24 48 +280 0	+ 25 +143 +477 - 57	+ 28 - 54 + 279 - 8	- 42 191 +1529 60	$\begin{array}{c} + 41 \\ -104 \\ -279 \\ + 44 \end{array}$
_3, 4—1 _2, _1,	+ 27 $-442$ $+297$	$-84 \\ +10 \\ +286$	+71 $-449$ $+310$	$-91 \\ +7 \\ +270$	- 89 +776 +362	—134 — 8 —258
1, 3—2 2, 3, 4,	$-375 \\ +1980 \\ +219 \\ -92$	+7336 1116 783 168	$-393 \\ +1987 \\ +51 \\ -104$	+7343 1271 672 102	+629 +3304 +151 -136	+7722 +2544 +1041 +158
0, 4—2 1, 2, 3,	0 —7737 —306 — 72	+5616 -206 - 78	+669 -7733 -235 + 59	—485 +5606 —258 — 52	$ \begin{array}{c} -601 \\ +12136 \\ +273 \\ -60 \end{array} $	-966 +8698 +910 +109
-2, 5-2 -1, 0, +1, +2,	+180 -625 0 - 61 + 40	-120 $-739$ $0$ $+719$ $+12$	+159 $-620$ $+62$ $-63$ $-13$	$   \begin{array}{r}     + 6 \\     -740 \\     - 56 \\     +725 \\     - 6   \end{array} $	-337 -1222 +167 + 72 - 17	$ \begin{array}{r} -37 \\ -1217 \\ -60 \\ +1109 \\ +67 \end{array} $
-4, 6-2 -3, -2, -1, 0,	+110.0 +282.3 +132 -8823 0	$\begin{array}{c} + \ 15.6 \\ - \ 73.2 \\ -486 \\ +6114 \\ 0 \end{array}$	+86.1 $+248.8$ $+237$ $-8829$ $+746$	+32.9 $-14.5$ $-557$ $+6121$ $-493$	—127.5 —413.6 —1131 —12973 +774	+39.4 $-75.7$ $-1461$ $-9020$ $+406$
-4, 7-2 -3, -2, -1, 0,	+280 +897 +1874 -1978 0	+ 8 441 1412 1117 0	+207 +727 +1913 -1995 +139	+ 45 632 1374 1097 + 90	-216 -1128 -3236 -2071 +144	+ 48 977 2195 +904 71

In the terms of  $\delta R$  introduced by the perturbations of Saturn, namely,  $\frac{\partial R}{\partial v'} \delta v' + \frac{\partial R}{\partial \rho'} \delta \rho'$ , the differentiation represented by  $D'_t$  should be performed by considering  $\delta v'$  and  $\delta \rho'$  as constant, although they are expressed as a function of the mean longitude of Uranus, as well as of Saturn. The mean longitude of Uranus thus introduced is therefore represented by U', which is regarded as constant in taking  $D'_t R$ , and U only supposed to vary.

Again, in the terms  $\frac{\partial R}{\partial v} \delta v + \frac{\partial R}{\partial \rho} \delta \rho$ , since  $\delta v$  and  $\delta \rho$  represent perturbations of

Uranus, their complete derivatives, with respect to the time, are to be taken. But their expressions contain the mean longitude of Saturn as well as Uranus. The mean longitude of Saturn thus introduced is represented by S', and is to be considered variable in obtaining  $D_t \delta R$ , while S is considered constant. The ratio of the coefficient of t to n in the various terms of this part of  $\delta R$  is given to the right of each corresponding term.

The value of  $D'_t \delta R$  being once obtained, there is no longer any distinction necessary between U, U', or between S and S'. The similar terms are therefore combined by putting S' = S; U' = U.

From the above values of  $2\delta D_t' R$  and  $2\delta \frac{\partial R}{\partial \rho}$ , we form the following value of

$$\frac{a_1}{m} \delta Q = \frac{2a_1}{m} \int \delta D'_t R dt + \frac{a_1}{m} \delta \frac{\partial R}{\partial \rho}$$

and of the other quantities which enter the perturbations of the co-ordinates. We shall begin with those terms which depend only on the mutual action of Saturn and Uranus, because they are few and small, and the only terms which are sensible are those in which the coefficient of the mean longitude of Saturn is —1. We shall therefore confine ourselves to these. And, instead of employing the condensed formulæ, we shall make the computation in full by (13).

$\frac{a_1}{m'} \delta Q$	$=2^{\circ}\frac{a_1}{m}\int \delta D'_{\delta}R$	$dt + \delta \frac{\partial R}{\partial \rho}$	$\frac{a_i}{m'}$	$\xi \delta Q$	$\frac{a_1}{m'}$	ηδ $Q$
$\begin{bmatrix} -1,-1 \\ 0 \\ 1 \\ 2 \end{bmatrix}$	$\begin{array}{c} \cos \\ " & " \\ + 47 \\ - 14 + 0.53t \\ - 24 + 0.02t \\ - 60 + 4.23t \\ - 525 + 0.31t \\ \end{array}$	+307-0.51t $+62-0.08t$ $-28+3.84t$ $+240-5.49t$	$\begin{array}{r} + 13 + 0.02t \\ - 41 + 2.37t \\ - 270 - 0.13t \\ + 7 + 2.09t \end{array}$		+36-0.06t +29-1.85t +250-0.13t	-164 + 2.11t + 85 - 2.70t + 14 - 1.92t
		cos 4δρ			δυ	
g l' 0,—1 1, 2, 3, 4,	+.001—.000 +.024+.000 +.333+.00 142—.000	$ \begin{array}{c cccc} 033t &03 \\ 437t &40 \end{array} $	sin '' 23+.00002t 66+.00033t 06+.00432t 7900169t	sin " " +0.002+0.0 +0.043+0.0 +0.620+0.0 +2.69 -0.0 +0.132	$ \begin{vmatrix} 0006t \\ 0098t \\ 0011t \end{vmatrix} $ $ \begin{vmatrix} +0.05 \\ +0.86 \\ +0.85 \end{vmatrix} $	cos 21+0.0000t 58+0.0000t 03-0.0097t 30-0.0153t 40+0.0000t

The computation of these terms being extremely complex, a check upon their accuracy is desirable. In the case of the secular variations of the coefficients, the coefficients of the time are easily obtained by substituting in the integrated perturbations the variations of the eccentricity and perihelion of Saturn. Thus I have found

The greatest discrepancy is found in the coefficient of  $\sin (3g - l)$ , and it amounts to  $0^{\circ}.0038t$ , or about  $0^{\circ}.4$  in a century. But, owing to the great period of this term, nearly 600 years, this difference, during any one century, will be nearly eliminated through the mean longitude and mean motion.

It may also be remarked that in this case the terms derived from the perturbations of the elements are undoubtedly the correct ones, and will therefore be employed.

The terms which the preceding integration fails to give, owing to the constant terms introduced into  $\xi \delta Q$  and  $\eta \delta Q$ , are found by (22).

We thus have

$$\begin{split} n\Sigma p_u k_v^{(u)} &= +0".36 \\ n\Sigma q_u k_v^{(u)} &= +0.27 \\ r_1^2 \delta \rho &= \frac{1}{4} Mnt^2 \left\{ 0".36 \sin g - 0".27 \cos g \right\} \\ \delta v &= \frac{1}{2} Mnt^2 \left\{ 0".36 \cos g + 0".27 \sin g \right\} \\ &= t^2 \left\{ 0".0000038 \cos g + 0".0000029 \sin g \right\}. \end{split}$$

The greatest effect of these terms amounts to less than one-twentieth of a second in a century. They may therefore be neglected in the present theory. The other terms containing the square of the time are yet smaller.

Applying the terms of the second order thus found to the terms of the first order depending on the corresponding arguments, the perturbations of Uranus by Saturn become

0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	81	,	co	s 48p
g l' -1,-1 0,-1 1,-1 2,-1 3,-1 4,-1 5,-1	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} \cos \\ " & " \\ + 0.039 \\ + 0.739 \\ + 8.580 \\ + 144.265 - 0.94T \\ + 116.69 - 1.38T \\ + 5.656 \\ + 0.329 \end{array}$	+ 0 11 +1753 87 237 55 4	sin  - 2 - 31 -244 -3114 +644 +140 + 10

The other terms remain the same as given on page 50.

The other terms remain the same as given on page 50.

Perturbations depending on the product of the masses of Jupiter and Siturn.

The values of  $\delta D'_{t}R$ ,  $\delta \frac{\partial R}{\partial \mathbf{v}}$ , and  $\delta \frac{\partial R}{\partial \rho}$ , depending on the products of the masses

of Jupiter and Saturn, are given on page 74. The computation from these data being conducted in the same way as in the case of the terms of the first order, it is not necessary to give much more than the results. These are shown in the following table. The indices to the left represent the coefficients of the mean longitudes of Uranus, Saturn, and Jupiter, all counted from the perihelion of Uranus. Column  $\nu$  gives the ratio of the mean motion of Uranus to the coefficient of the time in each argument. The perturbations of the common logarithm of the radius vector are expressed in units of the seventh place of decimals.

		ν	8	v	0.45	343 δρ
U S	J		sin ,	cos "	cos	sin
0, 1, 1, 3, 4,	-1	-0.2364 -0.3095 -0.4480 -0.8127	+0.002 $-0.020$ $+0.004$ $+0.016$	0 0 0.003 0.024	0 0 0 0	0 0 0 0
-2, 2,- -1, 0, 1, 2,	-1	$\begin{array}{c} -0.2960 \\ -0.4204 \\ -0.7254 \\ -2.6420 \\ +1.6090 \end{array}$	-0.007 $-0.108$ $-0.014$ $+0.164$ $+0.005$	-0.001 -0.007 -0.012 -0.267 -0.005	$ \begin{array}{c c}  & 0 \\  & -2 \\  & 0 \\  & +1 \\  & 0 \end{array} $	0 0 0 + 1 0
-3, 3,- -2, -1, 0,	-1	-0.6551 $-1.8997$ $+2.1115$ $+0.6786$	+0.012 $+0.175$ $+0.078$ $+0.007$	$\begin{array}{c} -0.002 \\ -0.015 \\ +0.512 \\ +0.024 \end{array}$	$\begin{array}{c} 0 \\ +1 \\ -2 \\ 0 \end{array}$	$\begin{array}{c} 0 \\ 0 \\ + 3 \\ 0 \end{array}$
—3, 4,— —2, —1,	-1	+0.754 $+0.430$ $+0.301$	$-0.030 \\ +0.043 \\ +0.001$	+0.081 $+0.005$ $-0.003$	$-{0\atop 1}\atop 0$	+ 1 0 0
1, 3,— 2, 3, 4,	-2	-0.2170 -0.2771 -0.3833 -0.6215	-0.002 $-0.051$ $-0.010$ $+0.032$	$-0.032 \\ +0.035 \\ +0.050 \\ +0.052$	$-{1\atop 0}\atop 0$	. — 1 — 1 — 1 — 1
0, 4,— 1, 2, 3,	-2	-0.3627 $-0.5692$ $-1.3210$ $+4.1150$	-0.010 $+0.075$ $-0.349$ $-0.510$	0.004 0.154 1.297 0.453	$ \begin{array}{c} 0 \\ -5 \\ -3 \\ +2 \end{array} $	$\begin{array}{c} 0 \\ -2 \\ +11 \\ -2 \end{array}$
—2, 5,— —1, 0, 1, 2,	-2	$\begin{array}{c} -0.5250 \\ -1.1051 \\ +10.5152 \\ +0.9132 \\ +0.4773 \end{array}$	-0.253 $-4.433$ $-0.546$ $+0.206$ $+0.012$	0.034 0.617 0.032 3.254 0.192	$     \begin{array}{r}       -3 \\       -43 \\       +2 \\       -2 \\       0     \end{array} $	$\begin{array}{c} 0 \\ + 7 \\ 0 \\ -36 \\ - 2 \end{array}$
-4, 6,- -3, -2, -1, 0,	.2	-0.9497 $-18.9250$ $+1.0558$ $+0.5136$ $+0.3393$	+1.824 $+40.650$ $+6.237$ $+0.467$ $+0.007$	-0.519 -10.500 -7.866 -0.539 -0.017	$   \begin{array}{c}     +19 \\     +32 \\     -63 \\     0 \\     0   \end{array} $	$   \begin{array}{r}     + 6 \\     +10 \\     -79 \\     - 2 \\     0   \end{array} $
-4, 7,— -3, -2, -1, -0,	2	+0.5558 $+0.3573$ $+0.2632$ $+0.2084$ $+0.1724$	$ \begin{array}{r} -0.050 \\ -0.046 \\ -0.045 \\ +0.006 \\ 0 \end{array} $	$\begin{array}{c} -0.003 \\ +0.032 \\ +0.032 \\ +0.007 \\ 0 \end{array}$	$\begin{array}{c} +1\\ +1\\ +1\\ 0\\ 0\\ 0\end{array}$	$\begin{array}{c} & 0 \\ + & 1 \\ + & 1 \\ 0 \\ 0 \end{array}$

## CHAPTER V.

# COLLECTION AND TRANSFORMATION OF THE PRECEDING PERTURBATIONS OF URANUS.

The terms of the perturbations which neither contain the elements of the disturbing planets, nor depend on the secular variations of the eccentricity and perihelion, admit of being greatly simplified by a slight change in the arbitrary elements. These terms are as follows:

## (1) In the longitude of Uranus

	"	"	"	"	"
Action of Jupiter,	+31.2116t	$+25.657 \sin g$	$+1.397 \sin 2g$	$-1.859\cos g$	$-0.087\cos 2g$
Action of Saturn,	+10.9690t	$+8.545\sin g$	$+0.461 \sin 2g$	$-4.735\cos g$	$-0.169\cos 2g$
Action of Neptune,	- 0.4262t	$+ 0.697 \sin g$	$+0.046 \sin 2g$	$-0.088\cos g$	$-0.005\cos 2g$
Total,	+41.7544t	$+34.899 \sin g$	$+1.904 \sin 2g$	$-6.682\cos g$	$0.261\cos 2g$

## (2) In the value of cos ψδρ, units of 7th place of decimals.

Action of Jupiter,
 
$$-10089$$
 $-492 \cos g$ 
 $-33 \cos 2g$ 
 $-2 \sin g$ 
 $+1 \sin 2g$ 

 Action of Saturn,
  $-3543$ 
 $-184 \cos g$ 
 $-15 \cos 2g$ 
 $-15 \sin g$ 

 Action of Neptune,
  $+138$ 
 $-1\cos g$ 
 $-1\cos 2g$ 
 $+1\sin g$ 

 Total,
  $-13494$ 
 $-677 \cos g$ 
 $-49\cos 2g$ 
 $-16\sin g$ 
 $+1\sin 2g$ 

Let us first consider the first or constant term in the perturbation of each co-ordinate. If we suppose a change of  $\delta n$  in the mean motion of a planet, the corresponding change in  $\delta \rho$  will be

$$\delta \rho = -\frac{2}{3} \frac{\delta n}{n}$$
.

If, then, we increase the mean motion of Uranus by 41".754, the corresponding change in  $\delta\rho$  will be -18045, and in  $\cos\psi\delta\rho$ , -18025. Subtracting these from the above perturbations, the secular term in the mean motion will disappear, and we shall have for the constant term of  $\cos\psi\delta\rho$ 

$$+4531$$

This same change in the mean motion will produce a secular term in the equation of the centre of the same nature with that produced by the secular variation of the perihelion. The differences of the values of the secular terms, found by the two methods employed in Chapters II. and III., proceeds from the fact that in the one case the effect of the above term in the mean motion is included, and in the other excluded.

If we subduct the effect in question when necessary, the remainder will be the effect of the secular variation of the longitude of the perihelion of Uranus, to which we shall revert presently.

Let us next introduce such a change in the eccentricity of Uranus as shall produce the term  $34''.899 \sin g$ , and ascertain its effect on the other terms. For this purpose we must determine  $\varepsilon e$  by the condition

$$(2 - \frac{3}{4}e^2) \delta e = 34''.899$$

which gives

$$\delta e = 17''.464 = .0000847.$$

A change of this amount in  $\delta e$  will introduce the following terms in  $\delta v$  and  $\delta \rho$ 

$$\delta v = 34''.899 \sin g + 2''.048 \sin 2g \cos 4\delta \rho = 20 - 844 \cos g - 59 \cos 2g.$$

Subtracting these terms from the expressions previously found we have

$$\delta v = -0''.144 \sin 2g - 6''.682 \cos g - 0''.261 \cos 2g.$$

$$\cos \psi \delta \rho = +4511 + 167 \cos g + 10 \cos 2g - 16 \sin g + 1 \sin 2g.$$

Again, let us put

$$e\delta\pi = 3''.342 = .0000162,$$

we shall have the elliptic terms

$$\delta v = -6''.682 \cos g - 0''.391 \cos 2g \cos \psi \delta \rho = -162 \sin g - 11 \sin 2g.$$

Subtracting these expressions the constant terms, independent of the mean longitude of the disturbing planets, are reduced to

$$\delta v = -0''.144 \sin 2g + 0''.130 \cos 2g.$$

$$\cos \psi \delta \rho = 4511 + 167 \cos g + 10 \cos 2g + 146 \sin g + 12 \sin 2g.$$

$$0.43429 \ \delta \rho = 1969 + 73 \cos g + 4 \cos 2g + 63 \sin g + 5 \sin 2g.$$

In the last equation we have introduced the constant +.0000008 produced in  $\delta \rho$  by the combined action of Venus, the Earth, and Mars. The effect of each planet is computed by the approximate formula

$$\delta \rho = \frac{1}{6} m' (b_i^{(0)} + \alpha D \alpha b_i^{(0)}).$$

#### Secular Variations.

The following inequalities result from the secular variations of the eccentricity and longitude of perihelion produced by each of the disturbing planets, T being the time expressed in centuries.

From the variation of the eccentricity

	"	"	11
Action of Jupiter,	$\delta v = -1.216 T \sin g$	$-0.072 T \sin 2g$	$-0.005 T \sin 3g$
Action of Saturn,	$-9.182 T \sin g$	$-0.538 T \sin 2g$	$-0.032 T \sin 3g$
Action of Neptune,	$-0.502 T \sin g$	$-0.030 T \sin 2g$	$-0.002 T \sin 3g$

Action of Jupiter, 
$$M\delta\rho = +13\,T\cos\,g + 1\,T\cos\,2g$$
  
Action of Saturn,  $+98\,T\cos\,g + 7\,T\cos\,2g$   
Action of Neptune,  $+6\,T\cos\,g$ 

The secular variation of the longitude of the perihelion is

	"
Action of Jupiter,	+122.1T
Action of Saturn,	+118.4T
Action of Neptune,	+ 51.1 T
Total,	$\delta\pi = +291.6T$

The effect of this secular variation on the longitude and radius vector is

Action of Jupiter, 
$$\delta v = -11.46 \, T \cos g$$
  $-0.671 \, T \cos 2g$   $-0.047 \, T \cos 3g$ 
Action of Saturn,  $-11.11 \, T \cos g$   $-0.651 \, T \cos 2g$   $-0.039 \, T \cos 3g$ 
Action of Neptune,  $-4.80 \, T \cos g$   $-0.281 \, T \cos 2g$   $-0.016 \, T \cos 3g$ 
Total,  $-27.37 \, T \cos g$   $-1.603 \, T \cos 2g$   $-0.102 \, T \cos 3g$ 

Action of Jupiter,  $M \delta \rho = -120 \, T \sin g$   $-8 \, T \sin 2g$ 
Action of Saturn,  $-117 \, T \sin g$   $-8 \, T \sin 2g$ 
Action of Neptune,  $-50 \, T \sin g$   $-3 \, T \sin 2g$ 

For the purpose of conveniently tabulating the perturbations, we shall express them in a form similar to that adopted in the theory of Neptune. Let us select, from the terms of the periodic perturbations produced by any planet, all those in which the difference between the indices *i* and *i'* is the same. For example, in the perturbations of the longitude produced by Jupiter, let us consider the terms

$$\delta v = +1.269 \sin ( - l) +0.002 \cos ( - l) -3.495 \sin (2g - l) -0.092 \cos (2g - l) +1.182 \sin ( g - 2l) +0.515 \cos ( g - 2l) +0.074 \sin (3g - 2l) -0.005 \cos (3g - 2l) -0.005 \sin (2g - 3l) +0.011 \sin (4g - 3l) -0.001 \cos (4g - 3l)$$

These terms may be expressed in the form

In general, a series of terms of the form

$$\Sigma a_i \sin(iA + sg) + \Sigma b_i \cos(iA + sg) + \Sigma a_i' \sin(iA - sg) + \Sigma b_i' \cos(iA - sg),$$

may be put in the form

$$\begin{aligned} & \{ \Sigma \left( a_i - a'_i \right) \cos iA - \Sigma \left( b_i - b'_i \right) \sin iA \} \sin sg \\ & + \{ \Sigma \left( a_i + a'_i \right) \sin iA + \Sigma \left( b_i + b'_i \right) \sin iA \} \cos sg. \end{aligned}$$

All the periodic terms containing only g and l in the arguments may be put into this form by taking

$$A = g - l$$

so that the coefficients of  $\sin sg$  and  $\cos sg$  may all be expressed as a function of the single variable argument A.

The perturbations of the elements may be reduced to perturbations of the co-ordinates expressed as the sum of several products of slowly varying functions into the sines and cosines of the multiples of g. We have, in fact,

$$\begin{split} \delta v &= \delta l \\ &+ \left(2 - \frac{3}{4} e^2\right) \delta e \times \sin g \\ &+ \left(2 - \frac{1}{4} e^2\right) e \delta g \times \cos g \\ &+ \left(\frac{5}{2} e - \frac{11}{6} e^3\right) \delta e \times \sin 2g \\ &+ \left(\frac{5}{2} e - \frac{11}{12} e^3\right) e \delta g \times \cos 2g. \\ &+ \text{etc.} \end{split}$$

It appears, therefore, that all the perturbations in which the arguments contain the mean longitudes of only two planets may be put in the form

$$\delta v = (v.c.0) + (v.c.1)\cos g + (v.c.2)\cos 2g + \text{etc.} + (v.s.1)\sin g + (v.s.2)\sin 2g + \text{etc.} M\delta \rho = (\rho.c.0) + (\rho.c.1)\cos g + (\rho.c.2)\cos 2g + \text{etc.} + (\rho.s.1)\sin g + (\rho.s.2)\sin 2g + \text{etc.}$$

We have next to reduce to the same form those terms which contain the mean longitudes of both Jupiter and Saturn, and which are given on page 78. We have here twenty-four terms, each greater than  $0^{\circ}.04$ . As most of these terms depend on three independent arguments, they cannot be included in a double entry table, while, if we include them as perturbations of the longitude in tables of single entry, we shall have to enter twenty-two tables with as many different arguments. But, by taking, for the argument A, the middle one in each series of arguments which depend on the same multiples of Jupiter and Saturn, and expressing the terms above and below it in each series as coefficients of  $\sin g$ ,  $\cos g$ ,  $\sin 2g$ , and

 $\cos 2g$ , we may reduce the number of arguments to eight, and the number of tables to seventeen. Consider, for instance, the terms of the second series,

$$\begin{array}{lll} -0.108 \sin \left(-g + 2S - J\right) & -0.007 \cos \left(-g + 2S - J\right) \\ -0.014 \sin \left(2S - J\right) & -0.012 \cos \left(2S - J\right) \\ +0.164 \sin \left(g + 2S - J\right) & -0.267 \cos \left(g + 2S - J\right). \end{array}$$

These terms may be allowed for by adding to (v.c.0), (v.s.1), (v.c.1), the terms

From the perturbations of longitude and radius vector already given, we readily find the following values of (v.c.0), (v.s.1), etc.

$$Action of Jupiter. \\ A_1 = l' - g$$

$$(v.c.0) = +53.064 \sin A_1 - 0.004 \cos A_1 \\ - 0.277 \sin 2A_1 + 0.036 \cos 2A_1 \\ - 0.025 \sin 3A_1$$

$$(v.c.1) = + 2.226 \sin A_1 - 0.090 \cos A_1 \quad (v.s.1) = -0.094 \sin A_1 - 4.764 \cos A_1 \\ - 1.256 \sin 2A_1 + 0.510 \cos 2A_1 \quad -0.520 \sin 2A_1 - 1.108 \cos 2A_1 \\ - 0.006 \sin 3A_1 \quad +0.016 \cos 3A_1 \\ -11''.46T \quad -1''.22T$$

$$(v.c.2) = + 0.121 \sin A_1 - 0.038 \cos A_1 \quad (v.s.2) = -0.056 \sin A_1 - 0.175 \cos A_1 \\ + 0.012 \sin 2A_1 - 0.014 \cos 2A_1 \quad +0.008 \sin 2A_1 + 0.042 \cos 2A_1 \\ + 0.029 \sin 3A_1 - 0.034 \cos 3A_1 \quad -0''.67T \quad (v.s.3) = -0.005T$$

$$(v.c.3) = -0.04T \quad (v.s.3) = -0.005T$$

$$(v.c.4) = -0.034 \sin A_1 + 2 \cos A_1 \\ + 2 \cos$$

Action of Saturn.

$$A_2 = \overline{t} - g$$

$$(v.e.0) = \begin{pmatrix} +20.774 \\ -0.06 T \end{pmatrix} \sin A_1 + 8.580 \cos A_2$$

$$-4.110 \sin 2A_1 & -0.009 \cos 2A_2 \\ -0.028 \sin 4A_2 & -0.008 \cos 4A_3 \\ -0.074 \sin 5A_4 & -0.008 \cos 5A_3 \\ -0.025 \sin 6A_2 & -0.008 \cos 5A_3 \\ -0.025 \sin 6A_2 & -0.003 \cos 5A_3 \\ -0.025 \sin 6A_2 & -0.030 \cos 5A_3 \\ -0.025 \sin 6A_2 & -0.030 \cos 5A_3 \\ -0.025 \sin 6A_2 & -0.030 \cos 3A_3 \\ -0.109 \sin A_2 & -0.030 \cos 3A_3 & -0.226 \sin 3A_4 & +0.307 \cos 2A_3 \\ -0.109 \sin A_2 & -0.030 \cos 3A_3 & -0.226 \sin 3A_4 & +0.097 \cos 4A_3 \\ -0.038 \sin 5A_2 & -0.030 \cos 5A_2 & -0.055 \sin 4A_4 & +0.097 \cos 4A_3 \\ -0.038 \sin 5A_2 & -0.130 \cos 5A_2 & -0.027 \sin 5A_2 & +0.038 \cos 5A_2 \\ -11''.11T$$

$$(v.c.2) = \begin{pmatrix} -52.026 \\ -0.27 T \end{pmatrix} \sin A_2 + \begin{pmatrix} +116.73 \\ -1.38 T \end{pmatrix} \cos A_2 & (v.s.2) = \begin{pmatrix} +116.650 \\ -1.38 T \end{pmatrix} \sin A_1 + \begin{pmatrix} 51.954 \\ +0.27 T \end{pmatrix} \cos A_4 \\ -0.081 \sin 3A_4 & -0.044 \cos 4A_3 & -0.177 \sin 3A_4 & +0.013 \cos 4A_4 \\ -0.005 \sin 5A_2 & -0.153 \cos 3A_3 & -0.177 \sin 3A_4 & +0.013 \cos 4A_4 \\ -0.005 \sin 5A_2 & -0.016 \cos 5A_2 & -0.016 \sin 5A_4 & +0.005 \cos 5A_3 \\ -0.07 \cos T \end{pmatrix}$$

$$(v.c.3) = -2.265 \sin A_4 & +5.656 \cos A_3 & +2.956 \sin A_4 & +2.265 \cos A_4 \\ +0.025 \sin 5A_4 & -0.004 \cos 5A_4 & -0.016 \sin 5A_4 & -0.005 \cos 5A_4 \\ -0.005 \sin 5A_4 & -0.004 \cos 5A_4 & -0.013 \sin 4A_4 & -0.005 \cos 5A_4 \\ -0.005 \sin 5A_4 & -0.002 \cos 5A_4 & -0.013 \sin 4A_4 & -0.005 \cos 5A_4 \\ -0.005 \sin 5A_4 & -0.003 \cos 3A_4 & +0.003 \sin 4A_4 & -0.005 \cos 5A_4 \\ -0.005 \sin 5A_4 & -0.003 \cos 3A_4 & +0.003 \sin 3A_4 & -0.005 \cos 5A_4 \\ -0.005 \sin 5A_4 & -0.003 \cos 3A_4 & +0.003 \sin 3A_4 & -0.005 \cos 5A_4 \\ -0.005 \sin 5A_4 & -0.003 \cos 3A_4 & +0.003 \sin 3A_4 & -0.005 \cos 5A_4 \\ -0.005 \sin 5A_4 & -0.003 \cos 3A_4 & +0.003 \sin 3A_4 & -0.005 \cos 5A_4 \\ -0.005 \sin 5A_4 & -0.003 \cos 3A_4 & +0.003 \sin 3A_4 & -0.005 \cos 5A_4 \\ -0.005 \sin 5A_4 & -0.003 \cos 3A_4 & +0.005 \cos 5A_4 \\ -0.005 \sin 5A_4 & -0.003 \cos 3A_4 & +0.005 \cos 5A_4 \\ -0.005 \sin 5A_4 & -0.003 \cos 3A_4 & +0.005 \cos 5A_4 \\ -0.005 \sin 3A_4 & -0.005 \cos 5A$$

+ 281 cos  $A_{\star}$ 

3 cos 3A,

 $9 \sin 2A_9 + 27 \cos 2A_1$ 

+

-8T

+ 9 sin 2 $A_2$  — 24 cos 2 $A_2$ 

 $(\rho. s.3) = -24 \sin A_2 + 61 \cos A_2$ 

+

 $(\rho, c.2) = -279 \sin A_2 - 103 \cos A_2$ 

 $(\rho. c.3) = -61 \sin A_2 - 24 \cos A_1$ 

- 3 sin 3 $A_{\star}$ 

 $-27 \sin 2A_2 + 9 \cos 2A_2$ 

+7T

 $+ 24 \sin 2A_2 + 9 \cos 2A_2$ 

```
Action of Neptune.
                                     A_3 = g - l'
(v.c.0) = -39.66 \sin A_3 -0.08 \cos A_3
        -35.36 \sin 2A_3
                          -0.03\cos 2A_3
        +17.29 \sin 3A_3
                           +0.23\cos 3A_3
        + 3.91 \sin 4A_3
                           +0.06\cos 4A_3
        + 0.99 \sin 5A_3
                           -0.04\cos 5A_3
        + 0.42 \sin 6A_3
                           -0.01\cos 6A_3
        + 0.19 \sin 7A_3
        + 0.09 \sin 8A_3
        + 0.02 \sin 9A_3
                    +81
(v.c.1) = -6.77 \sin A_3 - 0.53 \cos A_3
                                           (v.s.1) = -0.49 \sin A_3 + 1.75 \cos A_3
        -1.10 \sin 2A_3 + 0.07 \cos 2A_3
                                                    +0.12\sin 2A_3 - 2.48\cos 2A_3
        +23.25 \sin 3A_3 + 4.04 \cos 3A_3
                                                    +4.04 \sin 3A_3 -20.92 \cos 3A_3
        +6.05 \sin 4A_3 + 1.06 \cos 4A_3
                                                     +1.07 \sin 4A_3 - 5.42 \cos 4A_3
          -3.26 \sin 5A_3 -0.66 \cos 5A_3
                                                     -0.68 \sin 5A_3 + 3.47 \cos 5A_3
         -0.80 \sin 6A_3 -0.17 \cos 6A_3
                                                     -0.17 \sin 6A_3 + 0.91 \cos 6A_3
         -0.24 \sin 7A_3 -0.05 \cos 7A_3
                                                     -0.04 \sin 7A_3 + 0.30 \cos 7A_3
                                                     -0.02 \sin 8A_3 + 0.12 \cos 8A_3
         -0.12 \sin 8A_3 -0.02 \cos 8A_3
         -0.06 \sin 9A_3 -0.01 \cos 9A_3
                                                     -0.01 \sin 9A_3 + 0.06 \cos 9A_3
                                                                    + 0.04 \cos 10 A_3
         -0.04 \sin 10 A_3
                                                             +1.99835\delta e
               +1.99945e\delta g
(v.c.2) = -0.43 \sin A_3 - 0.03 \cos A_3 \quad (v.s.2) = -0.03 \sin A_3 + 0.13 \cos A_3
         -0.03 \sin 2A_3 + 0.01 \cos 2A_3
                                                    +0.02 \sin 2A_3 - 0.16 \cos 2A_3
        +0.75 \sin 3A_3 + 0.08 \cos 3A_3
                                                     +0.08 \sin 3A_3 - 0.60 \cos 3A_3
        -0.10 \sin 4A_3 -0.08 \cos 4A_3
                                                     -0.08 \sin 4A_3 + 0.15 \cos 4A_3
        -3.20 \sin 5A_3 -1.17 \cos 5A_3
                                                     -1.17 \sin 5A_3 + 3.22 \cos 5A_3
        -0.83 \sin 6A_3 -0.32 \cos 6A_3
                                                     -0.32 \sin 6A_3 + 0.86 \cos 6A_3
        +0.57 \sin 7A_3 + 0.22 \cos 7A_3
                                                     +0.22 \sin 7A_3 - 0.57 \cos 7A_3
        +0.14 \sin 8A_3 + 0.06 \cos 8A_3
                                                     +0.06 \sin 8A_3 - 0.14 \cos 8A_3
                                                     +0.02 \sin 9A_3 -0.06 \cos 9A_3
        +0.06 \sin 9A_3 + 0.02 \cos 9A_3
                                                     -0.01 \sin 10A_3 -0.03 \cos 10A_3
        +0.03 \sin 10 A_3 -0.01 \cos 10 A_3
                   +0.11722e^{s}g
                                                               +0.11713\delta e
(v.c.3) = -0.02 \sin \theta
                     A_3
                                            (v.s.3) =
                                                                     +0.02\cos
                                                     +0.01 \sin 3A_4 -0.04 \cos 3A_3
        +0.04 \sin 3A_3 + 0.01 \cos 3A_3
                                                     -0.05 \sin 4A_3 + 0.15 \cos 4A_3
         -0.15 \sin 4A_3 -0.05 \cos 4A_3
        -0.08 \sin 5A_3 -0.02 \cos 5A_3
                                                     -0.02 \sin 5A_3 + 0.08 \cos 5A_3
         -0.02 \sin 6A_3 -0.02 \cos 6A_3
                                                     -0.02 \sin 6A_3 + 0.02 \cos 6A_3
        +0.46 \sin 7A_3 + 0.25 \cos 7A_3
                                                    +0.25 \sin 7A_3 -0.46 \cos 7A_3
                                                    +0.07 \sin 8A_3 -0.11 \cos 8A_3
        +0.11 \sin 8A_3 + 0.07 \cos 8A_3
```

 $-0.08 \sin 9A_3 -0.05 \cos 9A_3$  $-0.03 \sin 10A_3 -0.02 \cos 10A_3$ 

 $+0.00714e^{s}g$ 

 $-0.05 \sin 9A_3 + 0.08 \cos 9A_3$ 

 $-0.02 \sin 10A_3 + 0.03 \cos 10A_3 + 0.00714 \delta e$ 

$$A_3 = g - l$$

$$(v.c.4) = -0.06 \sin 9A_3 - 0.05 \cos 9A_3$$

$$-0.09 \sin 10A_3 - 0.08 \cos 10A_3$$

$$+0.00044e^{\xi}g$$

$$(\rho.c.0) = +227 \cos A_3$$

$$+232 \cos 2A_3$$

$$+3 \sin 3A_3 -229 \cos 3A_3$$

$$-59 \cos 4A_3$$

$$-17 \cos 5A_3$$

$$-7 \cos 6A_3$$

$$+2 \sin 2A_3 - 9 \cos 2A_3$$

$$+23 \sin 3A_3 -141 \cos 3A_3$$

$$-18 \sin 4A_3 - 39 \cos 4A_3$$

$$-19 \sin 5A_3 + 43 \cos 5A_3$$

$$-1 \sin 7A_3 + 5 \cos 7A_3$$

$$-0.43322^*e$$

$$(\rho.c.2) = -1 \cos A_3$$

$$-1 \sin 3A_3 + 1 \cos 5A_3$$

$$-1 \sin 5A_3 + 1 \cos 5A_3$$

$$-1 \sin 7A_3 + 5 \cos 7A_3$$

$$-1 \sin 7A_3 + 5 \cos 7A_3$$

$$-1 \sin 7A_3 + 1 \cos 5A_3$$

$$-1 \sin 7A_3 + 1 \cos 7A_3$$

$$-1 \cos 7A_3$$

$$-1 \sin 7A_3 + 1 \cos 7A_3$$

$$-1 \cos 7A_3$$

$$-1 \sin 7A_3 + 1 \cos 7A_3$$

$$-1 \sin 7A_3 + 3 \cos 7A_3$$

$$-1 \sin 7A_3 + 3 \cos 7A_3$$

$$-1 \sin 7A_3 - 3 \cos 7A_3$$

$$-1 \sin 7A_$$

## PERTURBATIONS OF THE LATITUDE.

(The secular terms being omitted.)

Action of Jupiter.

#### Action of Saturn.

$$(b.c.0) = -0.08 \sin A_2 -0.03 \cos A_2$$

$$-0.03 \cos 2A_2$$

$$-0.01 \cos 3A_2$$

$$(b.s.1) = +1.34 \sin A_2 +2.88 \cos A_2 (b.c.1) = -1.56 \sin A_2 +2.50 \cos A_2$$

$$-0.01 \sin 2A_2 -0.10 \cos 2A_2 +0.02 \sin 2A_2 -0.10 \cos 2A_2$$

$$+0.03 \sin 3A_2 -0.06 \cos 3A_2 -0.04 \sin 3A_2 -0.06 \cos 3A_2$$

$$+0.02 \sin 4A_2 -0.03 \cos 4A_2 -0.02 \sin 4A_2 -0.02 \cos 4A_2$$

$$(b.s.2) = -0.09 \sin A_2 +0.10 \cos A_2 (b.c.2) = -0.09 \sin A_2 -0.05 \cos A_2$$

$$-0.05 \sin 2A_2 -0.09 \cos 2A_2 +0.07 \sin 2A_2 +0.02 \cos 2A_2$$

$$-0.01 \cos 3A_2 +0.01 \sin 3A_2$$

## Action of Neptune.

$$(b.c.0) = +0.01 \sin A_3 -0.04 \cos A_3$$

$$-0.01 \sin 2A_3 +0.00 \cos 2A_3$$

$$-0.01 \sin 3A_3 +0.04 \cos 3A_3$$

$$+0.01 \sin 4A_3 +0.01 \cos 4A_3$$

$$+0.01 \sin 5A_3$$

$$+0.01 \sin 6A_3$$

## Action of Jupiter and Saturn.

(Terms multiplied by the product of their masses.)

$$\begin{array}{lll} N_1 = & 2S - J \\ N_2 = - & U + 3S - J \\ N_3 = -2U + 4S - J \\ N_4 = & 3U + 3S - 2J \\ N_5 = & 2U + 4S - 2J \\ N_6 = & 5S - 2J \\ N_7 = -3U + 6S - 2J \\ N_8 = -3U + 7S - 2J \end{array}$$

Action of Jupiter and Saturn —Continued. (Terms multiplied by the product of their masses.)

$$\begin{array}{c} (v.c.0) = + \begin{array}{c} 0.08 \sin N_2 \\ + 0.04 \sin N_3 \\ - 0.01 \sin N_4 \\ - 0.05 \cos N_4 \\ - 0.35 \sin N_5 \\ - 1.30 \cos N_5 \\ - 0.55 \sin N_6 \\ - 0.03 \cos N_6 \\ + 40.65 \sin N_7 \\ - 0.05 \sin N_8 \\ + 0.03 \cos N_8 \end{array} \right\} \\ - 0.05 \sin N_1 \\ - 0.05 \sin N_1 \\ - 0.05 \sin N_1 \\ - 0.05 \cos N_1 \\ - 0.05 \sin N_1 \\ - 0.05 \cos N_1 \\ - 0.05 \sin N_1 \\ - 0.05 \cos N_2 \\ - 0.05 \sin N_1 \\ - 0.05 \cos N_2 \\ - 0.05 \sin N_1 \\ - 0.05 \cos N_2 \\ - 0.05 \sin N_1 \\ - 0.05 \cos N_2 \\ - 0.05 \sin N_2 \\ - 0.05 \cos N_1 \\ - 0.05 \cos N_2 \\ - 0.05 \cos N_2 \\ - 0.05 \cos N_2 \\ - 0.05 \cos N_3 \\ - 0.05 \cos N_4 \\ - 0.05 \cos N_4 \\ - 0.05 \cos N_5 \\ - 0.05$$

Two of these arguments, namely, 5S-2J, and -3g+6S-2J, are of very long period, that of the first being about 880, and that of the second about 1590 years. It will, therefore, be convenient to tabulate them both as functions of the time for the time during which the theory is to be used. To make their effect as small as possible during the period for which the provisional ephemeris is to be computed, we shall suppose the longitude of epoch, mean motion, and longitude of the perigee to be affected with the negative of the following corrections:

$$\delta \varepsilon = +27.27,$$
  
 $\delta \pi = +27.27,$   
 $\delta n = -0.1172.$ 

Reducing these corrections to corrections of the co-ordinates, and adding them to the terms of long period in the true longitude and logarithm of radius vector, we shall have for these terms,

$$(v.c.0) = - \begin{array}{c} " \\ 0.546 \sin N_6 - 0.032 \cos N_6 \\ + 40.650 \sin N - 10.500 \cos N_7 + 27.27 - 11.72 T \end{array}$$

$$(v.s.1) = \begin{array}{c} " \\ 2.63 \sin N_6 + 4.64 \cos N_6 + 7.35 \sin N_7 + 4.42 \cos N_7 \\ (v.c.1) = -4.22 \sin N_6 - 3.87 \cos N_6 + 8.06 \sin N_7 - 8.39 \cos N_7 - 1.10 T \end{array}$$

The values of these and of the other secular terms and terms of long period for the period during which Uranus has been observed, are given in the following table:

			(v.c.0)						
		Neptune (long per.)	Jupiter (lo	Sum.					
17	00	# +85.54		//  -4.86	+90.40				
17	50	+38.45		+1.90	+40.35				
	60	31.25		1.48	32.73				
	70	24.80		1.11	25.91				
	80	19.09		0.80	19.89				
	90	14.12		0.54	14.66				
18 18		9.89 6.42	Old Parket	+0.33	10.22				
18		3.69		0.17	6.59				
18		1.71	80.0	+0.07 0.00 3.76 1.71					
18	40	+ 0.48	3 200 -	-0.02	+ 0.46				
18		0.00	1 100	0.00	0.00				
18		+ 0.27		-0.06	+ 0.33				
18 18		$\frac{1.29}{+3.06}$	ATTENDED TO THE REAL PROPERTY OF THE PERTY O	+0.16 +0.30	+3.36				
	989-	0.5	VALUES OF (v.	e 1)					
		1 - 1 - 1				aviet.			
	(1) Jupiter (sec.)	(2) Saturn (sec.)	(3) Neptune (sec.)	(4) Neptune (long per.)	Jupiter & Saturn (long per.)	Sum.			
1700	+1.82	+13.77	+0.75		-10.18				
1750	+1.22	+ 9.18	+0.50	-141.97	- 9.11	-140.18			
1760	1.10	8.26	0.45	-127.76	- 8.83	-126.78			
1770	0.97	7.34	0.40	-113.55	- 8.54	-113.38			
1780 1790	0.85 0.73	6.43 5.51	0.35	- 99.33	- 8.24	- 99.94			
1800	0.73	4.59	0.30 0.25	-85.11 $-70.90$	-7.93 $-7.61$	- 86.50 - 73.06			
1810	0.49	3.67	0.20	<u></u>		- 59.61			
	0.36	2.76	0.15	- 42.49	- 6.94	- 46.16			
1820									
1830	0.24	1.84	0.10	- 28.31	- 6.60	- 32.78			
						$ \begin{array}{r} -32.73 \\ -19.31 \\ -5.91 \end{array} $			

-0.05

-0.10

-0.15

14.12

28.23

+42.32

-5.57

-5.23

- 4.89

+ 7.46

+ 34.16

20.82

12 May, 1873.

1860

1870

1880

-0.12

-0.24

-0.36

-0.92

-1.84

\_ 2.76

		T	VALUES OF (v.c	1)		181 113 -
	1	1	1	1	1	
	(1) Jupiter (sec.)	(2) Saturn (sec.)	(3) Neptune (sec.)	(4) Neptune (long per.)	Jupiter & Saturn (long per.)	Sam.
1700	+17.19	+16.67	+7.20	+37.63	1.98	+76.71
1750		+11.11	+4.80	+28.67	-2.28	+53.76
1760	+11.46 $10.31$	10.00	4.32	26.46	-2.36	48.73
1770	9.17	8.89	3.84	24.10	-2.45	43.55
1780	8.02	7.78	$\frac{3.36}{2.88}$	21.60 18.95	-2.53 $-2.61$	38.23 32.77
1790 1800	6.88 5.73	6.67 5.56	2.40	16.16	-2.69 -2.69	27.16
1810 .	4.58	4.44	1.92	13.23	-2.76	21.41
1820	3.44	3.33	1.44	10.15	-2.83	15.53
1830 1840	+ 1.15	2.22 + 1.11	$0.96 \\ +0.48$	+ 3.53	$-2.90 \\ -2.97$	+3.30
1850	0.00	0.00	0.00	0.00	-3.03	_ 3.03
1860	- 1.15	- 1.11	0.48	- 3.68	-3.08	-9.50
1870 1880	-2.29 $-3.44$	- 2.22 - 3.33	-0.96 -1.44	-7.51 $-11.49$	—3.13 —3.16	-16.11 $-22.86$
1000	- 5.11			= -0".14.	-0.10	22.00
	1	(v.s.2)	1	177710	1 / 1	
	(1)	(2)	(3)	(4)	(5)	Sum.
1700	+0.11	+0.81	+0.04			
1750	+0.07	+0.54	+0.03	-8.31	_0.70	-8.51
1760	0.06	0.49	0.03		-0.69	<del>-7.73</del>
1770	0.06	0.43	0.02	-6.64	-0.68	-6.95
1780 1790	0.05 0.04	$0.38 \\ 0.32$	0.02 0.02	—5.81 —4.98	$\begin{array}{c c} -0.66 \\ -0.65 \end{array}$	-6.16 $-5.39$
1800	0.04	0.32	0.02	<u>-4.15</u>	_0.64	<u>-3.33</u> <u>-4.60</u>
1810	0.03	0.22	0.01	-3.32	-0.63	-3.83
1820	0.02	0.16	0.01	-2.49	$\begin{array}{c c} -0.61 \\ -0.60 \end{array}$	-3.05 $-2.27$
1830 1840	0.01 +0.01	$0.11 \\ +0.05$	+0.01 $0.00$	-1.66 $-0.83$		-2.21 -1.49
1850	0.00	0.00	0.00	0.00	-0.57	-0.71
1860	-0.01	-0.05	0.00	+0.82	-0.56	+0.06
1870 1880	-0.01 $-0.02$	-0.11 $-0.16$	-0.01 $-0.01$	$1.65 \\ +2.48$	-0.54 -0.53	$0.84 \\ +1.62$
1300	-0.02	l				74.02
		(v.c.2)		+ 0".13.		
	(1)	(2)	(3)	(4)	(5)	Sum.
1700	+1.00	+0.98	+0.42	+2.20	_0.11	+4.62
1750	+0.67	+0.65	+0.28	+1.68	0.12	+3.29
1760	+0.60	0.59	0.25	1.55	-0.12	$\frac{3.00}{2.70}$
1770 1780	$+0.54 \\ +0.47$	$\begin{array}{c} 0.52 \\ 0.46 \end{array}$	$\begin{array}{c} 0.22 \\ 0.20 \end{array}$	1.41 1.26	-0.12 $-0.13$	2.70
1790_	+0.40	0.39	0.17	1.11	-0.13	2.07
1800	+0.34	0.33	0.14	0.94	-0.13	1.75
1810 1820	$^{+0.27}_{+0.20}$	$\begin{array}{c} 0.26 \\ 0.20 \end{array}$	0.11 0.08	0.77 0.59	-0.14 -0.14	1.40 1.06
1830	+0.13	0.13	0.06	0.39	-0.14	0.70
1840	+0.07	+0.07	+0.03	+0.20	-0.15	+0.35
1850 1860	0.00 0.07	0.00 0.07	0.00 0.03	0.00 $-0.21$	-0.15 -0.15	-0.02 $-0.40$
1870	-0.13	0.07 0.13	<u>-0.05</u> <u>-0.06</u>	-0.21 -0.43	0.16	-0.78
1880	-0.20	-0.20	-0.08	0.68	0.16	-1.19
-						

1700	F				(v.s.3)			
1700			Jupiter	Saturn	Neptune	Neptune	Jupiter & Saturn	Sum.
1760	Γ	1700		THE RESERVE OF THE PARTY OF THE		The second second second second		The second secon
1770	ı				0	-0.51		
1780	ı		The second secon					
1800	1		The state of the s	0.02	The state of the s		0	
1810	ı				AND THE RESERVE OF THE PARTY OF			
1820	ı							
1840	ı	1820	0					
1850	ı		0					
1870	ı	1850	0	0.00		0.00	0	0.00
1880   0   -0.01   0   +0.15   0   +0.14	ı							
(1) (2) (3) (4) Sum.  1700 +0.06 +0.06 +0.02 +0.13 +0.27  1750 +0.04 +0.04 +0.04 +0.02 +0.10 +0.09  1760 0.04 0.04 0.04 +0.01 +0.09 +0.18  1770 0.03 0.03 0.03 0.01 +0.08 +0.15  1780 0.02 0.02 0.01 +0.06 +0.12  1800 0.02 0.02 0.01 +0.06 +0.11  1810 0.02 0.02 +0.01 +0.05 +0.11  1810 0.02 0.02 +0.01 +0.05 +0.04  1830 +0.01 +0.01 0.00 +0.02 +0.04  1840 0.00 0.00 0.00 0.00 +0.02  1850 0.00 0.00 0.00 0.00 +0.01 +0.02  1850 0.00 0.00 0.00 0.00 0.00 0.00  1860 0.00 0.00 0.00 -0.01 -0.01  1870 -0.01 -0.01 0.00 -0.02 -0.01  1870 -0.01 -0.01 0.00 -0.02 -0.04  FOR THE RADIUS VECTOR. VALUES OF (p.c.0)  FOR THE RADIUS VECTOR. VALUES OF (p.c.0)  FOR THE RADIUS VECTOR OR TYPE ARE ARE ARE ARE ARE ARE ARE ARE ARE AR	ı							
1700	L				(v.c.3)			
1700	-	1 40 4	(1)	(2)	(3)	(4)	21 /200	Sum.
1750	Г		CONTRACTOR OF THE PARTY OF THE					
1760	ı							
1770	ı							
1790	ı	1770	0.03	0.03	0.01	+0.08	A Second	+0.15
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	ı							
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	ı							+0.11
1830	ı						1	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	ı						1	
$ \begin{array}{ c c c c c c c c c }\hline 1860 & 0.00 & 0.00 & 0.00 & -0.01 & -0.02 & -0.04 \\\hline 1870 & -0.01 & -0.01 & 0.00 & -0.02 & -0.04 & -0.06 \\\hline \hline \hline & FOR THE RADIUS VECTOR. VALUES OF (\rho.c.0) & Sum. \\\hline \hline & (1) & (2) & (3) & (4) & (5) & Sum. \\\hline \hline & (1) & (2) & (3) & (4) & (5) & Sum. \\\hline \hline & (1) & (2) & (3) & (4) & (5) & Sum. \\\hline \hline & (1) & (2) & (3) & (4) & (5) & Sum. \\\hline \hline & (1) & (2) & (3) & (4) & (5) & Sum. \\\hline \hline & (1) & (2) & (3) & (4) & (5) & Sum. \\\hline & (1) & (2) & (3) & (4) & (5) & Sum. \\\hline \hline & (1) & (2) & (3) & (4) & (5) & Sum. \\\hline \hline & (1) & (2) & (3) & (4) & (5) & Sum. \\\hline & (1) & (1) & (5) & Sum. \\\hline & (1) & (1) & (5) & Sum. \\\hline & (1) & (1) & (1) & (5) & Sum. \\\hline & (1) & (1) & (1) & (1) & (1) & (1) & (1) & (1) \\\hline & (1) & (2) & (3) & (4) & (5) & Sum. \\\hline & (1) & (1) & (1) & (1) & (1) & (1) & (1) & (1) \\\hline & (1) & (1) & (1) & (1) & (1) & (1) & (1) & (1) \\\hline & (1) & (1) & (1) & (1) & (1) & (1) & (1) & (1) & (1) \\\hline & (1) & (1) & (1) & (1) & (1) & (1) & (1) & (1) & (1) \\\hline & (1) & (1) & (1) & (1) & (1) & (1) & (1) & (1) & (1) \\\hline & (1) & (1) & (1) & (1) & (1) & (1) & (1) & (1) & (1) & (1) \\\hline & (1) & (1) & (1) & (1) & (1) & (1) & (1) & (1) & (1) \\\hline & (1) & (1) & (1) & (1$	ı	1840	0.00	0.00	0.00		1	+0.02
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	ı							
FOR THE RADIUS VECTOR. VALUES OF $(\rho.c.0)$ (1) (2) (3) (4) (5) Sum.  1700 +0.4 +3.5 -0.2 +164 +13 +181  1750 +0.3 +2.3 -0.1 +110 7 +120  1760 0.3 2.1 0 99 6 107  1770 0.2 1.9 0 88 5 95  1780 0.2 1.6 0 777 4 83  1790 0.2 1.4 0 67 3 72  1800 0.2 1.2 0 56 2 60  1810 0.1 0.9 0 45 2 60  1810 0.1 0.9 0 45 2 60  1810 0.1 0.7 0 34 +1 36  1820 0.1 0.7 0 34 +1 36  1830 +0.1 0.5 0 22 0 23  1840 .0 +0.2 0 +11 0 +11  1850 .0 0.0 0.0 0 -1 -1  1860 .0 -0.2 0 -11 -2 -1  1860 .0 -0.2 0 -11 -2 -1  1870 -0.1 -0.5 0 22 -2 -25	ı	1870	-0.01	-0.01	0.00	-0.02		-0.04
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	L	1880	-0.01	-0.01	0.00	-0.04	110	-0.06
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1			FOR THE RADI	US VECTOR.	VALUES OF (p.	2.0)	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	L	No.						
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	-	1700						
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	-							
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	-							
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	-	1780	0.2	1.6	0	77	4	83
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	-							
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		1810	0.1	0.9	0	45	2	48
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	-		The state of the s					
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	-	1840	.0	+0.2	0	+ 11	0	+ 11
1870 -0.1 -0.5 0 22 -2 -25	-						-1	- 1 - 19
	1	1870	-0.1	-0.5	0	22	- 2	- 25
1000 -0.1 -0.1 0 - 55 - 5 - 51		1880	-0.1	-0.7	0	— 33	- 3	<b>—</b> 37

		(p.s.1	) const.	= +63.		
	(1) Jupiter (sec.)	(2) Saturn (sec.)	(3) Neptune (sec.)	(4) Neptune (long per.)	Jupiter & Saturn (long per.)	Sum.
1700	+180	+176	+75	+396		+869
1750	+120	+117	+50	+302	-25	+627
1760 1770	108 96	105	45	280 255	26 28	575 520
1780 1790	84 72	82 70	35 30	228 200	29 30	463 405
1800 1810	60 48	59 47	25 20	170 139	31 32	346 285
1820 1830	36 24	35 23	15 10	106 72	33 34	222 158
1840	+ 12	+ 12	+ 5	+ 37	34	95
1850 1860	-12		_ 5	_ 39	35 36	$+ \frac{28}{-41}$
1870 1880	24 36	23 — 35	10 —15	80 —122	36 -37	—110 —182
		(ρ.c.1)	const. =	= + 73.		
	(1)	(2)	(3)	(4)	(5)	Snm.
1700			9	+2241	+104	+2242
1750 1760	—13 —12	— 98 — 88	—6 —5	+1496 1346	+ 94 91	+1546 $1405$
1770 1780	—10 — 9	- 78 - 69	_5 _4	1197 1047	88 85	1265 1123
1790	- 8 - 6	59	—4 —4 —3	897	82	981
1800 1810	<del> 5</del>	- 49 - 39	-2	747 598	78 74	840 699
1820 1830	- 4 - 3	- 29 - 20	$-2 \\ -1$	448 299	71 68	557 416
1840 1850	$-\frac{1}{0}$	— 10 0	-1	$+ \frac{149}{0}$ .	64 61	$\frac{274}{+134}$
1860 1870	$+\frac{1}{3}$	$+\ \frac{10}{20}$	+1	149	58 54	_ 6
1880	4	29	$\frac{1}{2}$	298 — 447	+ 51	— 147 — 288
		(ρ. ε. 2	const.	= +5.		
	(1)	(2)	(3)	(4)	(5)	Sum.
1700	+12	÷12	+4	+28	0 "	+61
1750 1760	+ 8	+87	+6 5 5	+21 19	0 0	+48 43
1770 1780	6	6	5 4	17 15	0 0	39 36
1790	6 5 4 3 2 2	6 5 4 3 2 2	4	13	0	32
1800 1810	3	3	4 3 2 2	11 8	0	27 21
1820 1830		$\frac{2}{2}$	1	6	0	17 14
1840 1850	+ 1 0	+ 1 0	$+\frac{1}{0}$	$+\frac{2}{0}$	0	10 + 5
1860 1870	$-\frac{1}{2}$	$\begin{bmatrix} -1 \\ -2 \end{bmatrix}$	—1 —1 —2	$-\frac{2}{4}$	0	_ 0 _ 4
1880	<u>- 2</u>	$-\frac{2}{2}$	<u>-1</u>	— <sup>4</sup> ·	0	_ <del>-</del> <del>1</del> 7

1		1		L	1		
	(1) Jupiter (sec.)	(2) Saturn (sec.)	Saturn Neptune Neptune Jupiter & Sa				
	"	"	"	11	"	"	
1700	-1	-10	0	+157	0	+150	
1750	-1	-7	0	+105	0	+101	
1760	-1	- 6	0	95	0	92	
1770	<b>—</b> l	- 6	0	84	0	81	
1780	-1	_ 5	0	74	0	72	
1790	-1	- 4	0	63	0	62	
1800	0	- 3	0	52	0	53	
1810	0	- 3	0	42	0	43	
1820	0	- 2	0	31	0	33	
1830	. 0	-1	0	21	0	24	
1840	0	- 1	0	+ 10	0	13	
1850	0	0	0	0	0	+ 4	
1860 1870	0	+1	0	- 10 21	0	- 5 -16	

## Reduced Expressions for the Latitude of Uranus.

If we represent by  $V_1$ ,  $V_2$ ,  $V_3$  the distances of Uranus from its descending nodes on the respective orbits of Jupiter, Saturn, and Uranus, we find the following perturbations of the latitude, which are independent of the mean longitude of the disturbing planets.

$$\delta\beta = -0.0114t \cos V_1$$

$$-0.0477t \cos V_2$$

$$-0.0125t \cos V_3$$

$$+0.245 \qquad "$$

$$+0.386 \sin g + 0.266 \cos g$$

$$-0.043 \sin 2g + 0.006 \cos 2g.$$

To find how far the last five terms may be represented by simple corrections to the elliptic elements, we first represent the effect of minute corrections to the inclination and node of Uranus as a function of its mean anomaly. Putting u for the argument of latitude of Uranus, we have to a sufficient degree of approximation

$$\delta\beta = \sin u\delta\phi - \sin\phi\cos u\delta\theta$$

$$u = g + \omega + 2e\sin g$$

$$\sin u = -e\sin\omega$$

$$+ \cos\omega\sin g + \sin\omega\cos g$$

$$+ e\cos\omega\sin 2g + e\sin\omega\cos 2g$$

$$\cos u = -e \cos \omega$$

$$+ \cos \omega \cos g - \sin \omega \sin g$$

$$+ e \cos \omega \cos 2g - e \sin \omega \sin 2g.$$

Substituting these values of  $\sin u$  and  $\cos u$  in the expression for  $\delta\beta$ , and putting  $\sin \phi \delta\theta = \delta'\theta$ , we have

$$\delta\beta = e \cos \omega \delta'\theta - e \sin \omega \delta \phi$$
+  $(\cos \omega \delta \phi + \sin \omega \delta'\theta) \sin g + (\sin \omega \delta \phi - \cos \omega \delta'\theta) \cos g$ 
+  $(e \cos \omega \delta \phi + e \sin \omega \delta'\theta) \sin 2g + (e \sin \omega \delta \phi - e \cos \omega \delta'\theta) \cos 2g$ .

To represent the numerical coefficients of  $\sin g$  and  $\cos g$  in  $\delta \beta$  we must put

$$\cos \omega \delta \phi + \sin \omega \delta' \theta = 0''.386$$
  
 $\sin \omega \delta \phi - \cos \omega \delta' \theta = 0.266$ .

Since  $\omega = 95^{\circ} 3'$ , this gives

$$\delta \phi = 0.231;$$
 $\delta' \theta = 0.409;$ 
 $\delta \beta = -0.013$ 
 $+0.386 \sin g + 0.266 \cos g + 0.018 \sin 2g + 0.013 \cos 2g$ 

Subtracting this expression from the corresponding terms of  $\delta\beta$ , we have left

$$\delta\beta = +0$$
".258 — 0".061 sin 2g — 0".007 cos 2g.

The first term of this expression shows that the mean orbit of Uranus at the present time is a small circle of the sphere one-quarter of a second north of its parallel great circle.

If we put

v = longitude of Uranus in its orbit, referred to the equinox and ecliptic of 1850, we have

$$V_1 = v - 127^{\circ} 37'$$
  
 $V_2 = v - 126 45$   
 $V_3 = v - 155 32$ 

Substituting these values in the first three terms of  $\delta\beta$ , and multiplying the last term by the factor  $(1 + \mu)$  by which the adopted mass of Neptune,  $\frac{1}{17000}$ , must be multiplied to obtain the true mass, we find

$$\delta\beta = (4".69 + 1".14\mu) T\cos v - (5".24 + 0".52\mu) T\sin v.$$

To these terms must be added those which arise from the motion of the ecliptic.

In the absence of any exhaustive investigation of the obliquity and motion of the ecliptic, I adopt the elements of Hansen, employed in his "Tables du Soleil," because they are a mean between the results of others, and are very accordant with recent observations. The secular motion of the obliquity there employed is

Hansen mentions — 5".39 as the corresponding motion at the equinox of 1850, found by Olufsen, but I cannot reproduce this result from the secular diminution with any masses of Mercury, Venus, and Mars, which seem to me probable. The expressions in terms of the masses given by Le Verrier are (Annales de l'Observatoire Imperial de Paris, tome ii, p. 101),

Secular change 
$$=$$
  $-47.59 - 0.52\nu - 28.90\nu' - 0.83\nu'''$   
Mot. at equinox  $=$   $+5.89 + 0.62\nu + 7.57\nu' + 0.73\nu'''$ .

In this expression the masses of Mercury, Venus, and Mars are represented by  $\frac{1+\nu}{3,000,000}$ ,  $\frac{1+\nu'}{401,847}$ , and  $\frac{1+\nu''}{2,680,337}$ , respectively. The influence of admissible changes in the masses of the other plants is insensible.

From the researches of Le Verrier on the motions of the four inner planets I conclude that the following are about the most probable distribution of the corrections of the masses necessary to produce the motion of the obliquity given by Hansen, namely,

$$\nu = -\frac{2}{5}$$
 $\nu' = -.018$ 
 $\nu''' = -\frac{1}{10}$ 

These values give for the motion at the equinox of 1850

Introducing the secular variation of these motions we have, for the change in the latitude of any celestial body near the ecliptic, arising from motion of the ecliptic,

$$\delta\beta = (5''.43T + 0''.19T^2)\cos v + (46''.78T - 0''.06T^2)\sin v.$$

Combining this with the change arising from the motion of the orbit of Uranus, we find

$$\delta\beta = \{(10''.12 + 1''.14\mu) \ T + 0''.19 \ T^2\} \cos v + \{(41''.54 - 0''.52\mu) \ T - 0''.06 \ T^2\} \sin v.$$

We may represent these expressions in the usual way by secular variations of the inclination and node of Uranus. But, owing to the small inclination, and consequent rapid motion of the node, it will be necessary to include the coefficients of the second power of the time. On the other hand, no distinction between  $\tau$  and  $\theta$  is necessary. Putting  $\phi$  for the inclination of the orbit,  $\theta$  for the longitude of the node referred to the equinox of 1850, and

$$p = \sin \phi \sin \theta$$
,  
 $q = \sin \phi \cos \theta$ ;

we have

$$\sin \beta = -p \cos v + q \sin v$$
  
 $\cos \beta \delta \beta = -\delta p \cos v + \delta q \sin v$ .

From the expressions for p and q we obtain

$$\cos \phi D_t \phi = \sin \theta D_t p + \cos \theta D_t q;$$
  
 $\sin \phi D_t \theta = \cos \theta D_t p - \sin \theta D_t q.$ 

And, neglecting  $(D_t\phi)^2 \times \sin \phi$ , we have farther,

$$\cos \phi D^2_{\iota} \phi = \sin \phi \ (D_{\iota} \theta)^2 + \sin \theta D^2_{\iota} p + \cos \theta D^2_{\iota} q;$$
  
$$\sin \phi D^2_{\iota} \theta = -2 \cos \phi D_{\iota} \theta D_{\iota} \phi + \cos \theta D^2_{\iota} p - \sin \theta D^2_{\iota} q.$$

Since  $\phi$  is only 46' we may put  $\cos \phi$  and  $\cos \beta$  both equal to unity in these expressions, while we have, for 1850,

$$\begin{array}{ll} \sin\theta = & 0.9573 \\ \cos\theta = & 0.2890 \\ D_t p = -10^{\circ}.12 - 1^{\circ}.14\mu \\ D_t q = +41.54 - 0.52\mu \\ D_t^2 p = -0.38 \\ D_t^2 q = -0.12 \\ \log\sin\phi = & 8.129606. \end{array}$$

The above formulæ then give

$$D_{t}\phi = + 2^{"}.31 - 1^{"}.24\mu$$

$$D_{t}\theta = - 3167^{"}.5 + 12^{"}.6\mu$$

$$D^{2}_{t}\phi = + 0^{"}.26$$

$$D^{2}_{t}\theta = + 5^{"}.6$$

$$\phi = \phi_0 + (2''.31 - 1''.24\mu) T + 0''.13 T^2 
\theta = \theta_0 - (3167''.5 - 12''.6\mu) T + 2.8 T^2,$$

or, adding Struve's precession, we have when  $\theta$  is counted from the mean equinox of date,

$$\theta = \theta_0 + (1857''.7 + 12''.6\mu) T + 3''.9 T^2.$$

Using the values of  $\phi$  and  $\theta$  given by these expressions, the latitude, secular variation included, will be given by the expression

$$\sin \beta = \sin \phi \sin (v - 0).$$

If we take from a table, as the principal term of the latitude, the value of  $\sin \phi_0 \sin (v - \theta)$ , the secular term to be added will be

$$\{(2".31 - 1".24\mu) \ T + 0".13 \ T^2\} \sin(v - \theta).$$

If we represent, as before, by  $\omega$  the variable distance of the perihelion from the node, this term will be allowed for by adding to (b.s.1), (b.c.1), etc., the terms

$$\begin{array}{ll} (b.c.0) = -e \sin \omega \delta \phi, \\ (b.s.1) = \cos \omega \delta \phi, \\ (b.c.1) = \sin \omega \delta \phi, \\ (b.s.2) = e \cos \omega \delta \phi, \\ (b.c.2) = e \sin \omega \delta \phi; \end{array}$$

where

$$\delta \phi = (2''.31 - 1''.24u) T + 0''.13 T^2$$

Putting in the above expressions

$$\omega = 95^{\circ}3' + 3459''T,$$
  
 $\cos \omega = -.0880 - .0167T,$   
 $\sin \omega = +.9961 - .0015T,$ 

we find

$$\begin{array}{l} (b.c.0) = - (0".11 - 0".06\mu)T \\ (b.s.1) = - (0.20 - 0.11\mu)T - 0".05T^2 \\ (b.c.1) = (2.30 - 1.24\mu)T + 0.12T^2 \\ (b.s.2) = -0.01T \\ (b.c.2) = (0.11 - 0.06\mu)T, \end{array}$$

We have, finally, to consider the terms of long period in  $\delta_{\eta}$  and  $\delta_{k}$  which have been omitted from the periodic perturbations produced by Neptune, in computing the terms of  $\delta_{\beta}$  on page 61, and which are as follows:

$$\xi_{7} = 1''.43\cos(2l'-g) - 0''.39\sin(2l'-g) 
- 2.12\cos(4l'-2g) + 1.00\sin(4l'-2g) 
+ 0.20\cos(6l'-3g) - 0.04\sin(6l'-3g) 
+ constant = 0''.00$$

For the period during which Uranus has been observed, these values of  $\delta_n$  and  $\delta k$  may be replaced by the following:

$$\delta n = -0^{\circ}.80 T$$
$$\delta k = +0.27 T$$

which are to be multiplied by the factor  $1 + \mu$ . The corresponding perturbation of the latitude will be

$$\delta\beta = \sin v \cdot \eta - \cos v \cdot k.$$

Putting for v its approximate value

$$v = g + \omega + 2e\sin g$$

and developing to quantities of the first order with respect to the eccentricities, we have

$$\sin v = \sin (g + \omega) + e \sin (2g + \omega) - e \sin \omega$$
$$\cos v = \cos (g + \omega) + e \cos (2g + \omega) - e \cos \omega.$$

13 May, 1873.

Substituting for  $\omega$  its value, 12°45′, and for  $\delta\eta$  and  $\delta k$  their above values in the expression for  $\delta\beta$ , we find that the terms of  $\delta\beta$  in question will add the following terms to (b.c.0), (b.s.1), etc.

$$\begin{array}{l} (b.c.0) = -.010 \ \delta \eta + .046 \ \delta k = +0".02 \ T \ (1 + \mu) \\ (b.s.1) = +.975 \ \delta \eta + .221 \ \delta k = -0 \ .72 \ T \ (1 + \mu) \\ (b.c.1) = +.221 \ \delta \eta - .975 \ \delta k = -0 \ .44 \ T \ (1 + \mu) \\ (b.s.2) = +.046 \ \delta \eta + .011 \ \delta k = -0 \ .04 \ T \ (1 + \mu) \\ (b.c.2) = -(b.c.0) = -0 \ .02 \ T \ (1 + \mu) \end{array}$$

These values will be employed in the construction of the provisional ephemeris, but not in the tables.

Collecting all three classes of terms discussed in this section, we have the following constant and secular terms in (b.c.0), (b.s.1), etc.

$$\begin{array}{l} (b.c.0) = +0^{\circ\prime}.26 + (-0^{\circ\prime}.09 + 0.08\mu)T \\ (b.s.1) = (-0^{\circ\prime}.92 - 0^{\circ\prime}.61\mu)T - 0^{\circ\prime}.05T^2 \\ (b.c.1) = (+1.86 - 1.68\mu)T + 0.12T^2 \\ (b.s.2) = -0.06 - 0.05T \\ (b.c.2) = -0.01 + (0.09 - .08\mu)T \end{array}$$

Positions of Uranus resulting from the preceding theory.

The next step in order is the preparation of an ephemeris of the planet for comparison with observations. As this provisional theory is, for future use, superseded by the tables appended to the present work, it seems unnecessary to enter very fully into the details of the computation of the ephemeris. The perturbations of the longitude, logarithm of radius vector, and latitude, were first computed by the formulæ already given.

$$\begin{split} \delta v &= (v.c.0) + (v.c.1)\cos g + (v.c.2)\cos 2g + \text{etc.,} \\ &+ (v.s.1)\sin g + (v.s.2)\sin 2g + \text{etc.,} \\ M\delta \rho &= (\rho.c.0) + (\rho.c.1)\cos g + (\rho.c.2)\cos 2g + \text{etc.,} \\ &+ (\rho.s.1)\sin g + (\rho.s.2)\sin 2g + \text{etc.,} \\ \delta \beta &= (b.c.0) + (b.c.1)\cos g + (b.s.1)\sin g. \end{split}$$

Each coefficient (v.c.0), (v.c.1), etc., is composed at most of the following quantities:

- 1. The five classes of secular, long period, or constant terms, the separate values of which, with the sum of all, are given on pages 89 to 93.
- 2. Periodic terms due to the action of Jupiter, Saturn, and Neptune, given on pages 83 to 87.
- 3. Terms depending on the product of the masses of Jupiter and Saturn, given on page 88, omitting those depending on  $N_6$  and  $N_7$ , because they are given in column 5 of the terms of the first class.

The sum of the perturbations thus computed is given in the third column of the following ephemeris.

An approximate value of the perturbations produced by Neptune alone is independently computed for every fourth date, and the result is given in the fourth

column. The secular and long period terms are here taken from columns (3) and (4) of the tables on pages 89 to 93.

The elliptic co-ordinates were then derived from the following elements, which are a little different from those employed in the computation of the perturbations.

Elements III. of Uranus.  $\pi$ , 168° 15′ 12″.0  $\varepsilon$ , 28 25 29 .5  $\theta$ , 73 11 58 .0  $\phi$ , 0 46 20 .0 e, .0469436 e, (in sec.) 9682″.81 n, 15426.196  $\log a$ , 1.2828989

Red. to Ecliptic, —9″.37 sin 2 (v —  $\theta$ )

The longitudes thus found are corrected for lunar, but not for solar nutation, and the results are given in the fifth column.

The column "correction" arises in this way: after the comparison of the ephemeris with observations was nearly completed, it was found that some errors had crept into the former, the most important of which was the employment of a mean anomaly, g, corrected for secular variation of the perihelion in the computation of the perturbations from the preceding formulæ. As a large portion of the computations on the provisional ephemeris had been made by assistants furnished by the Smithsonian Institution and Nautical Almanac, I deemed it prudent to make a careful recomputation of the perturbations for every sixth date during the entire period of the modern observations. The longitudes actually printed in the fifth column are the results of the original incorrect computation, while the numbers in the next column show the several corrections to be applied to obtain the results of my final revised computation.

During the period of the modern observations the ephemeris is computed for intervals of 120 days, and the selected dates are all exact multiples of that interval before or after the fundamental epoch, 1850, Jan. 0, Greenwich mean noon. For convenience of reference the dates are numbered from an epoch earlier by 212 intervals, and the number is given in the second column.

Between 1796 and 1801 no observations worth using were made on Uranus, the ephemeris has, therefore, not been extended over this interval.

Heliocentric Ephemeris of Uranus from the preceding Provisional Theory.

[The longitudes are corrected for lunar but not for solar nutation.]

Date. Greenwich mean noon.	No.	Sum of perturbations.	Approximate perturbations produced by Neptune.	Longitude.	Correction.	Latitude.	Logarithm Radins vector.
		, ,,	"	0 / //	"	, ,,	
1690, Dec. 23		+4 28.5	+236.1	59 40 35.2		-10 7.8	1.2876828
Dec. 24		+4 28.5		59 41 16.5		-10 7.3	1.2876789
1712, April 2		+8 37.9		155 24 42.6		+45 58.7	1.2626650
April 3		+8 37.9		155 25 29.0		+4558.8	1.2626640
1715, Mar. 4		+658.3	+136.2	169 10 21.4		+46 2.1	1.2623890
Mar. 5		+6 58.2	tion to the second	169 11 7.7		+46 2.1	1.2623893
Mar. 10		+6 57.5		169 15 0.0		+46 1.7	1.262391
April 29		+651.1	+134.8	169 53 42.2		+4558.0	1.262406
April 30		+651.1	0.00	169 54 28.8		+4557.9	1.262410
1748, Oct. 21		-0 28.9	- 65.0	316 13 19.3		-41 27.6	1.300185
Oct. 22		_0 28.8	** 0	316 13 58.8		-41 27.9	1.300187
1750, Sept. 13	HIL	+0 6.3	51.3	323 44 14.9		-43 47.2	1.301371
Sept. 14	100	+0 6.3	_ 50.8	323 44 54.0		<b>—43 47.3</b>	1.301373
Oct. 14 Oct. 15		+0 6.6	- 50.8	324 4 22.1		-43 52.4	1.301416
		+0 6.6	_ 40.0	324 5 1.0	100	<b>—43</b> 52.5	1.301418
Dec. 3 Dec. 4		$^{+0}_{+0}$ 8.0	<b>— 49.8</b>	324 36 49.5 324 37 28.5		-44 0.6	1.3014850
1753, Dec. 3		$\begin{array}{ccc} +0 & 8.0 \\ -0 & 5.6 \end{array}$	_ 25.6	336 25 0.6		-44 0.8	1.3014879 1.3025789
Dec. 4		-0 5.6	_ 20.0	336 25 39.3		-46  1.1 $-46  1.2$	1.302579
1756, Sept. 25		-0 49.5	- 0.4	347 25 34.9		-46 1.2 $-46$ 9.2	
Sept. 26		-0 49.5	- 0.4	347 26 13.6		-46   9.2 $-46   9.1$	1.3029363 1.3029363
764, Jan. 15		-0 45.5 $+1$ 24.0		16 13 35.0		-46 9.1 $-38$ 36.9	1.3029368
Jan. 16		+1 24.0		16 14 14.2		-38 36.7	1.3003486
768, Dec. 27		+1 33.1		36 3 35.2		-2742.4	1.295533
Dec. 29		+1 33.1	+106.9	36 4 44.1		-2741.5	1.2955274
Dec. 31		+1 33.1	100.0	36 6 5.0		-2740.7	1.2955216
769, Jan. 15		+1 33.5		36 16 4.6		-2734.2	1.2954758
Jan. 18	-	+1 33.5		36 18 4.5		<b>—27</b> 33.0	1.2954659
Jan. 21		+1 33.5	+106.9	36 20 4.5		-27 31.6	1.2954566
Jan. 24		+1 33.5	,	36 22 4.4		-27 30.3	1.2954476
781, Jan. 1	1	+357.46	+178.9	86 36 13.23	+0.16	+11 3.63	1.2785979
May 1	2	+3 53.41	1 - 1 - 1	88 2 34.70	7 0.20	+12 11.14	1.2780883
Aug. 29	3	+3 48.58		89 29 7.41		+13 18.33	1.2775834
Dec. 27	4	+3 43.09		90 55 51.40		+14 25.14	1.2770827
782, April 26	5	+3 37.18	+180.4	92 22 46.89		+15 31.53	1.2765870
Aug. 24	6	+3 30.97		93 49 53.89		+16 37.47	1.2760968
Dec. 22	7	+3 24.52		95 17 12.51		+17 42.88	1.2756124
783, April 21	8	+3 18.03		96 44 42.73		+18 47.73	1.2751345
Aug. 19	9	+3 11.87	+180.1	98 12 24.96		+1951.92	1.2746633
Dec. 17	10	+3 6.01		99 40 19.00		+2055.67	1.2742012
784, April 15	11	+3 0.78		101 8 25.13		+21 58.69	1.2737412
Aug. 13	12	+2 56.24		102 36 43.29		+23 0.92	1.2732907
Dec. 11	13	+252.82	+178.6	104 5 13.79	+0.23	+24 2.46	1.2728469
785, April 10	14	+250.58		105 33 56.61		+25 3.14	1.2724105
Aug. 8	15	+249.29		107 2 51.36		+26 3.05	1.2719806
Dec. 6	16	+2 49.35		108 31 58.18		+27  1.98	1.2715564
786, April 5	17	+250.53	+175.5	110 1 16.88		+2759.97	1.2711405
Aug. 3	18	+253.29		111 30 47.68		+28 57.02	1.2707299
Dec. 1	19	+257.31		113 0 30.11	+0.31	+29 53.03	1.2703265
787, Mar. 31 July 29	20	+3 2.38		114 30 23.81		+30 47.92	1.2699294
	21	+3 8.51	+171.0	116 0 28.62		+31 41.72	1.2695394
Nov. 26	22	+3 15.48		117 30 44.11		+32 34.33	1.2691551

1	Date.			Sum of	Approximate				Logarithm
Gre	enwich in noon.		No.	perturba- tions.	perturbations produced by Neptune.	Longitude.	Correction.	Latitude.	Radius vector.
				, ,,	"	0 1 11		, ,,	
1788,		25	23	+3 23.02		119 1 9.79		+33 25.72	1.2687775
		23 20	24	3 31.36	1 105 1	120 31 45.79	1000	34 15.81	1.2684065 $1.2680423$
1789	Mar.		25 26	3 39.82 3 38.67	+165.1	122 2 31.13 123 33 25.96	+0.28	35 4.58 35 51.99	1.2676852
1,00,		18	27	3 57.40		125 4 29.49		36 38.01	1.2673358
	Nov.		28	4 5.97		126 35 41.50		37 22.50	1.2669932
1790,		15	29	4 14.35	+157.8	128 7 1.70		38 5.50	1.2666599
	July		30	4 22.48		129 38 29.88	100	38 47.00	1.2663336
1701	Nov.		31	4 30.00		131 10 5.37	+0.25	39 26.85	1.2660167
1791,	July	10 8	32 33	4 36.95	11401	132 41 47.99 134 13 37.15		40 5.04 40 41.58	1.2657087
	Nov.	5	34	4 42.95 4 48.11	+149.1	135 45 32.62		41 16.44	1.2651215
1792,		4	35	4 52.33		137 17 34.16	No. 32 Train	41 49.53	1.2648434
	July	2	36	4 56.03	BA S	138 49 41.78	1000	42 20.89	1.2645770
-	The second second	30	37	4 58.32	+139.3	140 21 54.47	+0.46	42 50.35	1.2643210
1793,		27	38	4 59.50	33-16 VE 3	141 54 12.11		43 18.00	1.2640766
		27 25	39	4 59.85		143 26 34.79	15 4 5	43 43.81 44 7.75	1.2638448
1794.		22	40	4 58.84 4 56.80	+128.6	144 59 1.64 146 31 32.77		44 7.75	1.2634226
LIUT,		22	42	4 53.48	+125.0	148 4 7.47		44 49.85	1.263232
	Oct.	20	43	4 49.13	+122.9	149 36 45.84	+0.47	45 7.99	1.2630577
1795,	Feb.	17	44	4 44.20		151 9 27.73		45 24.24	
	1	17	45	4 38.00	COLUMN !	152 42 12.55	No. of the	45 38.44	de la constant
	Oct.	15	46	4 31.04		154 15 - 0.15		45 50.64	
1801,	Jan.		62	+3 22.92		179 3 50.23		+44 34.51	1.2627599
	Mar.	200.19	63	3 26.59	+ 57.3	180 36 54.94	Parket!	44 12.86	1.2628920
1000	Sept.		64	3 31.06		182 9 57.40		43 49.24	1.2630365
1802,		12	65	3 36.26 3 41.88		183 42 57.23 185 15 54.08		43 23.66 42 56.34	1.2631929
	Sept.	9	67	3 47.78	+ 43.7	186 48 46.54	+0.35	42 26.97	1.263538
1803,		7	68	3 54.01	1 10.1	188 21 35.11	+0.00	41 55.86	1.2637281
	Mar.	7	69	4 0.29	No Park	189 54 18.55	130 4	41 22.99	1.2639280
	Sept.	4	70	4 6.43	ALCOHOL:	191 26 56.80	Marie V.	40 48.28	1.2641386
1804,		2	71	4 12.95	+ 30.7	192 59 30.15	100	40 11.79	1.2643591
	Mar. Aug.	1 29	72	4 18.74	130 150	194 31 56.83 196 4 17.13	10.14	39 33.63 38 53.72	1.2645891
	-	27	73 74	4 24.38 4 29.34		196 <b>4</b> 17.13 197 36 30.24	+0.14	38 12.21	1.265077
1805.	April		75	4 33.60	+ 18.0	199 8 35.97	Tarley R.	37 29.07	1.2653360
	Aug.	24	76	4 37.42		200 40 33.91	MI ST-	36 44.40	1.265603
Sec.	Dec.	22	77	4 40.11	1	202 12 23.39	11.07 A	35 58.15	1.2658808
1806,	April		78	4 41.83		203 44 4.25	1000	35 10.48	1.2661674
	Aug.		79	4 42.55	+ 5.9	205 15 36.11	+0.21	34 21.34	1.266463
1807	Dec. April		80 81	4 42.19	Charle III	206 46 58.67 208 18 11.39		33 30.88 32 39.05	1.2667689
2001,	Aug.		82	4 40.52 4 37.43		209 49 13.98	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	31 45.96	1.2674103
	Dec.		83	4 33.71	- 5.0	211 20 6.96	The state of	30 51.63	1.2677459
1808,	April		84	4 28.30	45-73-115	212 50 49.02	1 28.65	29 56.12	1.2680929
	Aug.	8	85	4 21.63		214 21 20.46	+0.25	28 59.51	1.268449
1000	Dec.	6	86	4 14.32	31 15 15	215 51 41.72	199301	28 1.80	1.2688160
1809,	April	5	87	4 5.84	- 15.4	217 21 51.97	10 PT 1	27 3.03	1.269194
	Aug. Dec.	3 1	88	3 56.63	100	218 51 51.53 220 21 40.62	Part of	26 3.28 25 2.66	1.269582
1810,		31	89 90	3 47.07 3 37.16		220 21 40.62 221 51 19.10	100	24 1.10	1.270390
-010,	July		91	3 27.15	_ 24.3	223 20 47.07	+0.23	22 58.68	1.2708094
	Nov.		92	+3 17.52		224 50 4.83		+21 55.38	1.271237

	Date.	1.	Sum of	Approximate				Logarithm
	enwich	No.	perturba-	perturbations produced by	Longitude.	Correction.	Latitude.	Radius
mea	au noon.		tions.	Neptune.				vector.
			, ,,	"	0 / //	"	, ,,	
1811,	Mar. 26	93	+3 7.99		226 19 12.04		$+20\ 51.52$	1.2716759
	July 24		2 59.12	00.1	227 48 9.06		19 46.95	1.272121
1010	Nov. 21 Mar. 20	95	2 50.91 2 43.45	-32.1	229 16 55.87		18 41.69	1.2725760
1012,	July 18	96	2 37.26		230 45 32.41 232 13 59.13	+0.11	17 35.80 16 29.34	1.273038 $1.273507$
	Nov. 15		2 31.98		233 42 15.55	70.11	15 22.35	1.273983
1813,	Mar. 15	99	2 27.86	-39.1	235 10 21.88		14 14.92	1.274465
	July 13		2 25.05		236 38 18.26		13 7.03	1.274950
1014	Nov. 10 Mar. 10		$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		238 6 3.95		11 58.79	1.275440
1014,	July 8	102	2 22.54	_44.6	239 33 39.61 241 1 4.63	+0.22	10 50.21 9 41.32	1.275936 1.276436
	Nov. 5	104	2 24.24	_11.0	242 28 19.59	70.22	8 32.19	1.276937
1815,	Mar. 5	105	2 26.58		243 55 23.67	•	7 22.86	1.277440
	July 3	106	2 30.00		245 22 17.17		6 13.39	1.277945
1016	Oct. 31 Feb. 28	107	2 34.17	-49.3	246 48 59.79		5 3.80	1.278453
1010,	June 27	108 109	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	100 200	248 15 31.47 249 41 52.08	-0.01	3 54.09 2 44.46	$\begin{array}{c} 1.278900 \\ 1.279468 \end{array}$
	Oct. 25	110	2 50.43		251 8 1.42	-0.01	1 34.82	1.279972
1817,	Feb. 22	111	2 56.75	-54.4	252 33 59.49		+ 0 25.25	1.280476
	June 22	112	3 3.22		253 59 46.00		0 44.19	1.280979
010	Oct. 20		3 10.03	3	255 25 21.18		1 53.44	1.281478
1818,	Feb. 17 June 17	114	3 16.63 3 22.96	-54.7	256 50 44.48 258 15 55.79	0.00	3 2.48 4 11.23	1.281975 $1.282470$
	Oct. 15	116	3 28.90	-04.1	259 40 55.14	0.00	5 19.73	1.282959
1819,	Feb. 12	117	3 34.28		261 5 42.25		6 27.83	1.283446
	June 12		3 38.77	LI STELLY	262 30 17.04	13.00	7 35.52	1.283931
1000	Oct. 10	-	3 42.48	56.1	263 54 39.42		8 42.77	1.284414
1820,	Feb. 7 June 6	120 121	3 45.03 3 46.37		265 18 49.19 266 42 46.29	-0.01	9 49.52	1.284892 $1.285367$
	Oct. 4	121	3 46.38		268 6 30.67	0.01	10 55.76 12 1.40	1.285839
1821,	Feb. 1	123	3 45.07	-56.4	269 30 2.43		13 6.44	1.286308
	June 1	124	3 42.35		270 53 21.55		14 10.88	1.286775
	Sept. 29	125	3 38.08		272 16 27.96		15 14.57	1.287240
1822,		126	3 32.86	500	273 39 22.29	0.10	16 17.58	1.287703
	May 27 Sept. 24		3 26.18 3 18.32	56.2	275 2 4.25 276 24 34.06	-0.10	17 19.84 18 21.32	1.288163 $1.288621$
1823.	Jan. 22		3 9.68		277 46 52.38		19 22.01	1.289077
1200	May 22		3 0.24		279 8 59.05		20 21.89	
	Sept. 19	131	2 50.36	-56.1	280 30 54.82	•	21 20.91	1.289982
1824,	Jan. 17		2 40.10		281 52 39.71	0.05	22 19.10	1.290431
	May 16 Sept. 13		2 29.74 2 19.49		283 14 14.16 284 35 38.60	-0.07	23 16.40 24 12.78	1.290877 $1.291320$
825.	Jan. 11		2 9.25	-55.5	285 56 52.92		25 8.22	1.291760
,	May 11		1 59.46	00.0	287 17 57.80		26 2.71	1.292196
	Sept. 3		1 50.21		288 38 53.43		26 56.22	1.292629
826,	Jan. 6		1 41.44		289 59 40.04	0.00	27 48.71	1.293057
	May 6 Sept. 3		1 33.58	-54.5	291 20 18.03	0.09	28 40.26	1.293480
827	Jan. 1		1 26.44 1 20.21		292 40 47.50 294 1 8.83		29 30.76 30 20.16	$\begin{array}{ c c c c c }\hline 1.293898 \\ 1.294311 \\ \hline \end{array}$
,,	May 1		1 14.89	E Tricil	295 21 22.15		31 8.60	1.294718
	Aug. 29	143	1 10.52	-54.0	296 41 27.72		31 55.92	1.295119
1000	Dec. 27		1 7.22	1 = 1 = 1	298 1 25.72		32 42.14	1.295513
828,	April 25		1 4.79	3500	299 21 16.45	-0.07	33 27.24	1.295900
	Aug. 23 Dec. 21		$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	-52.9	300 41 0.14 302 0 36.75	THE PARTY OF	34 11.25 —34 54.11	1.296279 $1.296649$

		HELIOCENTI	кіс Ернемев	is of Uranus.—	-Continued	l.	
Date. Greenwich mean noon.	No.	Sum of perturba- tions.	Approximate perturbations produced by Neptune.	Longitude.	Correction.	Latitude.	Logarithm Radius vector.
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1829, April 20	148	+1 3.68		303 20 6.73	100 100	-35 35.77	1.2970111
Aug. 18 Dec. 16	149 150	1 5.15 1 7.37		304 39 30.08 305 58 46.96	S-14 7	36 16.26 36 55.60	1.2973630 $1.2977052$
1830, April 15	151	1 10.14	-52.3	307 17 57.34	+0.08	37 33.68	1.2980368
Aug. 13	152	1 13.74		308 37 1.72		38 10.56	1.2983571
Dec. 11	153	1 17.63	N. 12 12	309 55 59.75		38 46.13	1.2986661
1831, April 10	154	1 21.69	50.0	311 14 51.68	05.16	39 20.49	1.2989638
Aug. 8 Dec. 6	155 156	1 26.06 1 30.26	-52.2	312 33 37.76 313 52 17.74		39 53.54 40 25.29	1.2992501 1.2995247
1832, April 4	157	1 34.13		315 10 51.63	+0.05	40 55.74	1.2997873
Aug. 2	158	1 37.50		316 29 19.67		41 24.90	1.3000379
Nov. 30	159	1 40.39	-52.2	317 47 41.94	35 E	41 52.65	1.3002768
1833, Mar. 30 July 28	160 161	1 42.02 1 42.86	- 33 10 1	319 5 57.95 320 24 8.31	11 4 7	42 19.10	1.3005047 1.3007216
Nov. 25	162	1 42.86		321 42 12.89	19474	42 44.17 43 7.88	1.3009280
1834, Mar. 25	163	1 40.92	-52.5	323 0 11.92	+0.15	43 30.24	1.3011231
July 23	164	1 38.01		324 18 5.47		43 51.18	1.3013090
Nov. 20	165	1 34.01	35 0 14 T	325 35 53.99		44 10.74	1.3014851
1835, Mar. 20 July 18	166	1 28.76	50.0	326 53 37.59 328 11 16.27	. 3.48 5.	44 28.92	1.3016515 1.3018084
July 18 Nov. 15	167 168	1 22.19 1 14.89	-52.9	329 28 50.92	1	44 45.69 45 1.14	1.3018084
1836, Mar. 14	169	1 6.50	13/1/4 25	330 46 21.41	+0.19	45 15.12	1.3020960
July 12	170	0 57.31		332 3 48.20		45 27.71	1.3022265
Nov. 9	171	0 47.51	-53.9	333 21 11.76		45 38.98	1.3023482
1837, Mar. 9	172	0 37.27		334 38 32.35	10.7	45 48.84	1.3024612
July 7 Nov. 4	173	0 26.69 0 15.92		315 55 50.40 337 13 6.16	A REAL PROPERTY.	45 57.28 46 4.45	1.3025656 $1.3026622$
1838, Mar. 4	175	+0 5.23	-55.1	338 30 20.17	+0.17	46 10.04	1.3027503
July 2	176	_0 5.21		339 47 32.76		46 14.36	1.3028297
Oct. 30	177	0 15.76		341 4 43.81	Date L.	46 17.29	1.3029008
1839, Feb. 27	178	0 25.58		342 21 54.35		46 18.83	1.3029634
June 27 Oct. 25	179 180	0 34.82 0 43.68	-56.9	243 39 4.45 344 56 14.08		46 19.00 46 17.84	$\begin{array}{c} 1.3030176 \\ 1.3030630 \end{array}$
1840, Feb. 22	181	0 51.42		346 13 24.23	+0.17	46 15.28	1.3030996
June 21	182	0 58.36		347 30 34.70		46 11.29	1.3031269
Oct. 19	183	1 4.34	-58.4	348 47 46.09		46 6.01	1.3031447
1841, Feb. 16	184	1 9.47	THE REAL PROPERTY.	350 4 58.23		45 59.35	1.3031528
June 16 Oct. 14	185 186	1 13.36	PARCH BAY	351 22 11.79 352 39 26.97		45 51.33 45 41.91	$\begin{array}{c} 1.3031509 \\ 1.3031392 \end{array}$
1842, Feb. 11	187	1 17.73	-60.5	353 56 43.91	+0.15	45 31.07	1.3031352
June 11	188	1 18.13	-	355 14 2.89		45 18.90	1.3030817
Oct. 9	189	1 17.35	0841 35	256 31 24.13	5035	45 5.38	1.3030351
1843, Feb. 6	190	1 15.50	00.4	357 48 47.74	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	44 50.50	1.3029767
June 6 Oct. 4	191 192	1 12.83 1 9.27	-66.7	359 6 13.65 0 23 42.19	La la Carle	44 34.22 44 16.64	$\begin{array}{c} 1.3029060 \\ 1.3028228 \end{array}$
1844, Feb. 1	193	1 4.76		1 41 13.59	+0.07	43 57.59	1.3027267
May 31	194	0 59.91		2 58 47.55		43 37.23	1.3026173
Sept. 28	195	0 54.61	-64.9	4 16 24.34	COLUMN T	43 15.53	1.3024947
1845, Jan. 26	196	0 49.19	5000	5 34 3.83	MART A	42 52.43	1,3023588
May 26 Sept. 23	197 198	0 43.90 0 38.92	3 4 4	6 51 46.06 8 9 31.09	State S	42 27.99 42 2.22	1.3022095 $1.3020472$
1846, Jan. 21	199	0 34.37	-67.7	9 27 19.04	+0.15	41 35.11	1.3018722
May 21	200	0 30.55	3.5	10 45 9.82		41 6.76	1.3016851
Sept. 18	201	_0 27.21	Star to	12 3 3.39	1000	-40 37.01	1.3014861
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1847,		202	-0 25.64		13 21 0.27		<b>—40</b> 6.03	1.3012758
	May 16 Sept. 13	203 204	0 24.73 0 24.95	<b>—</b> 70.2	14 39 0.21 15 57 3.61		39 33.75 39 0.23	1.3010544 $1.3008219$
1848.	Jan. 11	204	0 26.43	The sure of	17 15 10.46	+0.06	38 25.40	1.3005790
2010,	May 10	206	0 28.95		18 33 21.30	10.00	37 49.42	1.3003263
	Sept. 7	207	0 32.75	-72.8	19 51 36.15		37 12.18	1.3000640
1849,		208	0 37.59		21 9 55.34 22 28 19.02		36 33.73	1.2997923 $1.2995115$
	May 5 Sept. 2	$\frac{209}{210}$	$0 \ 43.47 \ 0 \ 50.27$		22 28 19.02 23 46 48.13		35 54.16 35 13.36	1.2993115 $1.2992224$
	Dec. 31	211	0 57.74	<b>—</b> 75.3	25 5 22.56	_0.08	34 31.47	1.2989252
1850,	April 30	212	1 6.18		26 24 2.38		33 48.40	1.2986203
	Aug. 28	213	1 15.11		27 42 48.39		33 4.37	1.2983078
1051	Dec. 26	214	1 24.38	55.0	29 1 40.87		32 19.06	1.2979881 $1.2976615$
1001,	April 25 Aug. 23	215 216	1 34.33 1 44.28	-77.9	30 20 39.78 31 39 45.91		31 32.79 30 45.46	1.2976615
	Dec. 21	217	1 54.21		32 58 59.55	-0.09	29 57.09	1.2969894
1852,	April 19	218	2 4.12		34 18 20.89		29 7.71	1.2966436
	Aug. 17	219	2 13.61	80.5	35 37 50.43		28 17.33	1.2962916
1059	Dec. 15 April 14	220 221	$\begin{array}{cccc} 2 & 23.00 \\ 2 & 31.54 \end{array}$		36 57 28.19		27 25.95 26 33.62	1.2959338 $1.2955701$
1000,	Aug. 12	222	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		38 17 15.06 39 37 10.77		25 40.35	1.2952015
	Dec. 10	223	2 46.62	-82.6	40 57 16.17	_0.07	24 46.17	1.2948270
1854,	April 9	224	2 52.64		42 17 31.26		23 51.08	1.2944458
	Aug. 7	225	2 57.77		43 37 56.24		$22\ 55.08$	1.2940583
1055	Dec. 5	226	3 1.60	04.0	44 58 31.59		21 58.25	1.2936645 $1.2932645$
1899,	April 4 Aug. 2	227 228	3 4.03 3 5.35	-84.6	46 19 17.49 47 40 13.93		$\begin{bmatrix} 21 & 0.51 \\ 20 & 1.97 \end{bmatrix}$	1.2932643 $1.2928582$
	Nov. 30	229	3 5.32		49 1 21.26	-0.11	19 2.66	1.2924449
1856,	Mar. 29	230	3 3.95		50 22 39.57		18 2.55	1.2920239
	July 27	231	3 1.24	-86.1	51 44 9.08		17 1.67	1.2915954
1057	Nov. 24	232	2 57.62		53 5 49.32		16 0.03	1.2911592 $1.2907155$
1001,	Mar. 24 July 22	233 234	2 52.95 2 47.58	4 A 7 A 7 A	54 27 40.66 55 49 42.98		14 57.72 13 54.71	1.2902643
	Nov. 19	235	2 41.65	-87.9	57 11 56.10	_0.10	12 51.08	1.2898057
1858,	Mar. 19	236	2 35.18	UEL	58 34 20.16	4	11 46.89	1.2893395
	July 17	237	2 28.82		59 56 54.59		10 41.96	1.2888659
1850	Nov. 14 Mar. 14	238	2 22.46	00.0	61 19 39.71		$ \begin{array}{c c} 9 & 36.91 \\ 8 & 30.87 \end{array} $	1.2883853 $1.2878981$
1000,	Mar. 14 July 12	239 240	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	-88.6	62 42 35.14 64 5 41.38		7 24.61	1.2874049
	Nov. 9	241	2 5.17		65 28 57.59	-0.13	6 17.90	1.2869061
1860,	Mar. 8	242	2 0.67	12 5 119	66 52 24.15		5 10.84	1.2864023
	July 6	243	1 57.10	-89.1	68 16 0.90		4 3.42	1.2858941
1881	Nov. 3 Mar. 3	244	1 54.37		69 39 47.78		$\begin{bmatrix} 2 & 55.74 \\ 1 & 47.83 \end{bmatrix}$	1.2853816 $1.2848658$
1001,	Mar. 3 July 1	245 246	$\begin{array}{c} 1 & 52.61 \\ 1 & 51.92 \end{array}$		71 3 44.98 72 27 52.38		-0.39.69	1.2843468
	Oct. 29	247	1 52.43	89.3	73 52 10.31	0.19	+ 028.60	1.2838257
1862,	Feb. 26	248	1 53.51		75 16 38.24		1 37.00	1.2833029
	June 26	249	1 55.99	N. = 11 E.	76 41 16.65		2 45.46	1.2827788
1862	Oct. 24 Feb. 21	250	1 59.54	90 5	78 6 5.46		3 53.95 5 2.40	1.2822542 $1.2817290$
1000,	June 21	251 252	$ \begin{array}{cccc} 2 & 3.98 \\ 2 & 9.43 \end{array} $	-88.5	79 31 4.97 80 56 15.07		$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1.2812047
	Oct. 19	253	2 15.63		82 21 36.01	0.04	7 19.09	1.2806819
1864,	Feb. 16	254	2 22.52		83 47 7.95		8 27.25	1.2801609
	June 15	255	2 30.20	-87.2	85 12 50.83		9 35.22	1.2796421
	Oct., 13	256	-2 38.39		86 38 44.88		+842.95	1.2791263

Date. Greenwich mean noon.	No.	Sum of perturba-	Approximate perturbations produced by Neptune.	Longitude.	Correction.	Latitude.	Logarithm Radius vector.
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1865, Feb. 10	257	-2 47.06	57 23	88 4 50.26		+11 52.20	1.278614
June 10	258	2 55.93		89 31 7.17		12 57.54	1.278106
Oct. 8	259	3 5.01	-85.2	90 57 35.61	-0.09	14 4.34	1.277602
1866, Feb. 5		3 13.91		92 24 16.00		15 10.74	1.277104
June 5		3 22.61	LEF D. FT.	93 51 8.39	1000	16 16.70	1.276611
Oct. 3		3 30.79		95 18 13.06	1000	17 22.18	1.276123
1867, Jan. 31	263	3 38.49	-82.5	96 45 29.91		18 27.15	1.275641
May 31	264	3 45.25	Committee of	98 12 59.44		19 31.54	1.275165
Sept. 28	265	3 50.96	100	99 40 41.71	-0.08	20 35.37	1.274694
1868, Jan. 26	266	3 55.67		101 8 36.54		21 38.51	1.274229
May 25	267	3 59.06	-79.1	102 36 44.31		22 40.96	1.273770
Sept. 22	268	4 1.02		104 5 5.00		23 42.75	1.27331
1869, Jan. 20	269	4 1.71		105 33 38.41		24 43.69	1.272869
May 20	270	4 0.81	br 1	107 2 24.67	0.11	25 43.81	1.272426
Sept. 17	271	0 00.00	-75.1	108 31 23.55	-0.11	26 43.07 27 41.44	1.27155
1870, Jan. 15 May 15	272 273	3 54.96 3 50.23	E CONTRACT	110 0 34.97 111 29 58.50	75.0	28 38.77	1.27112
Sept. 12	274	3 44.34		112 59 33.91	2 200	29 35.16	1.27070
Sept. 12 1871, Jan. 10	275	3 37.90	-69.8	114 29 20.79	Mary Mary	30 30.41	1.27029
May 10	276	3 30.56	-09.0	115 59 19.11	1000	31 24.57	1.269879
Sept. 7	277	3 22.61	The second second	117 29 28.39	_0.18	32 17.57	1.269473
1872. Jan. 5	278	3 14.50	ALLEY EYE	118 59 48.05	-0.10	33 9.31	1.269073
May 4	279	3 6.19	-64.2	120 30 17.95	11-	33 59.79	1.26868
Sept. 1	280	_2 57.65	-01.2	122 0 57.87	-	+34 48.97	1.268293

The next operation would be to interpolate these co-ordinates to intervals of time suitable for the computation of a geocentric ephemeris, to correct the longitudes for solar nutation, and then to compute the geocentric right ascension and declination. This operation has not, however, been completely carried out except for most of the observations before 1830, and for three of the oppositions observed since, the latter being computed only as a check upon the accuracy of the comparisons. As a general rule, it may be said that wherever a complete geocentric ephemeris, with the heliocentric ephemeris from which it was computed, were available, these ephemerides were made use of in a manner which will be more fully described hereafter, while, in all other cases, the geocentric places were computed directly.

It may also be stated here that Hansen's Tables du Soleil have been adopted as giving the places of the sun to be used in computing the geocentric places.

## CHAPTER VI.

REDUCTION OF THE OBSERVATIONS OF URANUS, AND THEIR COMPARISON WITH THE PRECEDING THEORY.

THE observations of Uranus naturally divide themselves into two distinct classes. (1) The purely accidental ones, made previous to the recognition of the planet by Herschel in 1781, and therefore without any suspicion on the part of the observers that the object was not a fixed star, and (2) the systematic observations made since.

The first class are nearly all so uncertain in comparison with the second that I have hesitated over the question of employing them at all. If nothing but a determination of the elements of Uranus were called for, they would certainly not be worth using, since these elements may be determined with entire certainty from the observations which have been made during the entire revolution of the planet since 1781. But the mass of Neptune is also to be determined, and it is at least possible that these observations, uncertain though they are, may add materially to the weight of this determination. I have, therefore, determined to include them all, re-reducing them when there seemed to be good reason so to do.

The earliest observations are those of Flamstead, published in the Historiæ Cœlestis. The observations themselves, as printed, together with the principal elements for reduction, are given in the following tables.

The first column of the table gives the name of the star. The second gives the clock time of transit over the wire of the quadrant as given by Flamstead. The time, it will be seen, is only given to entire seconds. We must, therefore, expect to find a probable error, of which the mathematical minimum is 0°.25, and of which the minimum we can reasonably expect is much greater.

Next we have the apparent right ascensions of the stars as computed. For these data I am indebted to Prof. Coffin, Superintendent of the American Ephemeris. The mean places are mostly derived from the "Star Tables of the American Ephemeris," and from the two Greenwich Seven Year Catalogues, while the reduction to apparent place is made with the modern constants.

The fourth column gives the apparent clock correction for sidereal time, in which is included the effect of deviation of the instrument from the meridian.

The clock keeping mean time, the errors are in the next column reduced to those of sidereal time at the moment of the transit of Uranus.

The next two columns give the corrections for clock rate, and for deviation of the instrument from the meridian, as inferred from the observations themselves, both being referred to the time and position of the transit of Uranus. In the last column we have the seconds of concluded correction for clock and instrument to be applied to the observed time of transit of Uranus.

Star. Time of Tr. R. A. of star. Clock. C'. R. Dev. C''.  a Arietis, 7 48 40 1 49 52.1 -5 58 47.9 58 29.3 -1.1 -1.2 31.6  π Arietis, 8 30 54 2 32 8.4 -5 58 45.6 58 33.9 -0.7 +1.7 32.9  σ Arietis, 8 40 21 2 41 38.0 -5 58 46.0 58 34.7 -0.7 +2.9 32.5  ε Arietis, 8 52 44 2 54 3.0 -5 58 41.0 58 33.0 -0.6 -0.2 33.8  δ Arietis, 8 52 44 2 54 3.0 -5 58 33.4 58 31.1 -0.1 -1.3 32.5  Uranus, 9 41 49  A Tauri, 9 27 47 3 29 13.6 -5 58 31.9 58 32.4 0.0 -0.8 33.2  a Virginis, 19 4 15 13 8 58.2 -5 55 16.8 56 49.3  a Bootis, 19 58 31½ 14 1 34.0 -5 56 57.5 58 39.0  Hourly rate of clock, Deviation of instrument for each degree of Z. D.,  Transit of Uranus, Correction for clock and instrument (mean), Observed R. A. of the planet,  Z. D. observed. Refraction.  a Arietis, 29° 29′ 10″ +0′ 33″ 21° 58′ 53″ 51° 28′ 36″  π Arietis, 35 18 55 +0 41 16 9 4 51 28 40  σ Arietis, 37 41 0 +0 44 13 46 58 51 28 42  ε Arietis, 31 23 15 +0 35 20 4 37 51 28 27  δ Arietis, 32 55 55 +0 37 18 31 40 51 28 12  η Tauri, 28 20 55 +0 37 18 31 40 51 28 19  Uranus, 31 52 35 +0 36  A Tauri, 30 15 55 +0 34 21 12 3 51 28 32				169	00.	Decen	ber !	23.	Rio	ht.	4 scen	nsion				
α Arietis, $^{h}$ , $^{h}$ , $^{m}$ , $^{s}$ , $^{h}$ , $^{h}$ , $^{m}$ , $^{h}$ ,	Star	Time	of Tr							-					Dom	CII
α Arietis, 7 48 40 1 49 52.1 $-5$ 58 47.9 58 29.3 $-1.1$ $-1.2$ 31.6 $\pi$ Arietis, 8 30 54 2 32 8.4 $-5$ 58 45.6 58 33.9 $-0.7$ $+1.7$ 32.9 $\sigma$ Arietis, 8 33 17 2 34 31.0 $-5$ 58 46.0 58 34.7 $-0.7$ $+2.9$ 32.5 $\varepsilon$ Arietis, 8 40 21 2 41 38.0 $-5$ 58 43.0 $-5$ 83.0 $-0.6$ $-0.2$ 33.8 $\delta$ Arietis, 8 52 44 2 54 3.0 $-5$ 58 41.0 58 33.0 $-0.5$ $+0.5$ 33.0 $\pi$ Tauri, 9 27 47 3 29 13.6 $-5$ 58 31.9 58 32.4 0.0 $-0.5$ 40.5 32.0 Uranus, 9 41 49  A Tauri, 9 45 3 3 46 31.1 $-5$ 58 31.9 58 32.4 0.0 $-0.8$ 33.2 a Virginis, 19 4 15 13 8 58.2 $-5$ 55 16.8 56 49.3 a Bootis, 19 58 31½ 14 1 34.0 $-5$ 56 57.5 58 39.0  Hourly rate of clock, Deviation of instrument for each degree of Z. D., Transit of Uranus, 9 41 49.0 $-0.5$ 65 57.5 58 39.0  Hourly rate of clock and instrument (mean), $-5$ 58 32.8 $-0.5$ 59 32.8 $-0.5$ 59 32.8 $-0.5$ 59 32.8 $-0.5$ 59 32.8 $-0.5$ 59 32.8 $-0.5$ 50 50 50 50 50 50 50 50 50 50 50 50 50		h. m	. 8.													
σ Arietis, 8 33 17 2 34 31.0 -5 58 46.0 58 34.7 -0.7 +2.9 32.5 ε Arietis, 8 40 21 2 41 38.0 -5 58 43.0 .58 33.0 -0.6 -0.2 33.8 δ Arietis, 8 52 44 2 54 3.0 -5 58 41.0 58 33.0 -0.5 +0.5 33.0 γ Tauri, 9 27 47 3 29 13.6 -5 58 33.4 58 31.1 -0.1 -1.3 32.5 Uranus, 9 41 49  A Tauri, 9 45 3 3 46 31.1 -5 58 31.9 58 32.4 0.0 -0.8 33.2 α Virginis, 19 4 15 13 8 58.2 -5 55 16.8 56 49.3 α Bootis, 19 58 31½ 14 1 34.0 -5 56 57.5 58 39.0  Hourly rate of clock,				1	49	52.1			47.9						-1.2	
ε Arietis, 8 40 21 2 41 38.0 —5 58 43.0 ,58 33.0 —0.6 —0.2 33.8 δ Arietis, 8 52 44 2 54 3.0 —5 58 41.0 58 33.0 —0.5 +0.5 33.0 η Tauri, 9 27 47 3 29 13.6 —5 58 33.4 58 31.1 —0.1 —1.3 32.5 Uranus, 9 41 49  A Tauri, 9 45 3 3 46 31.1 —5 58 31.9 58 32.4 0.0 —0.8 33.2 α Virginis, 19 4 15 13 8 58.2 —5 55 16.8 56 49.3 α Bootis, 19 58 31½ 14 1 34.0 —5 56 57.5 58 39.0  Hourly rate of clock, Deviation of instrument for each degree of Z. D., Transit of Uranus, 9 41 49.0 —0.5 h. m. s. 9 41 49.0 —0.5 h. m. s. 9 41 49.0 —5 58 32.8 Observed R. A. of the planet, 9 41 49.0 —5 58 32.8 34 3 16.2  1690, December 23. Declination.  Z. D. observed. Refraction. Declination. Eq. point. 3 43 16.2  1690, December 23. Declination. Eq. point. 5 58 32.8 40 σ Arietis, 35 18 55 +0 41 16 9 4 51 28 40 σ Arietis, 37 41 0 +0 44 13 46 58 51 28 42 ε Arietis, 31 23 15 +0 35 20 4 37 51 28 27 δ Arietis, 32 55 55 +0 37 18 31 40 51 28 12 η Tauri, 28 20 55 +0 37 18 31 40 51 28 19 Uranus, 31 52 35 +0 36											58	33.9	-0.	7 -	+1.7	32.9
8 Arietis, 8 52 44 2 54 3.0 —5 58 41.0 58 33.0 —0.5 +0.5 33.0 η Tauri, 9 27 47 3 29 13.6 —5 58 33.4 58 31.1 —0.1 —1.3 32.5 Uranus, 9 41 49  A Tauri, 9 45 3 3 46 31.1 —5 58 31.9 58 32.4 0.0 —0.8 33.2 α Virginis, 19 4 15 13 8 58.2 —5 55 16.8 56 49.3 α Bootis, 19 58 31½ 14 1 34.0 —5 56 57.5 58 39.0  Hourly rate of clock, —0.5 h. m. s. 9 41 49.0 Correction for clock and instrument (mean), —5 58 32.8 Observed R. A. of the planet, 9 41 49.0 Correction for clock and instrument (mean), —5 58 32.8 Observed. Refraction. Declination.  Z. D. observed. Refraction. Declination.  Z. D. observed. Refraction. Declination.  α Arietis, 29° 29′ 10″ +0′ 33″ 21° 58′ 53″ 51° 28′ 36″ π Arietis, 35 18 55 +0 41 16 9 4 51 28 40 σ Arietis, 37 41 0 +0 44 13 46 58 51 28 42 ε Arietis, 31 23 15 +0 35 20 4 37 51 28 27 δ Arietis, 32 55 55 +0 37 18 31 40 51 28 12 η Tauri, 28 20 55 +0 31 23 6 53 51 28 19 Uranus, 31 52 35 +0 36											58	34.7	-0	7 -	+2.9	32.5
η Tauri, 9 27 47 3 29 13.6 —5 58 33.4 58 31.1 —0.1 —1.3 32.5 Uranus, 9 41 49  A Tauri, 9 45 3 3 46 31.1 —5 58 31.9 58 32.4 0.0 —0.8 33.2 a Virginis, 19 4 15 13 8 58.2 —5 55 16.8 56 49.3 a Bootis, 19 58 31½ 14 1 34.0 —5 56 57.5 58 39.0  Hourly rate of clock, —0.5 h. m. s. 9 41 49.0 Correction for clock and instrument (mean), —5 58 32.8 Observed R. A. of the planet, 9 41 49.0 Correction.  Z. D. observed. Refraction. Declination.  Z. D. observed. Refraction. Declination.  A Arietis, 29° 29′ 10″ +0′ 33″ 21° 58′ 53″ 51° 28′ 36″ π Arietis, 35 18 55 +0 41 16 9 4 51 28 40 σ Arietis, 37 41 0 +0 44 13 46 58 51 28 42 ε Arietis, 31 23 15 +0 35 20 4 37 51 28 27 δ Arietis, 32 55 55 +0 37 18 31 40 51 28 12 η Tauri, 28 20 55 +0 31 23 6 53 51 28 19 Uranus, 31 52 35 +0 36						38.0	_5	58	43.0	,	58	33.0	-0	6 -	-0.2	33.8
Uranus, 9 41 49  A Tauri, 9 45 3 3 46 31.1 —5 58 31.9 58 32.4 0.0 —0.8 33.2  a Virginis, 19 4 15 13 8 58.2 —5 55 16.8 56 49.3  a Bootis, 19 58 31½ 14 1 34.0 —5 56 57.5 58 39.0  Hourly rate of clock, Deviation of instrument for each degree of Z. D.,  Transit of Uranus, Correction for clock and instrument (mean), Observed R. A. of the planet,  2. D. observed. Refraction.  Beclination.  Z. D. observed. Refraction.  A Arietis, 29° 29′ 10″ +0′ 33″ 21° 58′ 53″ 51° 28′ 36″  π Arietis, 35 18 55 +0 41 16 9 4 51 28 40  σ Arietis, 37 41 0 +0 44 13 46 58 51 28 42  ε Arietis, 31 23 15 +0 35 20 4 37 51 28 27  δ Arietis, 32 55 55 +0 37 18 31 40 51 28 12  η Tauri, 28 20 55 +0 31 23 6 53 51 28 19  Uranus, 31 52 35 +0 36	δ Arietis,	8 5	2 44	2	54	3.0	-5	58	41.0		58	33.0	-0.	5 -	+0.5	33.0
A Tauri, 9 45 3 3 46 31.1 —5 58 31.9 58 32.4 0.0 —0.8 33.2 a Virginis, 19 4 15 13 8 58.2 —5 55 16.8 56 49.3 a Bootis, 19 58 31½ 14 1 34.0 —5 56 57.5 58 39.0  Hourly rate of clock, Deviation of instrument for each degree of Z. D.,  Transit of Uranus, Correction for clock and instrument (mean), Observed R. A. of the planet,  2. D. observed. Refraction.  2. D. observed. Refraction.  2. D. observed. Refraction.  3. Declination.  2. D. observed. Refraction.  A Arietis, 35 18 55 +0 41 16 9 4 51 28 40  5 Arietis, 37 41 0 +0 44 13 46 58 51 28 42  5 Arietis, 31 23 15 +0 35 20 4 37 51 28 27  5 Arietis, 32 55 55 +0 37 18 31 40 51 28 12  7 Tauri, 28 20 55 +0 31 23 6 53 51 28 19  Uranus, 31 52 35 +0 36	n Tauri,			3	29	13.6	-5	58	33.4		58	31.1	-0	1 -	-1.3	32.5
a Virginis, 19 4 15 13 8 58.2 —5 55 16.8 56 49.3 a Bootis, 19 58 31½ 14 1 34.0 —5 56 57.5 58 39.0  Hourly rate of clock, —0.6 Deviation of instrument for each degree of Z. D., —0.5  Transit of Uranus, 9 41 49.0 Correction for clock and instrument (mean), —5 58 32.8 Observed R. A. of the planet, 3 43 16.2  1690, December 23. Declination.  Z. D. observed. Refraction. Declination. Eq. point.  a Arietis, 29° 29′ 10″ +0′ 33″ 21° 58′ 53″ 51° 28′ 36″  π Arietis, 35 18 55 +0 41 16 9 4 51 28 40  σ Arietis, 37 41 0 +0 44 13 46 58 51 28 42 ε Arietis, 31 23 15 +0 35 20 4 37 51 28 27 δ Arietis, 32 55 55 +0 37 18 31 40 51 28 12 η Tauri, 28 20 55 +0 31 23 6 53 51 28 19 Uranus, 31 52 35 +0 36	Uranus,	9 41	49													
A Bootis, 19 58 31½ 14 1 34.0 —5 56 57.5 58 39.0  Hourly rate of clock, Deviation of instrument for each degree of Z. D.,  Transit of Uranus, Correction for clock and instrument (mean), Observed R. A. of the planet,  2. D. observed. Refraction.  2. D. observed. Refraction.  A Arietis, 3 5 18 55 +0 41 16 9 4 51 28 40  A Arietis, 3 7 41 0 +0 44 13 46 58 51 28 42  A Arietis, 3 1 23 15 +0 35 20 4 37 51 28 27  A Arietis, 3 2 55 55 +0 37 18 31 40 51 28 12	A Tauri,	9 48	3	3	46	31.1	-5	58	31.9		58	32.4	0.	0 -	-0.8	33.2
Hourly rate of clock, Deviation of instrument for each degree of Z. D.,  Transit of Uranus, Correction for clock and instrument (mean), Observed R. A. of the planet,  2. D. observed. Refraction.  Z. D. observed. Refraction.  Declination.  Z. D. observed. Refraction.  A Arietis, 3 29° 29′ 10″ +0′ 33″ 21° 58′ 53″ 51° 28′ 36″  A Arietis, 35 18 55 +0 41 16 9 4 51 28 40  A Arietis, 37 41 0 +0 44 13 46 58 51 28 42  A Arietis, 31 23 15 +0 35 20 4 37 51 28 27  A Arietis, 32 55 55 +0 37 18 31 40 51 28 12  Tauri, 28 20 55 +0 31 23 6 53 51 28 19  Uranus, 31 52 35 +0 36	a Virginis	19	1 15	13	8	58.2	-5	55	16.8		56	49.3				
Deviation of instrument for each degree of Z. D.,  Transit of Uranus,  Correction for clock and instrument (mean),  Observed R. A. of the planet,  2. D. observed. Refraction.  Z. D. observed. Refraction.  Arietis,  3 29° 29′ 10″ +0′ 33″ 21° 58′ 53″ 51° 28′ 36″  Arietis,  3 5 18 55 +0 41 16 9 4 51 28 40  Arietis,  3 7 41 0 +0 44 13 46 58 51 28 42  Arietis,  Arietis,  31 23 15 +0 35 20 4 37 51 28 27  Arietis,  32 55 55 +0 37 18 31 40 51 28 12  Tauri,  28 20 55 +0 31 23 6 53 51 28 19  Uranus,  31 52 35 +0 36	a Bootis,	19 58	$31\frac{1}{2}$	14	1	34.0	-5	56	57.5		58	39.0				
Deviation of instrument for each degree of Z. D.,  Transit of Uranus,  Correction for clock and instrument (mean),  Observed R. A. of the planet,  1690, December 23. Declination.  Z. D. observed. Refraction. Declination.  Eq. point.  a Arietis, 29° 29′ 10″ +0′ 33″ 21° 58′ 53″ 51° 28′ 36″  π Arietis, 35 18 55 +0 41 16 9 4 51 28 40  σ Arietis, 37 41 0 +0 44 13 46 58 51 28 42  ε Arietis, 31 23 15 +0 35 20 4 37 51 28 27  δ Arietis, 32 55 55 +0 37 18 31 40 51 28 12  η Tauri, 28 20 55 +0 31 23 6 53 51 28 19  Uranus, 31 52 35 +0 36	Ho	urly r	ate of	clo	ck.								7	No.	-0°.6	
Transit of Uranus, Correction for clock and instrument (mean), Observed R. A. of the planet,  1690, December 23. Declination.  Z. D. observed. Refraction. Declination.  2. D. observed. Refraction. Declination.  2. D. observed. Refraction. Declination.  3. 43 16.2  2. D. observed. Refraction. Declination.  4. Arietis, 29° 29′ 10″ +0′ 33″ 21° 58′ 53″ 51° 28′ 36″  5. Arietis, 35 18 55 +0 41 16 9 4 51 28 40  6. Arietis, 37 41 0 +0 44 13 46 58 51 28 42  6. Arietis, 31 23 15 +0 35 20 4 37 51 28 27  8. Arietis, 32 55 55 +0 37 18 31 40 51 28 12  7. Tauri, 28 20 55 +0 31 23 6 53 51 28 19  Uranus, 31 52 35 +0 36					100	nt for	each	de	gree	of !	Z. I	)				
Correction for clock and instrument (mean), —5 58 32.8 Observed R. A. of the planet, 3 43 16.2  1690, December 23. Declination.  Z. D. observed. Refraction. Declination. Eq. point.  a Arietis, 29° 29′ 10″ +0′ 33″ 21° 58′ 53″ 51° 28′ 36″  π Arietis, 35 18 55 +0 41 16 9 4 51 28 40  σ Arietis, 37 41 0 +0 44 13 46 58 51 28 42  ε Arietis, 31 23 15 +0 35 20 4 37 51 28 27  δ Arietis, 32 55 55 +0 37 18 31 40 51 28 12  η Tauri, 28 20 55 +0 31 23 6 53 51 28 19  Uranus, 31 52 35 +0 36									0					m.	s.	
Observed R. A. of the planet,  1690, December 23. Declination.  Z. D. observed. Refraction. Declination. Eq. point.  a Arietis, 29° 29′ 10″ +0′ 33″ 21° 58′ 53″ 51° 28′ 36″  π Arietis, 35 18 55 +0 41 16 9 4 51 28 40  σ Arietis, 37 41 0 +0 44 13 46 58 51 28 42  ε Arietis, 31 23 15 +0 35 20 4 37 51 28 27  δ Arietis, 32 55 55 +0 37 18 31 40 51 28 12  η Tauri, 28 20 55 +0 31 23 6 53 51 28 19  Uranus, 31 52 35 +0 36							1378									
1690, December 23. Declination.         Z. D. observed. Refraction.       Declination.       Eq. point.         a Arietis, $29^{\circ}$ 29' 10" +0' 33" 21° 58' 53" 51° 28' 36" $\pi$ Arietis, $35$ 18 55 +0 41 16 9 4 51 28 40 $\sigma$ Arietis, $37$ 41 0 +0 44 13 46 58 51 28 42 $\varepsilon$ Arietis, $31$ 23 15 +0 35 20 4 37 51 28 27 $\delta$ Arietis, $32$ 55 55 +0 37 18 31 40 51 28 12 $\eta$ Tauri, $28$ 20 55 +0 31 23 6 53 51 28 19         Uranus, $31$ 52 35 +0 36								ent	(mea	in),						
Z. D. observed. Refraction. Declination. Eq. point.  a Arietis, $29^{\circ} 29' 10'' + 0' 33'' 21^{\circ} 58' 53'' 51^{\circ} 28' 36''$ $\pi$ Arietis, $35$ 18 55 $+0$ 41 16 9 4 51 28 40 $\sigma$ Arietis, $37$ 41 0 $+0$ 44 13 46 58 51 28 42 $\varepsilon$ Arietis, $31$ 23 15 $+0$ 35 20 4 37 51 28 27 $\delta$ Arietis, $32$ 55 55 $+0$ 37 18 31 40 51 28 12 $\eta$ Tauri, $28$ 20 55 $+0$ 31 23 6 53 51 28 19  Uranus, $31$ 52 35 $+0$ 36	Ob	served	R. A	. of	the	plan	et,						3	43	16.2	
Z. D. observed. Refraction. Declination. Eq. point.  a Arietis, $29^{\circ} 29' 10'' + 0' 33'' 21^{\circ} 58' 53'' 51^{\circ} 28' 36''$ $\pi$ Arietis, $35$ 18 55 $+0$ 41 16 9 4 51 28 40 $\sigma$ Arietis, $37$ 41 0 $+0$ 44 13 46 58 51 28 42 $\varepsilon$ Arietis, $31$ 23 15 $+0$ 35 20 4 37 51 28 27 $\delta$ Arietis, $32$ 55 55 $+0$ 37 18 31 40 51 28 12 $\eta$ Tauri, $28$ 20 55 $+0$ 31 23 6 53 51 28 19  Uranus, $31$ 52 35 $+0$ 36				10	390	Dece	mher	23	T	eclin	ati	on.				
a Arietis, 29° 29′ 10″ +0′ 33″ 21° 58′ 53″ 51° 28′ 36″ π Arietis, 35 18 55 +0 41 16 9 4 51 28 40 σ Arietis, 37 41 0 +0 44 13 46 58 51 28 42 ε Arietis, 31 23 15 +0 35 20 4 37 51 28 27 δ Arietis, 32 55 55 +0 37 18 31 40 51 28 12 η Tauri, 28 20 55 +0 31 23 6 53 51 28 19 Uranus, 31 52 35 +0 36			,,											NIE.		
$\pi$ Arietis, 35 18 55 +0 41 16 9 4 51 28 40 $\sigma$ Arietis, 37 41 0 +0 44 13 46 58 51 28 42 $\epsilon$ Arietis, 31 23 15 +0 35 20 4 37 51 28 27 $\delta$ Arietis, 32 55 55 +0 37 18 31 40 51 28 12 $\eta$ Tauri, 28 20 55 +0 31 23 6 53 51 28 19 Uranus, 31 52 35 +0 36							1000									
$\sigma$ Arietis, 37 41 0 +0 44 13 46 58 51 28 42 $\varepsilon$ Arietis, 31 23 15 +0 35 20 4 37 51 28 27 $\delta$ Arietis, 32 55 55 +0 37 18 31 40 51 28 12 $\eta$ Tauri, 28 20 55 +0 31 23 6 53 51 28 19 Uranus, 31 52 35 +0 36		120											-			
ε Arietis, 31 23 15 +0 35 20 4 37 51 28 27 δ Arietis, 32 55 55 +0 37 18 31 40 51 28 12 η Tauri, 28 20 55 +0 31 23 6 53 51 28 19 Uranus, 31 52 35 +0 36		DO TO														
δ Arietis, 32 55 55 +0 37 18 31 40 51 28 12 η Tauri, 28 20 55 +0 31 23 6 53 51 28 19 Uranus, 31 52 35 +0 36		SECTION AND ADDRESS.														
η Tauri, 28 20 55 +0 31 23 6 53 51 28 19 Uranus, 31 52 35 +0 36																
Uranus, 31 52 35 +0 36																
	The second second second second									23	6	53	51	28	19	- H
A Tauri, 30 15 55 +0 34 21 12 3 51 28 32										01	10			00	00	
	AT	auri,		30 1	5 5	05	+0	34	100	21	12	3	51	28	32	
Circle reading for Uranus, corrected for refraction, 31° 53′ 11″	Circ	le rea	ding f	or U	ran	us, co	rrect	ed :	for re	efrac	etion	1,	31	° 53′	11"	
Equatorial point on circle, 51 28 30	Equ	atoria	poin	t on	circ	ele,							51	28	30	
Declination of Uranus, from observation, +19 35 19	Dec	linatio	n of	Uran	us,	from	obse	rvat	tion,				+19	35	19	
1810 A 70 B: 14 Accession					~10		70		. 7.							
1712, April 2. Right Ascension.																
Uranus, 9 35 19 h. m. s. m. s.		I	ranus	1-0-	-		-		-			32.	m •	dinan		
ε Virginis, 12 0 19 12 47 52.4 +47 33.4			THEFT	?					ш.							

The discordance of clock errors, and the time which intervened between the transit of the planet and that of the first star, seem to render an accurate reduction impossible.

e Virginis, 12 14 51ζ Virginis, 12 32 11

13 2 31.5

13 20 5.7

+47 40.5

+47 54.7

b Virginis,

1715,	March 4.	Right	Ascensio	n.
T.		R. A.		C.

C". h. m. s. 10 45 52.5 20.5 11 50 19 d Leonis, 12 27 Uranus, 11 45 23.6 —1 4 17.4 21.1 12 49 41

h. m. 12 27 Clock time of transit of Uranus, -1 4 20.8 Correction for clock and instrument,

Right ascension of Uranus from observation, 11 22 40.2

#### 1715, March 4. Declination.

	$\mathbf{Z}$ .	D.	R.	Dec.	Eq. point.
d Leonis,	46° 1	9' 40"	+1' 0"	+5° 8′	6" 51° 28′ 46"
Uranus,	46 3	3 10	+1 1		
b Virginis,	46 1	3 20	+1 0	5 14 1	7 51 28 37
Circle re	ading f	or Uran	us,		46° 34′ 11″
Equatori					51 28 42
Observed	declin	ation of	Uranus,		+4 54 31

## 1715, Murch 5. Right Ascension.

		T.			A.		C.		C'
	h. 1	m. 8.	h.	m.	8.	h.	m. s.		8.
d Leonis,		46 24	10	45	52.5	-1	0 31.	5 5	25.5
Uranus,	12 5	22 59:	: -						
b Virginis,	12 4	45 49	11	45	23.6	-1	0 25.	4	29.1
							1	n. m.	8.
Transit of	Uranu	18,					_ 1	12 22	59
Correction	for clo	ock and	instru	ıme	nt,		E	-1 0	27.7
Observed :	right a	scensio		1	11 22	31.5			

The large apparent clock rate, and the colons after the time of transit, both throw doubt on this observation.

#### Declination.

The circle readings for the stars are the same as on the day preceding, while that for Uranus is 50" less. The declination is therefore 50" greater, or

# +4° 55′ 21″. 1715, March 10. Right Ascension.

		T.				R. 4	A.			C.			C'.
d Leonis,		m. 25			h.	m.	s. 52.5				s. 5.5		g. 59.5
p³ Leonis,	11	32	28		10	52	25.1	-	-0	40	2.9		58.1
Uranus,	12	1	42										
b Virginis,	12	25	18		11	45	23.6		-0	39	54.4		58.2
S. L. LANDERS											h.	m.	8.
Clock time of t	rans	sit o	f U	ran	us,						12	1	42
Correction for clock and instrument, —0 39 58								58.6					
Observed right ascension of Uranus, 11 21 43.								43.4					

#### Declination.

		Z. D		I	3.	Dec		E	q. P	t.
d Leonis,	46°	19'	35"	+1'	1"	5° 8	6"	51°	28'	42"
p³ Leonis,	47	58	35	+1	3	3 29	25	51	28	63
Uranus,	46	27	0	+1	1					
b Virginis,	46	13	25	+1	0	5 14	17	51	28	42
Circle reading	for U	ranu	ıs,					46	28	1
Equatorial po	int on	circ	le,					51	28	49
Observed decl				us,				+5	0	48

## 1715. April 29. Right Ascension.

		T.			R.	Α.		C	C'.
σ Leonis,	8 8	т. 42	s. 11	h. 11	m. 6	s. 28.3		m. s. 24 17.3	18.7
Uranus,	8	50	44						
ν Virginis,	9	6	55	11	31	14.1	+2	24 19.1	16.4
17 Virginis,	9	43	38::	12	8	6.5	+2	24 28.5	19.8
z Virginis,	11	32	48.	13	57	47.6	+2	24 59.6	33.1

The discordance of the clock corrections makes a satisfactory determination of the right ascension very difficult. I deem it best to reject the doubtful observation of 17 Virginis, and the discordant one of z Virginis. The result will then be

	h.	m.	8.
Observed transit of Uranus,	8	50	44
Correction for clock and instrument,	2	24	17.6
Observed right ascension of Uranus,	11	15	1.6

#### Declination.

	Z	. D.		R			Dec		E	q. P	t.
σ Leonis,	43°	52'	40"	+0'	55"	70	34'	51"	51°	28'	26"
Uranus,	45	45	30	+0	59						
ν Virginis,	43	20	20	+0	54	8	7	11	51	28	25
17 Virginis,	44	34	10	+0	56	6	53	33	51	28	39
z Virginis,	60	23	5	+1	41	-8	55	42	51	28	64
Circle readir	ng fo	r U	ranus	,					45°	46'	29"
Mean equato	-							304	51	28	38
Observed de	tion	of I	Jranus,		10000			+5	42	9	

The next observations in the order of time are two by Bradley, discovered by Mr. Hugh Breen, but still unpublished. The following are the results as given by Mr. Breen in the Astronomische Nachrichten, No. 1463.

Mean Time.		R. A.	N. P. D.
1748, October 21,	h. m. s. 7 6 18.4	h. m. s. 21 4 37.93	107 29
1750. September 13.	10 8 57.8	21 40 0.23	104 42 33.9

Mr. Breen remarks: "The right ascensions are very accurate. It has been assumed that the N. P. D., on 1750, September 13, is identical with  $\mu$  Capricorni, with which it was compared. The first observation was by the transit instrument, and the second by the quadrant."

No ground is given for the above assumption respecting the N. P. D. for the second observation; it may, therefore, be omitted as valueless.

In the year 1750 we have also two observations by Le Monnier at Paris. For these, and all the other observations by the same observer, I shall adopt the results given by Bouvard in the Connaissance des Temps, for 1821, p. 341, with the corrections indicated by Le Verrier, in Connaissance des Temps, for 1849, pp. 125 and 126. The necessary uncertainty of the observations is such that, considering that Bouvard reduced them with the star positions of the "Fundamenta," scarcely anything will be gained by a new reduction.

1753, December 3, we have another observation of right ascension by Bradley. I adopt the result kindly communicated by my distinguished friend, Dr. Auwers.

1753, December 3, 
$$\stackrel{\text{h. m.}}{5}$$
 33. R. A.  $=$   $\stackrel{\text{h. m.}}{22}$   $\stackrel{\text{s.}}{23}$  21.59

1756, September 25. Observation by Mayer, at Gottingen. I adopt the result given by Bessel, in *Fundamenta Astronomiæ*, p. 284.

1756, September 25, 
$$10 \ 12$$
. R. A. =  $348 \ 0 \ 54.5$   
Dec. =  $-6 \ 1 \ 49.4$ 

The following is a tabular summary of the preceding results, with their comparison with the provisional theory. In the computation of the geocentric place the places of the sun were derived from Hansen's Tables. I am indebted to Professor Coffin for a duplicate computation of the geocentric places from the provisional ephemeris, which was executed by Mr. Joseph A. Rogers.

	Right Ascension.	Declination.	Correction to theory.				
Date.	Observation.	Observation. Upon discount of the other disc	R. A. Dec.	Long. $\frac{\partial l}{\partial \lambda}$ $\frac{\partial l}{\partial \rho}$			
Mar. 10 Apr. 29 1748, Oct. 21 1750, Sept. 13	11 22 40.2 38.7 11 22 31.5 29.1 11 21 43.4 41.0			$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			

	Date. Observation.		sion.	Declination.				Correction to theory.						
Date.			Observation.			Theory.	R. A.	Dec.	Long.	$\frac{\partial l}{\partial \lambda}$	$\frac{\partial l}{\partial \rho}$			
	0	,	"	"	0	,	"	,	"	"	"		100 1	
1750, Dec. 3		34 m	53.5 s	15.4 s	-14	53	20.2	32.4	+38.1	+12.2	+38.8	0.98	+.04	
1753, Dec. 3									+33.8		+35.6	1.00	+.04	
1756, Sept.25 1764, Jan. 15				25.0 56.4				46.0 56.2	+29.5 (—17.4)	-3.4	+25.7	1.05	+.013	
1768, Dec. 27 Dec. 30 1769, Jan. 15	31 31 31	26	52.0 45.8 7.7	32.6 38.0 :55.8	12 12 12	15 14 14	35.0 55.4 26.0:	30.6 55.9 29.7	+19.4 + 7.8 + 11.9:	$+4.4$ } $-0.5$ } $-3.7$ :	+13.0	1.02	+.045	
Jan. 16 Jan. 20 Jan. 21 Jan. 22	31 31	24	6.6	11.1 :43.7 14.1 :47.7	12 12	15 15	36.3 19.0 31.8 45.7	37.0 18.8 30.8	+12.3 $+22.9$ : $+19.7$	$\begin{bmatrix} -0.7 \\ +0.2 \\ +1.0 \\ \end{bmatrix}$	+12.5	1.01	+.04	
Jan. 23	The state of		28.5				7.5	44.7 :59.6	+17.0: $+4.3:$	$\begin{vmatrix} +1.0 \\ +7.9 \end{vmatrix}$	enteral	Switz	W THE	

Where no declination has been observed the observed corrections in right ascension have been changed to corrections in longitude on the hypothesis that the theoretical latitude is correct. The approximate formula is

$$\delta l = \frac{\delta a \cos \delta}{\sin E}$$
, where

 $\cos E = \sin \varepsilon \cos \alpha$ ,  $\varepsilon$  being the obliquity.

#### DISCUSSION OF THE MODERN OBSERVATIONS.

Reduction of the Published Results of Observations to a Uniform System.

We have now to discuss the great mass of observations made at the principal observatories of the world since the discovery of the planet by Herschel, in 1781. To make all the data of reduction rigorously homogeneous and uniform, it would be necessary to completely re-reduce the greater part of the observations made before 1850, using the modern values of the constants of reduction, and to compare each observation separately with the geocentric place deduced from the provisional theory. Such a reduction and comparison would be extremely desirable. Their execution would, however, involve an amount of labor far greater than it is now possible for the author to bestow upon the problem. We must, therefore, adopt the reductions which have been already made, applying such systematic corrections for reduction to a uniform system of star places as we have the means readily to determine. No reduced places are employed unless we can find data for some more or less accurate determination of these corrections, a rule which necessitates the rejection of a great mass of observations made at the minor observatories of the European continent, and published in the Astronomischen Nachrichten. We still have the following rich collection of materials at our disposal:

	1.	Observations at	Greenwich, 1781 to 1872.
	2.		Paris, 1802 to 1827, and 1837 to 1869
			Vienna, 1822, and 1827 to 1839.
			Speier, 1827–29.
			Edinburgh, 1836 to 1844.
			Berlin, 1838 to 1842.
			72 11 2012 1 2010
			Leiden, 1863 to 1871.
	12.		Santiago, 1854 and 1855.
-	2.		Daniel 1000.

As to the general distribution of these observations in time, we may remark that during the first three or four years the planet was zealously observed at Greenwich. Observations then began gradually to fall off until 1798, in which year we find but one. From this time until 1814 only one or two observations were made at each opposition. They become a little more numerous, until 1829, when there is a sudden increase. Few interruptions have occurred since. With regard to the other observatories it may be said that from 1802 until 1830 there is a gradual increase in the number of observations, and that since the latter year the number of observations is entirely satisfactory.

A great number of the observations were reduced with the star places of the Tabulæ Regiomontanæ, and the entire Paris series are reduced with the star positions of Le Verrier, given in his "Annales de l'Observatoire Imperial de Paris," Tome II. As a preliminary to the discussion of the systematic corrections to the principal published reductions, I have prepared the following table, showing the corrections which must be applied to the places of the equatorial fundamental stars in the above catalogues to reduce them to the adopted standard, namely, Dr. Gould's coast survey list in right ascension, and Auwers' standard in declination.

In the table of right ascensions the first column after name of the star gives the annual variation of that co-ordinate for the epoch 1860.0, as derived from Le Verrier's tables of right ascensions just cited. Next we have the correction to this annual variation, expressed in units of the fourth place of decimals, to reduce it to that given in the "Star Tables of the American Ephemeris," the positions in which are founded on Dr. Gould's Catalogue. The fourth column gives the correction to the right ascensions of Le Verrier for 1860, in hundredths of a second of time. Subtracting from this column sixth-tenths of the preceding, we have the corresponding corrections for 1800. The last four columns give the corresponding numbers for the right ascensions of the Tabulæ Regiomontanæ.

The table of declinations shows, for different epochs, the corrections necessary to reduce the tabular positions to those given by Auwers in his paper on the declinations of the fundamental stars

I. RIGHT ASCENSIONS.								
1010	Le Verrier's	Corrections to					Corrections to	
Date.	ann. var. 1860.	Ann. var.	R. A. 1860.	R. A. 1800.	Ann. var. of Tab. Reg. 1860.	Ann: var.	R. A. 1860.	R. A. 1800.
a Andromedæ,	+3.0844	+ 14	+ 2	_ 6	8 3.0840	+18	+ 8	_ 3
γ Pegasi,	3.0801	+ 15	+ 3	_ 6	3.0824	_ 8	_ 9	- 4
a Arietis,	3.3644	+ 12	0	- 7	3.3636	+20	+ 6	— 6
a Ceti,	3.1266	+ 10	+ 5	_ 1	3.1267	+ 9	+7	+ 2
a Tauri,	3.4346	_ 1	_ 1	0	3.4335	+10	+7	+ 1
β Orionis,	2.8797	+ 6	+ 2	_ 2	2.8800	+ 3	+ 5	+ 3
β Tauri,	3.7871	- 4	+ 1	+ 3	3.7888	-21	- 4	+ 9
a Orionis,	3.2460	+ 5	+ 4	+ 1	3.2464	+1	+ 3	+ 2
a Geminorum,	3.8409	- 2	0	+ 1	3.8386	+21	+18	+ 5
G Canis Min.	3.1462	+ 5	+ 9	+ 6	3.1455	+12	+7	0
β Geminorum,	3.6828	+ 5	+ 3	0	3.6807	+26	+13	— 3
a Hydræ,	2.9485	+ 12	+ 6	- 1	2.9469	+28	+16	- 1
a Leonis,	3.2030	+ 15	+ 6	- 3	3.2014	+31	+13	- 6
β Leonis,	3.0654	+ 11	+ 4	- 3	3.0640	+25	+12	— 3
a Virginis,	3.1495	+ 20	+ 5	- 7	3.1497	+18	+ 2	- 9
a Bootis,	2.7325	+ 16	+ 3	- 7	2.7327	+14	+ 5	_ 3
a² Libræ,	3.3044	+ 6	+ 3	- 1	3.3074	-24	- 6	+ 8
a Coronæ,	2.5378	+ 12	+ 1	- 6	2.5373	+17	+ 5	_ 5
a Serpentis,	2.9488	+ 8	+4	— 1	2.9513	-17	- 7	+ 3
a Scorpii,	3.6654	+ 16	+ 4	<u> </u>	3.6672	_ 2	- 4	— 3
a Herculis,	2.7322	+ 7	+ 2	_ 2	2.7319	+ 9	0	_ 5
a Ophiuchi,	2.7808	+ 10	0	<b>—</b> 6	2.7783	+34	+15	- 5
a Lyræ,	2.0312	+ 2	_ 1	_ 2	2.0305	+ 9	+1	- 4
γ Aquilæ,	2.8520	+ 9	+ 2	_ 3	2.8546	-17	- 8	+ 2
a Aquilæ,	2.9281	+ 4	+ 1	-1	2.9281	+ 4	_ 3	- 5
β Aquilæ,	2.9466	+ 5	+ 3	0	2.9496	-25	_12	+ 3
a <sup>2</sup> Capriconii,	3.3338	+ 4	+ 2	0	3.3349	- 7	_ 6	- 2
a Aquarii,	3.0829	+ 13	+ 4	- 4	3.0822	+20	+ 4	- 8
a Piscis Aust.	3.3311	+ 8	+ 4	- 1	3.3326	- 7	-16	-12
a Pegasi,	2.9828	+ 11	0	- 7	2.9830	+ 9	- 1	<b>—</b> 6
Sum,		+254	+81	-72		+210	+71	-55
Mean,		+8.5	+.027	024		+7.0	+.024	018

15 May, 1873.

II. Declinations.							
	Corrections to Tabulæ Regiomontanæ.				Corrections to Le Verrier.		
	1780.	1800.	1820.	1840.	1820.	1840.	
a Andromedæ,	1/1	10.9	10.1	//	//	"	
γ Pegasi,	+0.3	$+0.2 \\ +0.1$	$+0.1 \\ +0.4$	0.0	+0.2	0.0	
a Arietis,	_0.2	0.0	+0.3	+0.8	$+0.1 \\ +0.2$	+0.3	
a Ceti,		-0.1	+0.7	+1.6	+0.2	+0.3 +0.7	
a Tauri,	0.0	+0.1	+0.1	+0.2	+0.1	0.0	
β Orionis,	_0.5	+0.1	+0.6	+1.2	+0.3	+0.7	
β Tauri,	0.5	0.0	+0.6	+1.1	+0.3	+0.5	
a Orionis,		_0.6	0.0	+0.6	-0.2	+0.3	
a Geminorum,	_0.8	-0.5	0.1	+0.3	+0.5	+1.0	
a Canis Min.	0.2	0.0	+0.3	+0.6	+0.2	+0.5	
β Geminorum,	0.2	0.0	+0.3	+0.6	+0.2	+0.5	
a Hydræ,	0.2	+0.3	+0.7	+1.2	+0.3	+0.7	
a Leonis,	+0.3	+0.4	+0.4	+0.5	+0.4	+0.5	
β Leonis,	+0.2	+0.2	+0.2	+0.3	+0.2	+0.3	
a Virginis,	+0.2	+0.6	+1.1	+1.5	+0.5	+0.8	
a Bootis,	+0.4	+0.4	+0.3	+0.2	+0.4	+0.4	
a² Libræ,	+0.5	+0.5	+0.6	+0.6	+0.5	+0.6	
a Coronæ,	+0.7	+0.6	+0.4	+0.3	+0.4	+0.4	
a Serpentis,	+0.2	+0.6	+1.1	+1.5	+0.5	+0.9	
a Scorpii,	+0.1	+0.6	+1.0	+1.4	+0.4	+0.7	
a Herculis,	+0.6	+0.8	+1.0	+1.3	+0.5	+0.7	
a Ophinchi,	+0.4	+0.5	+0.5	+0.6	+0.4	+0.6	
a Lyræ,	+0.7	+0.8	+0.9	+1.0	+0.4	+0.4	
γ Aquilæ,	0.0	+0.3	+0.6	+1.0	+0.2	+0.4	
a Aquilæ,	+0.1	+0.4	+0.7	+1.0	+0.1	+0.4	
β Aquilæ,	+0.1	+0.6	+1.2	+1.7	+0.5	+0.8	
a <sup>2</sup> Capriconii,	+0.2	+0.9	+1.6	+2.3	+0.6	+1.1	
a Aquarii,	0.5	+0.1	+0.8	+1.5	+0.5	+1.0	
a Piscis Aust.	+1.0	+2.4	+3.9	+5.3	+1.7	+2.3	
à Pegasi,	+0.4	+0.3	+0.2	+0.1	+0.3	+0.2	
Mean	+0.03	+0.36	+0.69	+1.03	+0.36	+0.60	
						1000	

The correction to the reductions to apparent place given in the Tabulæ Regiomontanæ on account of the correction to the constant of Nutation is;—

In right ascension: -0".46 sin  $\Omega$  -0".18 sin  $\Omega$  sin  $\alpha$  tan  $\delta$  -0".24 sin  $\Omega$  cos  $\alpha$  tan  $\delta$ .

In declination:  $-0^{\alpha}18 \sin \Omega \cos \alpha + 0.24 \cos \Omega \sin \alpha$ .

The terms which contain  $\tan \delta$  as a factor may be entirely neglected, as they are small, periodic, and contain  $\tan \delta$  as a factor which is sometimes positive and sometimes negative. I shall also neglect the corrections in declination, as their sum is sensibly

$$0''.21 \sin (\alpha - \Omega)$$

the effect of which will generally be confounded with the accidental errors of observation.

The only correction we shall apply on account of nutation is, therefore,

$$\delta \alpha = -0^{\circ}.030 \sin \Omega.$$

The values of this expression at the dates when it is zero, a maximum, or a minimum, are as follows:—

. у.	s.	у.	s.
1778.5	03	1820.3	.00
1783.1	.00	1825.0	+.03
1787.7	+.03	1829.6	.00
1792.4	.00	1834.3	03
1797.0	03	1838.9	.00
1801.7	.00	1843.6	+.03
1806.3	+.03	1848.2	.00
1811.0	.00	1852.9	03
1815.6	03	1857.5	.00
1820.3	.00	Laure Cons	

Having adopted this system of standard positions, we may adopt two ways of reducing the observations to it. One is to compare the positions of the stars adopted in the published reductions with the standard, and apply the mean difference to the reduced place of the planet. Another is to make a similar comparison of the standard catalogue with the positions of the fundamental stars which have been deduced from the observations by a system of reduction uniform with that employed in reducing the observations of the planet, and to regard the mean difference as a correction applicable to all the positions of the planet. If the standard catalogue and the observations are both free from systematic error, the results obtained in these two ways should be substantially identical. These are, however, conditions which we cannot expect to find fulfilled. In the following discussions I have sometimes used one, sometimes the other, and sometimes

combined both, the choice being determined by circumstances. We shall consider the different series of observations in succession.

## Greenwich Observations from 1781 to 1830.

These observations are completely reduced by Airy and compared with Bouvard's Tables, in the work Reduction of the Observations of Planets made at the Royal Observatory, Greenwich, from 1750 to 1830. London, 1845. The concluded positions given in this work depend mainly on the star places of the Tabulæ Regiomontanæ, both in right ascension and declination. If we consider the first four oppositions—1781-1785—as forming a single group of which the mean epoch is 1783, we find that the general correction to the Tabulæ Regiomontanæ for this epoch is

In right ascension,  $-0^{\circ}.030$ ; In declination,  $+0^{\circ}.08$ .

If, on the other hand, we consider only the particular stars compared with Uranus, the result will be a little different. The number of times each of the fundamental stars has been compared with Uranus, and the correction in right ascension corresponding to each star, are nearly as follows:—

		S.	8.
a Arietis,	N=2	Cor. = -0.09	$N \times C =18$
α Tauri,	2	01	02
γ Pegasi,	2	03	<b>—</b> .06
β Tauri,	19	+.13	+2.47
a Orionis,	33	+.02	+0.66
a Canis Minori	s, 33	02	-0.66
β Geminorum,	34	07	-2.38
a Leonis,	7	11	77
β Leonis,	2	07	14

The mean correction from these data comes out  $-0^{\circ}.008$ , differing by  $0^{\circ}.022$  from the general mean correction. Our choice between the two corrections depends on whether we are to consider the relative positions of the Tabulæ Regiomontanæ, or those of the standard catalogue, as nearest the truth at the epoch 1783, and particularly upon whether we are to consider the large correction to the proper motion of  $\beta$  Tauri as real. In the absence of exact data for settling this question, the mean of the two results, or  $-0^{\circ}.020$ , has been adopted.

A similar anomaly is exhibited by the declinations. It is probable that the declinations of Uranus during this period mainly depend on stars in the first twelve hours in right ascension, for which the mean correction is about -0".30 instead of +0".08. I have adopted -0".16. Changing these corrections to longitude and latitude, we have, during the period 1781-1786:

Correction to observed longitude,  $=-0^{\circ}.30$ ; Correction to observed latitude, -0.19.

During the years 1788-1798 the above systematic difference in right ascension does not appear. The most probable correction seems to be

$$\Delta \alpha = -0^{\circ}.025; \qquad \Delta \delta = 0^{\circ}.00.$$
 Whence 
$$\Delta \log = -0^{\circ}.34; \qquad \Delta \text{ lat.} = -0^{\circ}.10.$$

Between the years 1800 and 1823 the stars used for comparison are so widely scattered that I consider it safe to apply only the general mean correction for the epoch 1813, which is

Whence 
$$\Delta \alpha = -$$
 \*.005;  $\Delta \delta = +0$ ".66.  $\Delta \log = 0$ ".00;  $\Delta \operatorname{lat} = +0$  .66.

From 1825 to 1830 more than half the weight of the right ascension comes upon the stars  $\alpha$ ,  $\beta$ , and  $\gamma$  Aquilæ, the mean correction to which, during this interval, is  $-0^{\circ}.035$ . The general mean correction at this epoch is  $+0^{\circ}.002$ . I think the right ascensions of these three stars in the Tabulæ Regiomontanæ are really too great at this epoch by the entire difference of these results. We may, in fact, hereafter regard the positions of the standard catalogue as sufficiently accurate. The mean corrections to be applied will then be

$$\Delta a = -0^{\circ}.017;$$
  $\Delta \delta = +0^{\circ}.83.$  Whence  $\Delta \log = -0^{\circ}.05;$   $\Delta \text{lat.} = +0^{\circ}.86.$ 

From the year 1831 until the present time the Greenwich observations are regularly reduced in the several annual volumes of observations. But a reduction of the observations from 1831 to 1835, executed by Mr. Hugh Breen, is given in an appendix to the volume for the year 1864. The results here given differ from those published by Pond in the several annual volumes for the same interval. The right ascensions are altered only by applying the constant correction —0°.030, which is found necessary to reduce Pond's right ascensions to those of the Tabulæ Regiomontanæ. This correction I have verified. The mean correction to reduce the right ascensions of the Tabulæ Regiomontanæ to our standard is at this time +0°.005. On the other hand, when we compare the concluded right ascensions of stars within six hours of Uranus, as given by Pond in the Greenwich observations for 1834, with our standard, we find a mean correction of —°.034 to reduce his positions to the standard, which implies a correction —°.004 to Breen's reduction. The two results being +°.005 and —°.004, I have applied no correction whatever.

In the paper in question the declinations are completely re-reduced, using improved data of reduction, but, so far as I see, making no changes in Pond's method. The results differ strikingly from those of Pond, and suggest the desirableness of a complete re-examination of all Pond's determinations of declination. Having no catalogue of observed declinations of standard stars reduced in this same way, we cannot directly determine the systematic correction to the declinations. I therefore proceed as follows: A comparison of Pond's observed declinations of standard stars with Auwers' normal catalogue show that the former require the following corrections near the parallel of Uranus:

In 
$$1831 - 1''.42$$
;  $1834 - 2.10$ .

Then comparing Airy's reduced declinations of Uranus with Pond's, we find the following mean differences:

In 1831, Airy — Pond = 
$$-3''.18$$
  
1834,  $-3.50$ .

To reduce Airy to Auwers we must there apply to the declinations

In 
$$1831 + 1$$
".76  $1834 + 1$ .40.

I have regarded the correction +1".60 as applicable throughout the period in question.

During this interval the corrections in right ascension have been derived by the following two sets of comparisons: (1) A comparison of the several collected six and seven year catalogues with Gould's standard, from which it appears that they require the following general corrections in right ascension:

Six year catalogue of 1840	$+0^{\circ}.047$
Six year catalogue of 1845	+0.002
Seven year catalogue of 1860	+0.003
Seven year catalogue of 1864	+0.022

(2) A comparison of the corrections applied to the right ascensions of the individual years to reduce them to the standard of the catalogue, as given in the introduction to each catalogue. The sum of these two numbers gives the corrections for each year.

A slightly different method is to regard the above correction for each catalogue as applicable to all right ascensions which depend fundamentally upon that catalogue. I have sometimes combined both methods so as to derive what seemed to be the most probable result, and sometimes used but one.

The corrections to the declinations during the interval in question have been derived from Auwers' "Tafeln zur Reduction der Declinationen verschiedener Sternverzeichnisse auf ein Fundamentulsystem," Astronomische Nachrichten, No. 1536. These tables include the Greenwich seven year catalogue for 1860, when the correction corresponding to the declination of Uranus is about +0".45. The corrections for the previous catalogues vary between 0".35 and 0".68. The correction corresponding to the interval 1861-67 has been derived by a direct comparison with Auwers' declinations, and the result is +0".44, agreeing with the two preceding catalogues. But, on making a similar comparison with the annual catalogue for 1869, a considerable change was found, the correction being -0".17, a change of more than half a second. I shall use this correction for and after the beginning of 1868, as the change is probably due to the introduction of a new constant of refraction in the reduction of the observations for 1868 and subsequent years.

# Cambridge.

An extended series of planetary observations was commenced here by Professor Airy, in 1827. The series was continued by him and Professor Challis, his successor, until 1842. During the first three or four years the combined right ascensions depend on a few special stars, and mainly on  $\alpha^2$  Capricorni. Taking the mean correction to the adopted right ascensions of the stars actually compared as they are given in the introduction to each annual volume, giving to each star a weight proportional to the number of comparisons, the following corrections are deduced:

$$\begin{array}{r}
 1828 & -0^{\circ}.10 \\
 1829-31 & -0.16 \\
 1832-37 & -0.19.
 \end{array}$$

In the introduction to the volume for 1838 it is stated that the adopted right ascensions are diminished by the average amount of  $0^{\circ}.083$ , which would still leave a correction of  $-0^{\circ}.107$ . Actual comparisons in two subsequent years give

1840, 
$$\Delta \alpha = -0$$
\*.087  
1842,  $-0$ .069.

Although the positions deduced from each year's work were adopted for clock correction the year following, without any change of equinox, it seems that there was, effectively, a progressive change of about 0.01 annually in the equinox as adopted.

No declinations were observed until 1830. On comparing the declinations deduced from several years' work with Auwers, it was evident that the correction increased with the polar distance of the star. The law of increase could be well enough represented by supposing the correction proportional to N. P. D. Thus the following corrections were deduced in three different years.

1834, 
$$\delta$$
 dec. =  $-\frac{1".78 \times N. P. D. \text{ in degrees}}{100}$   
1840,  $-\frac{1".00 \times N. P. D. \text{ in degrees}}{100}$   
1842,  $-\frac{1".03 \times N. P. D. \text{ in degrees}}{100}$ 

From which the correction for other years was deduced by interpolation. But, on applying these corrections, the results were found systematically different from those of other observatories, and on referring to Auwers' corrections to Airy's Cambridge Catalogue, it appeared that the mural circle required a large correction near the declination of Uranus during this period. The above results were therefore altered so as to conform as nearly as practicable to Auwers' law.

# Ellinburgh.

In reducing the observations of 1836 Henderson uses the right ascensions of the Tabulæ Regiomontanæ, to which the general correction is at this epoch + \*.007.

But, if we take only the stars near Uranus, with which the latter was necessarily most frequently compared, the corrections will be negative. Comparing the concluded positions of the stars from a Serpentis through  $0^{\rm h}$  to  $\beta$  Orionis, we find the following mean corrections:

In right ascension, 
$$-0^{\circ}.012$$
; in declination,  $-0^{\circ}.09$ .

In subsequent years it is stated that the adopted positions of clock stars used each year are derived from the right ascensions observed at Greenwich, Cambridge, and Edinburgh, during the year or the two years preceding, without any statement whether corrections were applied for difference of equinoxes. In some subsequent years the following corrections are deduced, sometimes from the adopted and sometimes from the concluded positions:

1837, 
$$\Delta \alpha = 0^{\circ}.000$$
;  
1840,  $\Delta a = +0.015$ ;  $\Delta \text{ Dec.} = 0^{\circ}.00$ ;  
1844,  $\Delta \alpha = +0.070$ ;  $\Delta \text{ Dec.} = +0.49$ .

#### Paris.

All the positions of planets given by Le Verrier, in his "Annales de l'Observatoire Imperial de Paris: Observations" depend both in right ascension and N. P. D. on his adopted positions of fundamental stars, the corrections to which have already been given. As the corrections to the individual star places used by Le Verrier are not generally of a systematic character, the general mean correction is employed, which is:—

In right ascension 
$$-0^{\circ}.024 + 0^{\circ}.085 T$$
,  
In declination  $+0^{\circ}.12 + 1^{\circ}.20 T$ ,

T being the fraction of a century after 1800.

In 1854 a new and larger catalogue was introduced, and for this and the following years the correction in declination is derived from Auwers' tables.

A summary of the adopted corrections after 1830, as deduced from the preceding comparisons and discussions, is given in the following table:—

Year.	ear. Greenwich.		Pa	ris.	König	sberg.	Ber	·lin.	Cambridge.		Edinburgh.	
	Δα.	Δδ "	Δα,	Δδ	Δα	Δδ	Δα	Δδ	Δα	Δδ	Δα	Δδ
1830					.00		8	+0.9	16	_1.7	.00	
1831	.00	+1.8	.00	+0.5	02	+0.9		+0.9	16	_1.6		
1832		+1.7			02	+0.9			19	_1.5		
1833		+1.6					04			-1.4		
1834		+1.4					05			-1.3		
1835		+1.2					05			1.2		
1836	04	+1.0	+.01	+0.6	02	+1.0	04	+1.0		-1.0	01	0
1837	03	+0.9					03			0.8	.00	0
1838	04	+0.8					02		11	-0.5	+.01	0
1839		+0.7				+1.0	01		10	-0.3	+.01	0

Year.	Green	wich.	Par	ris.	Königs	sberg.	Ber	lin.	Camb	ridge.	Edinb	urgh.
	Δα	Δδ	Δα	Δδ "	Δα	Δ8	Δα	Δδ	Δα	Δδ	Δα	Δ8
1842	02	+0.4	+.01	+0.6	8		+.03	111	s 07	-0.3	802	100
1843	+.07	+0.4	+.01	+0.6			+.04	$+1.1 \\ +1.1$			+.07	+0.3
1844	+.06	+0.4	+.01	+0.6			+.04	+1.1			+.07	$+0.4 \\ +0.6$
1845	+.08	+0.4	+.01	+0.6			+.04	+1.1	1111		T.01	70.
1846	+.04	+0.4	+.02	+0.6			+.03	+1.1			12.00	
1847	+.05	+0.4	+.02	+06			+.02	+1.1				
1848	+.05	+0.4	+.02	+0.6			+.01	+1.2			BE ST	
849-53	.00	+0.4	+.02	+0.6			.00	+1.2	Sant			
854-55	.00	+0.5	+.02	+0.2			01	+1.2	.00	+0.6		
856-60	01	+0.5	+.02	+0.2							Wash	ingtor
1861	01	+0.4	+.03	+0.2								
862-65	.00	+0.4	+.03	+0.2							.00	_0.
1866	.00	+0.4	+.03	+0.2							.00	+1.
1867	.00	+0.4	+.03	+0.2							.00	+1.
1868	.00	-0.2	+.03	+0.2							.00	+1.
1869	.00	-0.2	+.03	+0.2							.00	+0.
1870	+.01	-0.2									.00	+0.
1871	+.01	-0.2					****				.00	+0.
1872	+.02	-0.2									.00	+0.

Applying the preceding corrections to the positions of the planet as originally reduced and published, we have a series of observed positions as nearly homogeneous as it is possible to make them with the means now at our command. The next step in order will be the computation of the geocentric place of the planet from the provisional theory for the moment of every observation, to be compared with the results of the latter. The complete execution of this labor, ab initio, is, however, at present impracticable, and it is proposed to diminish it by making use of the published comparisons with the older tables. This can be done without danger of serious error, and with all the more ease that owing to the great distance of Uranus the errors of the solar tables are, for the most part, without appreciable effect upon the computed geocentric place of the planet. The method of making the comparison is different with different series of observations, and each series must therefore be described and discussed separately. The general plan, however, has been to replace observed and computed absolute positions by observed and computed corrections to the geocentric positions deduced from Bouvard's Tables. To carry out this plan it is necessary to have at our disposal an ephemeris both of the heliocentric and geocentric positions derived from these tables. The corrections to the latter given by the observations are then given by direct comparison. To obtain the corrections given by the provisional theory, the heliocentric longitudes, latitudes, and radii vectores given by that theory are interpolated to the dates of the heliocentric ephemeris from Bouvard's Tables, and compared with that ephemeris. The differences are then changed to differences of geocentric place by the usual differential formulæ, and thus the corrections given by theory are derived. The difference between the two sets of corrections is the difference May, 1873,

between the provisional theory and observation. A condensed summary of the results for each of the principal series of observations is here presented.

#### Greenwich, 1781-1830.

In Airy's reductions, already referred to, we have given for the moment of each individual observation a heliocentric place computed from Bouvard's Tables, and the geocentric longitudes and latitudes thence deduced. The observed right ascensions and declinations are then changed to longitudes and latitudes, and the apparent error of the tables thence deduced. The means of these errors are taken for groups of observations, and expressed in terms of the errors of heliocentric longitude, radius vector, and latitude. The mode in which these means have been treated is fully shown in the following table. The first column gives the mean date of each individual group of observations. The next three give the mean excesses of the co-ordinates interpolated from the heliocentric ephemeris, p. 100, and corrected for solar nutation, over those printed in the "Computations of tabular place, etc.," in the Greenwich reductions. In the fifth column these corrections are changed to corrections of geocentric longitude. In the next two columns we have the mean corrections to Bouvard's geocentric places given by observation. It is the negative of the mean error of tabular place printed in the "Reductions," corrected by the numbers already given to reduce the star places to a uniform system. Then we have the difference between these two sets of corrections, or, the mean correction to the geocentric place of the provisional theory as given by. observation. Lastly, we have the differential coefficients for expressing the errors of geocentric in terms of the errors of heliocentric co-ordinates taken without change from the Greenwich volume.

Mean Date.	Correct	n Provisi	bular pos	sition in		Observatio rrection to			ction to Theory.	$\frac{\partial l}{\partial \lambda}$	$\frac{\partial l}{\partial \rho}$
•	Long.	Log. R. V.	Lat.	Geoc. long.	Geoc. long.	Hel. lat.	No.of Obs.	Geoc. long.	Hel. lat.		
1781, Oct. 10 Nov. 13 Dec. 27 1782, Jan. 31 Mar. 4 Oct. 10 Nov. 26 1783, Jan. 11 Feb. 24 Oct. 10 Nov. 1 Dec. 15 1784, Jan. 29 Mar. 12 Oct. 30 Dec. 14	7.8 -7.5 -7.3 -7.4 -6.6 -5.6 -5.3 -5.0 -4.4 -3.5 -3.2 -3.3 -3.1 -2.6 -1.8 -1.5	— 159  — 121 	+0.9 +0.9 +0.3 +0.3 +0.2 -0.3 -0.3 -0.4 -0.5 -0.8	- 7.5 - 7.5 - 7.7 - 8.0 - 7:1 - 5.3 - 5.3 - 5.4 - 4 8 - 3.2 - 3.0 - 3.4 - 2.9 - 1.5 - 1.5	- 6.4 - 4.9 - 5.6 - 4.9 - 4.6 - 3.6 - 6.0 - 3.9 - 2.2 - 0.3 - 1.1 - 2.2 - 2.4 - 0.3 - 0.7 - 2.4	$\begin{array}{c} & & \\ & + 2.6 \\ & - 1.6 \\ & - 2.3 \\ & - 1.1 \\ & - 0.6 \\ & - 3.7 \\ & - 2.4 \\ & - 1.0 \\ & - 2.3 \\ & - 3.8 \\ & - 2.4 \\ & - 4.3 \\ & + 1.4 \\ & + 2.7 \\ \end{array}$	4 4 3 3 3 3 2 2 3 3 3 2 2 2 2		$ \begin{vmatrix} " \\ + 1.5 \\ - 2.7 \\ - 3.3 \\ - 2.0 \\ - 1.5 \end{vmatrix} $ $ - 4.4 \\ - 5.3 \\ - 4.0 \\ - 2.6 \\ - 0.7 \\ - 2.0 \\ - 3.4 \\ - 2.0 \\ - 3.8 \\ + 2.2 \\ + 3.6 \end{vmatrix} $	1.01 1.04 1.05 1.02 1.00 1.02 1.05 1.05	9 +1 +6 +9 -9 -5 +3 +9 -10 -9 -3 +5 +9 -9 -4

-		Frot	m Provis	ional The	eory.	From (	Observatio	ns.		102.55		
-	Mean Date.		ion to tal			Cor	rection to			otion to Theory.	$\frac{\partial l}{\partial \lambda}$	$\frac{\partial l}{\partial \rho}$
-		Long.	Log. R. V.	Lat.	Geoc. long.	Geoc. long.	Hel. lat.	No.of Obs.	Geoc. long.	Hel. lat.		1 Sel
A DAVIDAGE AND PROPERTY AND A COMMENCE.	1785, Jan. 16 Feb. 13 Mar. 20 Nov. 8 1788, Mar. 13	$ \begin{array}{c}     '' \\     -1.2 \\     -1.0 \\     -0.6 \\     +0.2 \\     +2.1 \end{array} $		" -1.0 -1.1 -1.1 -1.5 -3.2	-1.3 $-1.3$ $-0.9$ $+0.5$ $+1.8$	$ \begin{array}{c}     " \\     - 1.4 \\     - 1.2 \\     - 2.1 \\     + 1.2 \\     + 4.4 \end{array} $	- 1.4 - 1.1 - 5.2 - 1.7 - 4.9	2 2 2 2 3	-0.1 $+0.1$ $-1.2$ $+0.7$ $+2.6$	$ \begin{array}{r}     '' \\     -0.4 \\     0.0 \\     -4.1 \\ \hline     -0.2 \\     -1.7 \end{array} $	1.05 1.04 1.01 1.02 1.03	
-	Oct. 26 1789, Jan. 18 Apr. 8 Oct. 31	$+3.4 \\ +4.2 \\ +4.7 \\ +4.8$	224 	-3.6 -3.7 -3.8 -4.2	$+3.9 \\ +4.5 \\ +4.2 \\ +5.4$	$+3.0 \\ +10.4 \\ +9.4 \\ +4.7$	-2.2 $-14.5$ $-3.7$ $-1.1$	4 2	-0.9 $(+5.9)$ $+5.2$ $-0.7$	+ 0.1 $+ 3.1$	1.01 1.00	-10 $-1$ $+10$ $-10$
-	Nov. 5 1791, Jan. 29 Apr. 14	+ 5.0	— 254 — 258	-5.0 $-5.2$	+5.2 $+5.8$ $+5.4$ $+4.5$	+3.8 $+5.0$ $+4.5$ $+2.7$	- 2.6 - 2.3 - 3.8 - 4.8	3 3 1	$     \begin{array}{r}       -1.4 \\       \hline       -0.8 \\       -0.9 \\       -1.8     \end{array} $	$   \begin{array}{r}     + 1.8 \\     + 2.5 \\     + 1.2 \\     + 0.4   \end{array} $	1.06 1.00 1.06 1.01	-1 $-10$ $0$ $+10$
Second Miles	Nov. 10 1792, Feb. 5 Nov. 15 1793, Feb. 8	$+5.0 \\ +5.2 \\ +5.6 \\ +5.4$	- 234 	-5.4 $-5.6$ $-6.0$ $-6.1$	+5.6 + 5.5 + 6.2 + 5.7	+5.7 + 4.2 + 3.7 + 8.5	-4.0 $-4.0$ $-2.5$ $-5.0$	2 1 3 2	$+0.1 \\ -1.3 \\ -2.5 \\ +2.8$	+1.4  +1.6  +3.5  +1.1	1.00 1.06 1.00 1.06	-10 0 -10 0
ı	Nov. 14 1794, Feb. 15 Nov. 19	+5.6 + 5.7 + 5.4	- 100		$+5.9 \\ +6.0 \\ +5.6$	$+10.4 \\ +7.3 \\ +4.1$	-6.3 $-6.3$ $-5.1$	1 2 4	$+4.5 \\ +1.3 \\ \hline -1.5$	+0.1 +0.2 +1.6	0.99 1.06 1.00	-10 0 -10
۱	1795, Feb. 20 Nov. 29	+5.9 + 5.4	- 46 - 13	-6.9 -7.0	+6.3 + 5.5	+6.0 + 3.9	- 8.0 - 3.4	3 2		$\frac{-1.1}{+3.6}$	1.06 1.00	0 —10
	1796, Feb. 24 1797, Feb. 27	+ 5.1	+ 62	-7.2 -7.5	+ 5.6 + 5.4	+4.5 + 4.7 + 4.9	- 4.5 - 4.2	3	<u>-1.1</u> <u>-0.7</u>	+ 2.7	1.06	0
•	1800, Mar. 14  1814, May 22 1815, May 25 1818, June 10 1819, June 16 1823, July 1 1825, July 1 1826, July 16 1827, July 20 1828, July 23 1829, Aug. 7 Oct. 4 1830, July 30 Aug. 29 Sept. 20 Oct. 14 Nov. 13	- 0 1 0.0 - 2.4 - 4.5 - 6.6 - 9.8 -13.4 -14.2 -17.8 -18.2 -18.5 -18.9	+ 217 + 214 + 413 + 483 + 538 + 567 + 582 + 626 + 710 + 835 + 865 + 970 + 982 + 1009	$\begin{array}{c} -2.2 \\ -1.5 \\ -0.8 \\ +1.5 \\ +2.2 \\ +4.4 \\ +5.8 \\ +6.6 \\ +7.2 \\ +7.9 \\ +8.5 \\ +8.6 \\ +9.0 \\ +9.1 \\ +9.1 \\ +9.1 \end{array}$	- 0.1 0.0 - 2.5 - 4.7 - 6.9 -10.3 -13.7 -12.5 -18.8 -17.9 -17.2 -16.8	+ 4.9 + 1.1 + 1.4 - 1.1 - 1.4 - 2.6 + 0.2 - 4.8 - 3.6 - 7.2 - 6.9 - 16.3 - 13.0 - 21.4 - 20.0 - 19.1 - 17.3 - 17.8	$\begin{array}{c} -8.7 \\ +0.2 \\ -1.0 \\ +4.8 \\ +3.7 \\ +4.0 \\ +5.0 \\ +7.8 \\ +8.3 \\ +9.6 \\ +6.9 \\ +10.0 \\ +9.9 \\ +11.1 \\ +10.2 \\ +9.1 \\ +9.9 \\ +9.3 \end{array}$	2 4 2 4 2 4 2 4 6 3 14 8 3 5 12 11 8	0.0 +2.4 +2.6 -0.6 -1.0 -2.5 +0.2 -2.3 +1.1 -0.3 +3.4 -2.6 -2.6 -2.1 -1.9 -0.5 -1.0	+ 0.6 + 2.0 + 1.7 + 2.4 - 1.0 + 1.5 + 1.3 + 2.1 + 1.1 0.0 + 0.8	1.06 1.06 1.06 1.06 1.06 1.05 1.05 1.05 1.05 1.05 1.05	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

#### Paris, 1801-1827.

A complete reduction of this series is found in Le Verrier's Annales de l'Observatoire Imperial de Paris, Observations, tome 1. No comparison with any ephemeris is given here, nor is there any complete ephemeris to compare them with. A complete geocentric ephemeris was therefore computed from the provisional theory for the principal groups of the Paris observations. The individual observations being compared with it, the resulting mean corrections are given in the following table:

table.							
Mean date.	$\Delta \alpha$	$\Delta\delta$	N.	Mean date.	$\Delta \alpha$	$\Delta\delta$	N.
1801, March 24,	8.02	+1''.2	2	1813, May 20,	+*.19	+1''.8	6
1802, April 1,	+.08	+0.6	13	1814, May 27,	+.21	+0.8	4
1805, April 22,	+.10	+2.2	13	1815, May 24,	02	+2.2	5
1806, April 17,	<b>—</b> .01	-1.6	5	1816, June 1,	01	+0.8	7
1807, April 28,	+.17	+0.4	16	1817, June 5,	08	+1.6	5
1808, April 28,	+.02	+1.4	6	1818, June 7,	+.12	+2.2	9
1809, May 5,	+.20	+0.1	9	1819, June 18,	07	+1.8	7
1810, April 30,	+.22	+2.6	16	1820, June 20,	20	-2.4	8.5
1811, Febr'y 18,	+.21	+2.2	3	1821, June 22,	+.05	+1.0	5
1811, May 17,	+.14	+2.6	8	1823, July 18,	+.02	+1.8	5
1812, Febr'y 16,	+.28		2	1824, July 13,	+.04	0.0	7
1812, May 10,	+.16	+3.0	6	1827, July 25,	05	+0.6	5
1813, Febr'y 25,	+ .44		3	Tax p= _			
-	-						

Total number of observations in right ascension, 175.

The observations in this series exhibit numbers of discordances of that class which leave the astronomer in doubt whether the observation should be retained or rejected. This remark applies more especially to the declinations. If we determine the probable error of an observation in declination by the condition that it is that amount which the error falls short of as often as it exceeds, it is found to be about 2". Then, if the errors followed the commonly assumed law of probability, only about one in six of the errors should exceed 4", and one in twenty-three 6". But errors of these magnitudes are much more numerous, the deviations often amounting to six or eight seconds. I have rejected only a few in which the discordances approached 10".

## Bessel's Königsberg Observations, 1814–1835.

I have made a complete re-reduction of the right ascensions of this important series, and of most of the declinations. In order to avoid the necessity of applying systematic corrections, Dr. Gould's right ascensions and Dr. Auwers' declinations were used throughout in these reductions. In this work a selection of the fundamental stars observed by Bessel was made for each observation of the planet, to be used for clock error. These were chosen so that the mean of their right ascensions and declinations should be as near as practicable to those of Uranus, a condition, however, which could not generally be fulfilled for the declinations, owing to the southern position of the planet. Bessel's instrumental cor-

rections were applied to his observed times of transit over the mean wire, and the resulting time was employed as that of transit. Each time, compared with the computed right ascension of the star gave a value of the clock correction, which was reduced to the time of transit of the planet by the known daily rate. If the instrumental errors were always accurately determined, the mean of these clock corrections would be used to obtain the right ascension of Uranus. But it was frequently found that the clock error varied systematically with the declination of the star, so that it was deemed advisable to add to the clock correction a term varying as the simple declination, which was deduced from all the stars, and used to reduce the correction to the parallel of Uranus.

It was intended to give the results of this reduction for each observation, but on comparing the results with those of Fleming in the Astronomische Nachrichten, Band 30, it appeared that the results were not materially better than his. It does not, therefore, seem necessary to give more than the mean results for each opposition.

From Bessel's declinations, with the old Cary circle, I was unable to obtain any satisfactory results, owing, apparently, to a want of knowledge of some peculiarity of the instrument. Fleming's reductions were therefore adopted. They are designated by the letter F in the following list.

Mean Corrections to the Provisional Ephemeris given by Bessel's Observations at Königsberg, 1814–1829.

Mean date.	Δα	$\Delta\delta$	N.	Mean date.	Δα	$\Delta\delta$	N.
1814, May 22,	+*.11	+2".5F	9	1822, June 24,	+*.10	+1".8	7
1815, May 25,	+.13	+1.8F	11	1823, July 4,	05	-1.6F	2
1816, May 27,	+.06	+1.2F	11	1824, July 6,	+.01	-1.0F	5
1817, June 6,	+.13	+2.3F	8	1825, July 16,	+.01	-2.4F	5
1818, June 8,	+.02	+4.3F	13	1826, July 18,	01	-3.0F	7
1820, June 21,	+.02	+4.1	4	1828, July 25,	15	-3.5F	7
1821, June 23,	+.12	+1.5	5	1829, Aug. 1,	10	-1.0F	9
	The second secon	The same of the sa					

Total numbers of observations, 103.

Results of Observations at various Observatories, from 1827 to 1829 inclusive.

During these three years we have, besides the observations already quoted, the following:—

- 1. Observations by Schwerd, at Speier, of which the originals are given in Astronomische Beobachtungen angestellt auf der Sternwarte des Königl. Lyzeums in Speyer von F. M. Schwerd, Speyer, 1829-30, and of which the reduced results are found in the Astronomische Nachrichten, Band 8, S. 264.
- 2. The series by Airy, at Cambridge, commenced in 1828, and found in the Cambridge Observations.
- 3. Littrow's Vienna Observations, found in the first series of Annalen der K. K. Sternwarte in Wien.

The mean corrections to the provisional ephemeris given by these series are shown in the following table. The observations have been divided in the usual

way into groups of about a month each, and the mean date and mean correction found for each group. The Paris and Königsberg results are repeated for the sake of clearness. The small figures show, as usual, the number of observations employed in forming the mean.

			$\Delta \alpha$	$\Delta\delta$
	Date.	Observatory.	Original. Corrected.	
1827,	July 22,	Speier,	$-0^{\circ}.16_{\circ} -0^{\circ}.14$	
	July 25,	Paris,	$-0.03_{5} -0.05$	$+0".5_3$
	September 15,	Vienna,	$-0.11_{14} -0.10$	0.014
	October 14,	Vienna,	$-0.18_{s} -0.17$	$-2.2_{6}$
1828,	July 25,	Königsberg,	-0.15, -0.15	$-3.5_{7}$
	July 29,	Vienna,	$-0.24_2 -0.20$	$-1.4_{2}$
	August 14,	Vienna,	$-0.13_{10} -0.09$	+1.1,0
	August 27,	Speier,	$-0.10_{6} -0.09$	and the state of
	September 18,	Vienna,	$-0.03_9 + 0.01$	+1.09
	September 25,	Cambridge,	$-0.05_{6} -0.16$	
	October 17,	Vienna,	$-0.13_{14} -0.09$	0.014
	October 17,	Cambridge,	$-0.02_{10} -0.12$	grießWin
1829,	August 1,	Königsberg,	$-0.10_9$ $-0.10$	<b>—1</b> .0
	August 6,	Cambridge,	$+0.11_8 -0.08$	$-1.1_{17}$
	August 28,	Speier,	$-0.04_{5} -0.04$	17
	September 23,	Cambridge,	$+0.21_{10} +0.05$	
1	November 6,	Cambridge,	$+0.25_6 +0.09$	

### Observations from 1830 to 1872.

Since the year 1830 heliocentric and geocentric ephemerides of Uranus computed from Bouvard's Tables are at our disposal. We make use of those in the Berlin Astronomisches Jahrbuch for the years 1830 to 1833, and of those in the Nautical Almanac from 1834 forward. The system of comparison is the same as that already explained. That is to say, we deduce separately:

- (1) Mean corrections to the geocentric longitude and latitude of Uranus in the ephemeris as derived from observation.
- (2) Mean corrections to the same, given by the provisional theory, as derived from a comparison of the heliocentric positions of that theory with the heliocentric positions in the ephemeris.

Then (1) - (2) is the correction to the provisional theory given by observation. The process of forming (1) and (2) is shown quite fully in the following pages. Each individual printed observation was first compared with the printed ephemeris, and a correction to the latter was thence deduced. When this correction was given with the observations themselves, it was of course not recomputed, unless in some doubtful cases. The observations were then divided into groups, usually of about a month each, and coinciding in time with the grouping of the Greenwich results. The mean of the dates and the mean of the corrections were then taken separately for each group and each observatory. The separate results are shown

in the proper columns of the following table, under the head "Mean dates," Mean cor. in R. A., and Mean cor. in Dec. These means are those given by the observations as printed, without the application of the systematic corrections on pages 120 and 121. In the columns "Corrected mean" these corrections are applied; this column would therefore exhibit no systematic differences between the results of the different observatories, unless the observations of Uranus were affected by errors different from those which affect the positions of the fundamental stars. A careful comparison of the differences in various parts of the table shows that this is unfortunately the case. A weight is next assigned to each individual result depending on the number of observations, the general sufficiency of the data of reduction, the mean discordance of the individual observations, and the quality of the instruments. The critical reader will notice a lack of homogeneity among the weights assigned, of which I shall speak presently. The mean of the separate group-results is then taken with regard to these weights, and also the mean of the mean dates, using for the latter the relative weights adopted for the several right ascensions. Thus, we have a mean result derived from all the observations for each month, or other group-period, which is written under the horizontal lines.

These corrections to right ascension and declination are next changed to corrections of longitude and latitude, using for this purpose the following table, which is computed from the formulæ of Gauss:

$$\cos E = \sin \varepsilon \cos \alpha \sec b = \sin \varepsilon \cos l \sec \delta$$

$$\Delta l = \frac{\sin E \cos \delta}{\cos b} \Delta \alpha + \frac{\cos E}{\cos b} \Delta \delta$$

$$\Delta b = -\cos E \cos \delta \Delta \alpha + \sin E \Delta \delta.$$

The differential coefficients in this table are expressed as a function of the right ascension of Uranus only, which may be done because, owing to the small inclination and great distance of the planet, its geocentric position on the celestial sphere is never more than about 2 from some point of the projection of its heliocentric orbit. The coefficients of  $\Delta \alpha$  are multiplied by 15, that the right ascension may be expressed in time.

		T ERRORS OF RIG	Longia	CUDE A	ND LATI	TUDE.			4 4 -1
		Logarit	thms of			1812-1			
R. A.	$\frac{\partial l}{\partial \alpha}$	$\frac{\partial b}{\partial \alpha}$	$\frac{\partial l}{\partial \delta}$	E E	$\frac{\partial b}{\partial \delta}$	$\frac{\partial l}{\partial \alpha}$	$\frac{\partial b}{\partial a}$	$\frac{\partial l}{\partial \delta}$	$\frac{\partial b}{\partial \delta}$
0h 0m 10 20 30 40 50	1.1386 1.1387 1.1388 1.1389 1.1390 1.1391		+9.6000 +9.5996 +9.5983 +9.5963 +9.5934 +9.5896	- 4 - 13 - 20 - 29 - 38 - 47	9.9626 9.9626 9.9628 9.9632 9.9637 9.9645	+13.8+	-5.97+ 5.96 5.95 5.92 5.87 5.81	+0.40— 0.40 0.40 0.40 0.39 0.38	+0.92+
1 0 10 20 30 40 50	1.1392 1.1393 1.1394 1.1394 1.1395 1.1395	$\begin{array}{c} -0.7588 \\ -0.7525 \\ -0.7451 \\ -0.7365 \\ -0.7270 \\ -0.7162 \\ -0.7162 \\ -118 \end{array}$	+9.5849 +9.5794 +9.5730 +9.5656 +9.5573 +9.5479	- 55 - 64 - 74 - 83 - 94 -104	9.9653 9.9662 9.9673 9.9685 9.9698 9.9711	+13.8+	-5.74+ 5.66 5.56 5.45 5.33 5.20	+0.38- 0.38 0.37 0.37 0.36 0.35	+ 0.92+

		Logari	thms of					
		57	27	1 07	27	0.7	27	0.7
R. A.	$\frac{\partial l}{\partial t}$	$\partial b$	$\frac{\partial l}{\partial s}$	$\frac{\partial b}{\partial S}$	$\frac{\partial l}{\partial a}$	$\frac{\partial b}{\partial a}$	25	36
	дa	дα	28	03	oa	∂α	$\partial \delta$	86
2h 0m	1.1395	-0.7044 -129	+9.5375 —115	9.9725	+13.8+	-5.06+	+0.34-	+0.93-
10	1.1395	-0.0910 1.40	+9.0200 196	9.9740		4.91	0.33	
20	1.1395	-0.6773 155	+9.0104 _130	9.9756		4.75	0.32	
30 40	1.1395 1.1395	0.6450 -168	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9.9772 9.9788		4.58 4.41	0.31	PT A550
50	1.1394	-0.6266 - 184 $-0.6266 - 197$	$\begin{array}{c c} +9.4676 & -167 \\ -181 & -181 \end{array}$	9.9804		4.23	0.30	1
• •	1 1204			0.0001	1.10.01			1000
3 0	1.1394 1.1394	$\begin{array}{c c} -0.6069 & -215 \\ -0.5854 & -225 \end{array}$	+9.4495 $+9.4297$ $-198$	9.9821 9.9837	+13.8+	-4.05+	+0.28-	+0.96-
20	1.1393	0 5001 -400	10 4081 -210	9.9853		3.86 3.66	0.27	
30	1.1393	0.5368 -200	10 3814 -231	9.9869		3.45	0.24	
40	1.1392	-0.5094 -274 $-0.5094 -299$	+9.3586 -208	9.9883		3.24	0.23	
50	1.1391	$-0.4795 \begin{array}{r} -255 \\ -327 \end{array}$	$+9.3302 \frac{-264}{-312}$	9.9898		3.02	0.21	
4 0	1.1390	-0.4468	1.0.2000	9.9912	+13.8+	-2.80+	+0.20-	+0.98-
10	1.1390	_0 4100 -339	19 2644 -346	9.9925	1 2010 1	2.58	0.18	10.00
20	1.1389	-0.3710 $-399$ $-443$	+9.2259 -383	9.9938		2.36	0.17	
30	1.1388	-0.3207 400	+9.1828 -431 $-487$	9.9949	17-71	2.14	0.15	
40 50	1.1387	-0.4109	+9.1341560	9.9959		1.91	0.13	
90	1.1386	$-0.2198 \begin{array}{l} -571 \\ -659 \end{array}$	+9 0781 -651	9.9969	The state of the	1.67	0.12	
5 0	1.1385	-0.1539 0.0752 —786	+9.0130 -777	9.9977	+13.8+	-1.43+	+0.10-	+0.99
10	1.1384	-0.0100	+8.9353 -956	9.9984	1	1.19	0.08	
20	1.1383	-9.919	+8.8397 1940	9.9990		0.95	0.07	
30 40	1.1382 1.1381	-9.034 —175	0. (10 ) THEFF	9.9994	- 120	0.71	0.05	1
50	1.1380	-9.378 $-301$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	9.9997		0.48 0.24	0.03	
				0.0000		0.24	0.02	
6 0	1.1379	- œ	OC	0	+13.7+	0.00	0.00	+1.00-
10 20	1.1378	+9.010 1 201	-0.240 .1 300	9.9999		-0.24+	-0.02+	
30	1.1377 1.1376	+175	97157 +1757	9.9997 9.9994		0.48 0.71	0.03	
40	1.1375	10 070 -124	+1240	9.9990		0.95	0.03	
50	1.1374	+0.0743 + 96 + 783	$-8.9353 + 956 \\ -8.9353 + 777$	9.9984		1.18	0.08	
7 0	1.1373	⊥0 1596	0.0190	9.9977	11971	+1.42-	-0.10+	+0.99-
10	1.1373	100104 +000	0.0501 +001	9.9969	+13.7+	1.65	0.12	70.09-
20	1.1372	1 A 9759 +009	_9 1341 +300	9.9959		1.88	0.13	
30	1.1371	+0.3250 +497	-9.1828 + 487 $-9.2259 + 431$	9.9949		2.11	0.15	
40	1.1371	+0.3692 + 397	-0.2400   305	9.9938		2.34	0.17	
50	1.1370	$\begin{array}{c} +0.3032 \\ +0.4089 \\ +359 \end{array}$	-9.2644 + 346	9.9925		2.56	0.18	
8 0	1.1370	+0.4448 +325	-9.2990 +312	9.9912	+13.7+	+2.78—	-0.20+	+0.98-
10	1.1370	T-0.4113 1.902	-9.3302 1 994	9.9898		3.00	0.21	
20 30	1.1370	+0.00/1 1972	-9.3086 1258	9.9883		3.22	0.23	
40	1.1370 1.1370	+0.5344 $+253$ $+0.5597$ $+253$	-9.3844 $+237$ $-9.4081$ $+237$	9.9869		3.43	0.24	
50	1.1370	1.0 5020 +233	0 4207 +216	9 9837		3.63 3.83	0.26 0.27	30.00
9 0	1.1370	+214	+199					100
10	1.1370	+0.6044 + 197 + 0.6241 + 197	$\frac{-9.4495}{-9.4676}$ +181	9.9821	+15.7+	+4.02-	-0.28+	+0.96-
20	1.1370	10 6495 + 184	-9.4676 $-9.4843$ $+167$	9.9804 9.9788		4.20 4.38	0.29	Miles .
30	1.1371	+0.6594 + 169 + 0.6749 + 155	_9 4995 +192	9.9772		4.55	0.31	
40	1.1371	1/1/3	-9.5134 + 139	9.9756		4.72	0.32	
50	1.1372	+0.6892 + 131	$-9.5260 \begin{array}{l} +126 \\ +115 \end{array}$	9.9740		4.38	0.33	MIL.
0 0	1.1373	⊥0 7023	9 5375	9.9725	+13.7+	+5.04-	-0.34+	+0.93-
10	1.1374	+0.7142 +119	_9 5479 +104	9.9711	1 2011 7	5.18	0.35	3.00
20	1.1375	+0.7251 + 109	-9.5573 + 94	9 9698	2000-	5.31	0.36	
30 40	1.1376 1.1377	TU.1041 _ 87	-9.0000 i 74	9.9685	3 - 3	5.43	0.37	
50	1.1378	$\begin{array}{c} +0.7434 & + & 66 \\ +0.7510 & + & 65 \end{array}$	_9.5794· + 64	9.9673 9.9662		5.54 5.64	0.37 0.38	
1 0		The second secon	+ 99		TAKE L			
1 0	1.1379 1.1380	$+0.7575 \\ +0.7632 + 57$	-9.5849 + 47	9.9653	+13.7+	+5.72-	-0.38+	+0.92
20	1.1381	+0.7678 + 46	$\frac{-9.5896}{-9.5934} + 38$	9.9645		5.79 · 5.85	0.38	
30	1.1382	1 0 7719 + 30 1	-9 5963 + 29	9.9632		6.90	0.39	
40	1.1383	$+0.7737 \pm \frac{24}{17}$	$-9.5983 \pm \frac{20}{13}$	9.9628	100	5.94	0.39	
50	1.1385	+0.7754 + 7	-9.5996 + 13 + 4	9.9626		5.96	0.40	
2 0	1.1386	+0.7761	-9.6000	9.9626	+13.8+	+5.97-	-0.40+	+0.92-

We thus have, for the interval occupied by each group of observations, a mean correction to the geocentric longitude and latitude of the planet given by observations, which are found in the ninth and tenth columns of the table, on the same horizontal line with the mean corrections in right ascension and declination from which they are derived. The next step is to obtain the corresponding corrections given by the provisional ephemeris.

This correction has been first obtained for every twentieth day of each of the forty-two oppositions included in the table. The heliocentric longitude, latitude, and radius vector were interpolated to the most convenient twenty-day intervals, and compared with the corresponding co-ordinates in the heliocentric ephemeris. This ephemeris was of course the one corresponding to that with which the observations were compared, namely, the Berliner Jahrbuch for the years 1830–33, and the Nautical Almanac for subsequent years. These comparisons are fully given at the end of this chapter, and the resulting corrections to the printed ephemeris are given in the proper columns of the table.

These corrections to the heliocentric co-ordinates were then changed to corrections of geocentric longitude and latitude by the following formulæ. Put

r', the projection of the planet's radius vector on the ecliptic;

 $\rho'$ , the projection of the planet's distance from the earth on the same plane;

ρ, this distance itself;

2,8, the planet's heliocentric longitude and latitude;

L, the sun's geocentric longitude;

R, its radius vector;

M, the modulus of the common logarithms;

&, &b, the corrections to the geocentric longitude and latitude;

δρ, the correction to the common logarithm of the radius vector.

Then

$$\begin{split} \delta l &= \frac{r'^2}{\rho'^2} \left\{ 1 + \frac{R}{r'} \cos \left( L - \lambda \right) \right\} \delta \lambda \\ &- \frac{Rr'}{\rho'^2} \sin \left( L - \lambda \right) \frac{\delta \rho}{M \sin 1''} \\ &+ \frac{Rr'}{\rho'^2} \sin \left( L - \lambda \right) \tan \beta \delta \beta \\ \delta b &= \frac{r'}{\rho'} \left\{ 1 + \frac{r'R}{\rho^2} \tan^2 \beta \cos \left( L - \lambda \right) \right\} \delta \beta \\ &- \frac{r'^2 R}{\rho' \rho^2} \tan \beta \sin \left( L - \lambda \right) \delta \lambda \\ &+ \frac{rR^2}{\rho' \rho^2} \left\{ 1 + \frac{r'}{R} \cos \left( L - \lambda \right) \right\} \sin \beta \frac{\delta \rho}{M \sin 1''}. \end{split}$$

The last term in  $\delta l$  and the last two terms of  $\delta b$  have been omitted in the computation, as they scarcely ever exceed a few hundredths of a second.

17 May, 1873.

The values of  $\delta l$  and  $\delta b$  are printed in the last two columns of the table. The formula for  $\delta b$  might have contained the additional term

#### $\delta b = \sin l \delta \omega$

 $\delta\omega$  being the correction to the obliquity of the ecliptic adopted in the ephemeris to reduce it to that employed in the provisional theory. This correction is, however, deferred until we come to form the equations of condition.

From the values of  $\mathcal{E}l$  and  $\mathcal{E}b$  thus obtained we are to find the mean values during each group of observations. If these quantities varied uniformly, the proper value would be that corresponding to the mean date of each group. But the second differences are so large that this value would generally be in error by one- or two-tenths of a second. Owing to the minuteness of this difference, it has been considered that when the mean date was near the middle of a twenty-day interval, the correction  $\mathcal{E}l$  interpolated to that date without regard to second differences would furnish a sufficient approximation to the required mean value of  $\mathcal{E}l$  during an interval of about 30 days. In other case the value of  $\mathcal{E}l$  was interpolated to 5-day intervals through the period of each group of observations, and the mean value taken.

During the years 1850-1863 the sun's longitude employed in the ephemeris required a gradually increasing correction, amounting at the latter date to about 3". A small correction of which the maximum value is about 0",15 was applied to  $\ell l$  to reduce it to the value it would have had if Hansen's tables had been employed.

The corrected mean values of  $\ell l$  and  $\ell b$  thus obtained are given in the last two columns of the following table, being inclosed in brackets and printed immediately above the values of  $\Delta l$  and  $\Delta b$  derived from observation.

I deem it proper to mention that the mechanical labor of constructing these tables of comparisons, in the manner just described, was in great part performed by Dr. C. L. F. Kampf, who was employed by the Smithsonian Institution to assist me in the work. Before using it I subjected the whole of the work to a careful revision, altering especially the relative weights of the corrected means in many cases. As the assigned weights now stand, each set of results which are combined into a single mean has its own unit of weight, which does not necessarily coincide with that of any other set. The use of a uniform scale of weights through this series of observations, and the assignment to every final mean of a weight equal to the sum of the weights of the quantities whose mean was taken, would have led to weights in many cases quite fictitious, owing to the obvious presence of systematic errors in the results. For this reason I have made no further use of the weights found in this table, and their lack of homogeneousness therefore does no harm.

Mean Corrections to the Ephemeris of Uranus in the Berliner Jahrbuch and the Nautical Almanac.

Observatory.		Observed	correcti	ions in R.A.	Observed	correction	ons in Dec.	Corr. to	Geocentri
[R. A. of Uranus.]	Mean dates.	Mean.	No. of obs.	Corrected mean.	Mean.	No. of obs.	Corrected mean.	Longitude.	Latitude
Königsberg, Cambridge,	1830 July 29 July 29	8 —1.56 —1.51	7 6	8 —1.56 <sub>5</sub> —1.67,	+4.6	7	+4.6	"	"
[20 <sup>h</sup> 40 <sup>m</sup> ]	July 29		.::	-1.60				[—19.2] —20.8	[+9.5 + 10.3]
Königsberg, Cambridge,	Aug. 12 Aug. 25	—1.65 —1.36	2 4	$-1.65_{2}$ $-1.52_{2}$	+3.6	2	+3.6	F 10.57	
[20h 36m]	Aug. 19			-1.58				[—18.5] —20.8	+9.5 + 9.1
Cambridge, [20 <sup>h</sup> 37 <sup>m</sup> ]	Sept. 19	-1.46	7	—1.62 <sub>3</sub>	,			[—17.2] —21.2	
Cambridge, [20 <sup>h</sup> 36 <sup>m</sup> ]	Oct. 17	-1.34	8	-1.504				[—16.7] —19.5	
Cambridge, [20 <sup>h</sup> 37 <sup>m</sup> ]	Nov. 14	-1.36	8	-1.524				[—16.6] —19.8	
Greenwich, Cambridge,	1831 Aug. 3 Aug. 8	—1.72 —1.70	11 9	-1.72 <sub>4</sub>	+2.5	11	+4.3		
[20h 58m]	Aug. 6			-1.79				[—23.8] —23.4	[+10.0] $+11.1$
Greenwich, Cambridge,	Sept. 7 Sept. 15	—1.67 —1.60	5 6	-1.67 <sub>s</sub> -1.76 <sub>s</sub>	+3.5	5	+5.3	5 00 07	
[20h 52m]	Sept. 11			-1.72				[—22.0] —22.2	+10.0 $+11.8$
Greenwich, Cambridge,	Nov. 4 Oct. 26	—1.48 —1.54	7 16	-1.48 <sub>4</sub> -1.70 <sub>8</sub>	+3.1	7	+4.9	[—20.7]	
[20h 50m]	Oct. 31			-1.63					+9.8 $+10.8$
Greenwich, Königsberg,	1832 Aug. 9 Aug. 10	-2.02 -2.24	3 3	$-2.02_{2}$ $-2.24_{4}$	+1.7	2	+3.4,		
Cambridge, Vienna,	Aug. 15 Aug. 3	-1.99 $-2.33$	9 3	$-2.18_{8}$ $-2.33_{1}$	+0.2	3	+1.1	[—28.4]	1 10 9
[21h 17m]	Aug. 12			-2.19			+2.5	-29.2 $[-26.9]$	+11.9
Cambridge, [21 <sup>h</sup> 12 <sup>m</sup> ]	Sept. 12	-1.97	10	-2.164				—28.8 —28.8	
Cambridge, Vienna,	Oct. 6 Oct. 12	-1.91 -1.90	13 15	$-2.09_{6}$ $-1.90_{4}$	+1.9	15	+2.8	[—25.8][	110.0
[21h 9m]	Oct. 7			-2.01				-26.6 -26.6	
Cambridge, Vienna,	Nov. 16 Nov. 9	—1.85 —1.89	7 2	$-2.04_{7}$ $-1.89_{1}$	+1.1		+2.0	[—25.2] [	1 10 1
[21h 10m]	Nov. 15			-2.02					$+10.1 \\ +10.5$

	Marie 190	MEAN COL	RRECTIONS	то тп	Е ЕРИЕМЕ	eris of U	RANUS.	—Continu	ued	
	Observatory.		Observed	correction	ons in R.A.	Observed	correcti	ons in Dec.	Corr. to G	eoceutric
	[R. A. of Uranus.]	Mean dates.	Mean.	No. of obs.	Corrected mean.	Mean.	No. of obs.	Corrected mean.	Longitude.	Latitude.
ľ		1833	S		s	"		"	"	11
ł	Greenwich,	Aug. 22	-2.57	7	-2.572	-1.4	7	+0.26		
۱	Königsberg,	Aug. 12	-2.57	5	-2.574	-1.5	5	—1.5 <sub>5</sub>		
ı	Cambridge,	Aug. 15	-2.40	11	$-2.59_{5}$		9-1		[-33.8]	[+10.8]
ı	[21 <sup>h</sup> 32 <sup>m</sup> ]	Aug. 15			-2.58			-0.6	35.6	+10.9
ı	Greenwich,	Sept. 18	-2.33	5	-2.33,	_0.8	4	+0 8,		
l	Cambridge,	Sept. 19	-2.33	10	-2.52	+2.8	11	+1.4		
I	Vienna,	Sept. 11	-2.52	6	-2.56	+2.6	6	+1.2,	[-32.2]	F   10 07
ı	[21 <sup>h</sup> 28 <sup>m</sup> ]	Sept. 18			-2.47			+1.2	-33.4	+12.3
ı		Oct. 11	0.05	4	0.05	1	23/15			THE REAL PROPERTY.
ı	Greenwich, Cambridge,	Oct. 11 Oct. 12	-2.25 $-2.29$	12	$\begin{bmatrix} -2.25_1 \\ -2.48_5 \end{bmatrix}$	$+0.1 \\ +2.2$	13	$+1.7_{4}$ $+0.8_{13}$		10 -
ı	Vienna,	Oct. 14	-2.25 $-2.37$	19	$-2.40_{5}$ $-2.41_{2}$	72.2	10		E 01 07	5
I	[21 <sup>h</sup> 26 <sup>m</sup> ]	Oct. 12			-2.43			+1.0	[—31.2] —33.0	[+10.6] $+11.9$
ı			0.70	-	0.05			0.7		
ı	Cambridge, Vienna,	Nov. 18 Nov. 14	-2.16 $-2.24$	5 4	$-2.35_{3}$ $-2.28_{1}$	+ 1.3	4	0.1	E 00 07	5 . 70 . 7
ı	[21h 26m]	Nov. 16						0.1	$\begin{bmatrix} -30.3 \\ -32.0 \end{bmatrix}$	[+10.3] +10.4
1	[41 20 ]									
1	Cambridge,	1834 Aug. 15	_2.58	11	_2.775	1.3	11	-2.6,,		15/100
ı	Vienna.	Aug. 13	-3.07	4	-3.11	$\frac{-1.5}{-4.4}$	4	$-3.5_{1}$	F 40 07	C
ı	[21h 49m]	Aug. 14			_2.83			-2.7	[-40.6] $-39.7$	[+11.1] +11.3
ı		G 1 10	0.00	-	0.00		_			
ı	Greenwich,	Sept. 10 Sept. 16	-3.00 $-2.66$	5 18	-3.00 <sub>1</sub> $-2.85$ <sub>4</sub>	-4.4 $-1.2$	5 18	$\begin{array}{c c} -3.0_5 \\ -2.5_{18} \end{array}$		
۱	Cambridge,								[-39.0]	
۱	[21 <sup>h</sup> 45 <sup>m</sup> ]	Sept. 13			-2.88			-2.6	-40.5	+11.2
-	Greenwich,	Oct. 14	-2.74	10	-2.74	- 3.1	10	-1.710		
1	Cambridge,	Oct. 16 Oct. 20	-2.68 $-2.75$	16	-2.87,	- 0.8	16	$ \begin{array}{c c} -2.1_{16} \\ -0.4_{1} \end{array} $		1100
1	Vienna,		-2.13	4	-2.80,	1.3	4		[-37.5]	[+10.9]
	[21 <sup>h</sup> 41 <sup>m</sup> ]	Oct. 17			-2.83			1.9	39.5	+11.6
	Cambridge,	Nov. 16	-2.64	9	-2.834	0.7	11	-2.0 <sub>11</sub>		4819
	Vienna,	Nov. 12	-2.53	8	-2.58	_ 2.8	8	-1.94	[-36.7]	[+10.7]
	[21 <sup>h</sup> 41 <sup>m</sup> ]	Nov. 14			-2.77			-2.0	_38.7	+11.3
1	Cambridge,	Dec. 6	-2.71	5	_2.90,	_ 1.2	4	-2.5	3-11	
	Vienna,	Dee. 7	-2.55	1	$-2.59_0^2$	_ 2.1	i	-1.2	F-36 27	[+10.5]
	[21h 43m]	Dec. 7			-2.88			-2.4		+11.5
		1835								
-	Greenwich,	Aug. 17	-3.25	4	_3.25,	_ 6.6	4	-5.4		
1	Königsberg,	Aug. 20	-3.31	11	-3.31 <sub>8</sub>					
	Cambridge,	Ang. 14	-3.28	20	-3.47,	- 4.7	20	-5.920		TO THE
	Vienna,	Aug. 21	-3.30	1	_3.35 <sub>0</sub>	_ 8.8	1	<u>-7.9</u> <sub>1</sub>		[+11.3]
	[22h 4m]	Aug. 17		1	3.39			_5.9	-48.6	+11.8

Cambridge, Vienna,  [22h 1m]  Greenwich, Cambridge,  [21h 57m]  Greenwich, Cambridge,  [21h 57m]	1835 Sept. 15 Sept. 14 Sept. 15 Oct. 10 Oct. 17 Oct. 15 Nov. 27 Nov. 26 Nov. 26 July 22	8 -3.17 -3.303.27 -3.113.21 -3.00	9 9 4 8 6 10	8 -3.36 <sub>4</sub> -3.35 <sub>1</sub> -3.36 -3.27 <sub>2</sub> -3.30 <sub>4</sub> -3.29 -3.21 <sub>4</sub>	Mean.  " - 4.6 - 6.7 6.53 - 4.1	No. of obs.  9 9 4 8	mean.  "  -5.8 <sub>9</sub> -5.8 <sub>2</sub> -5.8  -5.3 <sub>4</sub>	Longitude.  " [—45.8] —48.1	"
Vienna,  [22 <sup>h</sup> 1 <sup>m</sup> ]  Greenwich, Cambridge,  [21 <sup>h</sup> 57 <sup>m</sup> ]  Greenwich, Cambridge,	Sept. 15 Sept. 14 Sept. 15 Oct. 10 Oct. 17 Oct. 15 Nov. 27 Nov. 26 Nov. 26	-3.17 -3.30  -3.27 -3.11  -3.21 -3.00	9  4 8  6 10	$ \begin{array}{r} -3.36_4 \\ -3.35_1 \end{array} $ $ \begin{array}{r} -3.36 \\ -3.27_2 \\ -3.30_4 \end{array} $ $ \begin{array}{r} -3.29 \end{array} $	- 4.6 - 6.7  - 6.53 - 4.1	9 4	-5.8 <sub>9</sub> -5.8 <sub>9</sub> -5.8 -5.3 <sub>4</sub>	[-45.8]	[+11.2]
Vienna,  [22 <sup>h</sup> 1 <sup>m</sup> ]  Greenwich, Cambridge,  [21 <sup>h</sup> 57 <sup>m</sup> ]  Greenwich, Cambridge,	Sept. 14 Sept. 15 Oct. 10 Oct. 17 Oct. 15 Nov. 27 Nov. 26 Nov. 26	-3.30  -3.27 -3.11  -3.21 -3.00	9  4 8  6 10	$     \begin{array}{r}       -3.35_1 \\       -3.36 \\       -3.27_2 \\       -3.30_4 \\       -3.29     \end{array} $	- 6.7 - 6.53 - 4.1	9 4	-5.8 <sub>9</sub> -5.8 -5.3 <sub>4</sub>		
[22 <sup>h</sup> 1 <sup>m</sup> ]  Greenwich, Cambridge,  [21 <sup>h</sup> 57 <sup>m</sup> ]  Greenwich, Cambridge,	Sept. 15 Oct. 10 Oct. 17 Oct. 15 Nov. 27 Nov. 26 Nov. 26	-3.27 -3.11  -3.21 -3.00	4 8  6 10	$ \begin{array}{r} -3.36 \\ -3.27_{2} \\ -3.30_{4} \\ -3.29 \end{array} $	- 6.53 - 4.1	4	-5.8 -5.3 <sub>4</sub>		
Cambridge,  [21 <sup>h</sup> 57 <sup>m</sup> ]  Greenwich, Cambridge,	Oct. 17 Oct. 15 Nov. 27 Nov. 26 Nov. 26	-3.11 -3.21 -3.00	8  6 10	-3.30 <sub>4</sub> -3.29	- 4.1				
[21 <sup>h</sup> 57 <sup>m</sup> ] Greenwich, Cambridge,	Oct. 15  Nov. 27  Nov. 26  Nov. 26  1836	-3.21 -3.00	6 10	-3.29		8	5 9		
Greenwich, Cambridge,	Nov. 27 Nov. 26 Nov. 26	-3.21 -3.00	6 10			F 17 (19)	5.3 <sub>8</sub>	[-44.4]	[+11.1]
Cambridge,	Nov. 26 Nov. 26	-3.00	10	_3.21			-5.3	-46.9	+11.4
	Nov. 26				- 5.6	7 9	-4.4,		
[21 31 ]	1836			-3.194	- 4.5		-5.7 <sub>9</sub>	[-43.0]	
				-3.20			-5.1	-45.6	+11.2
Greenwich,		_3.80	7	-3.84	_10.5	8	9.5.		
Cambridge,	July 25	-3.60	3	-3.89	- 8.9	2	-9.92	[-55.3]	C+11.5
[22h 24m]	July 23			-3.86			-9.6	-56.5	+11.8
Greenwich,	Aug. 24	-3.78	7	-3.82 <sub>s</sub>	- 9.8	8	- 8.8 <sub>8</sub>	No.	
Königsberg, Cambridge,	Aug. 30 Aug. 16	-3.63 -3.78	5 12	$-3.63_4$ $-3.97_5$	_ 9.3	12	-10.3,,	4 1 1	
Edinburgh,	Aug. 19	-4.09	9	-4.10 <sub>3</sub>	- 9.3	7	- 9.3,		
Vienna,	Aug. 20 Aug. 22	-3.77	1	-3.81 <sub>0</sub> -3.87	-12.5	1	-11.5° -9.6	[—54.6] —56.6	[+11.6] $+11.5$
								-50.0	<b>T11.0</b>
Greenwich, Cambridge,	Sept. 13 Sept. 16	-3.77 $-3.70$	7 10	$-3.81_{3}$ $-3.89_{4}$	- 8.8 - 8.4	6	$-7.8_{6}$ $-9.4_{10}$		
Edinburgh,	Sept. 16	-4.01	8	-4.02,	- 8.6	8	-8.6 <sub>8</sub>		
Vienna,	Sept. 15	-3.59	9	-3.63,	-10.4	9		[-53.4]	
[22 <sup>h</sup> 16 <sup>m</sup> ]	Sept. 15			-3.87			-8.8	-56.2	+12.1
Greenwich, Cambridge,	Oct. 12 Oct. 16	-3.67 -3.51	7 12	-3.71 <sub>2</sub>		8	-7.6 <sub>8</sub> -9.5 <sub>11</sub>	300	
Edinburgh,	Oct. 15	-4.05	8	$ \begin{array}{c c} -3.70_{5} \\ -4.06_{2} \end{array} $	<b>—</b> 7.9	4	-7.94	7	
Vienna,	Oct. 11	-3.57	10	-3.61 <sub>1</sub>	-10.2	10	-9.2 <sub>3</sub>	[-51.8]	[+11.3]
[22h 13m]	Oct. 15			-3.77			-8.6	-54.8	+11.7
Greenwich,	Nov. 13	-3.59	11	-3.635	- 9.1	11	-8.1 <sub>11</sub>	Add of	
Cambridge, Edinburgh,	Nov. 13 Nov. 17	-3.37 -3.78	8	$-3.56_4$ $-3.79_2$	<b>—</b> 7.9	7	—8.9 <sub>7</sub>		
Vienna,	Nov. 9	-3.56	3	-3.601	-10.2	3	-9.2 <sub>1</sub>	[-50.6]	[+11.1]
[22h 12m]	Nov. 13			-3.63			-8.5	-52.8	+11.0
Cambridge,	Dec. 12	-3.40	7	-3.59 <sub>s</sub>	- 8.0	7	-9.0,	178	
Edinburgh,	Dec. 12	-3.29	5	-3.30,	- 8.8	3		[-50.0]	
[22h 13m]	Dec. 12			-3.52			-8.9	_51.5	+10.1
Greenwich, [22h 40m]	1837 July 22	-4.23	4	-4.26,	_13.4	4	-12.5	$\begin{bmatrix} -62.9 \\ -63.2 \end{bmatrix}$	+12.0

$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	T		MEA	n Coi	RRECTIONS	то тн	е Ернеме	ris of Up	RANUS.	—Continu	ıed.	
Tranus.     Mean.   No. of   Corrected obs.   Mean.   No. of   Corrected   No. of   Corrected   Mean.   No. of   Corrected   No.		Observatory.			Observed	correction	ous in R.A.	Observed o	correction	ons in Dec.	Corr. to (	deocentric
Greenwich, Cambridge, Edinburgh, Aug. 18			Mean d	lates.	Mean.			Mean.			Longitude.	Latitude.
Cambridge, Edinburgh,   Aug. 18   -4.09   14   -4.28    -12.7   6   -12.7    6   -12.7    7   6   -12.7    7   7   7   7   7   7   7   7   7											"	"
Edinburgh, Paris, Aug. 22 $-4.40$   6 $-4.40$   $-12.7$   6 $-12.7$   6 $-12.7$   7 $-12.$												
Paris, Vienna,   Aug. 14			0							-12.7		
	P	aris,	Aug.	14	-4.34		-4.33	-12.0	10	-11.4		
	V	ienna,	Aug.	25	-4.29	4	$-4.33_{0}$	-12.6	4	-11.6,	F-62.97	Γ±11.77
Königsberg, Cambridge, Cambrid	1	[22 <sup>h</sup> 36 <sup>m</sup> ]	Aug	18	• • • •	• • • •	-4.33	• • • •		-12.5	-64.1	+12.2
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$							$-4.26_{cl}$	-13.4	14	-12.5,		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$							-4.13 <sub>6</sub>	11.0	15	10 5		2-12
Paris, Vienna,   Sept. 18										$-12.7_{14}$	38 115	C COLD
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$					-4.20		-4.19			-11.7,		13713
	V	ienna,				5	-4.15,		5	10 6	F 61 77	C 1 11 67
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	[	[22 <sup>h</sup> 32 <sup>m</sup> ]	Sept.	16			-4.21			-12.3	-62.3	+11.5
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	G	reenwich	Oct.	16	_4 13	11	_4 16	_12.9	11	_12.0		5 77
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$							-4.19	-11.6	11	-12.4,		1.00
	P	aris,					-4.04			-10.6		1000
	V	ienna,	Oct.	18	-4.44	2	<b>-4.47</b> ⅓	-15.5	$^2$	—14.5 <sub>½</sub>	[-59.8]	[+11.4]
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	[22 <sup>h</sup> 28 <sup>m</sup> ]	Oct.	17	••••		_4.16	• • • •		_12.0	-61.5	+11.3
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	G	reenwich,	Nov.	8	_4.10	5	-4.13,		5	—I1.5 <sub>5</sub>	-01	1/3/
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$									3	-13.1,		1 400
										17 0.		1270
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$						20			2			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			Nov.	6		•••	-4.11			- 100	-60.7	+11.3
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$									2			
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$									7	12.4 <sub>7</sub>		100
				- 3			-4.02 <sub>4</sub> -4.31 <sub>1</sub>			19 0.		1-100
Greenwich, Königsberg, Cambridge, Edinburgh, Paris, [22h 51m] Aug. 21 $[22h 51m]$ Aug. 22 $[22h 51m]$ Aug. 23 $[22h 51m]$ Aug. 24 $[22h 51m]$ Aug. 25 $[22h 51m]$ Aug. 26 $[22h 51m]$ Aug. 27 $[22h 51m]$ Aug. 28 $[22h 51m]$ Aug. 29 $[22h 51m]$ Aug. 20 $[22h 51m]$ Aug. 20 $[22h 51m]$ Aug. 20 $[22h 51m]$ Aug. 20 $[22h 51m]$ Aug. 21 $[22h 51m]$ Aug. 21 $[2$		The second	-									
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1	22 28 ]	Dec.	0	• • • •		-4.05		• • • •	-11.0	59.9	+11.1
						- 4	Till 10		191			11-19-1
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		, ,										1 177
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$												7.9
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$												1000
									9		C - 70 97	F 1 11 77
		[22h 51m]	Aug.	21			-4.76			-15.8		+12.3
	G	rcenwich.	Sent.	12	-4.62	8	-4 66	-16.2	8	-15.4.		3000
Cambridge, Sept. 16 $-4.61$   11 $-4.72_5$ $-14.9$   12 $-15.4_{12}$   Edinburgh, Sept. 15 $-4.74$   9 $-4.73_5$ $-15.8$   7 $-15.8_7$	K	önigsberg,	Sept.				_4.67,0		14	-17.5,		3. 13
Edinburgh,   Sept. 15   -4.74   9   -4.73,   -15.8   7   -15.8,			Sept.	16			$-4.72_{5}$	-14.9		$-15.4_{12}$		75 300
										-15.8 <sub>7</sub>		30,000
												0 13 19
Berlin, Sept. 6 $-4.72$ 7 $-4.74\frac{1}{2}$ $-17.5$ 7 $-16.5\frac{1}{3}$ $-70.47$ $-11.5$	В	erlin,									[70.4]	[+11.7]
	1	[22 <sup>h</sup> 47 <sup>m</sup> ]	Sept.	15			-4.70			_16.0		+12.0

[22h 42m] [Solution of the content o		MEAN Co	RRECTIONS	то тн	Е ЕРНЕМИ	eris of U	RANUS.	_Continu	ued.	
Tranus     Mean   No. of   Corrected   No.			Observed	correcti	ons in R.A.	Observed	correcti	ions in Dec.	Corr. to	Geocentric
Greenwich, Oct. 15		Mean dates.	Mean.			Mean.	No. of obs.	Corrected mean.	Longitude.	Latitude
Greenwich, Oct. 15		1838				"		"		
Cambridge, Oct. 16	Greenwich,	Oct. 15		7			7			"
Edinburgh,   Oct. 16	Cambridge,									2 7 5 6 7 7
Vienna, [22h 44m] Oct. 16			-4.56	The second second	-4.55	-15.0	8	-15.0		
Greenwich,   Nov. 9								-15.3,		
Greenwich, Cambridge, Edinburgh, Vienna, Paris, Greenwich, Cambridge, Paris, Aug. 24					1					
Cambridge, Edinburgh, Nov. 15									-69.7	+10.8
Edinburgh,   Nov. 16										
Vienna,   Nov.   7   -4.93   4   -4.95   -18.8   2   -17.3   -15.8	Edinburgh								Append to	
[22\(^h\) 42\(^m\)] Nov. 14  Greenwich,  Dec. 9	Vienna,							_17 2	Barrell Co.	
Greenwich, Cambridge, Pec. 15	[22h 42m]			1	-	1	1	-		
Cambridge, Dec. 15	-		0.00	2 3 4 5 7					-00.0	+10.9
Edinburgh, Dec. 17	Cambridge									
Paris, [22\( \) 43\( \) Dec. 10 \\ \text{1839} \\ Greenwich, \\ Cambridge, \text{Aug. 22} \\ -5.28 \\ Aug. 23 \\ -5.21 \\ 2 \\ -5.21 \\ 2 \\ -5.22 \\ -5.20 \\ -5.22 \\ -5.20 \\ -5.22 \\ -5.20 \\ -7.7 \\ -7.				The second second			7			
[22h 43m] Dec. 10	Paris,				-4.39			-145		N. S. R.M.
Greenwich, Cambridge, Aug. $22$ $-5.28$ $5$ $-5.32$ , $-20.7$ $7$ $-21.0$ , Aug. $24$ $-5.11$ $8$ $-5.22$ , $-20.7$ $7$ $-21.0$ , Aug. $23$ $-5.20$ $3$ $-5.20$ $3$ $-5.19$ , $-5.20$ , $-5.20$ , $-5.20$ , $-5.20$ , $-5.20$ , $-5.20$ , $-5.20$ , $-5.20$ , $-5.20$ , $-5.20$ , $-5.20$ , $-5.20$ , $-5.20$ , $-5.20$ , $-5.20$ , $-5.20$ , $-5.20$ , $-5.20$ , $-79.7$ , $-79$	[22h 43m]	Dec. 10			-				-65.8 $-65.7$	
Cambridge, Aug. 24		1839		1.24		un I I	1 30	- 38	71-61	
Cambridge, Paris, Aug. $24$ $-5.11$ $8$ $-5.22\frac{1}{4}$ $-20.7$ $7$ $-20.1\frac{1}{3}$ Paris, Edinburgh, Aug. $25$ $-5.20$ $3$ $-5.20$ $3$ $-5.20$ $4$ $-5.12$ $2$ $-5.20$ $4$ $-5.20$ $4$ $-5.20$ $4$ $-5.20$ $4$ $-5.22$ $-5.20$ $4$ $-5.22$ $-5.20$ $-79.7$ $-7$	Greenwich,		-5.28	5	-5.32,	-21.3	5	-20.6	MIN !	
Edinburgh, $[23^h \ 6^m]$ Aug. $25$ $-5.21$ $2$ $-5.20_4$ $-5.22$ $-20.7$ $-79.7$ $-7$	Cambridge,							-21.0,		
					-5.19,	-20.7	3	-20.13		
Greenwich, Königsberg, Sept. $10$ —5.14 $12$ —5.18 —21.0 $12$ —20.3 $_{12}$ —20.7 $_{6}$ Sept. $12$ —5.11 $12$ —5.13 —21.7 $12$ —20.7 $_{6}$ Sept. $10$ —5.10 $14$ —5.11 —21.1 $14$ —20.1 $_{7}$ Sept. $10$ —5.10 $14$ —5.11 —5.23 —20.0 $10$ —20.3 $_{10}$ Sept. $14$ —5.23 $10$ —5.22 $_{5}$ —20.7 $10$ —20.1 $_{10}$ Sept. $14$ —5.23 $10$ —5.22 $_{5}$ —20.5 $10$ —20.1 $_{10}$ Sept. $14$ —5.32 $10$ —5.15 $_{5}$ —20.5 $10$ —20.1 $_{10}$ Sept. $17$ —5.32 $10$ —5.15 $_{5}$ —20.5 $10$ —20.1 $_{10}$ Sept. $17$ —5.32 $10$ —5.15 $_{5}$ —20.5 $10$ —20.1 $_{10}$ —78.8 $11.0$ Sept. $17$ —5.32 $10$ —5.15 $_{5}$ —20.8 $11$ —20.3 $11$ —20.1 $_{10}$ —78.8 $11.0$ Sept. $11$ —5.33 $11$ —5.13 —19.2 $11$ —20.3 $11$ —78.8 $11.0$ Sept. $11$ —78.7 $11.0$ Sept. $11$ —78.7 $11.0$ Sept. $11$ —78.7 $11.0$ Sept. $11$ —78.7 $11.0$ Sept. $11.0$ Sept. $11$ —78.7 $11.0$ Sept. $11.0$ Sep				2					[-79.7]	[+11.7]
Königsberg, Berlin, Sept. 12				h Laborator II	Maria Calledon				-79.7	+11.0
Berlin, Cambridge, Paris, Edinburgh, Vienna, Sept. 14								-20.312		
Cambridge, Paris, Edinburgh, Vienna, Sept. 17 $=5.12$ $=5.12$ $=5.12$ $=5.12$ $=5.23$ $=5.22$ $=5.20$ , The sept. 16 $=5.16$ $=5.16$ $=5.16$ $=5.16$ $=5.16$ $=5.16$ $=5.16$ $=5.16$ $=5.16$ $=5.32$ $=5.33$				1 - 2 - 1 - 1				-20.76		
Paris, Edinburgh, Vienna, Sept. $14$ $-5.23$ $10$ $-5.22_5$ $-20.7$ $10$ $-20.1_{10}$ $-20.1_{1$								-20.1 <sub>7</sub>		
Edinburgh, Vienna, Sept. $16$ Sept. $17$ Sept. $16$ Sept. $17$ Sept. $17$ Sept. $14$ Sept. $17$ Sept. $14$ Sept. $15$ Sept. $14$ Sept. $15$ Se	Paris,						10	-20.1.		
Vienna, Sept. 17	Edinburgh,			100000000000000000000000000000000000000	-5.15		5	-20.5	Self I	
	Vienna,	Sept. 17	-5.32	9	-5.33		9	-19.8	70.07	1 11 67
Cambridge, Cambridge, Cot. 15					-5.17					+11.0
Cambridge, Oct. 15	Greenwich,		-5.18	5	_5.22	-20.2	5	-19.5		
Vienna, Oct. 10	Cambridge,			8	-5.18					
[22h 59m] Oct. 14				-			8	-19.98	BE - 1 3	
	vienna,	Oct. 10	-5.17	13	-5.18,	-20.5	13	-19.54	-77.47	+11.57
	[22h 59m]	Oct. 14			-5.18			-19.6		
Paris, Paris, Nov. 9	Freenwich,			6	-5.02,	-20.2	6.	-19.5		
Edinburgh, Nov. 11 $-4.90$ 3 $-4.89_1$ $-18.3$ 1 $-18.3_1$ $-18.3_2$ $-75.7$					A 1					
					A STATE OF THE PARTY OF THE PAR					
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				37.79	-		-			
Cambridge, Dec. 15 $-4.83$ 5 $-4.94\frac{1}{2}$ $-19.1$ 2 $-19.4\frac{1}{2}$ Paris, Dec. 3 $-4.90$ 3 $-4.89\frac{1}{2}$ $-17.8$ 3 $-17.2\frac{1}{3}$ Edinburgh, Dec. 28 $-4.96$ 4 $-4.95\frac{1}{4}$ $-18.5$ 3 $-18.5\frac{1}{3}$ [-73.9] [+11.0]		Autor State of the last		1000	STAR STAR		The same of		-15.1	+.10.4
Paris, Dec. 3 $-4.90$ 3 $-4.89$ $-17.8$ 3 $-17.2$ $-18.5$ 3 $-18.5$									Visit I	
Edinburgh, Dec. 28 -4.96 4 -4.95, -18.5 3 -18.5 <sub>s</sub> [-73.9] [+11.0]	Paris,						3	-17.2	Telle	
	Edinburgh,			CONTRACTOR OF THE PARTY				_18.5	72.07	111 07
	[22h 57m]	Dec. 12			_4.92			_18.2	-74.6	+11.0 $+11.2$

	MEAN Co	RRECTIONS	то тн	е Ернеме	eris of Up	RANUS	—Continu	ued.	
Observatory.		Observed of	orrection	ons in R. A.	Observed	correcti	ons in Dec.	Corr. to	Geocentric
[R. A. of Uranus.]	Mean dates.	Mean.	No. of obs.	Corrected mean.	Mean.	No. of obs.	Corrected meau.	Longitude.	Latitude.
	1840	8		s	"		"	"	"
Greenwich, Cambridge,	Aug. 14 Aug. 14	-5.77 -5.64	11	$-5.81_{3}$ $-5.73_{4}$	-24.5 $-25.0$	11	$ \begin{array}{c c} -23.9_{11} \\ -25.2_{1} \end{array} $		36 114
Edinburgh,	Aug. 31	<u>-5.65</u>	1	-5.64	-23.8	1	$-23.2_1$ $-23.7_1$	F 05 07	
[23 <sup>h</sup> 20 <sup>m</sup> ]	Aug. 16			-5.78			-23.9	[—87.9] —88.8	$\begin{bmatrix} +11.4 \\ +11.9 \end{bmatrix}$
Greenwich,	Sept. 15	5.66	8	-5.70,	-24.0	8	-23.4	100	
Königsberg,	Sept. 13	_5.74	6	-5.76	25.1	6	$-24.1_{3}^{8}$		
Cambridge,	Sept. 12	-5.43	1 13	-5.52	94.6	9	04.5		
Edinburgh, Paris,	Sept. 16 Sept. 6	-5.70 -5.60	4	-5.69 $-5.59$	-24.6 $-23.6$	4	$-24.5_9$ $-23.0_4$		
Berlin,	Sept. 14	-5.45	2	-5.451	-26.3	2	-25.3		
Vienna,	Sept. 9	-5.76	2	$-5.76_{1}$	-22.2	2	-21.2	[-87.6]	[+11.5]
[23 <sup>h</sup> 18 <sup>m</sup> ]	Sept. 13			-5.69			-23.8	-87.5	+11.4
Greenwich,	Oct. 10	5.61	9	-5.65 <sub>3</sub>	-24.5	9	-23.9 <sub>9</sub>		
Cambridge,	Oct. 9	-5.49	5	$-5.58_{2}$	-23.5	5	-23.75		TO SER
Edinburgh, Paris,	Oct. 15 Oct. 11	-5.64 -5.60	12	$-5.63_{3}$ $-5.59_{3}$	-23.3 $-23.3$	10	$-23.2_{10}$ $-22.7$		3, 3 (1)
Berlin,	Oct. 27	-5.50	1	$-5.50_{1}$	-22.8	1	-21.8.		-
Vienna,	Oct. 19	<b>—</b> 5.76	5	$-5.76_{\frac{1}{4}}$	-22.5	4	-21.5	[—85.8]	Γ±11 47
[23 <sup>h</sup> 14 <sup>m</sup> ]	Oct. 12			-5.62			-23.3	—86.3	+11.2
Greenwich,	Nov. 6	_5.58	7	-5.62	-23.5	6	-22.9		
Cambridge,	Nov. 3	-5.34	2	-5.43	-24.2	1	$-24.4_{1}$		- 120
Edinburgh, Paris,	Nov. 17 Nov. 4	5.41 5.52	8 2	$-5.40_{g}$ $-5.51$	-22.9 $-26.1$	1 2	$-22.8_{1}$ $-25.5_{2}$		
Vienna,	Nov. 15	-5.42	6	$-5.42_1$	-23.2	6	99.9	5 00 53	5 . 11 07
[23 <sup>h</sup> 12 <sup>m</sup> ]	Nov. 9			_5.48			-23.3	[—83.7] —84.4	+10.3
Greenwich,	Dec. 3	-5.36	8	-5.40,	-23.5	9	-22.9	1 200	-
Cambridge,	Dec. 3	-5.38	2	$-5.47_1$	-22.5	2	-22.7		1000
Edinburgh, Vienna,	Dec. 15 Dec. 4	-5.49 -5.50	3	-5.48 <sub>1</sub>	-22.6	2	$-22.5_{2}$		
[23 <sup>h</sup> 12 <sup>m</sup> ]	Dec. 6		•••	-5.44			_22.8	[—82.2] —83.7	[+11.0] +10.4
ALC: NO.	1841				=  -8-		- 192	SEC. 111	
Greenwich,	Aug. 20	-6.16	5	-6.202	-28.6	5	-28.15	# Pos	111111
Paris,	Aug. 19	-6.14	2	$-6.13_{1}$	-29.6	2	<u>-29.0</u> <sub>2</sub>	[—96.9]	
[23h 37m]	Aug. 20	••••	•••	-6.18		• • •	-28.3	<del>96.2</del>	+10.6
Greenwich,	Sept. 11	-6.16	10	-6.204	-29.0	10	$-28.5_{10}$	-31 (2)	- 198 10
Königsberg, Berlin,	Sept. 11 Sept. 14	-6.18 $-6.14$	5 7	-6.18 $-6.14$	-30.1 $-29.6$	5 7	$-29.1_{2}$ $-28.6_{3}$	EDS TO	-
Edinburgh,	Sept. 17	-6.11	7	$-6.15_{2}$	-28.2	5	$-28.0_{5}^{3}$		1 S 1 S 1 S
Paris,	Sept. 14	-6.16	5	$-6.15_{3}$	-29.0	3	$-28.4_{3}$	27t 15	5 7
Vienna,	Sept. 17	-6.37	11	<u>-6.37</u> <sub>1</sub>	-30.3	11	29.3 <sub>8</sub>	[—96.5]	[+11.4]
[23 <sup>h</sup> 33 <sup>m</sup> ]	Sept. 13			-6.18		• • •	-28.5	-96.3	+10.4
									44-1

2	MEAN Co	RRECTIONS	то тн	Е ЕРНЕМЕ	RIS OF U	LANUS.	—Continu	red.	
Observator		Observed	correcti	ons in R.A.	Observed	correction	ons in Dec.	Corr. to (	deocentric
[R. A. of Uranus.]	Mean dates.	Mean.	No. of obs.	Corrected mean.	Mean.	No. of obs.	Corrected mean.	Longitude.	Latitude.
	1841	S		8	"		"	"	"
Greenwich		-6.09	7	-6.13,	-28.2	7	-27.7		STATE OF THE PARTY OF
Berlin, Edinburgh	Oct. 20 Oct. 13	-5.87 -6.00	2 4	-5.87 <sub>1</sub> -6.04 <sub>1</sub>	$-28.2 \\ -27.2$	2 4	$-27.2_{1}$ $-27.0_{4}$		
Paris,	Oct. 21	-6.10	1	-6.09,	-27.2	1	-26.6		to the
Vienna,	Oct. 16	-6.14	9	-6.14	-28.8	9	-27.8	[-94.6]	F 1 11 97
[23h 28m]	Oct. 18			-6.06			-27.4	—94.1	+10.5
Greenwich	Nov. 17	-5.95	5	-5.99,	-28.0	. 5	-27.5		
Berlin,	Nov. 16	-6.15	2	-6.15,	-28.4	2	-27.4	27	
Edinburgh Vienna,	Nov. 2 Nov. 11	-5.89	3	-5.93,	-26.5	4	-26.3 <sub>4</sub> -29.0,		
		-5.98	4	-5.98	-30.0	4	-	[-92.6]	[+11.0]
[23h 26m]				-6.01			-27.2	-93.3	+10.4
Greenwich		-5.86	-8	-5.90,		8	-26.9 <sub>8</sub>		
Berlin, Edinburgh	Dec. 15 Dec. 20	-5.60 -5.68	3 4	$-5.60_1$ $-5.73_1$	-25.5	3	-24.52		
Paris,	Dec. 15	-5.78	4	$-5.77_{9}$	-26.7	4	-26.14		F
[23h 26m]	Dec. 16			_5.78			-26.3	[—90.5] —89.9	[+10.7] + 9.8
	1842								
Greenwich.		-6.62	5	-6.64,	_32.1	6	-31.7		
Cambridge		-6.48	2	-6.55	-32.7	2	-33.0	[—105.6]	C + 11 13
[23h 51m]	Aug. 21			-6.61			_32.0	_103.6	+10.0
Greenwich,	Sept. 12	-6.55	4	-6.57,	-32.2	4	_31.8,		12 1023
Königsberg		-6.69	10	-6.69,	-33.4	10	-32.4		*
Berlin,	Sept. 11	-6.70	3	-6.69	-31.7	3	-30.71		the same
Paris, Cambridge	Sept. 14	-6.65 -6.60	5 13	$-6.64_{3}$ $-6.67_{6}$	-32.1 $-31.9$	5 14	$-31.5_{5}$ $-32.2_{4}$		
Edinburgh		-6.57	4	-6.59	-31.9 $-30.9$	4	-30.6	Same of	
Pulkowa,	Sept. 17	-6.63	6	-6.64				Control 1	
Vienna,	Sept. 19	-6.81	2	-6.80 <sub>4</sub>	33.5	2	32.54	[-105.4]	[+11.27]
[23h 47m]	Sept. 16			-6.66			-32.0	-104.3	+10.3
Greenwich,		-6.66	12	-6.68	_31.8	12	-31.419		
Berlin,	Oct. 23	-6.54	4	-6.53	-30.7	4	-29.7		tana.
Paris, Cambridge	Oct. 17 Oct. 17	-6.64 -6.60	12	$-6.63_{6}$ $-6.67_{5}$	-31.5 $-31.4$	9	$-30.9_{9}$ $-31.7_{10}$	-	Make S
Edinburgh		-6.57	12	-6.59	_31.1	8	$-30.8_{\rm s}$		
Vienna,	Oct. 10	-6.74	4	-6.73	-34.6	5	-33,61	[—103.6]	[+11.07
[23h 44m]	Oct. 17			-6.64			-31.2	-103.7	+10.9
Greenwich	Nov. 23	-6.36	7	-6.38,	31.0	7	-30.6,		
Berlin,	Nov. 8	-6.42	2	-6.41	-30.2	2	-29.2		
Cambridge		-6.40	7 3	-6.47 <sub>3</sub>	_30.7	7	-31.0,		T. Carlo
Edinburgh Vienna,	Nov. 16 Nov. 20	-6.39 -6.39	3	$-6.32_1$ $-6.38_1$	-30.0	2	-29.04	5 100.03	C . 10 07
[23h 42m]	-						-30.6	$\begin{bmatrix} -100.8 \\ -100.2 \end{bmatrix}$	[+10.8] +10.0
[25" 42"]	Nov. 19			-6.41				100.2	710.0
							1		

	MEAN CO	RRECTIONS	то тн	е Ернеми	eris of Ui	RANUS.	— Contini	ied.	
Observatory.		Observed c	orrection	ons in R.A.	Observed	correcti	ons in Dec.	Corr. to G	leocentric
[R. A. of Uranus.]	Mean dates.	Mean.	No. of obs.	Corrected mean.	Mean.	No. of obs.	Corrected mean.	Longitude.	Latitude.
	1842	8		8	"		"	"	//
Greenwich,	Dec. 16	-6.31	8	-6.33 <sub>8</sub>	-30.2	8	$-29.8_{8}$		
Berlin,	Dec. 10	-6.16	4	-6.15	-31.4	4 5	$-30.4_{9}$ $-30.3_{5}$		4-1-6-1
Paris, Cambridge,	Dec. 14 Dec. 16	-6.23 $-6.22$	5 9	$ \begin{array}{c c} -6.22_{3} \\ -6.29_{4} \end{array} $	-30.9 -30.1	8	$-30.3_{5}$ $-30.4_{8}$		
Edinburgh,	Dec. 13	-6.25	2	$-6.18_{\frac{1}{4}}$	-50.1				TOTAL B
Pulkowa,	Dec. 13	-6.28	3	_6,282				r 00.03	F + 10 *7
[23 <sup>b</sup> 41 <sup>m</sup> ]	Dec. 15			-6.27			30.2	$\begin{bmatrix} - 98.9 \\ - 98.2 \end{bmatrix}$	+9.6
10 80								C 05 73	F 1 10 07
Edinburgh,	1843 Jan. 9	6.32	7	-6.25	-31.4	4	31.0	$\begin{bmatrix} -97.5 \\ -98.2 \end{bmatrix}$	+8.6
							24 5		200
Greenwich, Paris,	Aug. 20 Aug. 21	-7.11 -7.20	7 3	$-7.04_{3}$ $-7.19_{3}$	-35.1 $-37.5$	7 5	$-34.7_7$ $-37.1_5$	[—114.3]	[_L10 77
[0 <sup>h</sup> 6 <sup>m</sup> ]	Aug. 20			-7.10			-35.7	_111.9	
G	Cont 17	<b>—</b> 7.23	9	<b>—7.16</b> ,	-35.4	9	-35.0,		220
Greenwich, Paris,	Sept. 17 Sept. 15		11	$-7.16_{6}$		14	$-36.2_{14}$		
Edinburgh,	Sept. 18	_7.26	7	$-7.19_{2}^{6}$	<del>-36.8</del>	5	$-36.4_{5}$		1173
Pulkowa,	Sept. 22	-7.18	10	-7.18 <sub>10</sub>				C 11411	E + 10 e 7
[0h 3m]	Sept. 19			_7.17			<b>—</b> 35.8	[—114.1] —112.9	+10.6 $+10.0$
									-
Greenwich,	Oct. 18	-7.10	10	—7.03 <sub>3</sub>	-35.3	10	-34.9 <sub>10</sub>		
Paris,	Oct. 17	-7.07	$\frac{6}{12}$	-7.06 <sub>3</sub>	-37.1	5 5	$-36.5_{5}$ $-34.7_{5}$		118
Edinburgh,	Oct. 17	-7.05	12	-6.98 <sub>3</sub>	-35.1	3	-54.1 <sub>5</sub>	[—112.6]	[+10.5]
[23 <sup>h</sup> 59 <sup>m</sup> ]	Oct. 17		• • •	-7.02		• • •	-35.2	-110.6	+ 9.6
Greenwich,	Nov. 20	-7.01	9	-6.94	-34.3	9	-33.9		31111
Königsberg,	Nov. 11	-6.84	5	-6.83	-34.4	5	-33.4,		1600
Paris,	Nov. 15	-7.03	3	-7.02	-36.3	3	-35.7.		NO THE
Edinburgh,	Nov. 15	-6.93	8	-6.86	-35.7	6	-35.3°	[-110.17	Γ±10.47
[23 <sup>h</sup> 56 <sup>m</sup> ]	Nov. 15			-6.90			34.5	-108.6	
REAL TERMS	1844								Ser Day
Greenwich,	Jan. 3	-6.70	3	-6.64,	-34.1	3	_33.73		THE
Edinburgh,	Jan. 10	-6.67	6	-6.60	-01.1		-00.13		1110
Paris.	Jan. 3	-6.72	2	-6.71	-35.5	2	-34.92	C 10013	C 1 0 07
[23h 56m]	Jan. 7		• • • •	-6.64			_34.2	[—106.1] —105.0	[+9.9] + 8.2
	Ana 10	F F0	10	<b>L</b> 01	000	7.0	00.0		SIGN
Greenwich,	Aug. 19 Aug. 17	-7.73	10	-7.67 <sub>3</sub>	-39.6	10	$-39.2_{10}$		THE THE
Paris,		-7.70	3	<del>-7.69</del> ,	40.0	3	39.4 <sub>3</sub>	[-122.3]	
「Oh 22m]	Aug. 18			<b>—7.68</b>			-39.2	_121.2	+ 9.6
Greenwich,	Sept. 25	-7.74	11	-7.68	-39.9	11	-39.5 <sub>11</sub>		-1-0-
Edinburgh,	Sept. 19	-7.67	11	$-7.60_{3}$	-40.3	10	$-39.8_{10}$		9875
Königsberg,	Sept. 17	-7.65	10	-7.64,	-40.7	10	-39.7		
Paris,	Sept. 10	7.63	10	$-7.62_{5}$	-39.4	15	$-38.8_{15}$	[—122.6]	
[0 <sup>h</sup> 18 <sup>m</sup> ]	Sept. 17	••••	• • •	<b>—</b> 7.63		•••	-39.3	→120.6	+ 9.3
			ate l	THE REAL PROPERTY.					1120
						1			

	MEAN COL	RRECTIONS	то тн	Е ЕРНЕМЕ	E EPHEMERIS OF URANUS.—Continued.				
Observatory.	lay to a	Observed	correction	ons in R.A.	Observed c	orrecti	ons in Dec.	Corr. to G	eocentrio
[R. A. of Uranus.]	Mean dates.	Mean.	No. of obs.	Corrected mean.	Mean.	No.of obs.	Corrected mean.	Longitude.	Latitude.
	1844	8		s	"		"	"	"
Greenwich, Edinburgh,	Oct. 17 Oct. 13	-7.70 -7.58	9	$-7.64_{a}$ $-7.51_{2}$	-39.2 -40.5	9	$-38.8_9$ $-40.0_1$	[—121.5]	Γ±10.27
[0 <sup>h</sup> 15 <sup>m</sup> ]	Oct. 15			-7.59			39.0	-120.0	+ 9.4
Greenwich, Edinburgh,	Nov. 26 Nov. 19	-7.44 -7.41	9 7	-7.38 <sub>3</sub> -7.35 <sub>2</sub>	_38.7	9	—38.3 <sub>9</sub>	[—118.2]	Γ± 9.97
[0 <sup>h</sup> 12 <sup>m</sup> ]	Nov. 23			-7.37			-38.3		+ 8.8
Edinburgh, Paris,	Dec. 18 Dec. 22	-7.24 -7.10	5 2	-7.18 <sub>1</sub> -7.09 <sub>1</sub>	_39.3	3	<b>—38.7</b> <sub>3</sub>	[—115.7]	Γ± 9.67
[0 <sup>h</sup> 10 <sup>m</sup> ]	Dec. 20			-7.14		10	-38.7	_113.7	+ 7.1
1	1845						00.0		and Fifth to
Greenwich, Edinburgh,	Jan. 13 Jan. 14	-7.18 -7.16	8	$-7.10_1$ $-7.08_4$	-38.4	1	-38.0	[—114.0]	[± 9.5]
[0 <sup>h</sup> 11 <sup>m</sup> ]	Jan. 14		***	-7.08			-38.0	_112.5	+ 7.3
Greenwich,	Aug. 25	-8.25	5.	8.17,	-42.7	6	-42.3	[—131.0] —129.1	[+ 9.6] + 9.2
Greenwich, Königsberg,	Sept. 18 Sept. 30	-8.21 -8.16	10 5	-8.13, -8.15,		10 5	$-42.2_{10}$ $-42.4_{10}$		in move Sir
Paris,	Sept. 14	-8.24	5	-8.23°		3	-43.3 <sub>3</sub>	[—131 6]	[+ 9.9]
[0h 33m]	Sept. 22			-8.17		••	-42.5	-129.2	+ 9.1
Greenwich, Paris,	Oct. 17 Oct. 20	-8.22 -8.01	10 6	-8.14 <sub>4</sub> -8.00 <sub>3</sub>		10 6	$-41.8_{10}$ $-43.1_{6}$	[-130.2]	[+ 9.8]
[0h 29m]	Oct. 18			-8.08	·		-42.3	128.0	+ 8.9
Greenwich, [0 <sup>h</sup> 27 <sup>m</sup> ]	Nov. 9	-8.06	6	—7.98 	<b>—43.3</b>	7	<del>-42.9</del>	[—128.4] —126.9	[ + 9.6] $[ + 7.9 ]$
Greenwich, [0h 25m]	Dec. 14	<u>-7.85</u>	8	<u>-7.77</u>	<b>—49.2</b>	8	<del>-39.8</del>	[—124.8] —122.8	[+ 9.3] + 9.6
	1846	12 - 11		THE SE	中	1383	- 1		
Greenwich, Paris,	Sept. 8 Sept. 12	-8.80 -8.73	8 19	$-8.76_{3}$ $-8.72_{10}$		8 14	-45.8 <sub>8</sub> -46.3 <sub>14</sub>	[—139.9]	[+ 9.2]
[0h 50m]	Sept. 11			-8.73			-46.1	-138.2	+ 8.3
Greenwich, Königsberg,	Oct. 8 Oct. 4 Oct. 14	-8.74 -8.61 -8.69	7 11 13	-8.70 <sub>s</sub> -8.61 <sub>s</sub> -8.68 <sub>7</sub>	-44.8	7 11 13	-46.4 <sub>7</sub> -43.8 <sub>6</sub> -46.1 <sub>13</sub>		
Paris,	Oct. 14	-0.03		<del>-8.65</del>	-10.1		-45.8	[—139.7] —137.1	[+ 9.2] + 8.3
Greenwich, Paris,	Nov. 10 Nov. 16	-8.62 -8.48	6 9	-8.58 <sub>2</sub> -8.47 <sub>5</sub>	-46.8	6 9	-46.4 <sub>6</sub> -45.8 <sub>9</sub>	[—136.8]	Γ± 9.07
[0h 41m]	Nov. 14			-8.50			-46.0	-135.1	+ 7.6

		Observed	correction	ons in R.A.	Observed o	orrect	ions in Dec.	Corr. to G	eccentric
Observatory. [R. A. of Uranus.]	Mean dates.	Mean.	No. of obs.	Corrected meau.	Mean.	No.of obs.	Corrected mean.	Longitude.	Latitude.
Greenwich,	1846 Dec. 15	s 8.31	9	s -8.27 <sub>s</sub>		10		"	"
Paris, [0 <sup>h</sup> 39 <sup>m</sup> ]	Dec. 16	8.25	6	$-8.24_{3}$ $-8.26$	-46.1	4	$-45.5_{4}^{10}$ $-45.6$	[—134.5] —131.7	[+8.9] +6.5
Greenwich, Paris,	1847 Jan. 13 Jan. 11	-8.25 -8.14	4 6	$-8.20_{2}$ $-8.12_{3}$	—43.1 —45.4	6	-42.7 <sub>4</sub> -44.8 <sub>6</sub>	[—130.9]	[+8.6]
[0 <sup>h</sup> 40 <sup>m</sup> ]	Jan. 12			-8.15			-44.0	-129.6	+7.4
Greenwich, [1 <sup>h</sup> 6 <sup>m</sup> ]	Sept. 3	-9.21	8	-9.16	—49.4 ····	8	—49.0 ····	$\begin{bmatrix} -148.4 \\ -144.9 \end{bmatrix}$	[+8.7] +6.8
Greenwich, Paris,	Oct. 1 Oct. 12	-9.25 $-9.23$	6 18	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	-49.0 -49.2	6	$\begin{array}{r} -48.6_{6} \\ -48.6_{16} \end{array}$	[-148.0]	[+8.7]
[1 <sup>h</sup> 2 <sup>m</sup> ]	Oet. 10			-9.21			-10.0	-145.5	+7.8
Greenwich, Paris,	Nov. 3 Nov. 12	-9.10 $-9.08$	9	$ \begin{array}{c} -9.05_{3} \\ -9.06_{5} \end{array} $	-49.2 $-49.3$	9	$-48.8_{9}$ $-48.7_{9}$	[—146.2]	[+8.5]
[0 <sup>h</sup> 57 <sup>m</sup> ]	Nov. 8			-9.06			-48.8	-142.6	+7.2
Greenwich, Paris,	Dec. 3 •Dec. 12	-8.96 -8.84	9	$ \begin{array}{c c} -8.91_{2} \\ -8.82_{5} \end{array} $	-49.0 $-48.5$	7 7	-48.6, -47.9,	[—143.0]	
[0 <sup>h</sup> 54 <sup>m</sup> ]	Dec. 9		~	8.85	••••		-48.2	-140.6	+6.8
Greenwich, Paris,	Jan. 10 Jan. 11	—8.83 —8.53	5	$     \begin{array}{r}       -8.78_{2} \\       -8.51_{6}    \end{array} $	-47.1 $-47.6$	5	$-46.7_{2}$ $-47.0_{5}$	[—139.4]	[+8.1]
[0 <sup>h</sup> 54 <sup>m</sup> ]	Jan. 11			-8.57			-46.9	-136.2	+6.0
Greenwich, Paris,	Sept. 8 Sept. 22	-9.84 $-9.82$	11	$-9.79_{r}$ $-9.80_{n}$	—51.1 —51.5	7 9	$-50.7, \\ -50.9_{g}$	[—156.4]	[+8.0]
[1 <sup>h</sup> 19 <sup>m</sup> ]	Sept. 17			-9.80			-50.8	-154.1	+7.5
Greenwieh, Paris,	Oet. 19 Oct. 16	-9.82 $-9.79$	7	$\begin{array}{c c} -9.77, \\ -9.77, \\ \end{array}$	$-52.2 \\ -52.2$	7 10	51.8 <sub>7</sub> 51.6 <sub>10</sub>	[—156.4]	[+8.0]
[1 <sup>h</sup> 15 <sup>m</sup> ]	Oet. 17			—9.77			-51.7	—154.2	+6.9
Greenwich, Paris,	Nov. 13 Nov. 13	-9.68 $-9.55$	7 4	$-9.63_{7}$ $-9.53_{4}$	-52.3 $-52.2$	7 3	$-51.9_{7}$ $-51.6_{3}$	[154.6]	[+8.0]
[1 <sup>h</sup> 11 <sup>m</sup> ] Greenwich,	Nov. 13 Dec. 14	9.41	5	$-9.59$ $-9.36_{5}$	_51.2		-51.8 -50.8 <sub>5</sub>	_151.8	+6.3
Paris,	Dec. 9	-9.43	5	<u>-9.41</u> <sub>5</sub>	—51.2 —51.3	5 6	50.76	[—150.2]	[+7.7]
[Ih 9m]	Dec. 12 1849	• • • •	• • •	-9.38			-50.7	—150.2] —148.6	+6.2
Greenwich, Paris,	Jan. 6 Jan. 18	$ \begin{array}{c c} -9.37 \\ -9.11 \end{array} $	1	$ \begin{array}{c c} -9.37, \\ -9.09, \end{array} $	-51.2 -50.0	1 1	-50.8 <sub>1</sub> -49.4 <sub>1</sub>	Γ—147.7]	[十7.5]
[1 <sup>h</sup> 9 <sup>m</sup> ]	Jan. 12			-9.23			-50.1	—146.2	+6.0

Observatory.		Observed	correcti	ons in R.A.	Observed o	correcti	ions in Dec.	Corr. to G	eocentric
[R. A. of Uranus.]	Mean dates.	Mean.	No. of obs.	Corrected mean.	Mean.	No.of obs.	Corrected mean.	Longitude.	Latitude
	1849	8		8	"		"	"	"
Greenwich, [1 <sup>h</sup> 34 <sup>m</sup> ]	Sept. 16	—10.27 ····	3	—10.27 	—53.3 ····	3	—52.9 ····	$\begin{bmatrix} +165.1 \\ +160.8 \end{bmatrix}$	[+7.3] +6.2
Greenwich, Paris,	Oct. 28 Oct. 21	$-10.24 \\ -10.26$	6 5	$-10.24_{6} \\ -10.24_{5}$		6 5	$-53.5_6 \ -54.2_5$	[—164.4]	[+7.4]
[1 <sup>h</sup> 30 <sup>m</sup> ]	Oct. 25			-10.24			-53.8	-161.0	+5.8
Greenwich, Paris,	Nov. 16 Nov. 17	—10.12 —10.22	3 5	$-10.12_s$ $-10.20_s$	-54.4 -54.1	3 4	$-54.0_{3}$ $-53.5_{4}$	[—162.5]	[+7.3]
[1 <sup>h</sup> 26 <sup>m</sup> ]	Nov. 17			-10.17			-53.7	—160.1	+6.0
Greenwich, Paris,	Dec. 13 Dec. 16	—9.95 —9.88	6 2	$-9.95_{6}$ $-9.86_{v}$	-53.1 -54.4	9 2	-52.7 <sub>9</sub> -53.8 <sub>2</sub>	[—160.4]	[+7.1]
[1 <sup>h</sup> 24 <sup>m</sup> ]	Dec. 14			- 9.93			-52.9	-156.6	+5.7
	1850			0.51					
Greenwich, Paris,	Jan. 7 Jan. 5	-9.71 -9.77	1 2	-9.71, $-9.75,$	-53.0 $-53.0$	3	$-52.6_1$ $-52.4_3$		
[1h 24m]	Jan. 6			- 9.74			-52.5	[—156.8] —153.8	[+6.9] +6.2
Greenwich, [1 <sup>h</sup> 52 <sup>m</sup> ]	Sept. 6	—10.83 	9	_10.83 	_53.9	9	—53.5 	[—171.7] —168.1	[+6.5 +5.9
Greenwich, Paris,	Oct. 11 Oct. 17	—10.92 —19.87	8 7	-10.92 <sub>8</sub> -10.85 <sub>7</sub>		7 5	54.9, 55.7	[—173.3]	[+6.4
[1 <sup>h</sup> 47 <sup>m</sup> ]	Oct. 16			-10.87			-55.3	_169.6	+5.3
Greenwich, Paris,	Nov. 6 Nov. 10	—10.79 —10.89	5 3	-10.79 <sub>5</sub> -10.87 <sub>5</sub>	-55.7 -56.1	6	-55.3 <sub>6</sub> -55.5 <sub>4</sub>	[—172.4]	[+6.4
[1 <sup>h</sup> 43 <sup>m</sup> ]	Nov. 8			-10.82			-55.4	-169.1	+5.6
Greenwich, Königsberg,	Dec. 7 Dec. 15	—10.56 —10.50	8 2 .	$-10.56_{s}$ $-10.48_{2}$	-55.0 -56.0	9 2	-54.6 <sub>9</sub>	[—169.0]	[+6.3
[1 <sup>h</sup> 41 <sup>m</sup> ]	Dec. 9			-10.54			-54.6	-165.0	+5.2
	1851		1						- Sact
Greenwich, [1h 41m]	Jan. 19	—10.21 	4	10.21	<u>-54.8</u>	4	-54.4	$\begin{bmatrix} -163.5 \\ -160.4 \end{bmatrix}$	[+6.0 +3.5
Greenwich,	Sept. 11	-11.42	2	-11.42,		2	-55.32		-
Königsberg, Paris,	Sept. 19 Sept. 14	-11.41 $-11.59$	2 1	-11.41, -11.57,		1	_56.9,	[—180.0]	[+5.7
[2h 7m]	Sept. 14			-11.46			_55.8	—176.9	+4.4
Königsberg, Paris,	Oct. 22 Oct. 23	—11.75 —11.46	3 3	—11.75 —11.44		3	_57.4 	[—181.8]	[+5.8
[2h 2m]	Oct. 23			_11.56			_57.4	—179.1	+4.8

las de	Mean Co	RRECTIONS	то ти	е Ернемь	eris of U	RANUS	Contin	nued.	
Observatory.		Observed	correction	ons in R.A.	Observed c	orrecti	ons in Dec.	Corr. to G	eocentric
[R. A. of Uranus.]	Mean dates.	Mean.	No. of obs.	Corrected mean.	Mean.	No. of obs.	Corrected mean.	Longitude.	Latitude.
Greenwich,	1851 Nov. 2 Nov. 2	s -11.50 -11.48	5 2	s —11.50 <sub>5</sub> —11.46,	57.5 58.1	5	$-57.1_5$ $-57.5$	"	"
[2 <sup>h</sup> 0 <sup>m</sup> ]	Nov. 2			-11.49			-57.2	[—181.4] —178.1	[+5.7] +4.5
Greenwich, Paris,	Nov. 22 Nov. 14	—11.43 —11.39	5 1	$\begin{bmatrix} -11.43_5 \\ -11.37_1 \end{bmatrix}$	<b>—</b> 58.3	5		[—179.9]	[+5.6]
[1 <sup>h</sup> 58 <sup>m</sup> ]	Nov. 21			11.42			-57.9 <sub>5</sub>	-177.6	+3.8
Greenwich, Paris, [1h 54m]	Dec. 22 Dec. 25 Dec. 24	—11.15 —11.00	3	$ \begin{array}{c c} -11.15_{3} \\ -10.98_{1} \\ \hline -11.06 \end{array} $	-57.2	3	$ \begin{array}{r} -56.8_{3} \\ -56.6_{3} \\ \hline -56.7 \end{array} $	[—175.7] —172.3	[+5.3] +3.8
[1 94]	1852			-11.00	• • • •	• •	-56.7	-1,2.5	70.0
Greenwich, Paris,	Jan. 11 Jan. 14	—10.85 —10.89	7 5	$-10.85, \\ -10.87_{5}$		7 5	$-56.8_7$ $-55.9_5$	[—173.1]	[+5.2]
[1 <sup>h</sup> 54 <sup>m</sup> ]	Jan. 12		• • •	10.86	• • • •	• •	-56.4	169.4	+3.1
Greenwich, [2 <sup>h</sup> 22 <sup>m</sup> ]	Sept. 12	—12.06 ····	7	—12.06 <b>,</b>	<u>56.5</u>	7	<u>56.1</u>	[—187.4] —184.5	[+4.9] +3.9
Greenwich, Paris,	Oct. 17 Oct. 23	-12.23 $-12.06$	8 3	$-12.23_{s}$ $-12.04_{s}$	-58.6 $-59.6$	8 3	-58.2 <sub>8</sub> -59.0 <sub>3</sub>	[—189.6]	「十4.7]
[2 <sup>h</sup> 18 <sup>m</sup> ] Greenwich,	Oct. 19 Nov. 13 Nov. 15	-12.00	5	$-12.18$ $-12.00_{5}$	59.7	5	-58.4 -59.3 <sub>5</sub>	187.2	+3.1
Paris, [2 <sup>h</sup> 14 <sup>m</sup> ]	Nov. 14	—12.08 	5	$\frac{-12.06_{5}}{-12.03}$	60.2	4	$-59.6_{4}$ $-59.4$	[—188.9] —185.6	[+4.7] +2.4
Greenwich, Königsberg, Paris,	Dec. 19 Dec. 16 Dec. 19	-11.72 $-11.67$ $-11.77$	7 3 5	—11.72, —11.75,	-58.7 -59.3 -59.0	7 3 5	$-58.3_7$ $-58.3_2$ $-58.4_5$		
[2 <sup>h</sup> 10 <sup>m</sup> ]	Dec. 19						<u>—58.3</u>	[—184.8] —181.3	[+4.6] +2.8
Greenwich, Paris,	1853 Jan. 12 Jan. 15	—11.42 —11.46	7 4	—11.42, —11.44,	<b>—</b> 57.5	7	_57.1	5 101 07	
[2 <sup>h</sup> 9 <sup>m</sup> ]	Jan. 13			_11.43			_57.1	[—181.0] —176.8	[+4.4] +2.6
Greenwich, Paris,	Sept. 17 Sept. 16	-12.69 $-12.58$	4 2	-12.69 $-12.56$ $2$	_56.7 _57.0	4 2	-56.3 <sub>4</sub> -56.4 <sub>2</sub>	[—194.6]	[+4.0]
[2 <sup>h</sup> 39 <sup>m</sup> ]	Sept. 17		•••	-12.65	• • • •		-56.3	—191.6	+2.5
Greenwich, Paris, [2 <sup>h</sup> 34 <sup>m</sup> ]	Oct. 15 Oct. 27 Oct. 22	—12.69 —12.66	7 6	$ \begin{array}{r} -12.69_{7} \\ -12.64_{9} \\ \hline -12.66 \end{array} $	-58.8 -59.0	7 6	-58.4 <sub>7</sub> -58.4 <sub>8</sub> -58.4	[—196.7] —192.7	[+3.8] +1.7
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	MEAN CO	RRECTIONS	то тн	Е ЕРНЕМЕ	E EPHEMERIS OF URANUS.—Continued.					
Observatory.		Observed	correcti	ons in R.A.	Observed o	orrect	ions in Dec.	Corr. to G	eocentric	
[R. A. of Uranus.]	Mean dates.	Mean.	No. of obs.	Corrected mean.	Mean.	No.of obs.	Corrected mean.	Longitude.	Latitude.	
	1853	8		8	"		"	"		
Greenwich, Paris,	Nov. 12 Nov. 15	-12.65 $-12.67$	14	$-12.65_{14}$ $-12.65_{10}$	-59.4 $-59.2$	14 8	-59.0 <sub>14</sub> -58.6 <sub>8</sub>	[—196.0]	[+3.7]	
[2h 31m]	Nov. 14			12.65		.,	-58.9	—192.9	+1.9	
Paris,	Dec. 12	-12.28	1	12.26	-59.0	1	-58.4	[—193.4]	[+3.6]	
[2h 27m]					• • • • •		••••	-187.9	+1.5	
Greenwich,	1854 Jan. 13	-12.02	4	_12.02,	-59.7	4	-59.2		- No.	
Paris,	Jan. 20	-11.87	2	-11.85	-58.1	1	-57.9	[—188.1]	[+3.5]	
[2h 25m]	Jan. 15			-11.96			-58.9	-183.9	+0.1	
Paris, [2h 26m]	Feb. 8	-11.89	1	-11.87	<u>-57.8</u>	1	-57.6	[—184.5] —182.1	[+3.5] +0.7	
Greenwich,	Sept. 21	_13.12	6	_13.12	-56.0	6	-55.5	[-201.3]	[+3.0]	
[2h 53m]		-13.12		-10.12	-00.0			-196.9	+1.7	
Greenwich,	Oct. 26 Oct. 29	-13.24	7	-13.24,	-58.0	7	-57.5 <sub>9</sub>			
Paris,	Oct. 27	-13.12	1	$\frac{-13.10}{-13.22}$	_57.2 	3	$\frac{-57.0}{-57.3}$	$\begin{bmatrix} -203.7 \\ -199.0 \end{bmatrix}$	[+2.8] +1.2	
	Nov. 12	10.00						-100.0		
Greenwich, Paris,	Nov. 16	-13.22 -13.21	6	$-13.22_5$ $-13.19_6$	—58.2 —58.7	5	-57.5 <sub>5</sub> -58.5 <sub>1</sub>			
Santiago,	Nov. 17 Nov. 15	-13.20	4	-13.20 <sub>3</sub>	-58.7	3	-58.1,	[—203.0] —199.1	[+2.7] +1.2	
				_13.20			-57.8	-199.1	71.2	
Greenwich Paris,	Dec. '14 Dec. 9	-12.93 $-13.14$	7	-12.93, $-13.12,$	-58.6 $-56.9$	7 4	$-58.1_{2}$ $-56.7_{1}$		Fig. Eg.	
Santiago,	Dec. 15	12.85	10	_12.85,	-59.7	9	-59.1,	[-200.1]	[+2.6]	
[2 <sup>h</sup> 44 <sup>m</sup> ]	Dec. 14			_12.90			-58.0	-195.3	+0.7	
Greenwich,	1855 Jan. 18	-12.55	2.	_12.55,	-56.9	2	-56.4	[—194.6]	[+2.5]	
[2h 42m]								-190.1	+1.1	
Greenwich, Paris,	Oct. 13 Oct. 25	-13.71 -13.93	6 3	$-13.71_6$ $-13.91$	-55.7 -55.8	6 2	$-55.2_{3}$ $-55.6_{1}$	1214	1000	
[3h 9m]	Oct. 17	-13.33			-55.6		—55.3	$\begin{bmatrix} -209.2 \\ -204.9 \end{bmatrix}$	[+1.8] +0.1	
Greenwich,	Nov. 11	_13.85	4	_13.85,	-57.6	5	-57.1,			
Paris, Santiago,	Nov. 17 Nov. 16	-13.62 -13.82	4 5	-13.60, -13.82,	-56.6 -57.2	4 5	-56.4 -56.6			
[3h 5m]	Nov. 15	-15.62			-31.2		-56.7	$\begin{bmatrix} -209.4 \\ -205.3 \end{bmatrix}$	$\begin{bmatrix} +1.7 \\ -0.2 \end{bmatrix}$	
Greenwich,	Dec. 18	_13.48		-13.48,	_57.3	10	_56.8,		1.1.1.1	
Paris, Santiago,	Dec. 16 Dec. 18	—13.52 —13.53	2 6	-13.50, -13.53,	-56.7 -58.1	3 6	$-56.5_1$ $-57.5_2$	193	i espe	
[3h 0m]	Dec. 18	-13.55	1	—13.50 —13.50	-36.1		-57.0	$\begin{bmatrix} -206.2 \\ -202.1 \end{bmatrix}$	$\begin{bmatrix} +1.6 \\ -0.1 \end{bmatrix}$	
1		1		1		1				

		MEAN COI	RECTIONS	то ти	е Ернеме	RIS OF UR	ANUS	.—Contin	ued.	
	Observatory.		Observed o	correcti	ons in R.A.	Observed c	orrecti	ons in Dec.	Corr. to G	eocentric
	[R. A. of Uranus.]	Mean dates.	Mean.	No. of obs.	Corrected mean.	Mean.	No of obs.	Corrected mean.	Longitude.	Latitude.
	Greenwich,	1856 Jan. 22 Feb. 10	s —12.97 —12.87	6 2	s —12.97 <sub>6</sub> —12.85 <sub>2</sub>		6 2	$-55.6_{3}$ $-54.6_{1}$	"	"
ı	[2 <sup>h</sup> 58 <sup>m</sup> ]	Jan. 27			_12.94			-55.4	$\begin{bmatrix} -199.5 \\ -194.7 \end{bmatrix}$	[+1.4] $-0.5$
	Greenwich, Paris,	Oct. 16 Oct. 16	-14.36 $-14.38$	4 2	$-14.36_{4}$ $-14.36_{3}$	<b>—</b> 53.8	4	-53.3	[213.8]	[+0.7]
1	[3 <sup>h</sup> 27 <sup>m</sup> ]	Oct. 16			14.36			53.3	_211.0	-1.4
	Greenwich, Paris,	Nov. 18 Nov. 17	-14.23 $-14.32$	8	$-14.23_{s}$ $-14.30_{6}$	-54.8 $-54.0$	8 7	$-54.3_{8}$ $-53.8_{7}$	[—214.7]	[+0.7]
l	[3 <sup>h</sup> 22 <sup>m</sup> ]	Nov. 18		• • • •	-14.26	••••	• •	-54.1	210.2	-0.9
	Greenwich, Paris,	Dec. 18 Dec. 19	—13.92 —14.11	5 7	$-13.93_s$ $-14.09_{7}$	-55.9 -55.0	5 6	$-55.4_{s}$ $-54.8_{6}$	[—211.6]	[+0.6]
L	[3 <sup>h</sup> 17 <sup>m</sup> ]	Dec. 19 1857			-14.03	••••	• •	55.1	-207.7	-1.2
	Greenwich, Paris,	Jan. 21 Jan. 12	—13.59 —13.87	10	$\begin{array}{r} -13.60_{10} \\ -13.85_3 \end{array}$	—53.4 —55.3	8 3	$-52.9_{3}$ $-55.1_{1}$	[-206.4]	[+0.5]
ı	[3 <sup>h</sup> 15 <sup>m</sup> ]	Jan. 19			—13.66	• • • •	• •	<b>—</b> 53.5	202.3	-0.4
ľ	Greenwich, [3 <sup>h</sup> 46 <sup>m</sup> ]	Oct. 8	—14.68 	4	—14.69 ····	<del>-49.1</del>	4	<del>-48.6</del>	[—216.8] —213.0	[—0.3] —1.9
	Greenwich, Paris, Königsberg,	Nov. 6 Nov. 10 Nov. 19	-14.80 $-14.83$ $-14.77$	4 9 3	-14.81, -14.81, -14.75,	-51.3 $-51.5$ $-52.7$	5 8 3	$-50.8_5$ $-51.3_8$ $-51.5_2$		
ı	[3 <sup>h</sup> 41 <sup>m</sup> ]	Nov. 11			_14.80			_51.2	$\begin{bmatrix} -218.9 \\ -215.5 \end{bmatrix}$	$\begin{bmatrix} -0.4 \\ -2.4 \end{bmatrix}$
	Greenwich, Paris, Königsberg,	Dec. 11 Dec. 16 Dec. 8	—14.55 —14.48 —14.56	6 7 1	$-14.56_{6}$ $-14.46_{7}$ $-14.54_{2}$	-53.2 -52.8 -53.7	5 6 1	$-52.7_{5}$ $-52.6_{6}$ $-52.5_{1}$	[-217.1]	F 0 ""
۱	[3h 36m]	Dec. 13			-14.51			52.6	$\begin{bmatrix} -217.1 \\ -212.2 \end{bmatrix}$	—3.0
	Greenwich, Paris,	1858 Jan. 17 Jan. 16	-14.13 -14.19	13	$-14.14_{13} -14.17_6$	-52.8 -52.8	13 9	-52.3 <sub>15</sub> -52.6 <sub>9</sub>	[—211.8]	ר מפו
	[3 <sup>h</sup> 32 <sup>m</sup> .2]	Jan. 17			14.15			_52.4	-207.5	[-0.6] $-2.8$
1	Greenwich, Paris,	Feb. 11 Feb. 12	—13.81 —13.91	10 1	$\begin{array}{c} -13.82_{10} \\ -13.89_{1} \end{array}$	-52.1 -52.7	10 1	$\begin{array}{c} -51.6_{10} \\ -52.5_{1} \end{array}$	[—207.0]	[0.6]
	[3h 31m.9]	Feb. 11	• • • •	• • •	-13.83	••••		51.7	-203.1	-3.1
(	Greenwich, [4 <sup>h</sup> 3 <sup>m</sup> .3]	Oct. 17	<b>—15.</b> 06	5	—15.06 	<b>—</b> 46.4	5	<del>-4</del> 5.9	$\begin{bmatrix} -220.6 \\ -216.2 \end{bmatrix}$	[—1.4] —4.0
	Greenwich, Paris,	Nov. 14 Nov. 20	-15.16 $-15.19$	9	$-15.17_{10}$ $-15.17_{0}$	-48.2 -47.8	11 10	$\begin{array}{r} -47.7_{11} \\ -47.6_{10} \end{array}$	[222.1]	[—1.5]
L	[3 <sup>h</sup> 58 <sup>m</sup> .5]	Nov. 17	• • • • •	• • •	-15.17		• •	-47.7	218.6	-3.8

	MEAN CO	RRECTIONS	то тн	Е ЕРНЕМІ	ris of U	RANUS	.—Contin	ued.	
Observatory.		Observed o	correction	ons in R.A.	Observed o	correct	ions in Dec.	Corr. to G	eocentric
[R. A. of Uranus.]	Mean dates.	Mean.	No. of obs.	Corrected mean.	Mean.	No.of obs.	Corrected mean.	Latitude.	Longitude.
	1858	8		s	"		"	"	"
Greenwich, Paris,	Dec. 16 Dec. 16	-14.96 -14.78	6 5	$-14.97_6$ $-14.76_5$	-49.2 -49.5	6 3	-48.7 <sub>a</sub> -49.3 <sub>1</sub>	20.5	
[8h 53m.6]	Dec. 16			_14.87			-48.9	$\begin{bmatrix} -220.7 \\ -215.1 \end{bmatrix}$	$\begin{bmatrix} -1.6 \\ -4.1 \end{bmatrix}$
	1859		4 35-	dian.					1
Greenwich,	Jan. 19	-14.56		-14.57	-48.9	8	-48.4,		105.20
Paris,	Jan. 10	-14.72	4	-14.70	-48.2	4	-48.0 <sub>1</sub>	[-216.1]	An and
[3h 50m.0]	Jan. 16			-14.61			-48.3	211.5	-3.1
Greenwich, Paris,	Feb. 18 Feb. 11	-14.18 -14.37	5	-14.19 <sub>5</sub> -14.35 <sub>6</sub>	-48.1	5 4	-47.6 <sub>s</sub>	Town I had	
[3h 49m.3]	Feb. 14	-14.51		$-14.33_{6}$ $-14.28$	-48.3		-48.1 <sub>4</sub> -47.8	$\begin{bmatrix} -210.9 \\ -207.1 \end{bmatrix}$	[—1.6] —3.4
			13.73						Security 1
Greenwich, [4 <sup>h</sup> 20 <sup>m</sup> .8]	Oct. 25	—15.43 	6	-15.44	<u>-42.6</u>	6	-42.1	[—223.2] —219.6	[—2.2] —5.5
Greenwich, Paris,	Nov. 18 Nov. 17	-15.56 -15.61	6 8	$-15.57_{6}$ $-15.59_{8}$	-43.3 -43.0	5 9	-42.8 <sub>5</sub> -42.8 <sub>9</sub>	[-224.7]	[-2.2]
[4h 17m.2]	Nov. 17			15.58			-42.8	-221.9	-4.6
Greenwich, Paris,	Dec. 16 Dec. 11	—15.43 —15.46	9 5	—15.44 <sub>9</sub> —15.44 <sub>5</sub>	-45.2 -44.5	8 5	$-44.7_{8}$ $-44.3_{5}$	5 000 07	5 0 07
[4h 12m.5]	Dec. 14			_15.44			-44.5	[—223.9] —220.7	[-2.3] $-4.9$
	1860								
Greenwich,	Jan. 16	-15.08	*8	-15.09 <sub>8</sub>	-45.8	8	-45.3 <sub>s</sub>		
Paris,	Jan. 15	-15.08		-15.06 <sub>8</sub>	-44.3	5	-44.15	[-219.6]	
[4 <sup>h</sup> 8 <sup>m</sup> .0]	Jan. 16			-15.08			-44.8	-216.1	-4.5
Greenwich, Paris,	Feb. 17 Feb. 6	-14.64 -14.79	12 2	$-14.65_{12}$ $-14.77_2$	-45.0	12	-44.5		
	Feb. 15			—14.17 <sub>2</sub> —14.67			_44.5	$\begin{bmatrix} -213.9 \\ -210.4 \end{bmatrix}$	$\begin{bmatrix} -2.3 \\ -5.0 \end{bmatrix}$
			2						100
Greenwich, [4 <sup>h</sup> 40 <sup>m</sup> .9]	Oct. 13	-15.52		—15.52 ····	-35.2	3	<del>-34.7</del>	$\begin{bmatrix} -223.0 \\ -218.3 \end{bmatrix}$	$\begin{bmatrix} -2.9 \\ -5.4 \end{bmatrix}$
Greenwich,	Nov. 15	_15.88	9	_15.89	_38.3	9	_37.8,		
Paris,	Nov. 22	-15.79	5	-15.77	-37.3	5	-37.1,	[-226.6]	[-3.1]
[4h 35m.8]	Nov. 18			15.85			-37.6	-223.5	-5.8
Greenwich, Paris,	Dec. 12 Dec. 12	—15.77 —15.79	4 3	—15.78, —15.77,	-41.5 -38.5	5 3	$-41.0_5$ $-38.3_3$	Γ—226.2]	[-3.2]
[4h 31m.6]	Dec. 12			-15.78			-40.0	_223.2	_6.8
	1861		10						100
Greenwich, Paris,	Jan. 13 Jan. 13	—15.45 —15.52	10	$-15.46_{10} -15.49_{6}$	-40.5 $-40.2$	10 3	$-40.1_3$ $-40.0_1$	[—222.4]	[-3.2]
[4 <sup>h</sup> 26 <sup>m</sup> .8]	Jan. 13			-15.47			-40.1	-219.3	-5.8

<sup>19</sup> May, 1873.

	ME.	an Co	RRECTIONS	в то тн	е Ернем	eris of U	RANUS	Contin	nued.		
Observatory.			Observed	correcti	ons in R. A.	Observed	Observed corrections in Dec.			Corr. to Geocentric	
[R. A. of Uranus.]	Mean	dates.	Mean.	No. of obs.	Corrected mean.	Mean.	No.of obs.	Corrected mean.	Longitude.	Latitude	
Greenwich,	18 Feb.	<b>61</b>	s —15.12	2	s —15.13,	_40.7	3	" -40.3	"	"	
Paris,	Feb.		-15.12 $-15.23$	1	$-15.13_{2}$ $-15.20_{1}$	-40.1	3	-40.3	[-217.9]	[-3.17	
[4 <sup>h</sup> 21 <sup>m</sup> .0]	Feb.	8			_15.15			-40.3	_215.0	-6.0	
Greenwich, [4 <sup>h</sup> 56 <sup>m</sup> .4]	1	. 10	—15.99 ····	9	-16.00 <sub>9</sub>	_30.9	8	<u>-30.5</u>	[—226.2] —223.4	[-4.0] -6.1	
Greenwich, Paris,	Dec. Dec.		-16.01 $-16.04$	4 11	_16.02, _16.01,	-33.4 -32.8	13	-33.0			
Washington,	Dec.		-16.10	6	$-16.01_{11}$ $-16.07_{6}$	-02.0	10	—32.6° <sub>18</sub>	[-227.3]	[—4.0]	
[4 <sup>h</sup> 50 <sup>m</sup> .8]	Dec.	12			-16.03			-32.7	-221.5 $-224.4$	-6.4	
Greenwich,	186		17.05	0	15 05	05.1		0.4.5			
Paris,	Jan. Jan.	19 20	-15.67 $-15.72$	8 5	$-15.67_{8}$ $-15.69_{5}$	-35.1 -34.1	9 5	$-34.7_{9}$ $-33.9_{5}$	[—223.2]	L 103	
[4h 44m.9]	Jan.	19			<u>15.68</u>			-34.4	$\begin{bmatrix} -223.2 \\ -220.2 \end{bmatrix}$	[—4.0] —6.3	
Greenwich,	Feb.	22	-15.18	7	-15.18,	-34.3	7	-33.9,			
Washington, Paris,	Feb.	19 15	-15.31 $-15.47$	3 5	$-15.31_3$ $-15.44_5$	-34.6	6	-34.4	[—217.5]	F 4.07	
[4 <sup>h</sup> 43 <sup>m</sup> .1]	Feb.	19			_15.30			-34.1	-217.5 $-215.1$	$\begin{bmatrix} -4.0 \\ -6.0 \end{bmatrix}$	
Greenwich, [5 <sup>h</sup> 16 <sup>m</sup> .2]	Nov.	9	—16.13 	9	-16.13	<u>24.5</u>	9	<u>24.1</u>	$\begin{bmatrix} -226.2 \\ -223.6 \end{bmatrix}$	[—4.7] —7.1	
Greenwich,	Dec.	12	-16.27	7	_16.27,	-27.2	7	-26.8,			
Paris, Leyden,	Dec.	11 8	-16.27 $-16.16$	5 4	$-16.24_{5}$ $-16.13_{3}$	-26.5 $-25.2$	5 4	$-26.3_{s}$ $-25.2_{s}$	F 005 07		
[5 <sup>h</sup> 10 <sup>m</sup> .7]	Dec.	19			_16.23			-26.3	$\begin{bmatrix} -227.6 \\ -225.4 \end{bmatrix}$	$\begin{bmatrix} -4.7 \\ -7.2 \end{bmatrix}$	
G 1	186				MI TO						
Greenwich, Paris,	Jan. Jan.		-15.96 $-15.94$	2  -	$-15.96_{10}$ $-15.91_{2}$	-28.3 $-27.4$	10	$ \begin{array}{c c} -27.9_{10} \\ -27.2_{1} \end{array} $		200	
Washington, Leyden,	Jan. Jan.		-15.92 $-16.03$	4 -	-15.92 $-16.00$	-27.9	6	97.0		200	
[5 <sup>h</sup> 4 <sup>m</sup> .6]	Jan.	17			_15.96				-224.3] -222.2	[4.8] -6.8	
Greenwich,	Feb.	15	_15.55	10	-15.55 <sub>10</sub>	_29.2	10	-28.8 <sub>10</sub>			
Paris, Washington,	Feb.	15	-15.47 $-15.64$	17 -	$-15.44_{17}$ $-15.64_{2}$	-28.6	17	-28.4			
Leyden,	Feb.		-15.57	6 -	-15.54	-28.5	7	-28.5,	219.37	T—4.87	
[5 <sup>h</sup> 2 <sup>m</sup> .2]	Feb.	15			_15.50			-28.6	-216.0	-7.2	
Greenwich, Paris,	Mar. Mar.		-15.36 $-15.30$	2 -	-15.36 <sub>2</sub> -15.27 <sub>4</sub>	-29.0 $-28.0$	3 4	$-28.6_{3}$ $-27.8_{4}$		1000	
[5 <sup>h</sup> 2 <sup>m</sup> .2]	Mar.	4			-15.30	_20.0	1-		-215.9]   -213.3	4.8] 7.0	
										1197	
	K E	-	-								

	MEAN COL	RRECTIONS	то тн	в Ернеме	RIS OF UR	LANUS	.—Contin	ued.	
Observatory.	nall com s	Observed	correcti	ons in R.A.	Observed o	orrect	ions in Dec.	Corr. to Geocentric	
[R. A. of Uranus.]	Mean dates.	Mean.	No. of obs.	Corrected mean.	Mean.	No.of obs.	Corrected mean.	Longitude.	Latitude.
Paris,	1863 Nov. 29	s —16.33		8	"		"	"	"
Leyden,	Nov. 14	-16.33 $-16.23$	6	-16.30 <sub>3</sub> -16.20 <sub>4</sub>	-18.4 -18.1	6	—18.2 <sub>3</sub> —18.1 <sub>4</sub>	[-225.9]	[-5.6]
[5 <sup>h</sup> 34 <sup>m</sup> ]	Nov. 21			-16.24			-18.2	-224.1	-8.3
Greenwich, Leyden,	Dec. 19 Dec. 14	-16.32 $-16.51$	3 2	-16.32 <sub>3</sub> -16.48 <sub>1</sub>	$-20.0 \\ -17.1$	3	-19.6 <sub>3</sub> -17.1 <sub>1</sub>	[—226.8]	[-5.7]
[5 <sup>h</sup> 29 <sup>m</sup> ]	Dec. 18		3.1	-16.36			-19.0	-225.9	-7.0
Washington,	1864 Jan. 15	-16.01	4	-16.01 <sub>n</sub>		11		44	19 19
Leyden, [5 <sup>h</sup> 25 <sup>m</sup> ]	Jan. 10 Jan. 14	—16.07 	4	$-16.04_a$ $-16.02$	—20.0 	4	20.0	[—224.6] —221.4	[—5.8] —6.7
Washington, [5h 21m]	Feb. 15	-15.74	4	-15.74	—21.5 	9		[—219.6] —217.8	[-5.7]
Greenwich, [5 <sup>h</sup> 21 <sup>m</sup> ]	May 3	—15.57 	2	—15.57 	—22.2 	2	—21.8 <sub>2</sub>	[—216.1] —215.6	[—5.6] —7.3
Paris, Washington, Leyden,	Dec. 20 Dec. 10 Dec. 18	—16.32 —16.22 —16.19	4 2 5	-16.29 <sub>4</sub> -16.22 <sub>2</sub> -16.16 <sub>4</sub>	-13.2 -11.4 -12.4	4 4 5	—12.8 <sub>4</sub> —12.4 <sub>4</sub>	[-220.1]	
[5 <sup>h</sup> 49 <sup>m</sup> ]	Dec. 17		***	-16.22		11	-12.6	-223.1	-8.4
Greenwich, Paris, Washington, Leyden,	Jan. 5 Jan. 15 Jan. 17 Jan. 16	-16.28 -16.22 -16.11 -16.03	2 1 9 3	-16.28 <sub>2</sub> -16.19 <sub>2</sub> -16.11 <sub>9</sub> -16.00 <sub>2</sub>	—13.7 —15.1 —14.4 —14.7	2 2 9 3	-13.3 <sub>2</sub> -14.9 <sub>2</sub> -14.7 <sub>2</sub>	[—223.4]	[—6.5]
[5 <sup>h</sup> 45 <sup>m</sup> ]	Jan. 15			-16.13			-14.3	—220.0 —220.0	_8.8
Washington, Leyden,	Feb. 13	—15.77 —15.85	9 2	—15.77, —15.82,		6 2	-15.6	[-218.9]	[-6.4]
[5 <sup>h</sup> 41 <sup>m</sup> ]	Feb. 14			-15.78				-217.4	-8.6
Greenwich, Washington,	Oct. 10 Oct. 18	-15.59 $-15.59$	1 5	-15.59 <sub>1</sub> -15.59 <sub>5</sub>	- 2.4	1	- 2.0 <sub>1</sub>	[—215.3]	[-7.0]
[6 <sup>h</sup> 17 <sup>m</sup> ]	Oct. 17			-15.59			_ 2.0	—214.0	_8.1
Greenwich, Leyden, Washington,	Dec. 6 Dec. 7 Dec. 18	-16.13 -16.26 -16.17	2 2 8	$-16.13_{2}$ $-16.23_{2}$ $-16.17_{8}$	- 5.2 - 4.8 - 3.8	2 2 5	- 4.8 <sub>2</sub> - 4.6 <sub>2</sub>		1.00 S
[6 <sup>h</sup> 11 <sup>m</sup> ]	Dec. 14	-10.11		_16.17			4.7	[—222.2] —222.0	[—7.3] —8.8
			-5.3			14.6	E+1 FT		-11-201-30
243-5	- 63		N.	432					

	Mean Co	RRECTIONS	то ти	іЕ Ернеме	ris of U	RANUS	.—Contin	ued.	
Observatory.			correcti	ons in R.A.	Observed o	orrect	ons in Dec.	Corr. to G	eocentrio
[R. A. of Uranus.]	Mean dates.	Mean.	No. of obs.	Corrected mean.	Mean.	No. of obs.	Corrected mean.	Longitude.	Latitnde.
Greenwich, Paris, Washington, Leyden, [6h 5m] Greenwich,	1866 Jan. 10 Jan. 12 Jan. 17 Jan. 17 Jan. 14 Feb. 14	s —16.20 —16.04 —16.06 —16.02 	8 1 9 6 	$ \begin{vmatrix} 8 \\ -16.20_8 \\ -16.01_1 \\ -16.06_9 \\ -15.99_4 \\ -16.09 \\ -15.81_{10} \end{vmatrix} $	7.2 - 6.3 - 7.6 - 7.1	9 1 9 6	$ \begin{array}{c}     '' \\     - 6.8_4 \\     - 6.1_1 \\     - 6.5_4 \\     - 7.1_3 \\     - 6.6 \\     - 8.7_4 \end{array} $	[—221.6] —221.0	[— 7.3] — 9.0
Washington, Leyden, [6h 0m]	Feb. 14 Feb. 14 Feb. 14	—15.81 —15.75	6 8	$ \begin{array}{c c} -15.81_{6} \\ -15.72_{6} \\ \hline -15.79 \end{array} $	- 8.4 - 8.6	8 8	$ \begin{array}{r} -7.3_4 \\ -8.6_4 \end{array} $ -8.2	$\begin{bmatrix} -217.3 \\ -216.9 \end{bmatrix}$	[— 7.3] — 8.2
Greenwieh, Washington, Leyden, [6 <sup>h</sup> 0 <sup>m</sup> ]	Mar. 12 Mar. 9 Mar. 3 Mar. 9	—15.47 —15.49 —15.59	2 6 2	$ \begin{array}{r rrrr} -15.47_{2} \\ -15.49_{6} \\ -15.56_{2} \\ \hline -15.50 \end{array} $	- 8.1 - 9.7 - 9.0	2 6 2	$ \begin{array}{r} -7.7_1 \\ -8.6_2 \\ -9.0_1 \end{array} $ $ -8.5 $	[—212.9] —212.9	[— 7.1] — 8.5
Washington, [6 <sup>h</sup> 37 <sup>m</sup> ]	Oct. 13	—15.36 	5	—15.36 ····	+ 4.4	5	+ 5.5	$\begin{bmatrix} -209.6 \\ -211.2 \end{bmatrix}$	$\begin{bmatrix} -7.5 \\ -7.9 \end{bmatrix}$
Greenwich, Washington,	Nov. 9 Nov. 15	-15.65 $-15.72$	2 10	$ \begin{array}{r} -15.65_{2} \\ -15.72_{10} \\ \hline -15.71 \end{array} $		2 10	$+3.9_{1}$ $+4.9_{2}$	[—215.1]	[- 7.8]
Greenwich, Washington, Leyden, [6h 31m]	Dec. 11 Dec. 12 Dec. 10 Dec. 11	—16.01 —16.00 —15.87	10 7 2	$ \begin{array}{c c} -16.01_{10} \\ -16.00_{7} \\ -15.84_{2} \\ \hline -15.99 \end{array} $	+ 2.8 + 2.0 + 1.6	10 7 2	$\begin{array}{c} + \ 4.6 \\ + \ 3.2_{6} \\ + \ 3.1_{4} \\ + \ 1.6_{2} \\ \hline + \ 2.9 \end{array}$	-215.9 $[-218.2]$ $-219.7$	- 8.3 [- 8.0] - 9.7
Greenwich, Washington, Leyden, [6 <sup>h</sup> 24 <sup>m</sup> ]	1867 Jan. 21 Jan. 21 Jan. 9 Jan. 19	—15.89 —15.93 —15.82	5 12 4	$ \begin{array}{r} -15.89_{s} \\ -15.93_{12} \\ -15.79_{s} \\ \hline -15.90 \end{array} $		5 12 3	$ \begin{array}{c} -1.0_{3} \\ -0.1_{6} \\ -0.3_{1} \end{array} $ $ -0.4 $	[—217.8] —218.3	[— 8.0] — 9.3
Paris, Washington, Leyden, [6 <sup>h</sup> 20 <sup>m</sup> ]	Feb. 13 Feb. 15 Feb. 18	—15.72 —15.65 —15.54	3 9 3	$ \begin{array}{r} -15.69_{3} \\ -15.65_{0} \\ -15.51_{2} \\ \hline -15.64 \end{array} $	- 2.4 - 2.0 - 0.5	4 10 3	$ \begin{array}{r} -2.0_{a} \\ -0.9_{4} \\ -0.5_{s} \\ \hline -1.1 \end{array} $	[—214.5] —214.7	[— 7.9] — 8.6
Greenwich, Washington, [6 <sup>h</sup> 19 <sup>m</sup> ]	Mar. 2 Mar. 11 Mar. 5	—15.45 —15.32	7 4	$ \begin{array}{r} -15.45, \\ -15.32, \\ \hline -15.40 \end{array} $	- 2.9 - 2.5	8 2	$ \begin{array}{r} -2.5_{4} \\ -1.4_{2} \\ \hline -2.1 \end{array} $	[—211.1] —211.3	[— 7.8] — 9.0
Greenwich, Washington, [6 <sup>h</sup> 51 <sup>m</sup> ]	Dec. 11 Dec. 18 Dec. 13	—15.6I —15.70	5 3	-15.61 <sub>s</sub> -15.70 <sub>s</sub> -15.64	+ 8.5 + 6.9	5 3	$\begin{array}{c} + 8.9_{3} \\ + 8.0_{2} \\ \hline + 8.5 \end{array}$	[—213.1] —215.3	[— 8.6] —10.4

	MEAN COI	RRECTIONS	то ти	к Ерпеме	RIS OF UI	tanus	.—Contin	ued.	
Observatory.		Observed	correctle	ous in R.A.	Observed o	orrecti	ions in Deo.	Corr. to Geoceutric	
[R. A. of Uranus.]	Mean dates.	Meau.	No. of obs.	Corrected mean.	Mean.	No.of obs.	Corrected mean.	Longitude.	Latitude.
Greenwich, [6 <sup>h</sup> 45 <sup>m</sup> ]	1868 Jan. 13		4	s 15.67.	+ 6.9	4	+ 6.7.	" [—213.4] —215.5	[— 8.7] —10.1
Greenwich, Leyden, Washington, Paris,	Feb. 15 Feb. 5 Feb. 13	-15.43 -15.43 -15.50 -15.41	8 3 7 7	$\begin{array}{c} -15.43_{\scriptscriptstyle{6}} \\ -15.40_{\scriptscriptstyle{5}} \\ -15.50_{\scriptscriptstyle{6}} \\ -15.38_{\scriptscriptstyle{4}} \end{array}$	+ 4.8 + 5.9 + 4.9	8 3 6	+ 4.6 <sub>4</sub> + 5.9 <sub>3</sub> + 6.0 <sub>3</sub>	[—210.3]	[_ 8 A]
[6h 41m]	Feb. 14	• • • •	• • •	-15.44	• • • •		+ 5.3		- 9.7
Leyden, Washington,	Mar. 11 Mar. 19	-15.02 $-14.91$	2	$-14.99_1$ $-14.91_1$	$+4.6 \\ +3.4$	2	+4.6, +4.5,	[-205.0]	ſ— 8,5]
[6h 39m]	Mar. 15	• • • •		-14.95			+ 4.6		- 9.2
Washington, [7th 16th]	Oet. 18	—14.57 	6	—14.57 	+12.3	5	+13.3	[—198.3] —201.5	$\begin{bmatrix} -8.7 \\ -12.9 \end{bmatrix}$
Washington, [7 <sup>h</sup> 16 <sup>m</sup> ]	Nov. 7	—14.83 	5	—14.83 	+16.2	5	+17.3	[—202.0] —205.6	[— 9.1] — 9.3
Greenwich, Washington,	Dec. 25 Dec. 12	—15.24 —15.16	5	-15.24 <sub>a</sub> -15.16 <sub>a</sub>	$+15.1 \\ +14.6$	5 4	+14.9 <sub>a</sub> +15.6 <sub>e</sub>	[-206.5]	[- 9.2]
[7 <sup>h</sup> 10 <sup>m</sup> ]	Dec. 18	• • • •	• • •	15.20	••••	• •	+15.2	210.3	-10.0
Greenwich, Washington,	1869 Jan. 19 Jan. 18	—15.28 —15.31	1 8	-15.28 <sub>1</sub> -15.31 <sub>s</sub>	$+12.6 \\ +12.9$	1 8	$+12.4_{1} +13.4_{1}$	[—207.1]	r 9 31
[7 <sup>h</sup> 5 <sup>m</sup> ]	Jan. 18	• • • •		-15.31			+13.3	-211.4	_10.3
Greenwich, Washington, Paris,	Feb. 14 Feb. 14 Feb. 10	-15.04 $-15.13$ $-15.09$	10 13 10	$-15.04_{16}$ $-15.13_{19}$ $-15.06_7$		10 13 10	$\begin{array}{c} +10.9_{10} \\ +11.7_{10} \\ +12.2_{10} \end{array}$	[-204.7]	[— 9.2]
[7h 1m]	Feb. 13		• • •	-15.08			+11.7	-208.1	-10.2
Greenwich, Washington,	Mar. 3 Mar. 7	-14.81 -14.87	2 2	—14.81 <sub>3</sub> —14.87 <sub>2</sub>	$+10.8 \\ +11.4$	2 2	+10.6 <sub>3</sub> +11.9 <sub>3</sub>	[—201.5]	[- 9.2]
[6h 59m]	Mar. 5		• • •	-14.84			+11.3	-204.8	9.3
Greenwich, [7h 32m]	Dec. 8	—14.50 ····	2	—14.50 <sub>3</sub>	+21.1	2	+20.9	[—197.1] —202.1	[— 9.8] —10.3
Greenwich, [7h 25m]	1870 Jan. 19	-14.73	10	—14.72 <sub>a</sub>	+19.0	10	+18.8	[—199.3] —204.5	[— 9.9] —10.8
Greenwich, Washington,	Feb. 16 Feb. 16	—14.58 —14.49	7	-14.57 <sub>a</sub> -14.49 <sub>1</sub>	$+17.2 \\ +16.7$	7 2	+17.0 +17.1	[—197.2]	
[7º 21º]	Feb. 16	••••		-14.55			+17.0	-201.9	-10.9

	Мел	n Co	RRECTIONS	то тп	Е ЕРПЕМЕ	RIS OF UI	RANUS	.—Contin	ued.	
Observatory.			Observed	correcti	ons in R.A.	Observed corrections in Dec.			Corr. to Geocentric	
[R. A. of Uranus.]	Mean dates.		Meau.	No. of obs.	Corrected mean.	Mean.	No.of obs.	Corrected mean.	Longitude.	Latitude.
	187		8	-	8	, 10.0	2	+16.0	"	"
Greenwich, Washington,	Mar. Mar.	12 11	-14.29 $-14.30$	5 6	-14.28 <sub>5</sub> -14.30 <sub>5</sub>	$+16.2 \\ +15.9$	5 6	+16.0 $+16.3$	[—193.6]	[ 9 7]
[7 <sup>h</sup> 18 <sup>m</sup> ]	Mar.	12			-14.29			+16.2	_198.1	
	187	_								
Greenwich, [7 <sup>h</sup> 47 <sup>m</sup> ]	Jan.	9	—13.99 ····	5	13.98	+24.8	5	+24.6	$\begin{bmatrix} -190.0 \\ -196.1 \end{bmatrix}$	$\begin{bmatrix} -10.2 \\ -10.7 \end{bmatrix}$
Greenwich, [7h 41m]	Feb.	15	<u>13.92</u>	2	—13.91 	+21.8	2	+21.6	[—188.8] —194.4	$\begin{bmatrix} -10.1 \\ -11.5 \end{bmatrix}$
Greenwich, [7 <sup>h</sup> 38 <sup>m</sup> ]	Mar.	14	—13.82 ····	14	—13.81 	+20.7	14	+20.5	[—184.9] —192.8	[—10.0] —11.5
Greenwich, [8 <sup>h</sup> 11 <sup>m</sup> ]	Dec.	-	—13.16 ····	3	—13.15 	+29.2	3	+29.0	[—177.9] —186.5	$\begin{bmatrix} -10.4 \\ -11.4 \end{bmatrix}$
	187	2							3 3	
Greenwich, Washington,	Jan. Jan.	$\begin{array}{c} 6 \\ 21 \end{array}$	—13.32 —13.31	6 3	-13.31 $-13.31$	+28.3 $+27.8$	6 3	$+28.1_{3}$ $+28.2_{1}$	[—179.8]	г 10 cl
[8 <sup>h</sup> 6 <sup>m</sup> .1]	Jan.	18			_13.31			+28.1	-188.3	—11.3
Greenwich, Washington,	Feb. Feb.	15 21	—13.23 —13.24	7 3	-13.22 $-13.24$	$^{+26.2}_{+26.4}$	6 3	$^{+26.0_2}_{+26.8_1}$	[—179.3]	Γ—10.5]
[8h 1m.0]	Feb.	17			-13.23			+26.3	_186.6	-11.3
Greenwich, Washington,	Mar. Mar.	15 15	—13.04 —13.07	14 10	—13.03 <sub>4</sub> —13.07 <sub>5</sub>	$+25.4 \\ +24.5$	14 8	$+25.2_{2} +24.9_{1}$	[176.4]	[10_4]
[7 <sup>h</sup> 57 <sup>m</sup> .9]	Mar.	15			-13.05			+25.1	—183.7	—11.1
Washington, Greenwich,	April April	8	-12.79 $-12.77$	3	$-12.79_{s}$ $-12.76_{1}$	$+24.9 \\ +25.0$	3	$+25.3_{1} +24.8_{1}$	[-172.4]	Γ—10.27
[7h 57m.3]	April	8	. • • • •		-12.78	••••		+25.2		10.8

Corrections to be Applied to the Positions of Uranus in the Berlin Jahrbuch and the Nautical Almanac to reduce them to the Positions from the Provisional Theory.

1	Date.		Heliocentric.		Geocentric.		
		82	мδρ	δβ,,,	87 ,,	88,	
1830,	July 24	_18.0	+1001	+ 9.0	-19.3	+ 9.5	
	Aug. 13	18.3	1007	9.0	18.8	9.5	
	Sept. 2	18.4	1014	9.1	17.9	9.5	
	Sept. 22	18.5	1020	9.1	17.1	9.4	
	Oct. 12	18.7	1027	9.1	16.7	9.3	
	Nov. 1	19.0	1031	. 9.2	16.5	9.2	
	Nov. 21	_19.3	+1038	+ 9.2	-16.7	+ 9.1	
1831,	July 19	-22.5	+1112	+ 9.5	-24.5	+10.0	
	Aug. 8	22.6	1119	9.5	23.7	10.0	
	Aug. 28	22.7	1123	9.6	22.7	10.1	
	Sept. 17	22.8	1128	9.6	21.7	10.0	
	Oct. 7	22.9	1133	9.6	20.9	9.8	
	Oct. 27	23.2	1138 1142	9.7 9.7	20.6	9.6	
	Nov. 16 Dec. 6	23.5 —23.8	+1146	+ 9.7	-21.0	9.5	
	Dec. 6	-23.0					
1832,	Aug. 2	-26.9	+1198	+ 9.8	-28.7	+10.3	
	Aug. 22	27.2	1201	9.9	27.9	10.4	
	Sept. 11	27.4	1202	9.9	26.9	10.3	
	Oct. 1	27.6	1205	9.9	26.1	10.2	
	Oct. 21	27.8	1208	10.0	25.4	10.2	
	Nov. 10	28.0	1209	10.1	25.1	+10.0	
	Nov. 30	-28.3	+1209	+10.2	-25.2	+10.0	
1833,	July 28	-31.9	+1233	+10.2	-34.5	+10.7 $10.8$	
	Aug. 17	32.2	1236	10.3	33.7 32.7	10.8	
	Sept. 6	32.4	1240	10.3 10.3	31.8	10.7	
	Sept. 26	32.6	1242 1245	10.3	31.0	10.5	
	Oct. 16	32.9 33.2	1247	10.4	30.4	10.4	
	Nov. 5 Nov. 25	—33.5	+1250	+10.4	-30.2	+10.3	
	ESSENCE ST	-33.5	+1250				
1834,	July 23	-38.0	+1264	+10.5	-41.2	+11.0	
	Aug. 12	38.4	1266	10.5	40.7	11.1	
	Sept. 1	38.4	1268	10.6	39.6	11.1	
	Sept. 21	38.7	1270	10.6	38.6 37.7	10.9	
	Oct. 11	39.1	1275	10.6 10.6	36.9	10.8	
	Oct. 31	39.4	1277	10.7	36.6	10.7	
	Nov. 20	39.7	$   \begin{array}{c}     1282 \\     +1282   \end{array} $	+10.7	-36.1	+10.5	
	Dec. 10	-40.1	+1202	710.1		A POST AND A SECOND	
1835,	July 18	-43.9	+1309	+10.8	-47.7	+11.3	
	Aug. 7	44.5	1311	10.7	47.6	11.3	
	Aug. 27	44.5	1313	10.7	46.6	11.3 11.2	
	Sept. 16	45.1	1316	10.7	45.8 44.8	11.2	
	Oct. 6	45.4	1318	10.8	44.0	10.9	
	Oct. 26	45.9	1321	10.7	43.6	10.8	
	Nov. 15 Dec. 5	46.5 —46.6	1324 +1327	$10.8 \\ +10.7$	-42.5	+10.6	
1836,		-51.0	+1361	+11.0	-55.3	+11.4	
2000,	Aug. 1	51.3	1364	11.0	55.2	11.5	
	Aug. 21	51.5	1365	11.1	54.6	11.7	
	Sept. 10	-51.9	+1368	+11.0	-53.7	+11.6	

	Date.		Heliocentric.		Geoc	entric.
		δλ	Μδρ	$\delta \beta$	13	86 .
1836,	Sept. 30 Oct. 20 Nov. 9 Nov. 29 Dec. 19	-52.2 52.9 53.1 53.9 -53.8	+1370 1372 1375 1377 +1380	+11.0 11.0 11.0 11.0 11.0 +11.1	-52.4 51.6 50.5 50.4 -49.8	+11.5 11.3 11.1 11.0 +10.9
1837,	July 7 July 27 Aug. 16 Sept. 5 Sept. 25 Oct. 15 Nov. 4 Nov. 24 Dec. 14	58.3 58.4 59.2 59.2 60.0 60.0 61.0 61.3 62.1	+1387 1387 1388 1389 1391 1393 1394 1394 +1393	+11.0 11.0 11.1 11.1 11.0 11.0 11.0 11.0	62.9 62.9 63.1 62.0 61.3 59.6 59.1 58.257.1	+11.4 11.5 11.7 11.7 11.5 11.4 11.2 11.0 +10.9
1838,	Aug. 11 Aug. 31 Sept. 20 Oct. 10 Oct. 30 Nov. 19 Dec. 9 Dec. 29	66.4 67.2 67.7 68.1 68.5 68.9 69.4 69.7	+1395 1396 1395 1392 1390 1388 1388 +1389	+11.1 11.1 11.1 11.1 11.1 11.1 11.1 +11.2	-71.1 71.0 70.2 68.9 67.6 66.4 65.8 -65.4	+11.6 11.7 11.7 11.6 11.4 11.2 11.1 +11.0
1839,	Aug. 6 Aug. 26 Sept. 15 Oct. 5 Oct. 25 Nov. 14 Dec. 4 Dec. 24 Jan. 13	74.7 75.1 75.5 76.0 76.4 76.8 77.2 77.6	+1382 1381 1380 1379 1379 1379 1378 1377 +1376	+11.1 11.1 11.0 11.1 11.1 11.1 11.1 11.1	-80.0 79.7 79.0 77.9 76.5 75.2 74.0 73.5 -73.1	+11.6 11.7 11.6 11.5 11.3 11.1 10.9 +10.7
1841,	June 24 Aug. 20 Sept. 9 Sept. 29 Oct. 19 Nov. 8 Nov. 13 Dec. 13 Jan. 7	81.9 82.7 83.4 83.5 84.2 84.4 85.3 85.586.1	+1376 1374 1376 1377 1376 1376 1377 1378 +1377	+11.0 11.0 11.0 11.0 11.0 11.0 11.0 11.0 +10.9	86.0 87.9 87.8 86.4 85.5 83.5 82.7 81.5 81.3	+11.1 11.5 11.6 11.5 11.4 11.3 11.1 10.9 +10.7
	June 16 Aug. 15 Sept. 4 Sept. 24 Oct. 14 Nov. 3 Nov. 23 Dec. 13	-89.8 91.1 91.5 91.9 92.3 92.9 93.4 93.8	+1378 1384 1385 1388 1390 1392 1393	+10.8 10.8 10.8 10.7 10.7 10.7	-93.2 97.0 96.9 96.1 94.8 93.4 91.8	+10.8 11.3 11.4 11.3 11.2 11.1 10.9
1842,	Dec. 13 Jan. 2 Feb. 11	93.8 94.3 —95.0	1395 $1398$ $+1404$	10.8 10.8 +10.7	90.5 89.7 —89.6	10.3 $10.7$ $10.6$ $+10.3$

Aug. Aug. Sept. Oct. Nov. Dec. Dec. 843, Jan. Aug. Aug. Sept. Oct. Nov. Dec. Bec. 844, Jan. July Aug. Sept. Oct. Nov. Nov. Dec. Sept. Oct. Nov. Nov. Dec. 845, Jan. Jan. Aug. Sept. Sept. Oct. Nov. Nov. Dec. Sept. Oct. Oct. Oct. Oct. Oct. Oct. Oct. Oc	Date.			Heliocentric.	Geocentric.		
Aug. Aug. Sept. Oct. Nov. Dec. Dec. 843, Jan. Aug. Aug. Sept. Oct. Nov. Dec. Bec. 844, Jan. July Aug. Sept. Oct. Nov. Nov. Dec. 845, Jan. Jan. Aug. Sept. Sept. Oct. Nov. Nov. Dec. 846, Jan. Jan. Aug. Sept. Sept. Oct. Nov. Nov. Dec. Bec. Oct. Nov. Nov. Dec. Bec. Oct. Nov. Nov. Dec. Bec. Oct. Oct. Nov. Nov. Dec. Bec. Oct. Oct. Oct. Oct. Oct. Oct. Oct. Oc			δλ,,	мбр	$\delta \beta_n$	81,,	88,
Aug. Sept. Oct. Nov. Dec. Dec. 843, Jan. Aug. Aug. Sept. Oct. Nov. Dec. Bec. 844, Jan. July Aug. Sept. Oct. Nov. Nov. Dec. Sept. Oct. Nov. Nov. Dec. 845, Jan. Jan. Aug. Sept. Sept. Oct. Nov. Nov. Dec. Sept. Oct. Oct. Nov. Dec. Oct. Oct. Oct. Dec. Dec.		June 11	- 96.7	+1409	+10.6	- 98.5	+10.5
Sept. Oct. Oct. Nov. Dec. Dec. 843, Jan. Aug. Aug. Sept. Oct. Nov. Dec. B44, Jan. July Aug. Sept. Sept. Oct. Nov. Nov. Dec. Sept. Oct. Oct. Nov. Dec. Sept. Oct. Oct. Nov. Dec. Dec.		Aug. 10	99.1	1408	10.6	105.3	10.0
Oct. Oct. Nov. Dec. Dec. 843, Jan. Aug. Aug. Sept. Oct. Nov. Dec. B44, Jan. July Aug. Sept. Sept. Oct. Nov. Nov. Dec. Dec. Sept. Oct. Nov. Nov. Dec. Dec. Sept. Oct. Oct. Nov. Nov. Dec. Dec. Oct. Oct. Nov. Dec. Dec.		Aug. 30	99.6	1409	10.7	105.8	10.2
Oct. Nov. Dec. Dec. 843, Jan.  Aug. Aug. Sept. Oct. Nov. Dec. Dec. 844, Jan.  July Aug. Sept. Oct. Nov. Nov. Dec. Sept. Oct. Nov. Dec. Dec. Sept. Oct. Nov. Dec. Dec. Oct. Nov. Dec. Dec.			99.9 100.5	1409 1410	10.6	105.2	10.2
Nov. Dec. Dec. 843, Jan. Aug. Sept. Oct. Nov. Dec. Bept. Oct. Nov. Dec. Jan. Jan. Aug. Sept. Sept. Oct. Nov. Dec. Sept. Oct. Nov. Dec. Bept. Oct. Nov. Dec. Sept. Oct. Nov. Dec. Nov. Dec. Oct. Nov. Dec. Dec. Oct. Nov. Dec. Oct. Oct. Oct. Nov. Dec. Oct. Oct. Nov. Dec. Dec. Oct. Nov. Dec. Dec. Dec.	A STATE OF THE PARTY OF THE PAR	Management of the Control of the Con	100.9	1412	10.5 10.5	104.2 102.6	10.0
Aug. Aug. Aug. Sept. Oct. Oct. Nov. Dec. B44, Jan.  July Aug. Sept. Oct. Nov. Nov. Dec. Sept. Oct. Nov. Nov. Dec. Sept. Oct. Nov. Aug. Sept. Sept. Oct. Nov. Nov. Dec. Sept. Oct. Nov. Nov. Dec. Nov. Nov. Dec. Sept. Oct. Nov. Nov. Dec. Sept. Oct. Nov. Dec. Sept. Oct. Nov. Dec. Dec. Oct. Nov. Dec. Dec.			101.3	1413	10.5	100.8	10.8
Aug. Aug. Sept. Oct. Nov. Dec. Sept. Oct. Nov. Nov. Dec. Oct. Nov. Dec. Oct. Oct. Nov. Dec. Oct. Oct. Nov. Dec. Dec. Oct. Nov. Dec. Dec.			101.8	1414	10.5	99.2	10.6
Aug. Aug. Sept. Oct. Nov. Dec. 844, Jan. July Aug. Sept. Oct. Nov. Nov. Dec. 845, Jan. Jan. Aug. Sept. Sept. Oct. Nov. Nov. Dec. 846, Jan. Jan. Aug. Sept. Oct. Nov. Nov. Dec. 0ct. Nov. Dec. Oct. Nov. Dec. Oct. Oct. Nov. Dec. Dec.			102.2	1415	10.5	98.0	10.4
Aug. Sept. Oct. Nov. Dec. B44, Jan.  July Aug. Sept. Oct. Nov. Nov. Dec. Dec. Oct. Nov. Dec. Oct. Oct. Nov. Dec. Dec.	n. 17	Jan. 17	-102.5	+1417	+10.4	- 97.2	+10.2
Sept. Oct. Nov. Dec. 844, Jan. July Aug. Sept. Oct. Nov. Nov. Dec. 845, Jan. Jan. Aug. Sept. Oct. Nov. Nov. Dec. 846, Jan. Jan. Aug. Sept. Oct. Nov. Nov. Dec. Oct. Nov. Dec. Oct. Oct. Nov. Dec. Dec. Dec.			-107.2 107.7	+1422 1420	+10.3 10.2	-113.7	+10.7
Oct. Oct. Oct. Nov. Dec. Dec. 844, Jan. July Aug. Sept. Oct. Nov. Nov. Dec. 845, Jan. Jan. Aug. Sept. Oct. Nov. Nov. Dec. Sept. Oct. Nov. Nov. Dec. Sept. Oct. Nov. Nov. Dec. Oct. Nov. Dec. Oct. Nov. Dec. Oct. Oct. Nov. Dec. Dec.		Sept. 14	108.0	1420	10.1	114.4 114.3	10.7
Nov. Dec. Dec. S44, Jan.  July Aug. Sept. Oct. Nov. Nov. Dec. S45, Jan. Jan.  Aug. Sept. Sept. Oct. Nov. Nov. Cot. Nov. Nov. Dec. Sept. Oct. Nov. Dec. Sept. Oct. Nov. Dec. Sept. Oct. Nov. Dec. Dec. Oct. Nov. Dec. Dec.			108.5	1420	10.1	113.4	10.6
Dec. Dec. Dec. Sept. Sept. Oct. Nov. Dec. Jan. Jan. Aug. Sept. Oct. Nov. Nov. Dec. Sept. Oct. Nov. Dec. Sept. Oct. Nov. Dec. Sept. Oct. Nov. Dec. Oct. Nov. Dec. Oct. Oct. Dec. Dec. Dec.	t. 24	Oct. 24	109.0	1419	10.1	112.1	10.5
July Aug. Sept. Oct. Nov. Nov. Dec. Sept. Oct. Nov. Dec. Oct. Nov. Dec. Oct. Oct. Nov. Dec. Dec. Dec.		Nov. 13	109.4	1418	10.1	110.2	10.4
S44, Jan.  July Aug. Sept. Sept. Oct. Nov. Nov. Dec. S45, Jan. Jan.  Aug. Sept. Oct. Nov. Nov. Dec. Sept. Oct. Nov. Nov. Dec. Sept. Oct. Nov. Dec. Sept. Oct. Nov. Dec. Dec. Oct. Oct. Nov. Dec. Dec.			110.0	1418	10.1	108.6	10.3
July Aug. Sept. Oct. Nov. Nov. Dec. Sept. Oct. Nov. Nov. Dec. Sept. Oct. Nov. Nov. Dec. Sept. Oct. Nov. Dec. Oct. Nov. Dec. Oct. Oct. Nov. Dec. Dec. Dec.			110.4	1417	10.1	106.9	10.1
Aug. Sept. Sept. Oct. Nov. Dec. 845, Jan. Jan. Aug. Sept. Oct. Nov. Nov. Dec. 1846, Jan. Jan. Aug. Sept. Oct. Nov. Dec. Oct. Nov. Dec. Oct. Dec. Dec.	n. 12	Jan. 12	-110.8	+1418	+10.0	-105.9	+ 9.8
Sept. Sept. Oct. Nov. Nov. Dec. 845, Jan. Jan. Aug. Sept. Oct. Nov. Nov. Dec. 846, Jan. Jan. Aug. Sept. Oct. Nov. Dec. Oct. Nov. Dec. Dec.			-115.1	+1406	+ 9.7	-121.2	+10.0
Sept. Oct. Nov. Nov. Dec. 845, Jan. Jan. Aug. Sept. Oct. Nov. Nov. Dec. 946, Jan. Jan. Aug. Sept. Oct. Nov. Dec. Oct. Nov. Dec. Oct. Dec. Dec.		Aug. 19	115.4	1403	9.8	122.3	10.2
Oct. Nov. Nov. Dec. 1845, Jan. Jan. Aug. Sept. Sept. Oct. Nov. Dec. Jan. Jan. Aug. Sept. Oct. Oct. Nov. Dec. Dec. Dec.			115.8 116.3	1400 1397	9.8 9.8	122.7 122.4	10 3
Nov. Nov. Dec. Jan. Jan.  Aug. Sept. Oct. Nov. Nov. Dec. Jan. Jan.  Aug. Sept. Oct. Nov. Nov. Dec. Dec. Oct. Nov. Dec. Dec.			116.9	1396	9.7	121.3	10.3 10.2
Nov. Dec. Jan. Jan. Aug. Sept. Oct. Nov. Dec. Jan. Jan. Aug. Sept. Oct. Nov. Dec. Oct. Nov. Dec. Oct. Dec. Dec.			117.4	1392	9.6	119.7	10.0
Aug. Sept. Oct. Nov. Dec. Oct. Oct. Nov. Dec. Oct. Oct. Oct. Oct. Dec. Dec. Dec.			117.8	1389	9.6	117.6	9.8
Jan. Aug. Sept. Sept. Oct. Nov. Dec. S46, Jan. Jan. Aug. Sept. Oct. Nov. Dec. Dec.			118.3	1384	9.6	115.7	9.7
Aug. Sept. Oct. Nov. Dec. 1846, Jan. Jan. Aug. Sept Oct. Oct. Nov. Dec. Dec. Dec.			118.6	1381	9.5	114.3	9.4
Sept. Sept. Oct. Nov. Nov. Dec. 1846, Jan. Jan. Aug. Sept. Oct. Nov. Dec. Dec.	n. 26	Jan. 26	—119.1	+1378	+ 9.6	—113.3	+ 9.4
Sept. Oct. Nov. Nov. Dec. 1846, Jan. Jan. Aug. Sept. Oct. Oct. Nov. Dec. Dec.		Aug. 14	-123.5	+1340	+ 9.1	-130.4	+ 9.4
Oct. Nov. Nov. Dec. 1846, Jan. Jan. Aug. Sept. Oct. Oct. Nov. Dec. Dec.			123.9	1335	9.4	131.4	9.8
Nov. Nov. Dec. Jan. Jan. Aug. Sept. Oct. Oct. Nov. Dec. Dec.		Sept. 23 Oct 13	124.4 124.9	1330 1327	9.4 9.3	131.7 130.6	9.9
Nov. Dec. Jan. Jan. Aug. Sept. Oct. Oct. Nov. Dec. Dec.			125.3	1322	9.3	129.0	9.7
Aug Sept Oct. Oct. Nov. Dec. Dec.	ov. 22	Nov. 22	125.7	1318	9.2	127.0	9.5
Jan. Aug. Sept. Oct. Oct. Nov. Dec. Dec.	ec. 12	Dec. 12	126.2	1313	9.2	125.0	9.3
Aug. Sept Oct. Oct. Nov. Dec. Dec.			126.7	1309	9.2	123.2	9.2
Sept Oct. Oct. Nov. Dec. Dec.	n. 21	Jan. 21	-127.1	+1303	+ 9.2	-121.9	- 9.0
Oct. Oct. Nov. Dec. Dec.		Aug. 29	-132.0	+1253	+ 8.8	-139.5	+ 9.2
Oct. Nov. Dec. Dec.		Sept. 18 Oct 8	132.3 132.8	1249 1246	8.8 8.8	139.9 139.8	9.2 9.3
Nov. Dec. Dec.			133.2	1242	8.7	138.4	9.1
Dec. Dec.		Nov. 17	133.5	1238	8.7	136.4	9.0
	ec. 7	Dec. 7	134.1	1234	8.7	134.4	8.9
			134.6	1233	8.6	132.3	8.7
1847, Jan.	in. 16	Jan. 16	-134.9	+1230	+ 8.6	-130.5	+ 8.5
	47 / 18	Aug. 24	-139.5	+1197	+ 8.3	-146.7	+ 8.6
		C 10	140.0	1194	8.3	148.0	8.7
Oct.	ept. 13		140.5	1191	8.3	148.3	8.7

20 May, 1873.

	Date.		Heliocentric.	Geocentric.		
		δλ	мδρ	$\delta \beta$	81,,	· &b,,,
1847,	Nov. 12	-141.4	+1185	+8.2	-145.8	+8.5
	Dec. 2	141.9	1183	8.1	143.7	8.3
1848,	Dec. 22 Jan. 11	142.4 —142.8	+1182 + 1182	8.1 +8.1	141.4 —139.3	$^{8.2}_{+8.1}$
	Sept. 7	147.9	+1165	+7.6	-156.0	+7.9
	Sept. 27	148.3	1166	7.6	156.7	8.0
	Oct. 17	148.7	1164	7.6	156.4	8.0
	Nov. 6 Nov. 26	149.3 149.8	1164 1163	7.6 7.6	155.3 153.2	8.0 7.9
	Dec. 16	150.2	1162	7.6	150.7	7.8
1849,	Jan. 5	150.6	1161	7.5	148.3	7.5
	Jan. 25	151.3	+1161	+7.5	-146.6	+7.4
	Sept. 2	—155.8 156.9	+1149	+7.0	-164.6	+7.3
	Sept. 22 Oct. 12	156.2 156.5	1150 1149	7.0 7.0	165.1 165.1	7.3 7.4
	Nov. 1	156.8	1148	7.0	164.0	7.4
	Nov. 21	157.4	1149	7.0	162.4	7.3
	Dec. 11	157.9	1148	6.9	160.0	7.1
1850,	Dec. 31 Jan. 20	158.3 —158.6	1147 +1147	$^{6.8}_{+6.8}$	157.5 —155.0	$6.9 \\ +6.8$
	Aug. 28	-163.3	+1135	+6.2	_170.6	
	Sept. 17	163.7	1133	6.2	172.6	$+6.4 \\ 6.5$
	Oct. 7	164.2	1131	6.2	173.3	6.5
	Oct. 27	164.7	1129	6.1	173.1	6.4
	Nov. 16 Dec. 6	165.2 165.6	1127 1126	6.1	171.8 169.4	$\begin{array}{c} 6.4 \\ 6.3 \end{array}$
	Dec. 26	166.0	1127	6.0	166.7	6.2
1851,	Jan. 15	166.3	1127	6.1	163.8	6.1
	Feb. 4	-166.7	+1124	+6.0	-161.8	+5.9
	Sept. 12	-171.5	+1109	+5.5	-180.0	+5.7
	Oct. 2 Oct. 22	171.9 172.4	1105 1103	5.5	181.4	5.8
	Nov. 11	172.9	1103	5.5 5.4	181.9 180.8	5.8 5.7
	Dec. 1	173.3	1103	5.3	178.7	5 5
050	Dec. 21	173.8	1102	5.2	176.1	5.3
852,	Jan. 10 Jan. 30	174.3 —174.7	$+1001 \\ +1098$	5.2 · +5.1	173.4 —170.2	5.3 + 5.1
	Sept. 6	-179.0				
	Sept. 26	179.4	$+1074 \\ 1073$	+4.7	—186.8 · 188.9	+4.9 $4.8$
	Oct. 16	179.8	1071	4.5	189.7	4.7
	Nov. 5	180.3	1068	4.5	189.6	4.7
	Nov. 25 Dec. 15	180.7 181.2	1067 1065	4.4	187.8	4.6
853,	Jan. 4	181.5	1064	4.4	$ \begin{array}{c c} 185.3 \\ 182.3 \end{array} $	4.6 4.5
,	Jan. 24	181.8	1062	4.4	179.6	4.4
	Feb. 13	-182.1	+1060	+4.3	_176.9	+4.2
	Sept. 1	-185.8	+1055	+3.9	_192.4	+4.0
	Sept. 21	186.2	1055	3.8	195.2	3.9

CORRECTIONS TO BE APPLIED TO THE POSITIONS OF URANUS—Continued. Geocentric. Date. Heliocentric.  $\delta \beta_{"}$ 93  $M\delta\rho$ 13 δλ " +1054+3.6 -196.8 1853, Oct. 31 -186.8+3.81054 195.6 Nov. 20 187.1 3.5 3.7 1053 193.5 Dec. 10 187.5 3.5 3.6 1053 3.5 190.7 3.6 Dec. 30 187.9 1053 3.5 187.4 1854, Jan. 19 188.1 3.5 Feb. 8 -188.5+1052+3.5-184.5+3.5+3.0 +1034+2.9 . -200.5-192.2Sept. 16 192.6 1032 2.8 202.9 2.9 Oct. 6 1032 2.7 203.7 2.8 193.0 Oct. 26 203.0 Nov. 15 193.3 1032 2.6 2.7 1029 2.6 201.3 2.7 Dec. 5 193.7 2.5 198.6 2.6 1025 Dec. 25 194.0 1021 2.5 195.2 2.5 1855. Jan. 14 194.2 +2.4+2.4-192.0+1018Feb. 3 -194.5+1.8-198.3-207.9 +1.9 Oct. +10101 21 1009 1.7 209.6 1.8 Oct. 198.7 Nov. 10 199.0 1008 1.6 209.7 1.7 208.4 199.3 1007 1.5 1.6 Nov. 30 1006 206.0 1.6 Dec. 20 199.6 1.5 1856, Jan. 199.8 1005 1.5 202.6 1.5 9 199.2 1.4 1003 1.4 Jan. 29 200.1 +1001+1.3-196.1+1.3Feb. 18 -200.3+0.7+0.7 -213.9-203.3+ 962 Oct. 15 957 0.7 214.9 0.7 203.7 Nov. 4 953 0.7 214.5 0.7 Nov. 24 203.9 212.4 949 0.6 0.6 Dec. 14 204.3 209.3 0.6 945 0.6 1857, Jan. 3 204.4 205.6 0.5 Jan. 23 204.5 941 0.5 Feb. 12 + 934 +0.4-202.2+0.4-204.7+ 879 -02 -214.0-0.2Sept. 20 -206.9 217.1 0.3 874 0.3 207.2 Oct. 10 218.8 0.3 0.3 Oct. 30 207.5 868 207.8 861 0.4 219.0 0.4 Nov. 19 217.6 0.4 0.4 853 Dec. 9 208.0 Dec. 29 846 0.5 215.0 0.5 208.1 211.5 0.6 839 0.6 1858, Jan. 18 208.2 207.7 0.6 Feb. 7 208.3 830 0.6 + 823 \* -0.6-204.2-0.6Feb. 27 -208.4-1.3Oct. 5 Oct. 25 Nov. 14 + 741 -219.1-210.4-1.3221.4 1.5 1.4 732 210.6 1222.2 1.5 210.8 723 1.4 Dec. 4 Dec. 24 1.6 1.5 221.9 713 211.0 219.7 1.6 1.5 211.2 704 216.6 1.5 695 1.5 211.3 1859, Jan. 13 686 1.6 213.0 1.6 Feb. 2 211.4 -209.4-1.5Feb. 22 + 677 -1.5-211.6-222.8-2.2+ 576 -2.1-213.1Oct. 20 2.2 224.5 Nov. 9 Nov. 29 569 2.1 213.2 -2.2 +561-2.1-224.8-213.4

CORRECTIONS TO BE APPLIED TO THE POSITIONS OF URANUS-Continued. Heliocentric. Geocentric. Date.  $\delta \lambda$ Moo  $\delta \beta$ 81  $\delta b$ +554-2.2 1859, Dec. 19 -213.5-223.5-2.3Jan. 213.5 546 2.2 220.9 2.3 1860, 8 Jan. 28 213.6 539 2.2 217.4 2.3 Feb. 17 -213.7+533-2.3-213.5-2.3-2.8 Sept. 24 -214.7+456 -219.7-2.9214.8 2.8 Oct. 14 451 223.1 2.9 215.0 2.9 Nov. 3 444 225.6 3.0 Nov. 23 215.1 437 2.9 226.8 3.1 1861, Jan. 2 Jan. 22 215.2 431 3.0 226.3 3.2 215.3 424 3.1 223.8 3.2 215.3 221.0 417 3.1 3.2 Feb. 12 -215.3+411 -3.1-217.3-3.1Oct. 29 Nov. 13 \_3.7 -215.6+339 -3.9-225.0 215.6 333 3.8 226.9 4.0 215.7 Dec. 227.4 329 - 8 3.8 4.0 215.8 Dec. 28 324 3.8 226.3 4.0 1862, Jan. 17 215.8 320 223.5 3.9 4.0 Feb. 215.8 315 4.0 220.0 4.1 Feb. 26 +310 -215.9-4.0 -216.0-4.0+246 Oct. 24 -216.0-4.4 -224.2-4.6 216.0 226.6 Nov. 13 241 4.5. 4.7 Dec. 3 Dec. 23 237 216.0 4.5 227.7 4.7 215.9 232 4.6 227.2 4.8 1863, 215.8 226 Jan. 12 4.7 225.04.9 Feb. 1 Feb. 21 215.8 219 4.7 221.8 4.8 213 215.7 4.7 218.1 4.8 Mar. 13 -215.7+208-4.8-214.1-4.8Nov. 8 Nov. 28 -224.6 --215.3+139-5.3-5.5 215.2133 5.4 226.5 5.7 Dec. 18 215.1 126 5.4 226.85.7 1864, Jan. 7 Jan. 27 Feb. 16 215.0 120 5.5 225.4 5.8 214.9 222.7 114 5.5 5.7 214.8 108 5.6 219.3 5.7 March 7 -214.8+103 -5.6-215.3-5.6+ 21 Oct. 13 -213.8-6.0-217.8-6.1Nov. 2 Nov. 22 213.7 6.0 221.3 16 6.2 213.7 9 6.1 224.0 6.4 225.1 Dec. 12 213.6 1 6.2 6.5 1865, Jan. 1 Jan. 21 213.4 6 6.2 224.7 6.5 213.2 14 6.2 222.7 6.5 Feb. 10 20 213.1 219.6 6.2 6.4 March 2 -213.0\_ 27 -215.7-6.3-6.4 Oct. 8 Oct. 28 -211.6-103 -6.8 -213.5-6.9 211.4 110 6.8 217.2 7.0 Nov. 17 211.2 117 6.9 220.0 7.2 Dec. 7 Dec. 27 211.1 124 222.0 6.9 7.3 210.9 132 222.4 6.9 7.3 1866, Jan. 16 210.7 139 7.0 221.5 7.4 Feb. 5 Feb. 25 Mar. 17 210.6 145 7.0 218.8 7.3 210.4 151 7.0 215.4 7.2 -210.1-158-7.1-211.2

-7.1

Date.			Heliocentrie.		Geocentric.		
		δλ	Мδρ	δβ	.,, 13	88	
1866,	Oct. 3	-208.2	225	- 7.4	-207.3	- 7.4	
	Oct. 23	208.1	230	7.4	211.5	7.6	
	Nov. 12	207.9	235	7.5	214.9	7.8	
	Dec. 2	207.8	241	7.6	217.6	8.0	
1007	Dec. 22 Jan. 11	207.6	246	7.6	218.8 218.5	8.0 8.0	
1867,	Jan. 11 Jan. 31	207.4 207.2	251 256	7.6	216.7	8.0	
	Feb. 20	207.0	262	7.7	213.8	7.9	
	Mar. 12	-206.7	268	- 7.7	-209.8	- 7.8	
	Nov. 27	-203.2	— 351	- 8.2	-211.4	- 8.6	
1900	Dec. 17	203.0	358	8.2	213.5	8.6	
1868,	Jan. 6 Jan. 26	202.8 202.4	365 371	8.2 8.3	213.7 212.7	8.7	
	Feb. 15	202.4	376	8.3	210.3	8.6	
	Mar. 6	201.8	382	8.4	207.0	8.6	
	Mar. 26	-201.4	— 387	- 8.4	-202.9	- 8.4	
	Oct. 12	-198.0	<b>—</b> 458	- 8.6	-197.2	- 8.6	
	Nov. 1 Nov. 21	197.8 197.5	465	8.7	201.1 203.8	8.9 9.1	
	Dec. 11	197.2	473 481	8.8 8.8	206.2	9.2	
	Dec. 31	196.8	490 -	8.8	207.5	9.3	
1869,	Jan. 20	196.4	498	8.8	207.1	9.3	
	Feb. 9	196.0	507	8.8	205.4	9.2	
	Mar. 1	195.6	515	8.9	202.4	9.2	
	Mar. 21	-195.3	- 524	— 8.9	-198.4	- 9.0	
	Dec. 6	-190.0			-197.0	A STATE OF	
1000	Dec. 26	189.5		:	198.9	0.0	
1870,	Jan. 15 Feb. 14	189.0	- 665 676	- 9.4 9.4	199.5 198.7	- 9.9 9.9	
	Feb. 24	188.6 188.0	686	9.4	196.2	9.8	
	Mar. 16	187.5	697	9.4	193.0	9.6	
	April 5	-187.2	<b>—</b> 708	— 9.4	-189.4	- 9.4	
	Dec. 1	-181.5	— 846	- 9.6	-186.5	-10.0	
1051	Dec. 21	181.1	859	9.6	189.0	10.1	
1871,	Jan. 11 Jan. 30	180.5 179.8	872 883	9.7 9.8	190.3 190.1	10.2	
	Feb. 19	179.1	894	9.7	188.3	10.1	
	Mar. 11	178.4	906	9.7	185.6	10.0	
	Mar. 31	_177.0	— 919	- 9.8	—181.2	- 9.9	
	Dec. 16	-171.6	-1083	-10.0	-177.4	-10.4	
1872,	Jan. 5	171.0	1095	10.1	179.3 180.2	10.6	
	Jan. 25 Feb. 14	170.5 169.8	1107 1120	10.0 10.0	179.6	10.5	
	Mar. 5	169.3	1133	10.1	177.8	10.5	
	Mar. 25	168.7	1145	10.1	174.9	10.3	
	April 14	168.1	1156	10.1	171.3	10.1	
	May 4	-167.6	—1168	-10.1	-166.3	-10.0	

### CHAPTER VII.

FORMATION AND SOLUTION OF THE EQUATIONS OF CONDITION RESULTING FROM THE PRECEDING COMPARISONS.

In the preceding chapter we have obtained from observations a series of corrections to the geocentric positions of Uranus resulting from the provisional theory. The further operations are as follows:—

- 1. To reduce all the corrections in right ascension and declination to corrections in geocentric longitude and latitude. Most of the corrections are already so expressed, so that this reduction is necessary in only a few cases.
- 2. To find the mean value of the correction in geocentric longitude during each opposition, and to express this mean value in terms of the correction to the heliocentric co-ordinates.
- 3. To express these corrections to the heliocentric co-ordinates in terms of corrections to the elements of Uranus and the mass of Neptune.
  - 4. To solve the equations of condition thus formed.

The first of these processes is too simple to make it necessary to present any details of it. With regard to the second I have sought, not the simple correction to the geocentric longitude, but this correction multiplied by such a factor as it was supposed would make the probable error of the correction 0".5. The equations for expressing the error of geocentric longitude in terms of errors of heliocentric longitude and radius vector have been given on page 129. The first observation of Flamstead, p. 107, gives the equation

$$+22" = 1.04\delta\lambda + .027\delta\rho$$

 $\delta\lambda$  being the correction to the heliocentric longitude, and  $\delta\rho$  that to the Neperian logarithm of the radius vector. From the discordance of Flamstead's clock errors it may be estimated that the probable error of the first member of this equation is 10". Therefore we divide the equation by 20, which gives

$$\frac{1}{20}\delta l = 1".1 = .052\delta \lambda + .001\delta \rho.$$

In the opposition of 1715 we have four observations. The best were those of March 4 and 10, of which we may estimate the probable error at 10", and the worst that of March 5, of which the probable error may be estimated at 20", while that of April 29 is intermediate in certainty. The separate observations give the equations

March 4, 
$$\delta l = +28'' = 1.06\delta \lambda$$
; Weight, 4  
March 5,  $\delta l = +44 = 1.06\delta \lambda$ ; Weight, 1  
March 10,  $\delta l = +36 = 1.06\delta \lambda$ ; Weight, 4  
April 29,  $\delta l = +2 = 1.04\delta \lambda + .04\delta \rho$ ; Weight, 2.  
Mean  $\delta l = +27.6 = 1.056\delta \lambda + .003\delta \rho$ ; probable error = ±6".

Applying the correction —1".1 for equinox, and dividing by 12, the equation of condition becomes

$$\frac{1}{12} \ell l = +2^{\circ}.2 = 0.088 \delta \lambda.$$

In this way the following equations were obtained. It is deemed unnecessary to give the details of the process, as it is one which every one can go over for himself from the data already given, and can reproduce all the results, except so far as they depend on the relative weights assigned to the different groups of observations during one and the same opposition.

No.	Date.	Equations.	Number of
10.	Date.	Equations.	observations in R. A.
1	1691.0;	$\frac{1}{20}\delta l = + 1.1 = .052\delta \lambda + .001\delta \rho$	1
2	1715.2	$\frac{1}{12} = + 2.2 = .088$	4
3	1748.8	$\frac{1}{3} = +12.8 = .338 + .017$	1
4	1750.8	$\frac{1}{3} = +11.8 = .345 + .010$	3
5	1753.9	$\frac{1}{3} = +11.6 = .333 + .016$	1
6	1756.7	$\frac{1}{5} = + 5.0 = .210 + .003$	1
7	1769.0	$\frac{2}{5} = + 4.8 = .203 + .010$	.8
8	1782.0	$\frac{4}{3} = + 3.0 = 1.370$	21
9	1783.0	1 = + 1.25 = 1.030002	13
10	1784.0	1 = + 1.92 = 1.026008	13
11	1785.0	1 = -0.26 = 1.034 + .006	10
12	1788.0	$\frac{2}{3} = + 1.23 = 0.684 + .006$	5
13	1789.0	$\frac{1}{2} = + 1.58 = 0.504 + .008$	6
14	1790.0	$\frac{1}{2} = -0.52 = 0.514013$	4
15	1791.0	$\frac{2}{3} = -0.66 = 0.684010$	7
16	1792.0	$\frac{1}{3} = -0.12 = 0.340011$	3
17	1793.0	$\frac{1}{2} = -0.19 = 0.512015$	5
18	1794.0	$\frac{1}{3} = + 0.79 = 0.344006$	3
19	1795.0	$\frac{2}{3} = -0.66 = 0.683019$	7
20	1796.0	$\frac{1}{2} = -0.68 = 0.514015$	4
21	1797.1	$\frac{1}{2} = -0.35 = 0.528$	3
22	1800.2	$\frac{1}{3} = 0.00 = 0.352$	2
23	1801.2	$\frac{1}{3} = -0.26 = 0.352$	2
24	1802.3	1 = + 0.85 = 1.05	13
25	1805.3	1 = + 0.69 = 1.05	13
26	1806.3	$\frac{1}{2} = + 0.20 = 0.52$	5
27	-1807.3	1 = + 2.34 = 1.045	16
28	1808.3	$\frac{1}{2} = -0.04 = 0.52$	6
29	1809.3	$\frac{2}{3} = + 1.80 = 0.70$	9
30	1810.3	1 = + 2.39 = 1.05	16
31	1811.3	1 = + 1.49 = 1.04 = -0.01	11
32	1812.4	$\frac{1}{2} = + 0.8 = 0.53$	. 8
33	1813.4	$\frac{1}{2} = + 1.2 = 0.53$	9
34	1814.4	1 = + 1.7 = 1.05	15

No.	Date.		Equ	ations	J.		Number of observations in R. A.
35	1815.4	3 6	l = +	2.1	$=1.58 \delta $	λ	20
36	1818.4*	-	=+		=1.58		24
37	1819.4	ĩ	=-	0.8	=1.05		11
38	1820.5	1	=-	1.3	=1.05		14
39	1821.5	$\frac{2}{3}$	=+	0.9	=0.70		10
40	1822.5	23	=+	0.9	= 0.70		7
41	1823.5	থার প্রার	=	0.0	= 0.70		11
42	1824.5	1	=+	0.5	=1.05		12
43	1825.5	$\frac{2}{3}$	=-	0.4	= 0.70		7
44	1826.5	1	=+	0.3	=1.05		11
45	1827.7	2	=-	2.7	=2.07	$+0.04 \delta \rho$	37
46	1828.7	21/2	=-	2.7.	=2.57	+0.07	67
47	1829.7	$2\frac{1}{2}$	=-	2.4	= 2.59	+0.04	61
48	1830.7	$2\frac{1}{2}$	=-	4.9	= 2.56	+0.07	73
49	1831.7	2	=	0.0	= 2.06	+0.05	54
50	1832.7	2	=-	2.2	=2.07	+0.05	65
51	1833.8	$2\frac{1}{2}$	=-	4.1	= 2.58	+0.08	88
52	1834.8	$2\frac{1}{2}$	=-	3.9	=2.57	+0.08	91
53	1835.8	$2\frac{1}{2}$	=-	5.1	=2.59	+0.05	82
54	1836.8	3	=-	7.0	= 3.11	+0.08	157
55	1837.8	3	=-	3.6	= 3.11	+0.04	162
56	1838.8	3	=-	1.6	= 3.11	+0.06	193
57	1839.8	3	=-	1.2	= 3.11	+0.06	170
58	1840.8	3	=-	1.5	= 3.11	+0.06	124
59	1841.8	3	=+	0.8	= 3.10	+0.06	108
60	1842.8	3	=+	1.6	= 3.10	+0.06	169
61	1843.8	3	=+	4.7	= 3.12	+0.04	111
62	1844.9	3	=+	5.1	= 3.11	+0.03	106
63	1845.9	2	=+	4.2	= 2.08	+0.02	55
64	1846.9	3	=+	6.3	= 3.10	+0.04	98
65	1847.9	2	=+	5.8	=2.07	+0.03	74
66	1848.9	2	=+	4.4		+0.02	59
67	1849.9	2		6.6		+0.04	33
68	1850.9	2	=+			+0.01	46
69	1851.9	2	=+	6.3	=2.07	+0.04	42
70	1852.9	2			=2.07	+0.03	54
71	1853.9	2		7.9	= 2.09	+0.01	49
72	1854.9	2		8.9	= 2.09	+0.02	49
74	1855.9	2		8.5		+0.04	48
75	1856.9	2			=2.08	+0.04	45
76	1858.0	$2\frac{1}{2}$	=+1	0.3	= 2.61	+0.09	66

<sup>\*</sup> The results for 1816 and 1817 were omitted in this list through oversight.

No.	Date.	Equations,	Number of observations in R. A.
77	1859.0	$2\frac{1}{2}\delta l = +10.6 = 2.60 \delta \lambda + 0.03 \delta$	
78	1860.0	$2\frac{1}{3} = + 8.2 = 2.60 + 0.05$	64
79	1861.0	2 = +6.3 = 2.09 + 0.03	41
80	1862.0	$2\frac{1}{3} = + 7.0 = 2.60 + 0.05$	60
81	1863.0	$2\frac{1}{2} = + 6.6 = 2.59 + 0.08$	88
82	1864.0	2 = + 4.3 = 2.09 + 0.03	35
83	1885.0	$1\frac{1}{2} = + 3.9 = 1.57 + 0.04$	37
84	1866.0	$2\frac{1}{2} = + 1.1 = 2.60 + 0.06$	76
85	1867.0	$2\frac{1}{2} = -1.8 = 2.60 + 0.02$	83
86	1868.0	2 = -3.8 = 2.09 + 0.04	40
87	1869.0	$2\frac{1}{2} = -9.1 = 2.61 + 0.02$	68
88	1870.0	2 = -9.6 = 2.084 + 0.054	31
89	1871.0	$1\frac{1}{2} = -10.6 = 1.560 + 0.040$	21
90	1872.1	$2\frac{1}{3} = -19.1 = 2.600 + 0.070$	50
	c 1		0200

We have next to express the values of  $\delta\lambda$  and  $\delta\rho$  in terms of the corrections to the elements. Differentiating the expressions

$$\lambda = l + (2e - \frac{1}{4}e^3)\sin(l - \pi) + \frac{5}{4}e^2\sin(2l - 2\pi) + \frac{1}{12}e^3\sin e^3\sin(3l - 3\pi) + \text{etc.}$$

$$\rho = \pi + \frac{1}{4}e^2 + (-e + \frac{3}{8}e^3)\cos(l - \pi) - \frac{3}{4}e^2\cos(2l - \frac{2}{5}\pi) - \text{etc.},$$

with respect to l, e, and  $\pi$ , and reducing the coefficients to numbers, we find

$$\begin{split} \frac{\partial \lambda}{\partial l} &= 1 + 0.0939 \cos g + 0.0055 \cos 2g \\ \frac{\partial \lambda}{\partial e} &= 1.999 \sin g + 0.117 \sin 2g + 0.007 \sin 3g \\ \frac{\partial \lambda}{\partial \pi} &= -2.000 \cos g - 0.117 \cos 2g - 0.007 \cos 3g \end{split}$$

We have here put l for the mean longitude, or

$$l = nt + \varepsilon$$

whence

$$\frac{\partial \lambda}{\partial \varepsilon} = \frac{\partial \lambda}{\partial l}$$
$$\frac{\partial \lambda}{\partial n} = t \frac{\partial \lambda}{\partial l}$$

Also, from the expression for p

$$\begin{split} \frac{\partial \rho}{\partial l} &= -\frac{\partial \rho}{\partial \pi} = (e - \frac{3}{8}e^3) \sin g + \frac{3}{4}e^2 \sin 2g + \dots \\ \frac{\partial \rho}{\partial e} &= \frac{1}{2}e - (1 - \frac{3}{8}e^2) \cos g - \frac{3}{2}e \cos 2g - \text{etc.} \\ \frac{\partial \rho}{\partial n} &= t \frac{\partial \rho}{\partial l} - \frac{2}{3n} \end{split}$$

The values of these coefficients which depend only on g are shown in the following table:

21 May, 1873.

	22	$\partial \lambda$	<i>δ</i> λ	20	20	20
	$\partial \lambda$			$\partial \rho$	δρ	. 20
g	$\partial \varepsilon$	de	$ed\pi$	$\partial \varepsilon$	$\partial e$	$ed\pi$
00	+1.099	0	-2.124	0	_1.00	0
ĭ	1.099	+0.039	2.124	+0.001	1.00	-0.02
2	1.099	0.079	2.123	0.002	1.00	0.03
3	1.099	0.118	2.121	0.002	1.00	0.05
4	1.099	0.158	2.118	0.003	1.00	0.07
5	+1.099	+0.196	-2.114	+0.004	_1.00	-0.09
6	1.099	0.235	2.110	0.005	0.99	0.10
7	1.099	0.274	2.105	0.006	0.99	0.12
8	1.098	0.313	2.099	0.006	0.99	0.14
9	1.098	0.352	2.092	0.007	0.99	0.16
10	+1.098	+0.391	-2.085	+0.008	-0.98	-0.17
11	1.097	0.430	2.077	0.009	0.98	0.19
12	1.097	0.468	2.069	0.010	0.98	0.21
13	1.097	0.505	2.059	0.011	0.97	0.22
14	1.096	0.544	2.049	0.011	0.97	0.24
15	+1.096	+0.581	-2.038	+0.012	-0.97	-0.26
16	1.095	0.618	2.027	0.013	0.96	0.28
17	1.095	0.655	2.014	0.014	0.96	0.29
18	1.094	0.693	2.001 .	0.015	0.95	0.31
19	1.094	0.729	1.987	0.015	0.95	0.33
20	+1.093	+0.765	-1.973	+0.016	-0.94	-0.34
21	1.092	0.801	1.957	0.017	0.93	0.36
22	1.091	0.836	1.941	0.018	0.93	0.37
23	1.090	0.872	1.925	0.018	0.92	0.39
24	1.090	0.907	1.907	0.019	0.91	0.41
25	+1.089	+0.942	-1.890	+0.020	-0.91	-0.42
26	1.088	0.976	1.872	0.021	0.90	0.44
27	1.087	1.010	1.852	0.021	0.89	0.45
28	1.086	1.043	1.832	0.022	0.88	0.47
29	1.085	1.076	1.811	0.023	0.87	0 48
30	+1.084	+1.108	-1.790	+0.023	-0.87	-0.50
31	1.084	1.140	1.769	0.024	0.86	0.51
32	1.083	1.172	1.747	0.025	0.85	0.53
33	1.082	1.203	1.724	0.026	0.84	0.54
34	1.080	1.233	1.700	0.026	0.83	0.56
35	+1.079	+1.264	-1.676	+0.027	-0.82	-0.57
36	1.078	1.294	1.651	0.028	0.81	0.59
37	1.077	1.323	1.626	0.028	0.80	0.60
38 39	1.076	1.351	1.601	0.029	0.79	0.62
40	1.074	1.379	1.574	0.030	0.78	0.63
41	+1.073 $1.072$	+1.407 $1.434$	-1.548 $1.521$	+0.030	-0.77	-0.64
42	1.070	1.460		0.031	0.76	0.66
43	1.069	1.486	1.494	0.031	0.74	0.67
44	1.068	1.486	1.466	0.032	0.73	0.68
45	+1.067	+1.536	1.438 —1.409	0.033	0.72	0.70
46	1.065	1.561	1.380	+0.033	-0.71	-0.71
47	1.064	1.584	1.351	$0.034 \\ 0.034$	0.70	0.71
48	1.063	1.606	1.320	0.035	0.68	$0.72 \\ 0.74$
49	1.061	1.629	1.290	0.036	0.67	0.74
50	+1.060	+1.651	-1.260	+0.036	0.66	-0.76 -0.76
51	1.058	1.672	1.229	0.037	-0.64 $0.63$	0.77
52	1.057	1.692	1.197	0.037	0.63	0.78
53	1.055	1.712	1.165	0.037		0.18
54	1.054	1.731	1.133	0.038	0.60 0.59	0.19
55	+1.052	+1.750	-1.100	+0.038	-0.57	_0.80 _0.81
56	1.051	1.768	1.067	0.039	0.56	$-0.81 \\ 0.82$
57	1.049	1.785	1.034	0.039	0.54	0.83
58	1.047	1.802	1.002	0.040	0.53	0.84
59	+1.046	+1.817	-0.968	+0.040	-0.51	-0.85
				10.000	-0.01	
	V.I					

	da.	ðλ	<i>δ</i> λ	do	∂ρ	θρ
g		A STATE OF THE PARTY OF THE PAR			months .	Married Committee
	86	de	$ed\pi$	$\partial \varepsilon$	de	$ed\pi$
600	11.044	11 000	0.095	10.041	0.50	-0.86
61	+1.044 1.043	+1.833 1.848	-0.935 0.901	+0.041 0.041	-0.50 0.49	0.87
62	1.041	1.862	0.867	0.041	0.47	0.87
63	1.040	1.875	0.832	0.042	0.45	0.88
64	1.038	1.888	0.798	0.042	0.44	0.89
65	+1.036	+1.901	-0.763	+0.043	-0.42	-0.90
66	1.034	1.912	0.728	0.043	0.41	0.91
67	1.033	1.922	0.693	0.043	0.39	0.91
68	1.031	1.932	0.659	0.044	0.37	0.92
69	1.030	1.942	0.624	0.044	0.36	0.93
70	+1.028	+1.950	-0.588	+0.044	-0.34	-0.94
71 72	1.027 1.025	1.959 1.967	0.553 0.518	0.044 0.045	0.33 0 31	0.95 0.95
73	1.023	1.974	0.483	0.045	0.29	0.96
74	1.021	1.980	0.447	0.045	0.28	0.96
75	+1.019	+1.985	-0.412	+0.045	-0.26	_0.97
76	1.018	1.990	0.376	0.046	0.24	0.97
77	1.016	1.994	0.341	0.046	0.22	0.97
78	1.014	1.997	. 0.305	0.046	0.21	0.98
79	1.013	2.000	0.269	0.046	0.19	0.98
80	+1.011	+2.003	-0.233	+0.046	-0.17	-0.98
81	1.010	2.005	0.198	0.046	0.16	0.99
82	1.008	2.007	0.163	0.046	0.14	0.99
83 84	1.006 1.005	2.007 2.006	0.128 0.093	0.047 0.047	0.12 0.11	0.99
85	+1.003	+2.005	-0.057	+0.047	-0.09	-1.00
86	1.002	2.004	-0.022	0.047	0.07	1.00
87	1.000	2.002	+0.013	0.047	0.05	1.00
88	0.998	2.000	0.048	0.047	0.03	1.00
89	0.997	1.997	0 082	0.047	-0.02	1.00
90	+0.995	+1.993	+0.117	+0.047	0.00	-1.00
91	0.993	1.989	0.152	0.047	+0.02	1.00
92	0.992	1.984	0.186	0.047	0.03	1.00
93	0.990 0.988	1.978 1.972	0.220 0.254	0.047 0.047	0.05 0.07	1.00
94 95	+0.987	+1.965	+0.287	+0.047	+0.09	-1.00
96	0.985	1.958	0.321	0.047	0.11	0.99
97	0.984	1.950	0.354	0.047	0.12	0.99
98	0.982	1.943	0.387	0.046	0.14	0.99
99	0.980	1,933	0.421	0.046	0.16	0.99
100	+0.979	+1.924	+0.453	+0.046	+0.17	-0.98
101	0.977	1.914	0.487	0.046	0.19	0.98
102	0.976	1.903	0.519 0.551	0.046	$0.21 \\ 0.22$	0.98 0.97
103	0.974 0.972	1.893 1.882	0.582	0.046	0.24	0.97
104 105	+0.971	+1.869	+0.614	+0.045	+0.26	-0.97
106	0.969	1.857	0.645	0.045	0.28	0.96
107	0.968	1.844	0.677	0.045	0.29	0.96
108	0.967	1.829	0.707	0.045	0.31	0.95
109	0.965	1.815	0.737	0.044	0.33	0.95
110	+0.964	+1.800	+0.768	+0.044	+0.34	-0.94
111	0.962	1.786	0.798	0.044	0.36	0.93 0.92
112	0.961 0.959	1.770	0.827 0.855	0.044	0.37 0.39	0.92
113 114	0.959	1.754 1.738	0.884	0.043	0.41	0.91
115	0.956	+1.721	+0.913	+0.043	+0.42	-0.90
116	0.955	-1.704	0.942	0.042	0.44	0.89
117	0.954	1.686	0.970	0.042	0.45	0.88
118	0.953	1.668	0.997	0.041	0.47	0.87
119	+0.951	+1.650	+1.025	+0.041	+0.49	-0.87
			-			

				1	1	
	da.	da.	$\partial \lambda$	$\partial \rho$	$\partial \rho$	∂ρ
g			$\frac{\partial n}{\partial n}$	$\partial \varepsilon$	$\frac{\partial p}{\partial e}$	
9	$\partial \varepsilon$	de	$ea\pi$	OE.	oe .	$ed\pi$
1000	10000	11.001	11.051	+0.041	+0.50	0.00
120° 121	+0.950 0.949	+1.631 1.611	+1.051 $1.077$	0.040	0.51	-0.86 0.85
122	0.948	1.592	1.104	0.040	0.53	0.84
123	0.947	1.571	1.129	0.039	0.54	0.83
124	0.945	1.551	1.154	0.039	0.56	0.82
125	+0.944	+1.530	+1.180	+0.038	+0.57	-0.81
126	0.943	1.509	1.205	0.038	0.59	0.80
127	0.942	1.488	1.229	0.037	0.60	0.79
128	0.941	1.466	1.253	0.037	0.62	0.78
129	0.940	1.443	1.277	0.037	0.63	0.77
130	+0.939	+1.421	+1.300	+0.036	+0.64	-0.76
131 132	0.937 0.936	1.397	1.322 1.344	0.036 0.035	0.66 0.67	$0.75 \\ 0.74$
133	0.936	1.350	1.367	0.033	0.68	0.74
134	0.935	1.327	1.388	0.034	0.70	0.71
135	+0.934	+1.302	+1.409	+0.033	+0.71	-0.71
136	0.933	1.277	1.430	0.033	0.71	0.70
137	0.932	1.253	1.451	0.032	0.72	0.68
138	0.931	1.228	1.470	0.031	0.74	0.67
139	0.930	1.202	1.489	0.031	0.75	0.66
140	+0.929	+1.177	+1.508	+0.030	+0.76	-0.64
141 142	0.928	1.151	1.527	0.030	0.77	0.63
143	0.927 0.927	1.124 1.099	1.545 1.562	$0.029 \\ 0.028$	0.78 0.79	0.62
144	0.926	1.072	1.580	0.028	0.80	0.59
145	+0.925	+1.044	+1.596	+0.027	+0.81	-0.57
146	0.924	1.016	1.613	0.026	0.82	0.56
147	0.923	0.989	1.629	0.026	0.83	0.54
148	0.922	0:962	1.644	0.025	0.84	0.53
149	0.922	0.934	1.659	0.024	0.85	0.51
150 151	$+0.921 \\ 0.921$	+0.906	+1.674	+0.023	+0.86	-0.50
152	0.921	$0.878 \\ 0.849$	1.688 1.702	0.023	0.87	0.49
153	0.919	0.820	1.714	$0.022 \\ 0.021$	0.87 0.88	0.47 0.45
154	0.919	0.792	1.727	0.021	0.89	0.44
155	+0.919	+0.762	+1.740	+0.020	+0.90	-0.42
156	0.918	0.733	1.751	0.019	0.91	0.41
157	0.918	0.704	1.763	0.018	0.91	0.39
158	0.917	0.674	1.773	0.018	0.92	0.37
159	0.916.	0.645	1.783	0.017	0.93	0.36
160 161	+0.916 0.915	+0.615	+1.793	+0.016	+0.94	-0.34
162	0.915	$0.585 \\ 0.555$	1.803 1.811	0.015 0.015	0.95	0.33
163	0.915	0.525	1.820	0.015	$0.95 \\ 0.96$	$0.31 \\ 0.29$
164	0.915	0.494	1.829	0.013	0.96	0.28
165	+0.914	+0.465	+1.836	+0.012	+0.97	-0.26
166	0.914	0.435	1.843	0.011	0.97	0.24
167	0.914	0.403	1.849	0.011	0.97	0.22
168	0.913	0.373	1.855	0.010	0.98	0.21
169 170	0.913	0.343	1.860	0.009	0.98	0.19
171	+0.913 $0.912$	+0.311 $0.280$	+1.865	+0.008	+0.98	-0.17
172	0.912	0.280	$1.870 \\ 1.875$	0.007	0.99	0.16
173	0.912	0.219	1.879	0.006	$0.99 \\ 0.99$	0.14 0.12
174	0.912	0.187	1.882	0.005	0.99	0.12
175	+0.911	+0.156	+1.884	+0.004	+1.00	-0.09
176	0.911	0.126	1.886	0.003	1.00	0.07
177 178	0.911	0.094	1.888	0.002	1.00	0.05
178	$0.911 \\ +0.911$	$0.063 \\ +0.031$	1.889	0.002	1.00	0.03
* 10	70.311	70.031	+1.890	+0.001	+1.00	-0.02

In the equations of condition ten years has been adopted for the unit of time, in order to make the general value of the coefficients as nearly equal as possible, and the time has been counted from the epoch 1830.0, in order to have the positive and negative values of t in the equations more nearly balanced. To distinguish these values of  $\delta_{\varepsilon}$  and  $\delta_n$  they are marked with an accent. This unit of time gives 0.8914 for the value of  $\frac{2}{3n}$  in arc, whence

$$\frac{\partial \rho}{\partial n'} = t \frac{\partial \rho}{\partial l} - 0.891.$$

The equations of condition are now formed by putting in the preceding equations for heliocentric longitude and radius vector

$$\delta\lambda = \frac{\partial\lambda}{\partial\varepsilon}\delta\varepsilon + \frac{\partial\lambda}{\partial\upsilon}\delta\upsilon + \frac{\partial\lambda}{\partial\dot{e}}\delta\varepsilon + \frac{\partial\lambda}{e\partial\pi}e\delta\pi + \frac{\partial\lambda}{\partial\dot{\mu}}\delta\mu'$$
$$\delta\rho = \frac{\partial\rho}{\partial\varepsilon}\delta\varepsilon + \frac{\partial\delta}{\partial\boldsymbol{n}}\delta\upsilon + \frac{\partial\rho}{\partial\dot{e}}\delta\varepsilon + \frac{\partial\rho}{e\partial\pi}e\delta\pi.$$

For the coefficients  $\frac{\partial \lambda}{\partial \mu'}$  have been taken one-hundredth the perturbations of longitude produced by Neptune, as given in the heliocentric ephemeris at the end of Chapter V. The corrected mass of Neptune will then be

$$\frac{1}{17000}(1+\frac{\delta\mu'}{100})$$

Finally, I remark that all the preceding comparisons are made with the heliocentric ephemeris as printed, without the correction indicated in the column adjoining it, but in the following equations this correction is for the first time introduced.

Equations of condition given by the Corrections in Longitude.

	1		0 0			
1	0.05δε'	- 0.70£n'	-0.108e	$+0.03e\delta\pi$	$+0.12\delta\mu'$	=+1".1
2	0.10	- 1.11	+0.01	-0.19	+0.12	=+2.2
3	0.31	- 2.55	+0.33	+0.51	-0.22	=+12.8
4	0.32	- 2.52	+0.27	+0.58	-0.18	=+11.8
5	0.30	- 2.32	+0.12	+0.59	-0.09	=+11.6
6	0.19	_ 1.40	-0.01	+0.39	0.00	=+5.0
7	-0.19	_ 1.18	-0.29	+0.23	+0.22	=+4.8
8	1.41	- 6.75	-2.69	-0.75	+2.47	=+28
9	1.06	_ 5.01	-1.98	-0.72	+1.85	=+1.1
10	1.07	- 4.91	-1.94	-0.86	+1.85	=+1.7
11	1.09	_ 4.87	-1.86	-1.04	+1.85	=-0.5
12	0.73	- 3.06	-1.04	-0.97	+1.16	=+1.0
13	0.54	- 2.20	-0.71	-0.78	+0.82	=+1.4
14	0.55	- 2.19	-0.68	-0.81	+0.81	=-0.6
15	0.73	- 2.86	-0.82	-1.16	+1.03	=-0.9
16	0.37	- 1.39	-0.36	-0.60	+0.49	=-0.2
17	0.56	- 2.05	-0.47	-0.95	+0.70	=-0.4
18	0.37	- 1.33	-0.26	-0.65	+0.44	=+0.6
19	0.75	_ 2.59	-0.38	-1.34	+0.82	=-1.0
10	0.10	2.00		A CONTRACTOR OF THE PARTY OF TH	THE RESIDENCE OF	

20	0 5051	1 200 1	. 200	$-1.04e\delta\pi$	$+0.585\mu'$	=-0".9
20	0.56  Se'		$-0.22\delta e$	$-1.04e_0\pi$ $-1.12$	+0.55 $+0.55$	= -0.5
21	0.58	-1.92	-0.13		+0.24	= -0.3 = $-0.2$
22	0.38	- 1.15	+0.09	-0.74	+0.24	= -0.2 = $-0.3$
23	0.38	- 1.11	+0.15	-0.73	+0.21	
24	1.15	- 3.18	+0.65	-2.13	+0.50	=+0.6
25	1.13	-2.81	+1.11	-1.91	+0.19	=+0.5
26	0.56	<b>—</b> 1.33	+0.62	-0.89	+0.05	=+0.1
27	1.12	-2.54	+1.38	-1.68	0.00	=+2.1
28	0.56	-1.21	+0.75	-0.79	-0.04	= $-$ 0.1
29	0.70	-1.55	+1.09	-0.97	-0.10	=+1.6
30	1.11	-2.19	+1.73	-1.32	-0.23	=+2.2
31	1.09	-2.04	+1.81	-1.14	-0.29	=+1.3
32	0.56	-0.98	+0.96	-0.51	-0.18	=+0.7
33	0.55	-0.91	+1.00	-0.43	-0.21	=+1.1
34	1.08	<b>—</b> 1 69	+2.03	-0.71	-0.46	=+1.5
35	1.63	-2.37	+3.11	-0.82	-0.74	=+2.0
35'	1.07	-1.45	+2.08	-0.38	-0.52	=+0.4
35"	1.06	-1.33	+2.10	-0.22	-0.55	=+0.8
36	1.58	- 1.83	+3.18	-0.09	-0.85	=+0.3
37	1.05	- 1.11	+2.10	+0.08	0.59	= -0.8
38	1.04	-0.99	+2.07	+0.26	0.59	=-1.3
39	0.69	_ 0.58	+1.36	+0.27	-0.39	=+0.8
40	0.69	_ 0.51	+1.33	$\pm 0.38$	-0.39	= + 0.8
41	0.68	_ 0.44	+1.29	+0.47	-0.39	= 0.0
42	1.01	-0.56	+1.88	+0.84	-0.59	= + 0.3
43	0.67	_ 0.30	+1.20	+0.64	-0.38	= -0.5
41	1.00	-0.35	+1.72	+1.09	-0.57	=+0.2
45	1.95	-0.50	+3.21	+2.39	-1.12	= $-2.5$
46	2.42	-0.37	+3.77	+3.21	-1.36	= -2.6
47	2.42	-0.12	+3.53	+3.52	-1.37	= -2.4
48	2.39	+ 0.12	+3.22	+3.69	-1.33	= -4.9
49	1.91	+ 0.28	+2.37	+3.14	-1.07	=-0.1
50	1.91	+ 0.48	+2.15	+3.30	-1.08	=-2.4
51	2.37	+ 0.83	+2.34	+4.32	-1.34	=-4.5
52	2.36	+ 1.06	+2.02	+4.44	-1.36	=-4.3
53	2.37	+1.32	+1.68	+4.62	-1.37	= -5.5
54	2.85	+ 1.86	+1.66	+5.64	-1.68	=-7.5
55	2.84	+2.17	+1.22	+5.74	-1.71	=-4.1
56	2.84	+ 2.44	+0.81	+5.84	-1.74	= -2.1
57	2.83	$+\frac{2.71}{2.71}$	+0.40	+5.88	-1.78	= -1.7
58	2.83	$+\ \tilde{3.00}$	-0.06	+5.88	-1.82	= -2.0
59	2.82	+3.28	-0.44	+5.84	-1.86	= + 0.3
60	2.83	+3.57	-0.44	+5.81	-1.91	= + 1.2
61	2.85	+3.90	-0.04 $-1.27$	+5.78	-1.98	= + 4.4
62	2.85	+4.21	-1.74	+5.64	-2.02	= +4.8
63	1.91	+3.02	-1.42	+3.69	-2.02 $-1.39$	= + 4.0 = + 4.0
64	2.85	+ 4.78	-2.50	+5.52	-1.59 $-2.14$	= + 4.0 = $+ 6.0$
65	1.91	+ 3.39	-2.50 $-1.92$		-2.14 $-1.47$	= + 0.0 = + 5.6
66	1.92	$+\ 3.61$	-1.92 $-2.18$	+3.46		
67	1.93	+3.81 + 3.82	-2.18 $-2.40$	+3.32	-1.52	
68	1.94	+ 3.62 + 4.05	-2.40 $-2.65$	+3.17	-1.56	= + 6.6
69	1.94	$+4.05 \\ +4.20$	-2.03 $-2.83$	+2.98	-1.60	= + 7.3
00	1.01	7 1.20	-2.00	+2.80	-1.64	=+6.5

70	$1.95\delta\epsilon'$	$+4.44\delta n'$	-3.04£e	$+2.59e\delta\pi$	$-1.68\delta\mu$	=+6''.8
71	1.98	+ 4.72	-3.23	+2.37	-1.73	=+8.1
72	1.99	+ 4.93	-3.44	+2.15	-1.76	=+9.1
73	1.99	+ 5.13	-3.58	+1.91	-1.78	=+8.7
74	2.00	+5.35	-3.73	+1.64	-1.80	=+8.1
75	2.53	+7.02	-4.83	+1.73	-2.30	=+10.6
76	2.54	+ 7.34	-4.96	+1.33	-2.29	=+10.9
77	2.56	+ 7.64	-5.07	+0.97	-2.31	=+8.2
78	2.07	+6.38	-4.14	+0.47	-1.86	=+6.3
79	2.59	+ 8.25	-5.20	+0.21	-2.32	=+7.0
80	2.60	+ 8.51	-5.21	-0.15	-2.29	=+6.6
81	2.11	+ 7.14	-4.19	-0.51	-1.83	=+4.3
82	1.60	+ 5.56	-3.13	-0.58	-1.36	=+3.9
83	2.67	+ 9.59	-5.12	-1.37	-2.20	=+1.1
84	2.68	+ 9.92	-5.00	-1.80	-2.14	=-1.8
85	2.17	+ 8.22	-3.92	-1.75	-1.67	= -3.8
86	2.73	+10.61	-4.97	-2.59	-2.01	= -9.0
87	2.20	+ 8.78	-3.63	-2.33	-1.52	= -9.5
88	1.65	+ 6.74	-258	-1.96	-1.08	=-10.5
89	2.77	+11.61	-4.04	-3.61	-1.69	=-19.9

The following are the approximate normals to which these equations give rise. Inaccuracies being detected in several of the equations of condition after these normals were formed, they do not accurately correspond to those equations as written.

The values of the unknown quantities deduced from these normals were substituted in the equations of condition, and a farther approximation was made by solving the equations given by the residuals. The following are the first approximations given by the normals, and the finally concluded corrections

The final values of the corrections being substituted in the equations leave the following system of residuals, or outstanding excesses of the observed longitudes over theory. Column  $f \delta l$  gives the residual of the equation itself; the probable error of which has always been judged to be 0."5, while in column  $\delta l$  this residual is divided by f to obtain the residual correction of the longitude itself. The values of the factors f are found with the original equations on pages 159 and 160.

No.	of Eq.	Year.	$f\delta l$	87	No.	of Eq.	Year.	£87	87
	1	1691.0	-0.5	<b>—10.</b>		35"	1817.4	-0.3	- 0.3
		2002.0	12 1125			36	1818.4	-0.7	- 0.5
	2	1715.2	-0.8	<b>—10.</b>	H	37	1819.4	-1.4	- 1.4
	0	15400	115	1 15		38	1820.5	-1.4	_ 1.4
		1748.8	+1.5	+4.5		39	1821.5	+0.9	+ 1.4
		1750.8	+0.8	+ 2.4					
		1753.9	+2.2	+6.6			1822.5	+1.4	+ 2.1
	6	1756.7	-0.2	— 1.0			1823.5	+0.6	+ 0.9
	7	1769.0	-0.2	_ 1.0			1824.5	+1.2	+ 1.2
				1,500	10		1825.5	+0.7	+ 1.0
		1782.0	+0.1	+ 0.2		44	1826.5	+2.0	+ 2.0
	9	1783.0	-0.5	<b>—</b> 0.5		15	1007 7	110	1 0 5
		1784.0	+0.6	+ 0.6			1827.7	+1.0	+ 0.5
]	11	1785.0	-1.0	<b>—</b> 1.0			1828.7	+2.5	+ 1.0
	10	1700 0	119	1 1 2			1829.7	+2.8	+1.1
		1788.0	$+1.2 \\ +1.7$	+ 1.8 + 3.4			1830.7	+0.4	+ 0.2
		1789.0 1790.0	-0.5	<del>- 1.0</del>		49	1831.7	+4.1	+ 2.0
		1790.0	_0.7	$\frac{-1.0}{-1.0}$		50	1832.7	+1.8	+ 0.9
		1792.0	0.0	$\frac{-1.0}{0.0}$			1833.8	+0.5	+ 0.2
	10	1192.0	0.0	0.0			1834.8	+0.1	0.0
- y	17	1793.0	-0.1	- 0.2			1835.8	-1.4	- 0.6
		1794.0	+0.5	+ 1.5			1836.8	-3.4	- 1.1
		1795.0	-0.6	_ 0.9		01	1000.0		
2	20	1796.0	-0.5	_ 1.0		55	1837.8	-0.6	- 0.2
2	21	1797.1	-0.6	- 1.2	173		1838.8	+0.5	+ 0.2
							1839.8	-0.4	- 0.1
		1800.2	-1.4	<b>—</b> 4.2		58	1840.8	-1.7	- 0.6
		1801.2	-1.4	- 4.2	1	59	1841.8	-0.3	- 0.1
2	24	1802.3	-0.6	- 0.6					
S	25	1805.3	-1.4	_ 14		60	1842.8	-0.5	- 0.2
		1806.3	-1.0	-2.0		61	1843.8	+1.6	+ 0.5
		1807.3		- 0.1		62	1844.9	+0.7	
		1808.3	-1.0	- 2.0		63	1845.9	+0.6	+ 0.3
-		1000.0	3.0	~.0		64	1846.9	-0.4	- 0.1
2	29	1809.3	+0.1	+ 0.2					
3	80	1810.3	-0.1	- 0.1			1847.9	+0.6	+ 0.3
3	1	1811.3	-0.9	<b>—</b> 0.9			1848.9		
							1849.9	+0.2	
		1812.4	-0.3	<b>—</b> 0.6	1		1850.9	+0.3	
		1813.4	+0.1	+ 0.2		69	1851.9	-1.2	- 0.6
		1814.4	0.4	- 0.4		<b>~</b> 0	1000	1.0	0.0
		1815.4	-0.3	- 0.2			1852.9	-1.2	<b>-</b> 0.6
5	35'	1816.4	-0.8	- 0.8		71	1853.9	-0.2	<b>—</b> 0.1
					1				

No. of Eq.	Year.	f81	13	No. of Eq.	Year.	f8l	87
72	1854.9	+0.5	+ 0.2	81	1864.0	+0.7	+ 0.4
73	1855.9	0.0	0.0	82	1865.0	+2.2	+ 1.5
74	1856.9	-0.5	- 0.2	83	1866.0	+1.0	+ 0.4
75	1858.0	-0.2	- 0.1	84	1867.0	+0.5	+ 0.2
76	1859.0	+0.9	+ 0.4				
77	1860.0	-1.1	- 0.4		1868.0	+0.4	+ 0.2
78	1861.0	-0.6	- 0.3		1869.9	-1.9	- 0.8
79	1862.0	-0,6	- 0.2	87	1870.0	-0.1	0.0
		M SEA SEA		88	1871.0	-1.2	- 0.8
80	1863.0	+0.2	+ 0.1	89	1872.1	+0.4	+ 0.2

A simple glance at the course of the residuals shows (1) that their probable value is considerably greater than the probable error attributed to the equations of condition, being more nearly 0".7 than 0".5, and yet larger in the later years; (2) that during certain periods they are of a systematic character. During the years 1748 to 1753 the observations show a decided positive correction to the theory of a magnitude greater than we can consider probable, amounting to about one-third of a second of time in the mean of Bradley's two observations of 1748 and 1753. About 1800 the correction becomes negative, and so continues for 20 years with an average value of about 1". In 1821 it suddenly becomes positive, and so continues until 1833. From this year forward the residuals are not systematic in character.

In order to show clearly the general course of the outstanding corrections, they have been divided into groups, generally including about five years each. The mean outstanding correction for each group, taken with respect to the weights indicated by the factors f, is as follows. In the column  $\varepsilon$  is shown what the probable error of the residual should be if the weights assigned to the several equations were strictly correct, and no systematic errors were present either in theory or observation.

Year.	13		Year.	38	£ ,,
1715.2	-10.	+6.	1824.8	+ 1.50	+0.16
1751.1	+ 3.7	±0.8	1829.7	+ 0.91	±0.10
1769.0	_ 1.0	±2.5	1835.2	- 0.27	±0.09
1783.3	0.18	$\pm 0.23$	1839.8	- 0.17	士0.07
1790.0	+ 0.62	±0.40	1844.8	+ 0.14	$\pm 0.03$
1795.0	- 0.55	土0.41	1849.9	- 0.21	$\pm 0.11$
1802.0	- 1.25	$\pm 0.45$	1854.9	- 0.14	$\pm 0.11$
1806.5	_ 1.00	$\pm 0.31$	1860.0	- 0.13	土0.09
1810.5	- 0.37	$\pm 0.32$	1865.0	+ 0.36	$\pm 0.10$
1814.5	- 0.37	±0.23	1870.0	- 0.21	$\pm 0.11$
1819.5.	- 0.37	<b>±</b> 0.18			
22 May	, 1873.				

A simple glance at the residuals  $\delta l$  shows that they are much greater than the purely accidental residuals resulting from the theory of least squares. We may divide the possible causes of these systematic errors into three classes.

- 1. Systematic Errors of Observation.—These may result from deviation of the line of collimation of the instrument from a true great circle, or from any peculiarity of the observer which leads to his registering the transit of Uranus earlier or later than that of a fixed star. If we compare the corrections derived from the work of different observatories as given in the last chapter, we shall find frequent cases not only of systematic differences between the results of different observatories, but between those of the same observatory in two successive years. An instance which particularly attracted my attention on first preparing the comparisons of theory and observation is that of the Greenwich observations for 1831, which, as compared with observations at the same observatory during the years preceding and following, seem to be affected with some constant error in R. A. of about 2". I find that this discrepancy can be attributed only to the original observations.
- 2. Errors in the Theory compared.—These may arise from errors in the preceding theoretical computations, from the omission of the terms of the second order produced by Neptune, from the adoption of an erroneous mass of Saturn, or from the attraction of an unknown planet. With regard to the probability of these different sources of error it may be remarked that errors of computation seem possible only in the terms of the second order, that the mass of Saturn is taken from the exhaustive discussion of the Saturnian system by Bessel, in which an error sufficient to influence the theory of Uranus seems highly improbable, and that a trans-Neptunian planet large enough to produce a sensible deviation of the orbit of Uranus from an ellipse in the course of a century would be too large to have escaped detection. The choice of the elliptic elements of Uranus and Neptune is such that the terms of the second order, due to the action of Neptune, can scarcely become sensible within a century of the epoch.
- 3. Errors in the various Reductions by which Theory and Observation are compared.—In the method adopted for comparing theory and observation a number of small uncertainties incident to the imperfections of the older data of reduction necessarily creep in. In the early observations the imperfections arise principally from the uncertainty of the instrumental corrections, and the errors in the adopted positions of the fundamental stars, and indeed in nearly all the data of reduction. In the late years they arise principally from the great magnitude of the correction to Bouvard's tables, and the consequent rapid change of the corrections to the geocentric ephemerides, which make the determination of the corrections  $\Delta l$  and Errors from theory and observation somewhat uncertain. Errors from this source will necessarily be in part of a systematic character, and, in view of their possibility, I regret not having been able to completely re-reduce all the observations before 1840, and to compare all since directly with ephemerides computed from the provisional theory. In order, however, to test the question whether they are sensible, I have prepared an ephemeris from the provisional theory for the three recent oppositions of 1861-2, 1862-3, and 1872, and compared it directly with

the observations. The mean corrections in geocentric longitude for groups of observations are given in columns (2), column (1) showing the correction given by the work of the last chapter.

Opposition 1861-2	1862-3	1872
(1) (2)	(1) (2)	(1) (2)
+2''.8 + 2''.4	$+2''.6 + 2''.6_1$	$-8''.6$ $-9''.0_1$
2.9 2.43	$2.3   2.3_2$	$-8.5 -8.1_{2}$
$3.0  3.1_2$	$2.1   2.0_3$	$-7.3 -7.5_{3}$
$2.4   2.4_2$	3.3 2.94	-7.3 -7.7
	$2.6   2.7_1$	$-7.8 -7.6_1$
Mean +2.79 +2.62	+2.65 +2.50	-7.65 - 7.82

A systematic difference of 0".16 would seem to be indicated, and on account of it a correction of 0".10 was applied to the comparisons of the last few years in forming the equations of condition.

In view of the possibility of systematic errors from this source it may be considered that too great relative weight has been assigned to the results of the later observations. If the residuals arise from errors of comparison and of theory, their probable magnitude is nearly as great at one epoch as at another. It may therefore be interesting to inquire what result we should get if, instead of assigning such different weights to the comparisons at different epochs, we sought only for the best general agreement with observations during the period the planet has been observed. The preceding system of mean residuals will enable us to discuss this question quite easily. In the first solution we shall reject the results from Flamstead's observations, owing to their assured uncertainty, and those from Le Monnier's of 1769, owing to the possible maladjustment of his quadrant. The equations from the remaining residuals will be the following:

$1.0\delta^2\varepsilon'$	$-7.6\delta^2 n'$	$+0.8\delta^2e$	$+1.7e\delta^2\pi$	$-0.5\delta^2\mu'$	=+3''.7	Wt. 1
1.1	-5.0	-2.0	-0.8	+1.8	=-0.18	2
1.1	-4.4	-1.4	-1.6	+1.6	=+0.62	. 1
1.1	-3.9	-0.6	-2.0	+1.2	=-0.55	1
1.2	-3.2	+0.6	-2.1	+0.5	=-1.25	1
1.1	-2.6	+1.3	-1.8	0.0	=-1.00	2
1.1	-2.2	+1.7	-1.3	-0.2	=-0.37	2
1.1	-1.7	+2.0	-0.7	-0.5	=-0.37	2
1.0	-1.1	+2.1	+0.1	-0.6	=-0.37	2
1.0	-0.5	+1.8	+0.9	-0.6	=+1.50	2
1.0	0.0	+1.4	+1.4	-0.5	=+0.91	3
0.9	+0.5	+0.8	+1.8	-0.5	=-0.27	3
0.9	+0.9	+0.1	+2.0	-0.6	=-0.17	3
1.0	+1.4	-0.6	+1.9	-0.7	=+0.14	3
1.0	+1.9	-1.2	+1.6	-0.8	=-0.21	3
1.0	+2.5	-1.7	+1.1	-0.9	=-0.14	3
1.0	+3.1	-2.0	+0.4	-0.9	=-0.13	3
1.1	+3.7	-2.1	-0.4	-0.9	=+0.36	3
1.1	+4.4	-1.8	-1.2	-0.8	=-0.21	3

Giving these nineteen equations equal weights, we have the second of the following solutions, and the second of the series of residuals the first corresponding to the primitive solution. Solving them again and assigning the weights attached to the respective equations, which I judge to be those to which they are entitled when a liberal allowance is made for systematic errors of observation and of comparison of theory with observations, adding also the equations given by the observations of Flamstead and Le Monnier, which are as follows:

1690	$0.0\delta^{2}$	$\varepsilon' = 0.7\delta^2$	$n'=0.1\delta^2$	e + 0.0ec	$\delta^2\pi + 0.1\delta^2\mu$	u' = -0".5;	$f, \frac{1}{20};$	Wt, 1
						=-0.5		
1769	0.2	-1.2	-0.3	+0.2	+0.2	=+2.2	1/5	1

(2)

-0''.39

(3)

-0.21

we have the second solution, and the third series of residuals.

(I)

 $\delta^2 \varepsilon_1$ 

$\delta^2 n_1$	0	-0.38	-0.19
$\delta^2 e^{-}$	0	-0.33	-0.15
$e\delta^2\pi$	0	+0.25	+0.19
$\delta^2 \mu'$	0	-1.02	-0.49
m'	19110	19870	$\frac{1}{1}\frac{1}{97}\frac{1}{50}$
	WATER STATE OF THE		13,00
		RESIDUALS.	
Year.	$\Delta_1 l$	$\Delta_2 l$	$\Delta_3 l$
1001.0	10	1/	"
1691.0	10.	-14.	<b>—12.</b>
1715.2	-10.	— 9.	<b>— 7</b> .
1751.1	+ 3.7	+ 0.5	+ 2.0
1769.0	<b>—</b> 1.0	- 2.6	<b>—</b> 1.9
1783.3	- 0.18	- 0.30	-0.17
1790.0	+ 0.62	+ 0.93	+ 0.89
1795.0	-0.55	- 0.09	<b>—</b> 0.18
1802.0	-1.25	- 0.78	- 0.87
1806.5	<b>—</b> 1.00	<b>—</b> 0.69	-0.73
1810.5	<b>—</b> 0.37	- 0.10	- 0.05
1814.5	- 0.37	- 0.26	- 0.28
1819.5	- 0.37	- 0.34	- 0.37
1824.8	+ 1.50	+ 1.46	+ 1.41
1829.7	+ 0.91	+ 0.90	+ 0.81
1835.2	-0.27	- 0.43	-0.46
1839.8	- 0.17	- 0.56	- 0.48
1844.8	+ 0.14	- 0.31	- 0.18
1849.9	- 0.21	- 0.70	-0.52
1854.9	- 0.14	- 0.54	- 0.36
1860.0	- 0.13	- 0.23	-0.14
1865.0	+ 0.36	+ 0.70	+ 0.62
1870,0	- 0.21	+ 0.80	+ 0.44
			1 0.14

It will be seen that the effect of these changes of weights is, that the older observations are a little better, and the later a little worse represented. I conceive that our choice must lie between the first and third solutions, the first being the more probable if we conceive the outstanding residuals to be due to errors of observation only, and the third if we suppose them equally due to errors of computation. On the whole, I consider the mean of the two to be about the most probable, and this will give the mass of Neptune very near the round number

# $\frac{1}{19700}$

which will be adopted as the definitive value. The definitive corrections to Elements III (p. 99) will then be

$\delta \varepsilon'$ (1830)	— 3".56
δε (1850)	-12.45
$10\delta n$	- 4.44
δe	- 4.12
$e\delta\pi$	- 0.25
δμ	- 0.137

#### Corrections to the Inclination and Node.

These corrections have been derived entirely from the modern observations, the ancient ones being too uncertain to add anything to the weight of the result. The mode in which the correction to the latitude of the provisional ephemeris has been concluded from the observations has been sufficiently explained: it is only necessary to add that the immediate results from the data of the preceding chapter require two corrections, namely:

(1) A correction to the theoretical latitude for the change in the adopted mass of Neptune. The value of this correction, as derived from the data of Chapter V, is with sufficient approximation

$$\delta\beta = 0''.25 T\cos g.$$

(2) A correction to the observed latitude on account of the difference between the obliquity of the ecliptic adopted in the various ephemerides compared, and that of Hansen's Tables du Soleil, which having been adopted in the theory should be used throughout.

Applying the correction (2) - (1) to all the observed latitudes, we have the following corrections to the latitude of the provisional ephemeris derived from all the observations of each opposition since 1781. The third column gives the number of observations in declination. These numbers may, however, in some cases be inaccurate. The fourth and fifth columns give the sine and cosine of the argument of latitude, to be used in forming the equations of condition.

Year.	δβ	No. of obs.	sin u	cos u	Year.	$\delta \beta$ .	No. of obs.	sin u	cos 4
						"			
1782.0	-0.4	21	+0.31	+0.95	1830.7	+0.2	48	-0.82	-0.57
1783.0 1784.0	-3.5 -2.4	13 13	$0.38 \\ 0.45$	$0.92 \\ 0.89$	1831.7 1832.7	$+1.0 \\ +0.9$	23 20	0.87 $-0.90$	0.50 . $-0.44$
1785.0	-0.1	10	0.52	0.85	1833.7	+0.6	54	0.93	0.37
1788.0 1789.0	$-1.0 \\ +0.9$	5 6	$+0.71 \\ 0.77$	$+0.71 \\ 0.64$	1834.7 1835.7	$+0.3 \\ +0.2$	92	0.95 $-9.97$	0.31
1790.0	+2.6	4	0.81	0.58	1836.7	+0.1	135	0.98	0.17
1791.0 1792.0	+1.9 $+1.8$	3	0.86 + 0.90	0.51 + 0.44	1837.8 1838.8	0.0 $-0.2$	154 182	0.99	0.10 0.03
1793.0	+2.9	5	0.93	0.37	1839.8	-0.4	142	1.00	+0.03
1794.0 1795.0	$+0.5 \\ +0.7$	3	$0.95 \\ +0.97$	0.30 + 0.22	1840.8	-0.3 -0.7	106	0.99 $-0.98$	0.10 + 0.17
1796.0	+3.6	4	0.99	0.14	1841.8 1842.8	-0.7	145	0.97	0.24
1797.0 1800.2	+3.6 0.0	3 2	$1.00 \\ +0.98$	+0.05 $-0.21$	1843.8	-0.9 -1.0	88 87	0.95 $-0.93$	0.31 + 0.37
1801.2	+1.2	2	0.97	0.26	1844.9 1845.9	-0.6	55	0.90	0.44
1802.3 1805.3	+1.4	13	0.94 + 0.83	0.34 $-0.56$	1846.9	—1.1 —1.1	92 69	0.87 $-0.83$	$0.50 \\ +0.56$
1806.3	-1.4	5	0.78	0.63	1847.9 1848.9	-0.9	56	0.79	0.62
1807.3	+1.6 $+1.8$	16	0.72 + 0.67	0.69 $-0.74$	1849.9	-1.0	36	0.74 $-0.69$	0.67
1809.3	+1.3	9	0.60	0.80	1850.9 $1851.9$	-0.7 $-1.2$	46   35	0.64	$+0.72 \\ 0.77$
1810.3	+3.7 $+3.4$	16	0.53 + 0.45	0.85 $-0.89$	1852.9	-1.3	49	0.59	0.81
1812.4	+3.6	6	0.38	0.93	1853.9 1854.9	-1.8 $-1.0$	48 47	-0.53 $0.47$	$+0.85 \\ 0.88$
1813.4 1814.4	$+2.4 \\ +2.5$	6	$0.29 \\ +0.22$	0.96 0.98	1855.9	-1.3	49	0.41	0.91
1815.4	+2.2	16	0.14	0.99	1856.9 1858.0	-1.1 -1.7	41 65	-0.34 $0.26$	$+0.94 \\ 0.97$
1816.4 1817.5	+1.3 $+2.4$	18	0.06 0.01	1.00 —1.00	1859.0	-1.7	56	0.19	0.98
1818.5	+4.2	22	0.09	1.00	1860.0 1861.0	—1.9 —2.3	58 41	-0.12 0.05	+0.99 $1.00$
1819.5 1820.5	+1.7 $+1.0$	7 9	0.17 -0.24	0.99	1862.0	-1.6	52	+0.02	1.00
1821.5	+1.3	10	0.31	0.95	1863.0 1864.0	-1.7 $-2.2$	83	$+0.10 \\ 0.18$	+0.99 $0.99$
1822.5 1823.5	$+1.8 \\ +0.6$	7	0.38	0.92 $-0.89$	1865.0	_1.7	37	0.25	0.97
1824.5	-0.2	11	0.51	0.86	1866.0 1867.0	-0.9 -0.6	72 83	+0.33 $0.40$	$+0.95 \\ 0.92$
1825.5 1826.5	$+1.5 \\ +1.2$	5 7	0.57 -0.63	0.82 —0.78	1668.1	-0.9	32	0.47	0.88
1827.6	+2.0	5	0.68	0.73	1869.1 1870.1	-0.8 -0.4	65 32	+0.54 $0.60$	+0.84 $0.80$
1828.6	-1.5	7 9	0.73 -0.78	0.68	1871.1	_0.7	21	+0.66	0.75
1829.7	+0.9	9	-0.18	-0.63	1872.1	-0.4	. 47	+0.72	+0.69

It will be remembered that the observed declinations have, as far as possible, been reduced to Auwers' standard. We have no positive proof that this standard is correct. If it be affected by a constant error, the result will be that the orbit of the planet on the celestial sphere, as deduced from observation, instead of being a great circle, as we know the real orbit to be, will be a small one, and the comparison of a uniform series of observations extending through an entire revolution of the planet, after making the best correction to the position of the orbit, will leave a constant residual. Now, we can best determine this residual by including it as an unknown quantity in our equations.

Again, the error of the standard is not necessarily constant, but may contain a term proportional to the time, arising from erroneous proper motions of the standard stars. Therefore, instead of supposing the residual constant, we shall suppose it of the form a + bt. Each observed correction to the theoretical latitude will then give the equation,

$$\sin u\delta \phi - \cos u\phi \delta \theta + a + bT = \delta \beta.$$

To facilitate the solution of these equations they have been divided into groups, each group usually comprehending three oppositions, and combined into a single equation multiplied by such a factor as would make its probable error half a second. The factor by which the correction of the latitude is multiplied in the equation is the same with the coefficient of a. The year 1840.0 is taken as the epoch for b. Thus we have the following:

Equations of Latitude.							
Dates of oppositions.	No. of opp.			Equation.			
1782.0-85.0	4	0.4δφ	—0.9¢89	+1.0a	-0.6b = -1.6		
1788.0-91.0	4	0.8	-0.5 pos	+1.04	$-0.5b \equiv -1.0$ $-0.5b \equiv +1.1$		
1792.0-94.0	3	0.5	-0.2	+0.5	-0.2 = +0.9		
1795.0-97.1	3	0.3	0.0	+0.5	-0.2 = +0.7		
1800.2-02.3	3	0.0	+0.3	+1.0	-0.4 = +1.0		
1805.3-07.3	3	0.8	+0.6	+1.0	-0.3 = +0.7		
1808.3-10.3	3	0.6	+0.8	+1.0	-0.3 = +2.6		
1811.3-13.4	3	0.4	+0.9	+1.0	-0.3 = +3.1		
1814.4-16.4	3	0.2	+1.5	+1.5	-0.4 = +3.0		
1817.4-19.5	3	-0.1	+1.5	+1.5	-0.3 = +4.8		
1820.5-22.5	3	-0.5	+1.4	+1.5	-0.3 = +2.0		
1823.5-25.5	3	-0.5	+0.9	+1.0	-0.2 = +0.6		
1826.5-28.6	3	-0.7	+0.7	+1.0	-0.1 = +0.6		
1829.6-31.7	3	-1.2	+0.8	+1.5	-0.1 = +1.1		
1832.7-34.7	3	-2.8	+1.1	+3.0	-0.2 = +1.8		
1835.7-37.8	3	-2.9	+0.5	+3.0	-0.1 = +0.3		
1838.8-40.8	3	-3.0	_0.1	+3.0	0.0 = -0.9		
1841.8-43.8	3	-2.9	-0.7	+3.0	+0.1 = -2.3		
1844.8-46.8	3	-2.7	-1.3	+3.0	+0.2 = -2.7		
1847.8-49.9	3	-2.4	_1.9	+3.0	+0.3 = -3.0		
1850.9-52.9	3	-1.9	-2.3	+3.0	+0.4 = -3.2		
1853.9-55.9	3	-1.4	-2.6	+3.0	+0.4 = -4.1		
1856.9-59.0	3	-0.8	-2.9	+3.0	+0.5 = -4.5		
1860.0-62.0	3	-0.2	-3.0	+3.0	+0.6 = -5.8		
1863.0-65.0	3	+0.5	-3.0	+3.0	+0.7 = -5.6		
1866.0-68.0	3	+1.2	<b>—2.8</b>	+3.0	+0.8 = -2.4		
1869.1-70.0	2	+1.1	-1.6	+2.0	+0.6 = -1.2		
1871.1-72.1	2	+1.4	-1.4	+2.0	+0.6 = -1.1		

Treating these equations by the method of least squares, we find the normal equations

The solution of these equations gives

$$\delta \phi = +0$$
".28 + 0".75  $a = +0$ ".54  
 $\phi \delta \theta = +1.57 + 0.686a + 0.205b = +1$ ".75  
 $a = +0.35$   
 $b = -0.28$ 

These values of a and b indicate that at the epoch 1840 Auwers' equatorial declinations are too great, or his north polar distances are too small by 0".35, and that this error is diminishing at the rate of 0".28 per century. If the older measures in declination had been comparable in precision with those made at the present time, and if the possible periodic error in the reduced right ascensions had been carefully eliminated, I should regard this determination as entitled to considerable weight. In view of the great uncertainty of the declinations previous to 1820, it can be regarded as little more than a rough attempt at a determination. For this reason the first two normal equations have been solved, leaving a and b indeterminate, so as to show the valves of  $\delta \phi$  and  $\phi \delta \theta$  in terms of these quantities. It will be seen that had we neglected a and b entirely, the value of  $\delta \phi$  would have been smaller by 0".26, and that of  $\phi \delta \theta$  smaller by 0".18 than those actually concluded. As the observations with the Washington Transit Circle, and those with the Pulkowa Vertical Circle, both indicate an increase of Auwers' polar distances, I shall take for the definitive corrections to the inclination and node those which follow from the above values of a and b, or,

$$\delta \phi = +0^{\circ}.54$$

$$\phi \delta \theta = +1.75.$$

The following table shows the residuals of the equations, and the mean outstanding corrections to the latitude, (1) when the concluded values of  $\delta \phi$  and  $\phi \delta \theta$  a and b are all used, and (2) when a and b are supposed zero, and the values of  $\delta \phi$  and  $\phi \delta \theta$ , corresponding to this supposition, are used:

Year.	Residu	als.		$\delta eta$
	(1)	(2)	(1)	(2)
1783	-0.8	-0.3	-0.8	-0.3
1789	+1.2	+1.8	+1.2	+1.8
1793	+0.7	+1.1	+1.4	+2.2
1796	+0.3	+0.6	+0.6	+1.2
1801	-0.5	+0.3	-0.5	+0.3
1806	-1.2	-0.5	-1.2	-0.5
1809	+0.5	+1.2	+0.5	+1.2
1812	+0.9	+1.6	+0.9	+1.6
1815	-0.3	+0.6	-0.2	+0.4
1818	+1.6	+2.5	+1.1	+1.7
1821	-0.7	-0.1	-0.5	-0.1
1824	-1.3	-0.7	-1.3	-0.7
1827	-0.6	-0.3	-0.6	-0.3

Year.	Resid	duals.	$\delta \beta$	
	(1)	(2)	(1)	(2)
1830	-0.2	+0.2	-0.1	+0.1
1833	+0.3	+0.9	+0.10	+0.30
1836	0.0	+0.3	0.00	+0.10
1839	-0.1	+0.1	-0.03	+0.03
1842	-0.5	-0.4	-0.17	-0.13
1845	+0.1	0.0	+0.03	0.00
1848	+0.6	+0.7	+0.20	+0.23
1851	+0.9	+0.9	+0.30	+0.30
1854	+0.3	+0.3	+0.10	+0.10
1858	+0.1	+0.3	+0.03	+0.10
1861	-1.4	-1.0	-0.47	-0.33
1864	-1.5	-1.0	-0.50	-0.33
1867	+1.1	+1.7	+0.37	+0.57
1869	+0.5	+1.0	+0.17	+0.33
1871	0.0	+0.7	0.00	+0.23

The sum of the squares of the residuals is in the first case 17".94, and in the second 25".41, so that the introduction of a and b makes a decided improvement in the representation of the observations.

I have not attempted a rigorous investigation of the probable error of any of these results for the reason that the values of the probable error deducible by the method of least squares would, in a case like the present, be entirely untrustworthy. It is, however, very desirable that we should be able to form some judgment of the uncertainty of the mass of Neptune. From the last system of equations of condition the value of  $\mu'$  comes out with the weight 3.13, or nearly that assigned to the mean result of each five years of modern observations. Regarding these results as independent, their mean error would be about 0".5, so that the probable error of  $\mu'$  would be 0.5, and that of  $\mu$  would be .005, or about  $\frac{1}{200}$  the entire mass of Neptune. A probable error derived from the original equations would have been much smaller, and when, in the last equations, we allow for the systematic character of the residuals, it will be larger. If we suppose the theory to be perfect, I conceive we may fairly estimate the probable error of the mass of Neptune to be  $\frac{1}{100}$  of its entire amount, and its possible error two or three times greater. If there is any error or imperfection in the theory, the error may be much larger.

## CHAPTER VIII.

# COMPLETION AND ARRANGEMENT OF THE THEORY TO FIT IT FOR PERMANENT USE.

In the preceding discussions the terms of the second order due to the action of Neptune have been neglected, the elements of Uranus and Neptune being so chosen that these terms can scarcely become sensible within a century of the epoch. But this very choice will make them larger in the course of centuries than if mean elements had been chosen. They will be most sensible in the case of the great inequality of 4300 years between Uranus and Neptune, an inequality which will make centuries of observation necessary to an accurate determination of the mean elements of the two orbits. The uncertainty arising from the great inequality is probably of the same order of magnitude with the omitted terms of the second order, and, such being the case, the theory would really be made but little more accurate by the addition of those terms. I conceive, however, that the theory will be made much more satisfactory by the computation of at least the largest of the terms in question, if only to arrive at a certain determination of their order of magnitude, and of their effect on the planet during the period in which it has been observed.

The term in question, being of very long period, may be most advantageously treated by the method of variation of elements, more especially as it has in the theory been already treated as such a perturbation. The largest of the perturbations in question are those of the mean longitude which are multiplied by the square of the integrating factor  $\nu$ , which is nearly 51, but which also contain the eccentricities as factors, and those of the eccentricity and perihelion which are independent of the eccentricities, but are multiplied by only the first power of  $\nu$ . These terms will probably comprise nearly or quite nine-tenths of those arising from the term of long period.

Let us begin with the perturbations of mean longitude. These are given by the integration of the equation

$$\frac{d^2l}{dt^2} = -3m'\alpha n^2 \left\{ ek_1 \sin(2l'-l-\pi) + e'k_2 \sin(2l'-l-\pi') \right\}$$

 $k_1$  and  $k_2$  being functions of the ratio of the mean distances, or  $\alpha$ . If we integrate this equation, supposing all the quantities in the second member except l' and l to be constant, and these two to be of the form  $nt + \varepsilon$ , n and  $\varepsilon$  being constants, we shall reproduce the principal term of long period already found. But in the second approximation we must suppose all the elements variable. It is not, however, necessary to take into account the variations of  $\alpha$ , n, and k, because these are

of a lower order of magnitude. The perturbations to be added will be those of  $l, l', e, e', \pi$ , and  $\pi'$ .

The point from which the longitudes are counted being arbitrary, we shall take the position of the perihelion of Uranus for 1850.0 as the origin, and put, as before, g for the mean longitude of Uranus counted from this point, and let l' represent the mean longitude of Neptune counted from the same point. The terms of  $\frac{d^2l}{dt^2}$  within the brackets will thus become

$$ek_1 \sin(2l'-g-\delta\pi) + e'k_2 \sin(2l'-g-(\pi'-\pi))$$

or, if we put

$$2l'-g = N$$

$$e' \sin (\pi' - \pi) = l'$$

$$e' \cos (\pi' - \pi) = l'$$

and notice, that to terms of the first order we have,  $\sin \delta \pi = \delta \pi$ ,  $\cos \delta \pi = 1$ , we shall have

$$\frac{d^2l}{dt^2} = -3m'\alpha n^2 \{(ek_1 + k'k_2) \sin N - (ek_1\delta\pi + h'k_2) \cos N\}$$

differentiating the quantities, of which the perturbations are to be considered with respect to the sign  $\delta$ , we find for the terms of the second order.

$$\begin{split} \delta \frac{d^2 l}{dt^2} &= -3m' a n^2 \left\{ (k_1 \delta e + k_2 \delta k' + h' k_2 \delta N) \sin N \right. \\ &+ \left( (e k_1 + k' k_2) \delta N - e k_1 \delta \pi - k_2 \delta h' \right) \cos N \right\}. \end{split}$$

We have now to substitute in this expression the numerical values of the quantities within parentheses. Those of the perturbations of Uranus have already been given in Chapter III, but it is necessary to diminish them by the factor  $0.145^*$  for the altered mass of Neptune. Those of Neptune are taken from my investigation of the orbit of that planet (p. 38). The mass of Uranus there adopted is  $\frac{1}{21000}$ , while the investigation of Dr. Von Asten,† from the observations of Struve and others, shows it to be  $\frac{1}{22000}$ . The perturbations are therefore diminished by  $\frac{1}{2200}$ . In accordance with the system adopted throughout both investigations, constants are added to all the perturbations to make them vanish at the epoch 1850.0. A term is also added to make  $\frac{dl}{dt}$  also vanish at the epoch; this corresponds to the constant which ought to be added to  $\delta a$ . The numerical values thus obtained, are:

<sup>\*</sup> This factor was adopted before the mass of Neptune to be employed had been finally decided upon. Hence the difference between it and that in the preceding chapter.

<sup>†</sup> Mémoires de l'Académie de St. Pétersbourg, tome xviii, vii série.

$$\delta N = + 7260'' \sin N - 6658'' + 4''.26t$$

$$e\delta \pi = - 414 \sin N + 380$$

$$\delta e = - 414 \cos N - 165$$

$$\delta k' = + 120 \sin N - 110$$

$$\delta k' = + 120 \cos N + 48$$

$$k_1 = -1.234$$

$$k_2 = + 0.452$$

$$k' = + 0.00695$$

$$k' = -0.00486$$

Substituting these values in the expression for  $\delta \frac{d^2l}{dt^2}$  and integrating twice, we find, putting b for the coefficient of the time in N, of which the value, taking the century as the unit, is +0.1472, and putting T for the time in centuries,

$$\delta l = \frac{3}{2} m' \alpha \nu^{2} \left\{ (411'' + \frac{102''.8}{b} + 2''.6T) \sin N + (1837'' + \frac{5''.3}{b} - 51.''4T) \cos N - 109''.3 \sin 2N - 5''.5 \cos 2N \right\}$$

$$- 16''.5 m' \alpha n^{2} t^{2} + cT + c',$$

c and c' being the arbitrary constants of integration, which are to be chosen so that both  $\delta l$  and its first differential coefficient shall vanish at the epoch. Reducing to numbers, we find

$$\delta l = (140''.70 + 0''.32T) \sin N + (232.60 - 6.37T) \cos N - 13.60 \sin 2N - 0.70 \cos 2N - 0.03 T2 + 34.27 T - 46.76,$$

the last two terms being arbitrary.

When we carry the perturbations of the eccentricity and perihelion to quantities of the second order, we are troubled by the introduction of large terms depending on the square of the disturbing force, which disappear from the rigorous expressions for the co-ordinates. These may be avoided by substituting for the eccentricity and perihelion the quantities h and k determined by the condition

$$h = e \sin \pi$$
$$k = e \cos \pi$$

If, as before, we count the longitudes from the perihelion of Uranus at the epoch 1850, we should substitute  $\delta \pi$  for  $\pi$  in these expressions. The values of h and k will then be given by the integration of the equations

$$\frac{dh}{dt} = m'ank_1 \cos N$$

$$\frac{dk}{dt} = -m'ank_1 \sin N.$$

Differentiating with respect to  $\delta$ , we find for the terms of the second order

$$\delta \frac{dh}{dt} = -m'\alpha n k_1 \sin N\delta N$$
$$\delta \frac{dk}{dt} = -m'\alpha n k_1 \cos N\delta N.$$

Substituting for  $\delta N$  its numerical value just given and integrating, we find

$$\begin{split} & \{ h = m' \alpha \nu k_1 \{ -2895'' \sin N - (6658'' - 4''.26t) \cos N + 1815'' \sin 2N \} \\ & - 3630'' m' \alpha k_1 nt + \text{constant}; \\ & \{ k = m' \alpha \nu k_1 \{ -2895'' \cos N + (6658'' - 4''.26t) \sin N + 1815'' \cos 2N \} \\ & + \text{constant}; \end{split}$$

the constants being so chosen that  $\delta h$  and  $\delta k$  shall vanish at the epoch.

Reducing the values of  $\delta h$  and  $\delta k$  to numbers, they become

the last two terms being arbitrary constants.

Computing the values of these terms of  $\delta l$ ,  $\delta h$ , and  $\delta k$ , for intervals of 50 years, from 1600 to 2000, we find them to be as follows:

Year	13	£ħ	\$18
1600	-1".34	+0".10	-0".02
1650	-0.71	+0.05	-0.02
1700	-0.31	+0.02	-0.01
1750	-0.10	0.00	-0.01
1800	-0.01	0.00	0.00
1850	0.00	0.00	0.00
1900	0.00	0.00	0.00
1950	+0.04	0.00	-0.01
2000	+0.18	-0.01	-0.02

We see that although the ultimate effect of these terms is very considerable, their effect, during the period that Uranus has been observed, is insignificant.

## Concluded Elements and Perturbations of Uranus.

The corrections found in the last chapter being applied to the final provisional elements (p. 99) give the following elements for 1850, affected by the great inequality produced by Neptune:

#### Elements IV of Uranus.

Epoch, 1850, Jan. 0, Greenwich mean noon.

π,	168°	15'	6'	.7
ε,	28	25	17	.05
θ,	73	14	8	.0
φ,	. 0	46	20	.54
е,	.04	6923	6	

e (in sec.), 9678".69 n, 15425.752  $\log a$ , 1.2829072  $\log a$ , 1.2831044

Log  $a_1$  includes, as before, the constant term in the perturbations of the logarithm of the radius vector which, with the corrected mass of Neptune, is +.0001972.

To find the corresponding elements at any other epoch, the following secular and long-period perturbations are to be applied. Those produced by Neptune are derived from the expressions in Chapter III by correcting them for the new mass of Neptune, and for the change in the value of the small divisor 2n'-n produced by the correction of the elements of Uranns. The logarithms of the factors for correction are,

Correction of mass of Neptune 9.93598 Correction of divisor 0.00051 Log. factor for  $\delta l$  9.93496 Log. factor for  $\delta e$ ,  $\delta \pi$ ,  $\delta \nu$  9.93547

Including the perturbations of the second order just found, we have, by putting

$$N = 2l' - g,$$

$$= 113^{\circ} \ 30' \ 46''.0 + 8^{\circ} \ 26' \ 51''.9 T,$$

$$\delta l = (-2850''.41 + 0''.32 T) \sin N + (387''.67 - 6''.37 T) \cos N + 112 .72 \sin 2N - 47.28 \cos 2N - 7 .72 \sin 3N + 4.33 \cos 3N + 0.55 \sin 4N - 0.46 \cos 4N - 0.03 T^2 - 83''.78 T + 2811''.41.$$

$$\delta h = -412''.18 \sin N + (14''.03 - 0''.86 T) \cos N + 29 .20 \sin 2N - 6 .09 \cos 2N - 3 .11 \sin 3N + 1 .19 \cos 3N + 0 .28 \sin 4N - 0 .13 \cos 4N + 14 .76 T + 398 .33$$

$$\delta k = -411''.53 \cos N - (13''.65 - 0''.86 T) \sin N + 29 .33 \cos 2N + 6 .17 \sin 2N - 3 .12 \cos 3N - 1 .21 \sin 3N + 0 .29 \cos 4N + 0 .13 \sin 4N - 5 .453 T - 124 .72$$

do (in units of the 7th place of decimals).

$$= 1963 \cos N + 103 \sin N$$

$$- 171 \cos 2N - 67 \sin 2N$$

$$+ 15 \cos 3N + 6 \sin 3N$$

$$+ 511.0.$$

The perturbations of  $e\delta\pi$  and  $\delta e$  are here replaced by those of h and k, defined by the equations

$$h = e \sin (\pi - \pi_0)$$

$$k = e \cos (\pi - \pi_0)$$

 $\pi_0$  representing the perihelion of  $1850 = 168^{\circ} 15' 6''.7$ . We then have for the eccentricity and longitude of perihelion at any epoch

$$e \sin (\pi - \pi_0) = \delta h$$
  

$$e \cos (\pi - \pi_0) = e_0 + \delta k.$$

In the above terms multiplied by the time we have included the secular variations produced by Jupiter and Saturn. If the perturbations of the elements due to each particular planet are required, we have

Action of Jupiter, 
$$\delta h = +5''.73\,T; \ \delta k = -0''.608\,T.$$
 Action of Saturn, 
$$\delta h = +5''.56\,T; \ \delta k = -4.589\,T.$$

Subtracting these from the above expressions all the remaining terms will be due to the action of Neptune. The values of  $\delta l$  and  $\delta n$  are due entirely to the action of Neptune.

For the sake of rigor, we may suppose the perturbations produced by each planet to be multiplied by a factor representing the number by which the adopted mass of the planet must be multiplied to obtain the true mass.

It will add to the homogeneousness of the theory to express the perturbations of long period, which are multiplied by the product of the masses of Jupiter and Saturn, as perturbations of the elements. These terms, as found on page 88, are

These terms, together with the arbitrary corrections of the elements which have been applied to make them very small at the epoch, may be replaced by the following corrections to the elements:

$$\begin{split} \delta l &= - \ 0''.55 \sin N_6 - \ 0''.03 \cos N_6 \\ &+ 40.65 \sin N_7 - 10.50 \cos N_7 \\ &+ 27''.27 - 11''.72T. \\ \delta h &= + \ 2.09 \sin N_6 + \ 1.94 \cos N_6 \\ &- \ 2.13 \sin N_7 + \ 3.71 \cos N_7 \\ &+ 1''.28. \\ \delta k &= + \ 1.32 \sin N_6 + \ 2.32 \cos N_6 \\ &+ \ 3.68 \sin N_7 + \ 2.21 \cos N_7 \end{split}$$

$$27 \sin N_7 + 104 \cos N_7 + 76 \text{ (in units of the 7th decimal)}.$$

The amount of the perturbations of the elements for every half century, from the year 1000 to 2200, is given in the following table. Column (1) gives the perturbations by Neptune, Saturn, and Jupiter, computed from the expressions

on page 182; column (2) those ju	st given depending o	n the product of the masses
of Jupiter and Saturn.		

Year.	87		δħ		δk		δα		δα	δη
	(1),,	(2)	(1),,	(2)	(1),,	(2)	(1)	(2)	"	
1000	+2050.31	+160.69	+ 42.66	+1.94	389.51	+6.08	+1955	_140	-2.06	+1.20
1050	1841.17	149.08	27.79	3.60	375.65	6.68	1882	156	2.10	1.37
1100	1638.76	136.39	14.03	4.99	360.31	6.82	1802	169	2.12	1.54
1150	1444.87	122.87	+ 1.45	6.01	343.49	6.47	1717	178	2.08	1.66
1200	1260.24	108.85	9.90	6.60	325.27	5.64	1626	183	2.02	1.77
1250	+1085.76	+ 94.67	19.84	+6.75	305.69	+4.42		+183	-1.94	+1.86
1300	921.76	80.67	28.34	6.49	284.90	2.86	1426	180	1.84	1.91
1350	769.32	67.12	35.27	5.90	252.90	+1.16	1318	173	1.70	1.92
1400	629.00	54.35	40.56	5.08	239.78	-0.57	1205	161	1.54	1.91
1450	501.39	42.62	44.11	4.16	215.68	2.17	1086	147	1.37	1.85
1500	+ 387.18	+ 32.11	45.83	+3.24	190.66	-3.52	+ 963	+129	-1.19	+1.74
1550	286.65	22.78	45.63	2.42	164.84	4.52	835	110	0.99	1.60
1600	200.65	15.38	43.46	1.80	138.31	5.12		90	0.80	1.42
1650	129.43	9.34	39.20	1.41	111.22	5.30	568	68	0.61	1.20
1700	73.46	4.86	32.79	1.23	83.70	5.09	430	48	0.44	0.95
1750	+ 33.06	+ 1.90	24.16	+1.23	55.90	-4.56		+ 29	-0.27	+0.66
1800	8.51	0.33	<b>—</b> 13.26	1.36	27.93	3.81	+ 145	+ 11	-0.12	+0.34
1850	0.00	0.00	0.00	1.52	0.00	2.96	0	_ 5	0.00	0.00
1900	7.64	0.71	+ 15.65	1.63	+ 27.74	2.10	- 145	18	+0.10	-0.36
1950	31.47	2.23	33.70	1.59	55.09	1.34		26	0.16	0.73
2000	+ 71.43	+ 4.25	+54.20	+1.34	+ 81.81	0.73		32	+0.20	-1.10
2050	127.33	6.52	77.12	0.85	107.77	0.34		30	0.20	1.47
2100	198.86	8.75	102.46	+0.13	132.67	0.14		27	0.17	1.83
2150	285.72	10.59	130.15	-0.77	156.33	0.11	843	20	0.11	2.17
2200	387.11	+ 11.77	+160.15	-1.76	+178.48	-0.19	968	<b>—</b> 9	+0.02	-2.48

## Mean Elements of Uranus.

If, instead of the elements of Uranus affected by the great inequality, we wish the absolute mean elements, these are to be obtained by adding to the elements already given the constants applied to the perturbations  $\delta l$ ,  $\delta h$ ,  $\delta k$ , and  $\delta n$  to make the perturbations vanish at the epoch 1850.0, and also the corrections (p. 113) which we have subtracted from the elements and added to the perturbations to reduce the latter to a small quantity during the period for which the tables are likely to be used. We thus find the following mean elements:

Elements V of Uranus. Epoch, 1850, Jan. 0, Greenwich mean noon. Longitude of the perihelion  $170^{\circ} 38' 48''.7 + 8698''. \mu$ Mean longitude at epoch, 29 12 43 .73 + 2811 .4 $\mu$ Longitude of the node, 73 14 37.6 + $29.6\mu$ Inclination of the orbit, 0 46 20.92 +  $0.38\mu$ Eccentricity,  $.0463592 - 5236 \mu$ Eccentricity in seconds,  $9562''.27 - 108''.0\mu$  $15424.797 - 0''.838\mu$ Mean motion, Log mean distance (uncorrected),  $1.2829251 + 179\mu$ The same corrected,  $1.2831223 + 179\mu$  $1 + \mu$ True mass of Neptune, 19700

Supposing the mass of Neptune to be uncertain by one-fiftieth of its entire amount, which is quite possible, it will be seen the longitude of the mean perihelion is from this cause uncertain by more than two minutes, the mean longitude of Uranus itself by nearly a minute, and the mean motion by nearly two seconds in a century.

It will be seen that the logarithm of the mean distance just given does not accurately correspond to that of elements IV plus the constant term of  $\delta n \times 0.4343$ , as it should. This difference arises from the rejection of the terms of the second order in  $\delta n$ , which can not affect the geocentric longitude of the planet by a tenth of a second for a number of centuries.

It is to be remarked that these mean elements are those to be used in the general theory of the secular variation of the planetary orbits.

## Concluded Theory of Uranus.

The elliptic longitude and radius vector of Uranus, affected by the secular and long period perturbations of the elements, will be given by the following equations. Put

$$l_0 = n_0 t + \epsilon_0,$$
  
 $l = l_0 + \delta l,$   
 $g = l - \pi_0,$   
 $h = \delta h,$   
 $k = e_0 + \delta k,$   
 $e^2 = h^2 + k^2,$ 

the zeros indicating elements IV, and  $\delta h$ ,  $\delta k$ , and  $\delta l$  being the perturbations of these three elements just given. Then

Elliptic longitude in orbit = l

$$\begin{split} &+\left\{2-\frac{1}{4}e^2+\frac{5}{96}e^4\right\}\left\{k\sin g-h\cos g\right\} \\ &+\left\{\frac{5}{4}-\frac{11}{24}e^2\right\}\left\{(k^2-h^2)\sin 2y-2hk\cos 2g\right\} \\ &+\left\{\frac{13}{12}-\frac{43}{64}e^2\right\}\left\{(k^3-3k^2k)\sin 3g-(3hk^2-h^3)\cos 3g\right\} \\ &+\left\{\frac{103}{96}\left\{(k^4-6k^2h^2+h^4)\sin 4y-(4k^3h-4kh^3)\cos 4y\right\}\right\} \\ &+\left\{\frac{1097}{960}\left\{(k^5-19k^3h^2+5kh^4)\sin 5g-(5k^4h-10k^2h^3+k^5\cos 5g\right\}\right\} \\ &\text{Neperian logarithm of } r=p+\frac{1}{4}e^2+\frac{1}{32}e^4 \\ &-\left\{1-\frac{3}{8}e^2\right\}\left\{k\cos g+h\sin g\right\} \\ &-\left\{\frac{3}{4}-\frac{11}{24}e^2\right\}\left\{(k^2-h^2)\cos 2g+2hk\sin 2g\right\} \\ &24\quad \text{May, 1873.} \end{split}$$

$$-\frac{17}{24} \left\{ (k^3 - 3kh^2) \cos 3g + (3k^2h - h^3) \sin 3g \right\}$$

$$-\frac{71}{96} \left\{ (k^4 - 6k^2h^2 + h^4) \cos 4g + (4k^3h - 4kh^3) \sin 4g \right\}$$

In computing these expressions it will be sufficient for several centuries before or after 1850 to develop h,  $\delta k$ , and  $\delta l$  to their first dimensions: it will, however, be more convenient to correct the mean anomaly g for the perturbation  $\delta l$  before obtaining the equation of the centre. Developing the perturbations of h and k to terms of the first order, we have for the effects of the perturbations of those elements:

$$(v.s.1) = \left(2 - \frac{3}{4}e_0^2\right)\delta k$$

$$(v.c.1) = -\left(2 - \frac{1}{4}e_0^2\right)\delta h$$

$$(v.s.2) = \left(\frac{5}{2}e_0 - \frac{11}{6}e_0^3\right)\delta k$$

$$(v.c.2) = -\left(\frac{5}{2}e_0 - \frac{11}{24}e_0^3\right)\delta h$$

$$(v.s.3) = \frac{13}{4}e_0^2\delta k$$

$$(v.c.3) = -\frac{13}{4}e_0^2\delta h$$

$$(v.s.4) = \frac{103}{24}e_0^3\delta k$$

$$(v.c.4) = -\frac{103}{24}e_0^3\delta h$$

$$(\rho.c.0) = \delta n + \frac{1}{2}e_0\delta k$$

$$(\rho.c.1) = -\left(1 - \frac{3}{8}e_0^2\right)\delta h$$

$$(\rho.c.2) = -\frac{3}{2}e_0\delta h$$

$$(\rho.c.2) = -\frac{3}{2}e_0\delta h$$

$$(\rho.c.3) = -\frac{17}{8}e_0^2\delta h$$

$$(\rho.c.3) = -\frac{17}{8}e_0^2\delta h$$

These coefficients for  $\rho$  must, of course, be multiplied by the modulus 0.434294 to reduce the perturbations to those of the common logarithm of the radius vector.

Among the elliptic terms may be included the effect of the following minute constants introduced by the perturbations.

$$\begin{array}{c} (v.s.2) = -0".144 \\ (v.c.2) = +0.130 \\ 0.4343 \, (\rho.c.0) = +1972 \, \text{ in units of the 7th place} \\ 0.4343 \, (\rho.s.1) = +63 \, \qquad \text{of decimals.} \\ 0.4343 \, (\rho.c.1) = +73 \\ 0.4343 \, (\rho.s.2) = +5 \\ 0.4343 \, (\rho.c.2) = +4 \end{array}$$

This term  $(\rho.c.0)$  is that added as a correction to the logarithm of the mean distance.

To the coefficients (v.s.1), (v.c.1), etc., are still to be added the following periodic terms:—

- 1. The periodic terms due to the action of Jupiter, given in Chapter V, omitting the terms multiplied by T, which are included in the perturbations of the elements.
- 2. The periodic terms produced by Saturn, including those terms multiplied both by T and by  $\sin A_2$  or  $\cos A_2$ , but omitting those multiplied by T only for the same reason as in the case of Jupiter.
- 3. The periodic terms produced by Neptune, multiplied by the factor 0.86294 on account of the correction to the mass of that planet, and omitting the terms multiplied by  $\delta l$ ,  $\delta e$ , and  $e \delta g$ .
- 4. The periodic terms multiplied by the product of the masses of Jupiter and Saturn, given on page 88, omitting the terms multiplied by the sine and cosine of  $N_6$  and  $N_7$ , because they are replaced by the terms of  $\delta l$ ,  $\delta h$ , and  $\delta k$ , given on page 183, and tabulated in the columns headed (2) on page 184. The result will be the same whether we employ the terms of (v.c.0), (v.s.1), etc., given at the bottom of page 88 and the top of page 89, omitting the numbers in the columns 2 on page 184 from the expressions on page 186, or whether we include the latter and omit the former.

The true anomaly of Uranus will then be:

 $g_0 + \delta l +$  (equation of centre from elements IV, using for mean anomaly  $g_0 + \delta l$ )

$$+\Sigma(v.s.i)\sin ig + \Sigma(v.c.i)\cos ig.$$

The logarithm of the radius vector will be:

log r in elliptic orbit from elements IV.  

$$+ \Sigma (\rho.s.i) \sin ig + \Sigma (\rho.c.i) \cos ig$$

care being taken to multiply the coefficients by the modulus where that has not already been done. All the terms in Chapter V are so multiplied.

To pass from the true anomaly to the true longitude we must investigate the secular motion of the planes of the orbit and of the ecliptic. The effect of this motion on  $\phi$ ,  $\theta$ , and  $\tau$  will be found by successive approximations from the formulæ

(34), correcting the data for the new mass of Neptune. We shall also use the same motion of the ecliptic adopted on p. 95. We have thus:

$$\frac{dp}{dt} = -4^{\circ}.53$$

$$\frac{dp'}{dt} = +5 .43 + 0^{\circ}.38T.$$

$$\frac{dq}{dt} = -5 .17$$

$$\frac{dq'}{dt} = -46 .78 + 0 .12T.$$

As a first approximation we have

Substituting these values in (34) and integrating we find

$$\phi = \phi_0 + 2''.47T + 0''.13T^2 
\theta = \theta_0 - 3168.42T + 3.00T^2 
\tau = \tau_0 - 3168.76T + 3.00T^2$$

For tabulating we shall use, instead of  $\theta$  and  $\tau$ , the distance of the perihelion from the ascending node, or  $\pi - \tau$ , and the value of  $\theta$  corrected for Struve's precession. Since the mean motion has been derived without making any distinction between  $\tau$  and  $\theta$ , it will be necessary to correct the motion of mean anomaly by the difference of those quantities. We thus obtain for the values of the three principal arguments:—

$$\begin{array}{l} g = 220^{\circ} \ 10' \ 10''.35 + 1542574''.86 \, T + \delta l \\ \omega = \ 95 \quad 0 \ 58.70 + 3168.76 \, T - 3.00 \, T^2 \\ \theta = \ 73 \ 14 \quad 8.00 + 1856.82 \, T + 4.12 \, T^2 \end{array}$$

If we represent all the inequalities of the true longitude by  $\Delta l$ , so that we shall have for the true anomaly

$$f = g + \Delta l$$

the argument of latitude will be

$$u = f + \omega$$
.

The reduction to the ecliptic will then be

$$R = -(9''.37 + 0''.016T) \sin 2u$$

the true longitude on the ecliptic referred to the mean equinox of date,

$$\lambda = u + \theta + R,$$

and the sine of the elliptic latitude,

$$\sin \beta_0 = \sin \phi_0 \sin u.$$

The perturbations of the latitude will be

$$(b.c.0) + (b.c.1) \cos g + (b.s.1) \sin g + \text{etc.}$$

The periodic terms of (b.c.0), (b.s.1), (b.c.1), etc., are given in Chapter V, on pages 86 and 87, and are to be taken without any farther modification than the multiplication of those due to the action of Neptune by the factor 0.863. The constant, secular, and long period terms are

$$\begin{array}{l} b.c.0 = +0^{\prime\prime}.26 & -0^{\prime\prime}.12T & -0.011\delta\eta + 0.046\delta\varkappa \\ (b.s.1) = -0.22T - 0.05T^2 + 0.975\delta\eta + 0.221\delta\varkappa \\ (b.c.1) = +2.47T + 0.12T^2 + 0.221\delta\eta - 0.975\delta\varkappa \\ (b.s.2) = -0.06 & -0.01T + 0.046\delta\eta + 0.011\delta\varkappa \\ (b.c.2) = -0.01 & +0.12T + 0.011\delta\eta - 0.046\delta\varkappa \end{array}$$

The values of  $\delta_{n}$  and  $\delta_{x}$  to be used in these expressions are those the expressions for which are given on page 97, and which are tabulated in the last two columns of the table on page 184.

The following tables are based on the elements and theory laid down in this chapter.

### CHAPTER IX.

#### GENERAL TABLES OF URANUS.

Enumeration of the Quantities contained in the several Tables.

The first six tables are designed to give the values of the three arguments of the elliptic motion, g,  $\omega$ , and  $\theta$ , and of the nine arguments of the tables of perturbations. The argument  $\omega$  is, however, diminished by 3', the sums of the constants added to the perturbations of (v.c.0) to make these quantities positive, and  $\theta$  by 10", the constant added to the reduction to ecliptic. The expressions for the arguments of perturbations are as follows, the mean longitude of each planet, counted from the perihelion of Uranus, being represented by the initial letter of the planet. All these arguments are expressed in units, of which 600 make an entire circumference, so that each unit is 36'. The time t is counted in Julian years from the fundamental epoch,

1850, January 0, Greenwich mean noon.

Table I gives the corrections which must be applied to the values of the arguments at any time during the nineteenth century to reduce them to the corresponding time in any preceding or following century between the Christian era and the year 2300. Since  $\omega$  and  $\theta$  each contains a term proportional to the square of the time, the correction for these quantities is not constant during each century, but is of the form

$$\omega + \omega' T$$

 $\omega$  and  $\omega'$  being constant during each century, and T being the fraction of the century counted from its beginning.

Table II gives the value of g,  $\omega = 3'$ ,  $\theta = 10''$ , and the above nine arguments for Greenwich mean noon of Jan. 0 of each leap year from 1752 to 1948, and for January = 1 of the years 1800 and 1900, corresponding to December 30 of the years 1799 and 1899. The corrections for the perturbations of long period are not

applied in this table. The numbers at the bottom of this table, in the line  $\Delta_{120}^{(1)}$ , show the variation of the corresponding quantity in 120 days, for the epoch 1850.0. In the line "Factor T" is given the change of this variation in a century, while  $\Delta_{120}^{(2)}$  is the second difference for intervals of 120 days. By means of these numbers, when the arguments are computed for any date, their values for other dates at intervals of 120 days may be found by successive addition.

Table III gives the motion of the several arguments between the epochs of the preceding table and the zero day of each month in the course of a four-year cycle. The variable motions,  $\omega$  and  $\theta$ , correspond to the epoch 1850, and rigorously they each require a correction for any other four-year cycle than that between 1848 and 1852. But, owing to the small inclination of the orbit of Uranus it is not necessary that either  $\omega$  or  $\theta$  should be exact, if only their sum is exact. The column  $\theta$  of this table, therefore, gives the correction which must be applied to the motion of  $\theta$  at the end of a century (1950) in order that, being applied to  $\theta$  alone,  $\omega + \theta$  may be exact. This correction is, in fact, that for the secular variation of the precession.

Tables IV and V give the motion of the arguments for days and hours. The motion for hours is, however, not necessary in the case of any argument but g, as all the others can be readily enough interpolated to fractions of a day.

Table VI gives the corrections to the arguments on account of the terms of long period from 1000 to 2200. The terms in question are, in the case of Jupiter, the great inequality produced by the action of Saturn, in the case of Neptune the great inequality produced by Uranus, and, in the case of Uranus, the inequalities in the mean longitude tabulated in the preceding chapter. The numerical expressions are

$$\&J = 0.535 \sin (116^{\circ} 21' + 40^{\circ} 45' 20'' T)$$
  
 $\&U = \&l$   
 $\&N = -0.75 \&l$ .

The corrections to the several arguments are

$$\begin{array}{lll} \delta g &=& \delta l \\ \delta \ \mathrm{arg.} \ 1 &=& \delta J - \delta l \\ \delta \ \mathrm{arg.} \ 2 &=& - \delta l \\ \delta \ \mathrm{arg.} \ 3 &=& \delta l - \delta N = 1.75 \ \delta l \end{array}$$

No correction to the mean longitude of Saturn is applied, all its inequalities being taken account of in the terms of the second order.

The corrections, expressed in seconds, have been reduced to units of the argument by dividing them by 2160".

Outside the limits of the table these corrections must be computed from their formulæ.

Table VII gives the equation of the centre, and the elliptic part of the logarithm of the radius vector. No constant is applied to the former, but the latter is diminished by .0003400, the sum of the constants added to  $(\rho.c.0)$  in Tables VIII, IX, X and XVII.

The formulæ for the Tables are

```
\begin{array}{c} \text{Equation of centre} = & 19352''.06 \sin \\ & + 567.24 \sin \\ & + 23.05 \sin 3g \\ & + 1.07 \sin 4g \\ & + 0.05 \sin 5g \end{array} \begin{array}{c} \text{Elliptic log. } r = & 1.2833435 \\ & - .0003400 \\ & - .0203618 \cos g \\ & - .0007165 \cos 2g \\ & - .0000318 \cos 3g \\ & - .0000016 \cos 4g. \end{array}
```

Table VIII gives the coefficients (v.c.0), (v.c.1), etc., for the perturbations of the longitude and logarithm of radius vector produced by the action of Jupiter. They are computed from the periodic terms of the formulæ on page 83, with the addition of the following constants to make all the numbers of the table positive:

Constant of 
$$(v.c.0) = 55''$$
.  
 $(v.s.1) = 6$ .  
 $(v.c.1) = 4$ .  
 $(v.s.2) = 0.20$   
 $(v.c.2) = 0.20$   
 $(\rho.c.0) = 1200$   
 $(\rho.s.1) = 150$   
 $(\rho.c.1) = 100$   
 $(\rho.s.2) = 10$   
 $(\rho.c.2) = 10$ 

Table IX gives the periodic part of the coefficients due to the action of Saturn, taken without change from the expressions on page 84, together with the secular variations, the latter including only the terms of (v.s.1), (v.c.1), (v.s.2), and (v.c.2), which are multiplied by T and by  $\sin A_2$  or  $\cos A_2$ . The coefficients of T are given in the columns Sec. Var. and each number is increased by the constant 1".50 to make it positive. The term -0".06 $T \sin A_2$  in (v.c.0) is omitted entirely, as it will not amount to a tenth of a second until after the year 2000. The constant terms added to the quantities of these tables to make all the numbers positive, are:

Constant of 
$$(v.c.0) = 30$$
.  
 $(v.s.1) = 150. + 1.50T$   
 $(v.c.1) = 150. + 1.50T$   
 $(v.s.2) = 130. + 1.50T$   
 $(v.c.2) = 130. + 1.50T$   
 $(v.s.3) = 8$ .  
 $(v.c.3) = 6$ .  
 $(v.s.4) = 1$ .  
 $(v.c.4) = 1$ .

Constant of 
$$(\rho.c.0) = 800$$
  
 $(\rho.s.1) = 1500$   
 $(\rho.c.1) = 1500$   
 $(\rho.s.2) = 400$   
 $(\rho.c.2) = 400$   
 $(\rho.s.3) = 100$   
 $(\rho.c.3) = 100$ 

Table X gives the coefficients produced by the action of Neptune, computed from the periodic terms on pages 85 and 86 without any other change than the multiplication of all the numbers by the factor 0.863 to reduce them to the new mass of Neptune. The constants added to the several quantities, are

Constant of 
$$(v.c.0) = 92.85$$
  
 $(v.s.1) = 20.00$   
 $(v.c.1) = 31.00$   
 $(v.s.2) = 5.00$   
 $(v.c.2) = 5.00$   
 $(v.c.3) = 1.00$   
 $(v.c.3) = 1.00$   
 $(v.c.4) = -1.00$   
 $(v.c.4) = -1.00$   
Constant of  $(\rho.c.0) = 400$   
 $(\rho.s.1) = 200$   
 $(\rho.s.2) = 40$   
 $(\rho.s.2) = 40$ 

Tables XI to XVI give the terms of the second order and of short period which contain the products of the masses of Jupiter and Saturn, which, with the constants added to the numbers of the several tables, are as follows:

```
(v.c.0) = +0".08 sin A_5 + 0".51 cos A_5; Table XII; const = 0".60
         +0.04 \sin A_6 + 0.01 \cos A_6;
                                              XIII;
                                                           = 0.05
                                                            = 0.05
                                              XIV;
         -0.01 \sin A_7 + 0.05 \cos A_7;
                                                XV;
                                                            = 1.35
         -0.35 \sin A_s - 1.30 \cos A_s;
                                               XVI;
                                                            = 0.10
         -0.05 \sin A_9 + 0.03 \cos A_9;
                                                               2.15
       Sum of constants added to these tables
                                          Table XI; const = 0''.40
(v.s.1) = +0".26 sin A_1 + 0".27 cos A_1;
                                                            = 0.20
         -0.04 \sin A_5 - 0.17 \cos A_5;
                                                XII;
                                                            = 0.10
         +0.08 \sin A_6 + 0.03 \cos A_6;
                                               XIII;
                                                            = 0.10
                                               XIV;
         -0.02 \sin A_7 + 0.08 \cos A_7;
                                                               0.75
                                                XV;
         +0.30 \sin A_s - 0.58 \cos A_s;
                                                               0.10
                                               XVI;
          -0.04 \sin A_9;
    June, 1873.
```

The term of  $(\rho.c.0)$ 

$$11 \sin A_s - 3 \cos A_s$$

is omitted from the tables entirely.

Tables XVII a and XVII b give the constant, secular, and long-period terms of (v.s.1) (v.c.1), computed from the formulæ p. 186, with the following additions:

- 1. The constant terms introduced by the perturbations, given on p. 187.
- 2. The negatives of the constants added to the tables VII to XVI inclusive to make the numbers of those tables positive. The values of these terms are

	Pert. Const.	Tables VIII to XVI.	(1)— $(2)$
(v.s.1)	0	177''.65 + 1''.50 T	-177''.65 - 1''.50T
(v.c.1)	0	186.65 + 1.50 T	-186.65 - 1.50 T
(v.s.2)	<b>—</b> 0″.14	135.20 + 1.50T	-135.34 - 1.50T
(v.c.2)	+0.13	135.20 + 1.50T	-135.07 - 1.50T
(v.s.3)	0	9.00	- 9.00
(v.c.3)	0	7.00	- 7.00
$(\rho.c.0)$	[+1972]	1000	+1000
$(\rho.s.1)$	+ 63	1850	-1787
$(\rho.c.1)$	+ 73	1800	-1727
$(\rho.s.2)$	+ 5	450	<b>—</b> 445
$(\rho.c.2)$	+ 4	450	<b>—</b> 446

The perturbation constant of  $(\rho.c.0)$ , being added to log a in forming the elliptic radius vector, is not included in this table.

Table XVIII gives the reduction to the ecliptic

$$-9''.37 \sin 2u$$
.

The constant 10" is added to make the numbers always positive, which constant has been already subtracted from  $\theta$ .

Table XIX gives the principal term of the latitude

$$46' \ 20''.54 \times \sin u.$$

Table XX gives the coefficients (b.s.1) and (b.c.1) for the perturbations of the latitude produced by Jupiter. They are given by the formulæ

$$(b.s.1) = 0$$
".65 cos  $(J - U + 40^{\circ})$   
 $(b.c.1) = 0$  .65 sin  $(J - U + 40^{\circ})$ 

The constant 0".70 is added to make all the numbers of the table positive.

Table XXI gives the corresponding coefficients for the action of Saturn, computed from the expressions on p. 87 with the addition of the following constants.

Const. of 
$$(b.c.0) = 0$$
".10  
 $(b.s.1) = 3.30$   
 $(b.c.1) = 3.10$   
 $(b.s.2) = 0.20$   
 $(b.c.2) = 0.20$ 

Table XXII gives the coefficients for the action of Neptune from the formulæ on p. 87, all the numbers being multiplied by the factor 0.863 to reduce them to the adopted mass of Neptune. The following constants are added:

To 
$$(b.c.0)$$
 . . . . 0".06  
 $(b.s.1)$  1 .00  
 $(b.c.1)$  1 .20  
 $(b.s.2)$  0 .20  
 $(b.c.2)$  0 .20

Table XXIII gives the secular and long-period terms for various epochs computed from the formulæ of p. 189. The sums of the several constants added in the three preceding tables are here subtracted again so that these expressions become

$$\begin{array}{lll} b.c.0 & -\Sigma c = & 0".10 - 0".12T - & .011\delta\eta + .046\delta\varkappa \\ (b.s.1) & -\Sigma c = -5 .00 - 0 .22T - 0".05\,T^2 + .975\delta\eta + .221\delta\varkappa \\ (b.c.1) & -\Sigma c = -5 .00 + 2 .47T + 0 .12\,T^2 + .221\delta\eta - .975\delta\varkappa \\ (b.s.2) & -\Sigma c = -0 .46 - 0 .01\,T + & .046\delta\eta + .011\delta\varkappa \\ (b.c.2) & -\Sigma c = -0 .41 + 0 .12\,T + & .011\delta\eta - .046\delta\varkappa \end{array}$$

Precepts for the use of the Tables.

Express the date for which the position of Uranus is required in years, months, days, and hours of Greenwich mean time, according to the Julian Calendar if the date is earlier than 1500, according to the Gregorian Calendar if it is later than 1600, and according to either calendar between these epochs.

Enter Table I with the beginning of the century, and take out the values of g,  $\omega$ ,  $\theta$ ,  $\theta$ , and arguments 1 to 9. Multiply  $\omega$  and  $\theta$  by the fraction of a century corresponding to the date, and write the products with their proper algebraic signs under  $\omega$  and  $\theta$ . If the calendar is the Julian, the century marked J must be taken, and if the Gregorian, that marked G. Between the dates 1752 and 1951 it is not necessary to enter Table I at all.

If Table I was not entered, enter Table II with the year, or the first preceding year found therein. If Table I was entered, enter Table II between the year 1800 and 1896 as if the number of the century were changed to 18. Take out the values of g,  $\omega$ ,  $\theta$ , and the arguments, and write them under the corresponding quantities from Table I.

Enter Table III with the excess of the actual year over that with which Table II was entered, and with the month. Write the corresponding values of g,  $\omega$ ,  $\theta$ , and the arguments under the previous values. Multiply  $\theta'$  by the fraction of a

cen ary after 1850, corresponding to the date with which Table II was entered, and write the product under  $\theta$ , or add it to it in writing  $\theta$ . If Table II was entered with a date before 1850, this product is negative.

Enter Table IV with the day of the month and write down the corresponding

values of g,  $\omega$ , etc., under the former values.

If the date does not correspond to Greenwich mean noon, the motion of g for the hours must be computed from Table V, and the other quantities must be interpolated to the fraction of a day in entering Table IV.

Enter Table VI with the year, find by interpolation the values of g, and arguments 1, 2, and 3, corresponding to the date, and write them under the former values.

Add up all the partial values of g,  $\omega$ ,  $\theta$ , and the arguments, attending to the algebraic signs of the products. Subtract from the arguments as many times 600 as possible, and the results will be the final values of those quantities.

Enter Table VII with g as the argument, the seconds being first reduced to fractions of a minute, and interpolate the quantities E and  $\log r$ . When g exceeds 180° the former quantity is to receive the negative sign; the latter is always positive.

Enter Tables VIII to XVI inclusive with their respective arguments, and take out the values of the quantities (v.c.0), (v.s.1), (v.c.1), etc.,  $(\rho.c.0)$ ,  $(\rho.s.1)$ , etc., so far as they are found in the tables, writing the quantities having the same designation under each other. In Table 1X the quantities Sec. Var. must be multiplied by the centuries and fraction of a century of the actual date after 1850, and the product must be included with the corresponding quantities, (v.s.1), (v.c.1), etc. Before 1850 this product will always be negative; afterward always positive. All the quantities taken from these tables are positive except (v.s.4) and (v.c.4) in Table 1X, which are negative.

Add up all the partial values of (v.c.0), (v.s.1), etc., thus obtained from Tables VIII to XVI, and from their sum take the corresponding quantities obtained from Table XVII by interpolating to the date. The required quantities are all given in Table XVIIb; Table XVIIa being only an expansion of a part of XVIIb for the present century. The final values of (v.s.1), (v.c.1), (v.s.2), etc.,  $(\rho.s.1)$ ,  $(\rho.c.1)$ , etc., thus obtained are to be multiplied by the sines and cosines of the corresponding multiples of g, in doing which four place logarithms are sufficient if the computation is carefully made. The products are then all added together, and to g,  $\omega$ , E, and (v.c.0); in the case of v, and to log. r,  $(\rho.c.0)$  in the case of  $\rho$ . That is, we are to form the expressions:

$$u = g + \omega + E + (v.c.0) + (v.s.1) \sin g + (v.c.1) \cos g + (v.s.2) \sin 2g + (v.c.2) \cos 2g + \text{etc.} + \text{etc.}$$

$$\log r = \log r \text{ (from Table VII)} + (\rho.c.0) + (\rho.s.1) \sin g) + (\rho.c.1) \cos g + (\rho.s.2) \sin 2g) + (\rho.c.2) \cos 2g + (\rho.s.3) \sin 3g) + (\rho.c.3) \cos 3g.$$

u will then be the true argument of latitude, and  $\log r$  the logarithm of the radius vector with seven places of decimals.

Under u write  $\theta$ ; enter Table XVIII with the argument u and take out the reduction to the ecliptic. Add it to u and  $\theta$ , and the sum of the three quantities will be the heliocentric longitude of Uranus referred to the mean equinox and ecliptic of the date. Applying nutation the longitude will be reduced to the true equinox.

Enter Table XIX with u as the argument, or, when u exceeds 180°, with  $u-180^\circ$ , and take out the principal term of the latitude, which will be positive when u is less than 180°, and negative when it is greater.

Enter Tables XX, XXI, XXII, and XXIII with their respective arguments, the argument for the last being the date, and add up the various quantities having the same designation, noticing that in the first three tables all the quantities are positive, while in the last they are all negative except (b.c.0). Then form the expression,

$$(b.c.0) + (b.s.1) \sin g + (b.c.1) \cos g + (b.s.2) \sin 2g + (b.c.2) \cos 2g$$

and add it to the principal term of the latitude, with regard to the algebraic signs. The sum will be the heliocentric latitude of Uranus above the ecliptic of the date.

When an ephemeris of Uranus is to be computed for a series of years, some modifications may be introduced, which will save the computer labor. In the first place an equidistant series of dates being selected for computation, it will be sufficient to compute g,  $\omega$ ,  $\theta$ , and the arguments for every sixth, eighth, or tenth date, and to fill in the arguments for the intermediate dates by adding the nearly constant differences corresponding to the adopted intervals. The agreement of the numbers thus obtained for the last date with those found by the original computation will prove the whole process. This interval may be as great as 120 days without detracting from the accuracy with which the places for the immediate dates can be interpolated, and the differences for this interval may be deduced from the numbers at the bottom of Table II. If these numbers are used without change the values of  $\omega$  and  $\theta$  for the last date may not always come out right. But these errors, if less than a second, will be of no importance if the one quantity comes out as much too great as the other is too small, and they may be avoided entirely by making a small change in the constant difference to be added.

Tables XI to XVI, inclusive, need be entered only for every third or fourth date, and the sums of the quantities can be then interpolated to every date, and added up with the corresponding quantities from the other tables.

Again, it will be found convenient to compute the sum of the small terms  $(v.s.3) \sin 3g + (v.c.3) \cos 3g + (v.s.4) \sin 4g + (v.c.4) \cos 4g$ , as well as the corresponding terms of the radius vector, and all the terms of the latitude, not for the dates adopted, but for every fourth entire degree of g. Having a series of values computed in this way, the sum can be interpolated to the value of g corresponding to the date. To facilitate the formation of the smaller products for entire degrees of g, a table of products of numbers by the sine and cosine of every degree is appended to these tables, by which the products in question can be formed at sight

whenever the coefficient to be multiplied is less than 32''. The values of these coefficients, (v.s.3), (v.c.3), etc., corresponding to the entire degrees of g, may be either formed by interpolation at sight from those corresponding to the dates of computation, or the values of the arguments 2 and 3 corresponding to the required degrees of g may be computed, and the values of (v.s.3), etc., corresponding to these values of the arguments may be taken from Tables IX and X, while Table XVII must be entered with the corresponding dates.

If the heliocentric ephemeris is computed for ten years at a time, the last of these modifications in the mode of computation will greatly facilitate the computation of the smaller terms. We first find the date, and the values of arguments 1, 2, and 3, to one place of decimals, for some entire degree of g preceding that which corresponds to the first date, and then find the dates and the values of the arguments corresponding to successive values of g, differing by  $2^{\circ}$  or  $4^{\circ}$ , until we pass the last date of computation. We then take out the values of (v.s.3), (v.c.3), (v.s.4), (v.c.4),  $(\rho.s.3)$ ,  $(\rho.c.3)$ , (b.c.0), (b.s.1), (b.c.1), (b.s.2), and (b.c.2), with these values of the dates and arguments, form their products by the sines and cosines of the corresponding multiples of g by means of the supplementary tables, and add the proper products together so as to form three small tables with g as the argument. These terms are then interpolated to the values of g corresponding to the original dates of computation.

As a first example of the use of the Tables we will compute the heliocentric co-ordinates of Uranus for Greenwich mean noon of the date 1753, Dec. 3. In computing the arguments we shall make use of Table I, though it is not necessary to do so. The computation of the arguments is as follows:

		g		100	ω			θ	Ar	g. 1
Table I, 1700 Product by 0.5392 Table II, 1852 III, Y. 1, Dec. IV, 3 days VI, 1753.92	291 228 8 0		7. 0.73 43.38 6.70 32.30	359 94 0	7 59 1	5.33 -3.24 2.03 0.73 0.26	359 2 73 1	7 7 7 89 11.4 —4.4 4 35.1 0 35.5 0.1	5 1 306 9 85 5	3.092 3.010 3.252 3.357
1753, Dec. 3	168 Arg	30	30.48	94	7	11.59	72 4 6	4 17.8		.218
Table I, 1700 II, 1852 III, Y. 1, Dec. IV, 3 days VI, 1753.9	3. 25.	319 785 349 109 014		880 709 029	216 517 19 0	262 87 6 0	139 90 32 0	537 276 36 0	59.4 272.1 10.3 0.0	401 177 38 0
1753, Dec. 3	506.	548	352.0	317	152	355	261	249.	341.8	16

	(v.c.0)	(v.s.1)	(v.c.1)	(v.s.2)	(v.c.2)	(v.s.3)	(v.c.3)	(v.s.4)	(v.c.4)
	(0.0.0)	(0.3.1)	(0.0.1)	(0.0.2)	(0.0.2)	"	"	"	(0.0.4)
Table VIII	83.58	9.97	6.61	0.37	0.31				
IX	21.32	22.24	223.49	60.92	238.89	1.42	11.07	0.32	1.64
X	71.08	19.02	18.30	6.64	5.38	0.70	1.19	-0.95	-1.04
XI		.13	.47						
XII	.13	.36	.10	-					
XIII	.06	.11	.01						
XIV	.01.	.04	.03						
XV	2.38	1.40	1.12						
XVI	.12	.09	.11						
Σ	178.68	53.36	250.24	67.93	244.58	2.12	12.26		
Table XVII		-292.55	—140.91 ·	-140.73	_131.03	-9.41	-6.85		
	-	-239.19	+109.35 -	<b>—</b> 72.80	+113.55	-7.29	+5.41	-0.63	+0.60
	(p.c.0	) (0	.s.1)	(p.c.1)	(ρ.8.5	2) (0	.c.2)	(p.8.3)	(p.c.3)
Table VIII	251		188	32	(,	, ,	,	(10.0)	(1.0.0)
IX	1086		741	360	621		597	154	111
X	326		259	222	21		42		
	1663	9.	1188	614	642		639	154	111
XVII	1104		1321	-500	-412		-360	-98	-94
	2767		133	+114	+230		279	+56	+17
								100	1
				STREET, STREET,	Table 17 to make the		and the same	and the same	A CONTRACTOR OF
log (v.s.1) —			(c.1) + 2.0		g (v.s.2)			v.c.2 + 2	
log sin +	9.2994	log co	sg = 9.9	912 lo	$g \sin 2g$ -	9.5916	log c	os $2g + 9$	.9641
	9.2994	log co		912 lo		9.5916	log c		.9641
log sin +	9.2994	log co	sg = 9.9	912 lo	$g \sin 2g - g (\rho.s.2) - g (\rho.s.2)$	-9.5916 + 2.362	log c	$\cos 2g + 9$ (c.2) + 9	0.9641 2.446
$\log \sin + \log (\rho.s.1)$	9.2994	log co	sg = 9.9	9912 lo 957 lo	$g \sin 2g - g (\rho.s.2) - g (\rho.s.2)$	-9.5916 + 2.362	log c	os $2g + 9$	.9641
$\log \sin + \log (\rho.s.1)$	9.2994 2.124 • '	log co log (ρ.α	sg = 9.9	9912 lo 57 lo Table	$g \sin 2g - g (\rho.s.2)$	-9.5916 $+2.362$ $b.s.1)$	log c log ( (b.c.1)	$\cos 2g + 9$ (c.2) + 9	0.9641 2.446
$\log \sin + \log (\rho.s.1) - g$	9.2994 2.124 0 /	log co log (ρ.α " 30.48	sg = 9.9	9912 lo 57 lo Table	$g \sin 2g - g (\rho.s.2)$	-9.5916 $+2.362$ $b.s.1)$ $".06$	log c log ( (b.c.1) 0".62	$\begin{array}{c} \cos 2g + 9 \\ o.c.2) + 9 \\ (b.s.2) \end{array}$	0.9641 2.446 (b.c.2)
$\log \sin + \log (\rho.s.1) - g$ $E$ $(v.c.0)$	9.2994 2.124 0 / 168 30 94 7 1 0 2	log co log (ρ. α " 30.48 11.59 46.21 58.68	sg = 9.9	Table	og sin 2g - og (ρ. s. 2) - (XX (XXI 3 XXII	- 9.5916 + 2.362 b.s.1) ".06 4.91 .84 4.81	log c log ( (b.c.1) 0".62 5 .88 1 .36 7 .86	$ \begin{array}{c} \cos 2g + 9 \\ \rho.c.2) + 2 \\ (b.s.2) \\ 0.41 \\ 0.18 \\ 0.59 \end{array} $	0.9641 2.446 (b.c.2) 0.17 0.17 0.34
$\log \sin + \log (\rho.s.1) - \frac{g}{\omega}$ E $(v.c.0)$ $(v.s.1) \sin g$	9.2994 2.124 0 / 168 30 94 7 1 0 2	log co log (p. 6 " 30.48 11.59 46.21 58.68 -47.66	sg = 9.9	Table	g sin 2g - g (ρ.8.2) - (β. XX - g X - g X - g X - g X - g X - g X - g X	- 9.5916 + 2.362 b.s.1) ".06 5.91 .84 4.81 4.28	log c log ( (b.c.1) 0".62 5 .88 1 .36 7 .86 -6 .88	$\begin{array}{c} \cos 2g + 9 \\ \cos 2g$	0.9641 2.446 (b.c.2) 0.17 0.17 0.34 0.51
$\log \sin + \log (\rho.s.1) - \frac{g}{\omega}$ E $(v.c.0)$ $(v.s.1) \sin g$ $(v.c.1) \cos g$	9.2994 2.124 0 / 168 30 94 7 1 0 2	log co log (p. 6 " 30.48 11.59 46.21 58.68 -47.66 47.15	sg = 9.9	Table	g sin 2g - g (ρ.8.2) - (β. XX - g X - g X - g X - g X - g X - g X - g X	- 9.5916 + 2.362 b.s.1) ".06 5.91 .84 4.81 4.28	log c log ( (b.c.1) 0".62 5 .88 1 .36 7 .86 -6 .88	$ \begin{array}{c} \cos 2g + 9 \\ \rho.c.2) + 2 \\ (b.s.2) \\ 0.41 \\ 0.18 \\ 0.59 \end{array} $	0.9641 2.446 (b.c.2) 0.17 0.17 0.34
$\log \sin + \log (\rho.s.1) - \frac{g}{\omega}$ E (v.c.0) (v.s.1) sin g (v.c.1) cos g (v.s.2) sin 2g	9.2994 2.124 0 / 168 30 94 7 1 0 2 ———————————————————————————————————	log co log (p. 6 " 30.48 11.59 46.21 58.68 -47.66 47.15 28.43	sg = 9.9	Table	g sin 2g - g (ρ.8.2) - (β. XX - g X - g X - g X - g X - g X - g X - g X	- 9.5916 + 2.362 b.s.1) ".06 5.91 .84 4.81 4.28	log c log ( (b.c.1) 0".62 5 .88 1 .36 7 .86 -6 .88	$\begin{array}{c} \cos 2g + 9 \\ \cos 2g$	0.9641 2.446 (b.c.2) 0.17 0.17 0.34 0.51
$\log \sin + \log (\rho.s.1) - \frac{g}{\omega}$ E $(v.c.0)$ $(v.s.1) \sin g$ $(v.c.1) \cos g$ $(v.s.2) \sin 2g$ $(v.c.2) \cos 2g$	9.2994 2.124 0 / 168 30 94 7 1 0 2 1	log co log (p. 6 " 30.48 11.59 46.21 58.68 -47.66 47.15 28.43 44.55	sg = 9.9	1912 ld 157 lo Table X	g sin 2g - g (ρ.8.2) - (β. XX - g (γ.8.1) - (β. XX	- 9.5916 + 2.362 b.s.1) ".06 5.91 .84 4.81 4.28	log c log ( (b.c.1) 0".62 5 .88 1 .36 7 .86 -6 .88	$\begin{array}{c} \cos 2g + 9 \\ \cos 2g$	0.9641 2.446 (b.c.2) 0.17 0.17 0.34 0.51
$\log \sin + \log (\rho.s.1) - \frac{g}{\omega}$ E $(v.c.0)$ $(v.s.1) \sin g$ $(v.c.1) \cos g$ $(v.s.2) \sin 2g$ $(v.c.2) \cos 2g$ $(v.s.3) \sin 3g$	9.2994 2.124 0 / 168 30 94 7 1 0 2 1 1	log co log (p. 6 " 30.48 11.59 46.21 58.68 -47.66 47.15 28.43 44.55 -4.13	g(g) = g(g) = g(g)	1912 ld 157 lo Table X	$\begin{array}{c} \operatorname{g} \sin 2g \\ \operatorname{g} (\rho.s.2) \end{array}$	- 9.5916 + 2.362 b.s.1) ".06 .91 .84 4.81 4.28 -	$\begin{array}{c} \log c \\ \log (6.c.1) \\ 0".62 \\ 5.88 \\ 1.36 \\ \hline 7.86 \\ -6.88 \\ -6.98 \end{array}$	$\begin{array}{c} \cos 2g + 9 \\ \rho.c.2) + 9 \\ (b.s.2) \\ 0.41 \\ 0.18 \\ \hline 0.59 \\ -0.43 \\ +0.16 \end{array}$	0.9641 2.446 (b.c.2) 0.17 0.17 0.34 -0.51 -0.17
$\log \sin + \log (\rho.s.1) - \frac{g}{\omega}$ E $(v.c.0)$ $(v.s.1) \sin g$ $(v.c.1) \cos g$ $(v.s.2) \sin 2g$ $(v.c.2) \cos 2g$ $(v.s.3) \sin 3g$ $(v.c.3) \cos 3g$	9.2994 2.124 0 / 168 30 94 7 1 0 2 1 1	log co log (p. 6 " 30.48 11.59 46.21 58.68 -47.66 47.15 28.43 44.55 -4.13 -4.46	sg = 9.9 $s.1) + 2.0$	9912 lo 57 lo Table XX XX	$\begin{array}{c} \operatorname{g} \sin 2g \\ \operatorname{g} (\rho.s.2) \end{array}$ $\begin{array}{c} (\sigma.s.2) \\ (\sigma.s.$	- 9.5916 + 2.362 b.s.1) ".06 91 .84 4.81 4.28 - 0.53	log c log ( (b.c.1) 0".62 5 .88 1 .36 7 .86 -6 .88 +0 .98	$\begin{array}{c} \cos 2g + 9 \\ \cos 2g$	0.9641 2.446 (b.c.2) 0.17 0.17 0.34 -0.51 -0.17
$\log \sin + \log(\rho.s.1) - \frac{g}{\omega}$ E $(v.c.0)$ $(v.s.1) \sin g$ $(v.c.1) \cos g$ $(v.s.2) \sin 2g$ $(v.c.2) \cos 2g$ $(v.s.3) \sin 3g$ $(v.c.3) \cos 3g$ $(v.s.4) \sin 4g$	9.2994 2.124 0 / 168 30 94 7 1 0 2 1 1	log co log (p. 6 " 30.48 11.59 46.21 58.68 -47.66 47.15 28.43 44.55 -4.13 -4.46 0.47	Table $(\rho.c)$	7 10 10 10 10 10 10 10 10 10 10 10 10 10	g sin 2g - g (ρ.8.2) - (π. XX XXI 3 XXII - (π. XXII - π. XIII - π. XIIII - π.	- 9.5916 + 2.362 b.s.1) ".06 91 .84 4.81 4.28 - 0.53	$\begin{array}{c} \log c \\ \log (6.c.1) \\ 0".62 \\ 5.88 \\ 1.36 \\ \hline 7.86 \\ -6.88 \\ -6.98 \end{array}$	$\begin{array}{c} \cos 2g + 9 \\ \cos 2g$	0.9641 2.446 (b.c.2) 0.17 0.17 0.34 -0.51 -0.17 ' 3."73 0.16
$\log \sin + \log(\rho.s.1) - \frac{g}{\omega}$ E $(v.c.0)$ $(v.s.1) \sin g$ $(v.c.1) \cos g$ $(v.s.2) \sin 2g$ $(v.c.2) \cos 2g$ $(v.s.3) \sin 3g$ $(v.c.3) \cos 3g$ $(v.s.4) \sin 4g$ $(v.c.4) \cos 4g$	9.2994 2.124 0 / 168 30 94 7 1 0 2 	log co log (p. 6 " 30.48 11.59 46.21 58.68 -47.66 47.15 28.43 44.55 -4.13 -4.46 0.47 0.41	Table ( $\rho.c$ ( $\rho.s$ )	7 10 10 10 10 10 10 10 10 10 10 10 10 10	$g \sin 2g - g (\rho.s.2)$ $g (\rho.s.2)$ $XX$ $XXI$ $XII$ $g (\rho.s.2)$ $g $	- 9.5916 + 2.362 b.s.1) ".06 91 .84 4.81 4.28 - 0.53	log c log ( (b.c.1) 0".62 5 .88 1 .36 7 .86 -6 .88 +0 .98	$\begin{array}{c} \cos 2g + 9 \\ \cos 2g$	0.9641 2.446 (b.c.2) 0.17 0.17 0.34 -0.51 -0.17 7 3.773 0.16 0.09
log sin + log (ρ.s.1) —  g ω Ε (υ.c.0) (υ.s.1) sin g (υ.c.1) cos g (υ.s.2) sin 2g (υ.c.2) cos 2g (υ.s.3) sin 3g (υ.c.3) cos 3g (υ.s.4) sin 4g (υ.c.4) cos 4g	9.2994 2.124 ° ' 168 30 94 7 1 0 2 —1 1 —2 263 40	log co log (p. 6 " 30.48 11.59 46.21 58.68 -47.66 47.15 28.43 44.55 -4.13 -4.46 0.47 0.41 57.42	Table ( $\rho.c$ ( $\rho.s$ ( $\rho.c$ )	7 Table XXX XX X	$g \sin 2g - g (\rho.s.2)$ $g (\rho.s.2)$ $XX$ $XXI$ $XII$ $g (\rho.s.2)$ $g $	- 9.5916 + 2.362 b.s.1) ".06 s.91 .84 4.81 4.28 - 0.53 - β <sub>0</sub> Ta (b.c.	log c log (6.c.1) 0".62 5 .88 1 .36 7 .86 -6 .88 +0 .98	$\begin{array}{c} \cos 2g + 9 \\ \cos 2g$	0.9641 2.446 (b.c.2) 0.17 0.17 0.34 -0.51 -0.17 7 3.773 0.16 0.09 0.20
log sin + log (ρ.s.1) —  g ω Ε (υ.c.0) (υ.s.1) sin g (υ.c.1) cos g (υ.s.2) sin 2g (υ.c.2) cos 2g (υ.s.3) sin 3g (υ.c.3) cos 3g (υ.s.4) sin 4g (υ.c.4) cos 4g	9.2994 2.124 0 / 168 30 94 7 1 0 2 	log co log (p. 6 " 30.48 11.59 46.21 58.68 -47.66 47.15 28.43 44.55 -4.13 -4.46 0.47 0.41 57.42 17.87	Table $(\rho.c. (\rho.s. (\rho.s$	7 10 1.3 .0) .1) sin g .1) cos g .2) sin 2g	$g \sin 2g - g \cos 2g - g \cos 2g - g \cos 2g - g \cos 2g \cos 2$	- 9.5916 + 2.362 b.s.1) ".069184 -4.81 -4.280.53 - β <sub>0</sub> Ta (b.e.6)	log c log (6.c.1) 0".62 5 .88 1 .36 7 .86 -6 .88 +0 .98	$\begin{array}{c} \cos 2g + 9 \\ \cos 2g$	0.9641 2.446 (b.c.2) 0.17 0.17 0.34 -0.51 -0.17 7 3.773 0.16 0.09 0.20 +0.11
log sin + log (ρ.s.1) —  g ω E (υ.c.0) (υ.s.1) sin g (υ.c.1) cos g (υ.s.2) sin 2g (υ.c.2) cos 2g (υ.s.3) sin 3g (υ.c.3) cos 3g (υ.s.4) sin 4g (υ.c.4) cos 4g  u θ R	9.2994 2.124  ° ' 168 30 94 7 1 0 2 -1 1 1 - 263 40 72 44	log co log (p. 6 "" 30.48 11.59 46.21 58.68 -47.66 47.15 28.43 44.55 -4.13 -4.46 0.47 0.41 57.42 17.87 7.95	Table $(\rho.c. (\rho.s. (\rho.c. (\rho.s. (\rho.s. (\rho.s. (\rho.s. (\rho.c. (\rho.s. (\rho.s$	7 10 1.3 1.3 1.0 1.1 1.3 1.0 1.1 1.3 1.0 1.2 1.3 1.0 1.2 1.3 1.0 1.2 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3	$g \sin 2g - g \cos 2g - g \cos 2g - g \cos 2g \cos 2g \cos 2g$	- 9.5916 + 2.362 b.s.1) ".06918484819.53	log c log (6.c.1) 0".62 5 .88 1 .36 7 .86 -6 .88 +0 .98 ble XIX c.0) Table	$\begin{array}{c} \cos 2g + 9 \\ p.c.2) + 9 \\ (b.s.2) \\ \hline 0.41 \\ 0.18 \\ \hline 0.59 \\ -0.43 \\ +0.16 \\ \hline \end{array}$	0.9641 2.446 (b.c.2) 0.17 0.17 0.34 -0.51 -0.17 0.16 0.09 0.20 +0.11 -0.96
log sin + log (ρ.s.1) —  g ω E (υ.c.0) (υ.s.1) sin g (υ.c.1) cos g (υ.s.2) sin 2g (υ.c.2) cos 2g (υ.s.3) sin 3g (υ.c.3) cos 3g (υ.s.4) sin 4g (υ.c.4) cos 4g  u θ R Long. mean Eq.	9.2994 2.124 0 / 168 30 94 7 1 0 2 -1 1 1 - 263 40 72 44	log co log (p. 6 "" 30.48 11.59 46.21 58.68 -47.66 47.15 28.43 44.55 -4.13 -4.46 0.47 0.41 57.42 17.87 7.95 23.24	Table $(\rho.c. (\rho.s. (\rho.c. (\rho.s. (\rho.s$	VII 1.3  O) 1) sin g 2) sin 2g 2) cos 2g 3) sin 3g	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	- 9.5916 + 2.362 b.s.1) ".06 .91 .84 4.81 4.28 - 0.53 - β <sub>0</sub> Ta (b.s.6) (b.s.6) (b.s.6)	log c log (6.c.1) 0".62 5 .88 1 .36 7 .86 -6 .88 +0 .98 ble XIX c.0) Table s.1) sin g s.2) sin 2g	$\begin{array}{c} \cos 2g + 9 \\ \rho.c.2) + 9 \\ (b.s.2) \\ \hline 0.41 \\ 0.18 \\ \hline 0.59 \\ -0.43 \\ +0.16 \\ \hline \end{array}$	0.9641 2.446 (b.c.2) 0.17 0.17 0.34 -0.51 -0.17 0.16 0.09 0.20 +0.11 -0.96 -0.06
log sin + log (ρ.s.1) —  g ω E (υ.c.0) (υ.s.1) sin g (υ.c.1) cos g (υ.s.2) sin 2g (υ.c.2) cos 2g (υ.s.3) sin 3g (υ.c.3) cos 3g (υ.s.4) sin 4g (υ.c.4) cos 4g  u θ R	9.2994 2.124  o	log co log (p. 6 "" 30.48 11.59 46.21 58.68 -47.66 47.15 28.43 44.55 -4.13 -4.46 0.47 0.41 57.42 17.87 7.95	Table $(\rho.c. (\rho.s. (\rho.c. (\rho.s. (\rho.s$	VII 1.3  O) 1) sin g 1) cos g 2) sin 2g 2) cos 2g 3) sin 3g 3) cos 3g	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	- 9.5916 + 2.362 b.s.1) ".06 3.91 3.84 4.81 4.28 - 0.53 - (b.6) (b.6) (b.6) (b.6)	log c log ((b.c.1) 0".62 5 .88 1 .36 7 .86 -6 .88 - +0 .98 · ble XIX c.0) Table s.1) sin g c.1) cos g s.2) sin 2g c.2) cos 2g	$\begin{array}{c} \cos 2g + 9 \\ \rho.c.2) + 9 \\ (b.s.2) \\ \hline 0.41 \\ 0.18 \\ \hline 0.59 \\ -0.43 \\ +0.16 \\ \hline \end{array}$	0.9641 2.446 (b.c.2) 0.17 0.17 0.34 -0.51 -0.17 3."73 0.16 0.09 0.20 +0.11 -0.96 -0.06 -0.16

As a second example we will take the computation of an ephemeris for the years 1876 and 1877. We take as the extreme dates 1875, December 15, and 1878, April 3, between which are seven intervals of 120 days each, which we adopt as those of computation. We first form the arguments for the extreme dates as follows:

	I. Fo	or 1875,	Dec.	15 =	1875.90	3.			
	g			ω			θ	A	rg. 1
Table 1I, 1872 III, 3 Y. Dec. IV, 15 days VI, 1875.96	16 46	55.70 33.76 33.50 2.20	95 0		35.64 4.06 1.30	73 2 0	0 46.6 1 12.7 0.7	2 170	4.815 0.072 1.784 0.426
For 1875, Dec. 15	331 23	5.16	95	11	41.00	73 2	2 0.1	5 14'	7.097
	Arg. 2	3		4	5	6	7	8	9
Table II, 1872 III, 3 Y. Dec. IV, 15 days VI, 1875.96	268.328 51.785 0.543 — 1			114 39 0	154 13 0	423 65 1	49 73 1	380.3 21.1 0.2	577 78 1
For 1875, Dec. 15	320.655	179.	739	153	167	489	123	401.6	56

	II. F	or 1878,	Apr	il 3 =	= 1878.2	6.			
	g			ω			θ	Λ1	g. 1
Table II, 1876 III, 2 Y. April IV, 3d VI, 1878.26		18.70 53.62 6.70 2.62	95 0	11 1	# 42.33 11.23 0.26	73 2	22 1.0 0 41.7 0.1	5 9	3.576 7.643 .357 .421
For 1878, April 3	341 14	21.64	95	12	53.82	73 2	2 42.9	3 240	3.997
	Arg. 2	3		4	5	6 .	7	8	9
Table II, 1876 III, 2 Y. April IV, 3d VI, 1878.26	321.237 29.732 .109 — .001	179.8 7.8 .0 + .0	68 29	153 22 0	168 7 0	489 37 0	123 42 0	401.9 12.1 0	57 45 0
For 1878, April 3	351.077	187.7	88	175	175	526	165	414.0	102

We now fill in the values of g, the arguments 1-9, and the times with which Table XVII is to be entered, for the intermediate dates, by adding the nearly constant differences deduced from the numbers at the bottom of Table II. The seconds of g are first reduced to fractions of a minute, with which to enter Table VII. In making the subsequent computation we have used none of the devices previously described except in the case of the small longitude terms, as follows:

	0	0	0	0	0	0	0
g	330	332	334	336	338	340	342
3g	270	276	282	288	294	300	306
4g	240	248	256	264	272	280	288
	"	"	"	"	"	"	"
(v.s.3) $(v.c.3)$	-1.14 $-2.46$	-1.12 $-2.56$	-1.13 -2.66	-1.16 $-2.76$	-1.23 -2.88	-1.33 -3.01	-1.48 $-3.16$
(v.s.4)	+ 0.59	+ 0.60	+ 0.59	+ 0.55	+ 0.50	+ 0.43	+ 0.36
(v.c.4)	-0.10	- 0.20	-0.30	-0.40	- 0.47	-0.57	-0.64
$(v.s.3) \sin 3g$	+1.14	+1.12	+1.11	+1.11	+1.12	+1.15	+1.20
$(v.c.3)\cos 3g$	.00	-0.26	-0.55	-0.85	-1.17	-1.50	-1.86
(v.s.4) sin 4g	51	56	57	55	50	42	34
$(v.c.4)\cos 4g$	+ .05	+ .07	+ .07	+ .04	02	10	19
Sum	+ 0.68	+ 0.37	+ 0.06	-0.25	-0.57	- 0.87	-1.19

It will be seen that we have here computed twice as many numbers as are necessary to interpolate with all attainable accuracy.

The rest of the computation is fully given on the four following pages. First we have the values of g and the nine arguments for the intermediate dates, filled in by successive addition of the nearly constant difference. The arguments thus obtained for the last date may be compared with those just computed on the preceding page.

The numerals in the first columns of the sections of computation following indicate the arguments with which tables are entered to obtain the separate values of the quantities (v.c.0), (v.s.1), (v.c.1), etc. The negative terms in Table XVII being taken from the sum of all the periodic terms from Tables VIII to XVI with argument 1 to 9, we have the final values of (v.c.0), (v.s.1), etc.

The final computation of the products (v.s.i) sin ig, etc., and the addition of the separate terms which make up the three co-ordinates, are shown on page 205. The expressions c.0, s.1, etc., are employed for brevity, instead of (v.c.0), (v.s.1) sin g, etc.

The longitude finally given by the tables is referred to the mean equinox, and must therefore be corrected for nutation before being used to compute the geocentric place.

							M. C.	
Date, {	1875, Dec. 15 1875.955.	1876, Apr. 13 1876.283.	Ang. 11 1876.612.	Dec. 9 1876.940.	1877, Apr. 8 1877.269.	Aug. 6 1877.597.	Dec. 4 1877.925.	1878, Apr. 3 1878.254.
	° '	332 47.554	° ' 334 12.021	° ' 335 36.489	° ' 337 0.957	° '	o / 339 49.893	。 , 341 14.361
Arg. 1	147.097	161.368	175.639	189.910	204.182	218.453	232.724	246.995
2	320.655	325.001	329.346 182.038	333.692 183.188	338.038 184.338	342.383 185.488	346.729 186.638	351.074
3 4	179.739 153.	180.889 156.	159.	163.	166.	169.	172.	187.788 175.
5	167.							175.
6 7	489. 123.	494. 129.	500. 135.	505. 141.	511. 147.	516. 153.	521. 160.	527. 166.
8	401.6	403.4	405.2	407.0	408.7	410.5	412.3	414.1
9	56.	63.	69.	75.	82.	88.	95.	101.
(v.c.0) 1	108.01	107.74	106.29	103.68	99.98	95.25	89.62	83.21
2 3	15.80 72.43	14.71 73.60	13.66 74.77	12.65 $75.94$	11.68 77.10	10.76 78.26	9.90 79.42	9.09 80.56
5	.59	.58	.58	.57	.56	.56	.55	.54
6	.02	.02	.02	.03	.03	.03	.03	.03
7 8	.07 1.68	.07 1.65	.06 1.63	1.60	.06 1.58	.06 1.55	.05 1.53	.05 1.50
9	.09	.09	.09	.09	.08	.08	.08	.07
(v.c.0)	198.69	198.46	197.10	194.62	191.07	186.55	181.18	175.05
(v.s:1) 1	6.84	7.68	8.40	8.99	9.44	9.74	9.91	9.98
sec. 2	132.20	125.48	118.82	112.21	105.67	99.24	92.89	86.69
sec. 2	1.09	.20 1.07	.22 1.08	.23 1.12	.25 1.19	.27 1.29	.29 1.41	.31 1.56
4	.13	.12	.11	.10	.10	.09	.09	.08
5 6	.19	.19	.19	.19	.19 ·.05	.20	.20	.20
7	.14	.14	.13	.13	.12	.12	.11	.07
8 9	1.28 .08	1.28	1.27	1.26	1.26	1.25	1.24	. 1.23
	142.17	.08	.08	.08	.07	.07	.07	.07
Tab.XVII	-154.21	136.28 —153.84	130.34 —153.47	124.36 —153.10	118.34 —152.73	112.33 —152.36	106.27 151.99	100.29 $-151.62$
(v.s.1)	12.04	<b>— 17.56</b>	23.13	28.74	<b>—</b> 34.39	40.03	- 45.72	- 51.33
(v.c.1) 1	5.64	6.03	6.38	6.67	6.85	6.91	6.82	6.59
sec. 2	5.01	6 00	7.31	8.90	10.80	13.00	15.49	18.25
3	23.20	24.09	$   \begin{array}{r}     .72 \\     24.95   \end{array} $	.74 25.82	$\begin{array}{c} .75 \\ 26.68 \end{array}$	.77 27.53	$\begin{array}{c c} .79\\28.37 \end{array}$	.80 29.19
4	.47	.48	.49	.50	.50	.51	.52	.52
5 6	.37	.37	.37	.37	.37	.37	.37	.37
7	.15	.14	.13	.13	.12	.18 .12	.18	.18
8 9	0.66	0.64	0.63	0.61	0.60	0.59	0.57	0.56
	$\frac{.07}{36.42}$	.07	.06	.06	.05	.04	.04	.03
Tab.XVII	<b>—205.86</b>	38.70 —206.08	41.21 —206.29	43.98 206.51	$ \begin{array}{c c} 46.90 \\ -206.73 \end{array} $	-206.94	53.26 207.15	56.59 <b>—</b> 207.37
(v.c.1)	-169.44	-167.38	_165.08	-162.53	-159.83	_156.92	_153.89	150.78
(v.s.2) 1	.06	.10	.15	.21	.26	.31	.34	.37
sec. 2	54.12	49.37	44.78	40.37	36.15	32.11	28.30	24.70
3	2.05	2.19	2.31	2.45	2.60	2.76	2.91	3.07
Tab. XVII	56.62 —134.34	52.08 —134.32	47.68	43.50	39.50	35.69	32.08	28.70
(v.s.2)	$\frac{-134.34}{-77.72}$	$\frac{-134.32}{-82.24}$	$\frac{-134.31}{-86.63}$	$\frac{-134.29}{-90.79}$	$\frac{-134.27}{-94.77}$	$\frac{-134.26}{-98.57}$	<u>134.24</u>	<u>134.22</u>
			00.00	00.10	- 04.11	- 98.97	-102.16	105.52

Date, {	1875, Dec. 15 1875.955.	1876, Apr. 13 1876.283.	Aug. 11 1876.612.	Dec. 9 1867.940.	1877, Apr. 8 1877.269.	Aug. 6 1877.597.	Dec. 4 1877.925.	1878, Apr. 3 1878.254.
	0 /	0 1	0 1	0 /	0 1	0 1	0 /	0 /
g	331 23.086	332 47.554	334 12.021	335 36.489	337 0.057	338 25.425	339 49.893	341 14.36
(v.c.2) 1	.31	.30	.29	.29	.29	.30	.30	.31
sec. 2	25.34	28.93	32.71	36.73	40.93	45.35	49.93	54.69
. 3	6.23	6.40	. 6.56	6.70	6.85	6.99	.80 7.10	7.20
Tab. XVII	32.64 —136.57	36.39 —136.59	40.33 —136.60	44.50 —136.62	48.86 —136.64	53.43 —136.65	58.13 —136.67	63.00 —136.69
(v.c.2)	103.93	-100.20	- 96.27	- 92.12	87.78	- 83.22	- 78.54	- 73.69
(v.s.3) 2 3	6.92 0.87	6.89 0.91	6.84 0.94	6.78 0.98	6.70 1.01	6.61 1.04	6.51	6.37
	7.79	7.80	7.78	7.76	7.71	7.65	7.59	7.49
Tab.XVII	-8.92	-8.92	-8.91	-8.91	-8.91	-8.91	-8.91	7.48 —8.91
(v.s.3)	-1.13	-1.12	-1.13	-1.15	-1.20	-1.26	1.32	-1.43
(v.c.3) 2	3.19	3.12	3.05	2.98	2.90	2.82	2.75	2.67
3	1.34	1.34	1.34	1.34	1.33	1.33	1.31	1.29
Tab. XVII	4.53 —7.06	4.46 —7.06	4.39 —7.06	4.32 —7.06	4.23 —7.06	4.15 —7.06	4.06 —7.06	3.96 —7.06
(v.c.3)	-2.53	-2.60	2.67	-2.74	-2.83	-2.91	-3.00	-3.10
(v.s.4) 2 3	1.48	1.48	1.47 —0.88	1.45 —0.89	1.43	1.40	3.36	1.33
				-	-0.89	-0.91	-0.93	94
(v.s.4)	+0.60	+0.60	+0.59	+0.56	+0.54	+0.49	+0.43	+0.39
(v.c.4) 2	0.83	0.77	0.72	0.66	0.61	0.57	0.51	0.47
3	-1.00	-1.02	-1.03	-1.04	-1.05	-1.06	-1.07	-1.08
(v.c.4)	-0.17	-0.25	0.31	-0.38	-0.44	-0.49	-0.56	-0.61
(p.c.0) 1	1230	1063	899	741	594	460	344	246
2 3	98 11	99	101	104	108	113	118	126
Tab.XVII		968	968	967	967	967	966	966
(ρ.c.0)	2307	2140	1977	1821	1677	1548	1436	1347
(p.s.1) 1	248	240	230	221	211	203	194	187
2	2835	2822	2807	2789	2769	2748	2723	2696
3	173	168	165	161	158	155	151	148
Σ m-1 VVIII	3256	3230	3202	3171	3138	3106	3068	3031
Tab. XVII (ρ. s. 1)	-1984 $+1272$	<u>—1987</u>	—1989 1913	—1991 1180	—1993 1145	—1996 1110	<del>-1998</del> 1070	1031
(p.s.1)	+1212	1243	1213	1100	1140	1110	1010	1031
(p.c.1) 1	123	112	97	83	69	55	41	31
3	1266 66	1202 66	1138 67	1074 67	1009 68	947 70	886 72	827 74
Σ	1455	1380	1302	1224	1146	1072	999	932
Tab.XVII		-1981	-1986	-1990	-1994	-1998	-2002	2006
(p.c.1)	- 522	- 601	- 684	<b>—</b> 766	- 848	- 926	-1003	-1074

Date, {	1875, Dec. 15 1875.955.	1876, Apr. 13 1876,283.	Aug. 11 1876.612.	Dec. 9 1867.940.	4877, Apr. 8 1877.269.	Aug. 6 1877.597.	Dec. 4 1877.925.	1878, Apr. 3 1878.254.
	0 /	o / 332 47.554	0 /	o / 335 36,489	。 , 337 0.957	929 95 495	0 /	0 /
g								
(p.s.2) 2	174 26	181 25	189 25	196 24	204 24	213	223 23	$\begin{array}{c} 232 \\ 23 \end{array}$
Σ	200	206	214	220	228	237	246	255
Tab.XVII		<b>—459</b>	<b>—459</b>	<b>—459</b>	-460	-460	<b>—460</b>	<b>-460</b>
(p.s.2)	_259	253	-245	239	-232	-223	-214	<b>—</b> 205
(p.o.2)								
(p.c.2) 2	559	568	576	584	592	600	607	614
3	33	33	34	35	36	37	39	40
Σ	592	601	610	619	628	637	646	654
Tab.XVII	464	<del>-464</del>	<b>—4</b> 64	<u>-465</u>	465	465	<del>-465</del>	466
(p.c.2)	+128	137	146	154	163	172	181	188
(p.s.3) 2	28	31	34	39	43	47	. 52	57
Tab.XVII	101	-101	-101	-101	-101	-101	-101	-101
(p.s.3)	<b>—</b> 73	70	<u> </u>	<b>—</b> 62	58	_ 54	<del>- 49</del>	44
			1/1					
(ρ.c.3) 2 Tab. XVII	155 —102	$-159 \\ -102$	162 —102	-166 $-102$	$-169 \\ -102$	172	175	177
(ρ.c.3)	+ 53	57	60	64	67	$\frac{-102}{70}$	$\frac{-102}{73}$	$\frac{-102}{75}$
							10	10
(b.c.0) 2	0.12	0.12	0.13	0.13	0.14	0.14	0.15	0.15
Tab. XXIII	0.11	0.11	0.11	0.11	$0.11 \\ 0.07$	0.11	0.11	0.11
(b.c.0)	0.30	0.30	0.31	0.01	0.32	0.07	0.07	0.07
(0.0.0)		0.00	0.51	0.51	0.52	0.32	0.33	0.33
(b.s.1) 1	0.30	0.22	0.16	0.12	0.08	0.06	0.05	0.06
$\begin{bmatrix} 2 \\ 3 \end{bmatrix}$	0.12	0.09	0.06	0.05	0.04	0.04	0.05	0.06
	1.11	1.11	1.12	1.12	1.13	1.13	1.14	1.14
Tab.XXIII	1.53 5.23	1.42 5.24	1.34	-5.24	1.25	1.23	1.24	1.26
(b.s.1)	_3.70	-3.82	-3.24 $-3.90$			5.25	5.25	5.25
(0.0.2)	-3.10	-0.02	-3.90	3.95	3.99	4.02	_4.01	-3.99
(b.c.1) 1	1.21	1.14	1.06	0.98	0.90	0.80	0.70	0.61
2 3	0.96	1.06	1.17	1.28	1.39	1.51	1.63	1.75
Σ	1.01	1.00	1.00	0.99	0.99	0.99	0.98	0.98
Tab.XXIII	3.18 -4.45	3.20 —4.44	3.23 -4.43	3.25	3.28	3.30	3.31	3.34
(b.c.1)	-1.27	-1.24	<del>-4.45</del> <del>-1.20</del>	$\begin{array}{c c} -4.43 \\ \hline -1.18 \end{array}$	$\begin{array}{c c} -4.42 \\ -1.14 \end{array}$	<u>-4.41</u> <u>-1.11</u>	$\frac{-4.41}{-1.10}$	$\frac{-4.40}{-1.06}$
47 41							-1.10	1.00
$(b.s.2) \ 2 \ 3$	0.02	0.02	0.03	0.04	0.04	0.05	0.06	0.07
Tab.XXIII	0.16 0.48	0.16 0.48	0.16 0.48	0.15	0.15	0.15	0.15	0.15
(b.s.2)	-0.30	-0.30	<del>-0.48</del> <del>-0.29</del>	$\begin{array}{c c} -0.48 \\ \hline -0.29 \end{array}$	-0.48 $-0.29$	-0.48		-0.48 $-0.26$
					-0.40			0.20
(b.c.2) 2	0.31	0.32	0.33	0.34	0.34	0.35	0.36	0.36
Tab.XXIII	0.10 0.38	0.10	0.10	0.10	0.11	0.11	0.11	0.11
(b.c.2)			-0.38	-0.38	-0.38	0.38		<u>0.38</u>
(0.0.2)	+0.03	+0.04	+0.05	+0.06	+0.07	+0.08	+0.09	+0.09

No.								
Date, {	1875, Dec. 15 1875.955.	1876, April 13 1876.283.	Aug. 11 1876.612.	Dec. 9 1876.940.	1877, April 8 1877, 269.	Aug. 6 1877.597.	Dec. 4 1877.925.	1878, April 3 1878.254.
	0 /	0 /	0 /	0 /	0 /	0 /	0 /	0 /
g	331 23.086	332 47.554	334 12.021	335 36.489	337 0.957	338 25.425	339 49.893	341 14.361
$\log (v.s.1)$ $\sin q$	-1.0806 -9.6803	-1.2445 $-9.6601$	-1.3642 -9.6386	-1.4585 $-9.6159$	-1.5365 $-9.5916$	-1.6024 $-9.5655$	-1.6601 $-9.5375$	-1.7104 $-9.5073$
log (p.8.1)	+3.1045	3.0944	3.0838	3.0719	3.0588	3.0453	3.0294	3.0132
log (v.c.1)	-2.2290	-2.2237	-2.2177	-2.2109	-2.2036	-2.1957	-2.1872	-2.1784
cos g	+9.9434	9.9491	9.9544	9.9594	9.9641	9.9685	9.9725	9.9763
log (ρ.c.1)	-2.718	-2.779	-2.835	-2.884	-2.928	-2.967	-3.0013	-8.0310
log (v.s.2)	—1.8905 —9.9247	-1.9151 -9.9102	-1.9376 -9.8941	-1.9580 -9.8763	-1.9766 -9.8566	-1.9937	-2.0093	-2.0233
	-2.413	-2.403	-2.389	-2.378	-2.365	-9.8350 -2.348	-9.8111 -2.330	-9.7846 $-2.312$
	-2.0167	-2.0009	-1.9835	-1.9644	-1.9434	-1.9202	_1.8951	-1.8674
$\log (v.c.2)$ $\cos 2g$	+9.7335	9.7649	9.7932	9.8189	9.8421	9.8630	9.8821	9.8994
log (p.c.2)	+2.107	2.137	2.164	2.187	2.212	2.236	2.258	2.274
	0 ' "	0 ' "	0 / //	0 / "	0 / "	0 / //	0 / //	0 / "
Δg	1 24 28.065		1 24 28.066	1 24 28.067	1 24 28.068	1 24 28.068	1 24 28.069	
g w	331 23 5.16 95 11 41.00	332 47 33.225 95 11 51.40	95 12 1.291 95 12 1.81	95 12 12.21	337 0 57.424 95 12 22.61	95 12 33.01	95 12 43.42	95 12 53.82
E	-2 42 49.15	-2 35 33.18	-2 28 10.63	-2 20 41.76	-2 13 6.93	-2 5 26.43	-1 57 40.55	—1 49 49.66
c.0 s.1	3 18.69 5.77	3 18.46 8.03	3 17.10 10.07	3 14.62 11.87	3 11.07 13.43	3 6.55 14.72	3 1.18 15.76	2 55.05 16.51
c.1	-2 28.72	-2 28.86	-2 28.62	-2 28.00	-2 27.13	-2 25.93	-2 24.43	-2 22.80
8.2 c.2	$\begin{array}{c} 1 & 5.34 \\ - & 56.27 \end{array}$	1 6.88 — 58.31	$\frac{1}{-}$ $\frac{7.87}{59.80}$	1 8.28 —1 0.71	1 8.12 —1 1.03	$\begin{array}{cccc}  & 1 & 7.40 \\  & -1 & 0.70 \end{array}$	1 6.13 - 59.87	1 4.26 — 58.45
(3+4)	0.46	0.25	0.03	- 0.19	- 0.41	- 0.63	- 0.83	- 1.00
The state of			100.00.1	00.00 5.00		<b>11</b> 00 00 10	+0 F F + 0 +	74 90 10 90
u 0	63 53 2.28 73 22 0.15	65 24 57.89 73 22 6.26	66 56 59.12 73 22 12.37	68 29 5.68 73 22 18.48	70 1 17.15 73 22 24.60	71 33 33.48 73 22 30.71	73 5 54.37 73 22 36.82	74 38 19.36 73 22 42.93
R	2.58	2.91	3.25	3.61	3.98	4.37	4.79	5.22
Longitude	137 15 5.01	138 47 7.06	140 19 14.74	141 51 27.77	143 23 45.73	144 56 8.56	146 28 35.98	148 1 7.51
log ro	1.2647392	1.2644735	1.2642196	1.2639778	1.2637486	1.2635319	1.2633280	1.2631370
c.0	- 2307	2140	1977	1821 —487	1677 —447	1548 —408	1436 —369	1347 — 332
s.1 c.1	-609 -458	—568 —535	—528 —615	-697	<del>-111</del> <del>-780</del>		-941	-1017
8.2	$^{+218}_{+69}$	206	192	179 101	167 113	152 126	138 138	125 149
c.2 s.3	+ 69 + 73	69	91 65	60	54	49	43	37
c.3	+ 4	8	13	19	23	29	36	41
log r	1.2648996	1.2646135	1.2643391	1.2640774	1.2638293	1.2635954	1.2633761	1.2631720
	, ,	, "	, ,,	, ,,	' "	, ,,	, ,,	' "
β,	+41 36.64	42 8.48	42 38.54	43 6.78	43 33.14 0.32	43 57.62 0.32	44 20.23 0.33	44 41.19 0.33
c.0 s.1	$+0.30 \\ +1.77$	0.30 1.75	0.31 1.70	0.31 1.63	1.57	1.48	1.38	1.29
c.1	-1.11	-1.10	-1.08	-1.07	-1.05 0.21	-1.03 0.19	-1.03 0.17	-1.00 0.16
8.2 c.2	$^{+0.25}_{+0.02}$	0.24   0.03	0.23	0.22 0.04	0.21	0.19	0.17	0.07
Latitude	+41 37.87	42 9.70	42 39.73	43 7.91	43 34.24	43 58.64	44 21.15	44 42.04
- Indiana	11 01.01	12 0.10	12 00.10					

		TABLE I.—C	ORRECTIONS OF A	RGUMENTS FO	OR PAST AND FUT	URE CENTUR	IES.
	Century.	g	ω	ω	θ	$\theta'$	Arg. 1
		0 / 1/	0 / //	"	0 1 11	"	
8	0J	207 15 59.32	343 52 17.36	+108.00	351 6 26.89	-148.32	408.924
1	100	275 45 34.18	344 46 54.12	102.00	351 34 55.39	-140.08	552.952
1	200	344 15 9.04	345 41 24.88	96.00	352 3 32.13	-131.84	96.980
	300	52 44 43.90	346 35 49.64	90.00	352 32 17.11	-123.60	241.008
	400	121 14 18.76	347 30 8.40	84.00	353 1 10.33	-115.36	385.036
ı	500	189 43 53.62	348 24 21.16	+-78.00	353 30 11.79	-107.12	529.064
1	600	258 13 28.48	349 18 27.92	72.00	353 59 21.49	- 98.88	73.092
ı	700	326 43 3.34	350 12 28.68	66.00	354 28 39.43	- 90.64	217.120
ı	800	35 12 38.20	351 6 23.44	60.00	354 58 5.61	- 82.40	361.148
ı	900	103 42 13.06	352 0 12.20	54.00	355 27 40.03	- 74.16	505.176
1	1000	172 11 47.92	352 53 54.96	+ 48.00	355 57 22.69	<b>—</b> 65.92	49.204
ı	1100	240 41 22.78	353 47 31.72	42.00	356 27 13.59	- 57.68	193.232
1	1200	309 10 57.64	354 41 2.48	36.00	356 57 12.73	<b>—</b> 49.44	337.260
1	1300	17 40 32.50	355 34 27.24	30.00	357 27 20.11	41.20	481.288
1	1400	86 10 7.36	356 27 46.00	24.00	357 57 35.73	32.96	25.316
ı	1500J	154 39 42.22	357 20 58.76	+ 18.00	358 27 59.59	_ 24.72	169.344
ı	1500G	154 32 39.89	357 20 57.89	18.00	358 27 59.08	- 24.72	168.155
	1600	223 2 14.75	358 14 4.65	12.00	358 58 31.18	<b>—</b> 16.48	.312.183
	1700	291 31 7.37	359 7 5.33	6.00	359 29 11.47	- 8.24	456.092
	1800	0 0 0.00	0 0 0.00	0.00	0 0 0.00	0.00	0.000
	1900	68 28 52.63	0 52 48.67	- 6.00	0 30 56.77	+ 8.24	143.908
1	2000	136 58 27.49	1 45 31.43	- 12.00	1 2 1.83	16.48	287.936
1	2100	205 27 20.11	2 38 8.11	- 18.00	1 33 15.08	24.72	431.845
1	2200	273 56 12.74	3 30 38.78	- 24.00	2 4 36.57	+ 32.96	575.755

Year.		g			ω			6		Arg. 1
	0	,	"	0	,	"	0	-,	"	
1752	160	15	8.10	94	6	10.48	72	43	42.30	162.101
1756	177	23	31.10	94	8	17.46	72	44	56.25	335.869
1760	194	31	54.09	94	10	24.43	72	46	10.22	509.623
1764	211	40	17.09	94	12	31.39	72	47	24.21	83.384
1768	228	48	40.08	94	14	38.34	72	48	38.20	257.148
1772	245	57	3.08	94	16	45.28	72	49	52.21	430.907
1776	263	5	26.07	94	18	52.22	72	51	6.23	4.668
1780	280 -	13	49.06	94	20	59.14	72	52	20.27	178.429
1784	297	22	12.06	94	23	6.05	72	53	34.32	352.190
1788	314	30	35.05	94	25	12.96	72	54	48.38	525.951
1792	331	38	58.05	94	27	19.85	72	56	2.46	99.712
1796	348	47	21.04	94	29	26.74	72	57	16.54	273.473

			TABLE	I.—Continue	ed.			
Century.	2	3	4	5	6	- 7	8	9
0Ј	191.528	299.485	280	512	102	61	470.0	15
100	314.245	49.520	64	250	563	124	410.6	214
200	436.962	399.555	449	589	424	188	351.2	413
300	559.679	149.590	233	327	285	251	291.7	13
400	82.396	499.625	18	65	146	314	232.3	212
500	205.113	249.660	402	403	7	378	172.9	411
600	327.830	599.695	187	142	468	441	113.5	10
700	450.547	349.730	571	480	329	504	54.1	209
800	573.264	99.765	356	218	190	567	594.6	409
900	95.981	449.800	140	556	51	31	535.2	8
1000	218.698	199.835	524	295	512	94	475.8	207
1100	341.415	549.870	309	33	373	157	416.4	406
1200	464.132	299.905	93	371	234	221	357.0	5
1300	586.849	49.940	478	109	95	284	297.5	205
1400	109.566	399.975	262	448	556	347	238.1	404
1500J	232.283	150.010	47	186	417	411	178.6	3
1500G	231.921	149.914	47	186	417	410	178.3	2
1600	354.638	499.949	431	524	278	473	118.8	201
1700	477.319	249.975	216	262	139	537	59.4	401
1800	0.000	0.000	0	0	0	0	0	0
1900	122.681	350.025	385	338	461	63 .	540.6	199
2000	245.398	100.060	169	76	322	127	481.2	398
2100	368.079	450.086	554	415	183	190	421.8	597
2200	490.760	200.111	338	153	44	253	362.3	196

	TABLE II.—Continued.												
Year.	2	3	4	5	6	7	8	9					
						41.41.		.,					
1752	481.104	345.855	133	348	229	213	331.6	578					
1756	534.013	359.856	172	362	296	287	353.2	58					
1760	586.921	373.858	212	375	362	362	374.8	138					
1764	39.830	387.859	251	389	429	436	396.4	218					
1768	92.739	401.860	290	402	495	511	418.1	298					
1772	145.647	415.862	330	416	562	585	439.7	377					
1776	198.556	429.863	369	429	28	60	461.3	457					
1780	251.465	443.865	408	443	95	134	482.9	537					
1784	304.373	457.866	448	457	161	209	504.6	17					
1788	357.282	471.868	487	470	227	283	526.2	97					
1792	410.191	485.869	527	484	294	358	547.8	177					
1796	463.100	499.870	566	497	360	433	569.4	25					
1800	515.972	513.862	5	511	427	507	591.1	337					

			Т	ABLE	II	_Continu	ed.			
Year.	Year. g							6	)	Arg. 1.
		,		0	,		0	,		
1800	5	55		94	31	33.53	72	58	30.59	447.115
1804	23		24.80	94	33	40.39	72	59	44.71	20.876
1808	40	11	47.79	94	35	47.25	73	0	58.84	194.638
1812	57	20	10.79	94	37	54.09	73	2	12.98	368.399
1816	74	28	33.78	94	40	0.93	73	3	27.13	542.160
1820	91	36	56.77	94	42	7.76	73	4	41.30	115.921
1824	108	45	19.77	94	44	14.58	73	5	55.48	289.683
1828	125	53	42.76	94	46	21.38	73	7	9.67	463.444
1832	143	2	5.76	94	48	28.18	73	8	23.88	37.205
1836	160	10	28.75	94	50	34.97	73	9	38.10	210.966
1840	177	18	51.75	94	52	41.75	73	10	52.33	384.727
1844	194	27	14.74	94	54	48.52	73	12	6.58	558.488
1848	211	35	37.74	94	56	55.28	73	13	20.84	132.249
1852	228	44	0.73	94	59	2.03	73	14	35.11	306.010
1856	245	52	23.73	95	1	8.77	73	15	49.40	479.771
1860	263	0	46.72	95	3	15.50	73	17	3.70	53.532
1864	280	9	9.71	95	5	22.22	73	18	18.01	227.293
1868	297	17	32.71	95	7	28.94	73	19	32.34	401.054
1872	314	25	55.70	95	9	35.64	73	20	46.67	574.815
1876	331	34	18.70	95	11	42.33	73	22	1.03	148.576
1880	348	42	41.69	95	13	49.01	73	23	15.39	322.337
1884	5	51	4.69	95	15	55.69	73	24	29.77	496.098
1888	22	59	27.68	95	18	2.35	73	25	44.16	69.860
1892	40	7	50.68	95	20	9.01	73	26	58.57	243.621
1896	57	16	13.67	95	22	15.65	73	28	12.98	417.382
1900	74	23	54.43	95	24	22.20	73	29	27.36	591.024
1904	91	32	17.43	95	26	28.83	73	30	41.81	164.785
1908	108	40	40.42	95	28	35.44	73	31	56.26	338.546
1912 1916	125 142	49 57	3.41 26.41	95	30	42.05	73	33	10.74	512.307
1920	160	5	49.40	95 95	32 34	48.64	73 73	34	25.22 39.72	86.068
1924	177	14	12.40	95	37	55.23 1.81	73	35 36	54.23	259.830 433.591
1928	194	22	35.39	95	39	8.38	73	38	8.75	7.352
							1			
1932	211	30	58.39	95	41	14.94	73	39	23.29	181.113
1936	228	39	21.38	95	43	21.48	73	40	37.84	354.874
1940 1944	245	47	44.38	95	45	28.02	73	41	52.40	528.635
1944	262	56	7.37	95	47	34.55	73	43	6.97	102.396
	280	4	30.36	95	49	41.07	73	44	21.56	276.158
Δ (1)	1	24	28.007			10.411			6.100	14.2715
Factor T			+0.222			020			+.027	0012
Δ <sub>120</sub> <sup>(2)</sup>			+ .0007			0001			+.0001	0

TABLE II.—Continued.														
	2	3	4	5	6	7	8	9						
1800	515.972	513.862	5	511	427	507	591.1	337						
1804	568.881	527.863	45	524	493	582	12.7	417						
1808	21.790	541.865	84	538	560	56	34.3	497						
1812	74.698	555.866	124	551	26	131	55.9	577						
1816	127.607	569.868	163	565	93	205	77.5	57						
1820	180.516	583.869	202	578	159	280	99.2	137						
1824	233.424	597.870	242	592	225	354	120.8	217						
1828	286.333	11.872	281	6	292	429	142.4	297						
1832	339.242	25.874	320	19	358	503	164.0	377						
1836	392.150	39.875	360	32	425	578	185.7	457						
1840	445.059	53.876	399	46	491	52	207.3	537						
1844	497.968	67.878	439	59	557	127	228.9	17						
1848	550.876	81.879	478	73	24	201	250.5	97						
		95.880	517	87	90	276	272.1	177						
1852	3.785	109.882	557	100	157	350	293.8	257						
1856 1860	56.694	123.883	596	114	223	425	315.4	337						
1864	109.602	137.885	35	127	290	499	337.0	417						
1868	162.511	151.886	75	141	356	574	358.6	497						
	215.420					The same of	380.3	577						
1872	268.328	165.888	114	154	423	49	401.9	57						
1876	321.237	179.889	153	168	489	123 198	423.5	137						
1880	374.146	193.890	193	181	555	272	445.1	217						
1884 .	427.054	207.892	232	195	22	347	466.7	297						
1888	479.963	221.893	271	208	88									
1892	532.872	235.895	311	222	155	421	488.4	376						
1896	585.780	249.896	350	235	221	496	510.0	456						
1900	38.653	263.889	390	249	287	570	531.6	536						
1904	91.562	277.890	429	262	354	45	553.2	16 96						
1908	144.470	291.891	468	276	420	119	574.9							
1912	197.379	305.892	508	290	487	194	596.5	176						
1916	250.288	319.894	547	303	553	268	18.1	256						
1920	303.197	333.895	587	317	20	343	39.7	336						
1924	356.105	347.897	26	330	86	417	61.4	416						
1928	409.014	361.898	65	344	152	492	83.0	496						
1932	461.923	375.900	105	357	219	566	104.6	576						
1936	514.831	389.901	144	371	285	41	126.2	56						
1940	567.740	403.902	184	384	352	116	147.8	136						
1944	20.649	417.904	223	398	418	190	169.5	216						
1948	73.557	431.905	262	411	485	265	191.1	296						
- 68 B	4.3457	1.1500	3.2	1.1	5.4	6.1	1.78	6.6						
	0001	+ .0002	0	0	0	0	0	(						
	0	0	0	0	0	0	0	(						

27 June. 1873.

TABLE III.—Reduction of the Epochs and Arguments to the beginning of each Month in a Cycle of four years.

				g			ω			$\theta$	$\theta'$	Arg. 1
Year 0 January February March April May June	0 0 0 0 0 0 0 0	0 0 0 1 1	0 21 42 4 25 46	0.00 49.24 14.00 3.24 10.24 59.48	0 0 0 0 0	, 0 0 0 0 0	0.00 2.69 5.21 7.89 10.50 13.19	0 0 0 0 0	0 0 0 0 0 0 0 0	0.00 1.58 3.05 4.63 6.15 7.73	0.00 0.00 0.00 0.00 0.01 0.01	0.000 3.687 7.136 10.823 14.391 18.078
July August September October November	0 0 0 0 0 0 0	2 2 3 3 3 3	51 12 34 55	53.48 6.48 55.71 44.95 51.95 41.19 48.19	0 0 0 0 0	0 0 0 0 0 0	15.79 18.48 21.17 23.77 26.46 29.06	0 0 0 0 0	0 0 0 0 0	9.25 10.83 12.40 13.93 15.51 17.03	0.01 0.01 0.01 0.02 0.02 0.02 0.02	21.647 25.333 29.019 32.587 36.274 39.842
February March April May June July	0 0 0 0 0 0 0 0 0 0	4 4 4 5 5 6 6 6	17 39 59 20 42 3 25 46	37.42 26.66 9.19 58.43 5.43 54.67 1.67 50.90	0 0 0 0 0 0	0 0 0 0 0 0	31.75 34.44 36.87 39.56 42.16 44.85 47.46 50.14	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0	18.61 20.18 21.61 23.18 24.71 26.28 27.81 29.38	0.02 0.02 0.03 0.03 0.03 0.03	43.529 47.216 50.546 54.233 57.801 61.488 65.056
September (October November December Year 2 January	0 0 0 0 0	7 7 7 8	8 29 51 12	40.14 47.14 36.38 43.38	0 0 0 0	0 0 0 1	52.83 55.44 58.13 0.73	0 0 0 0 0 0 0	0 0 0 0	30.96 32.48 34.06 35.59	0.04 0.04 0.04 0.04 0.04	68.742 72.429 75.997 79.684 83.252 86.939
March April (May June July August (May May May May May May May May May May	)	8 9 9 10 10 11	56 16 37 59 20 41 3	21.85 4.38 53.62 0.62 49.86 56.86 46.09	0 0 0 0 0 0	1 1 1 1 1 1	6.11 8.54 11.23 13.83 16.52 19.12 21.81	0 0 0 0 0 0 0	0 0 0 0 0 0	38.74 40.16 41.74 43.26 44.84 46.36 47.94	0.05 0.05 0.05 0.05 0.05 0.06 0.06	90.626 93.956 97.643 101.211 104.898 108.466 112.153
November (December (Vear 3 January (		11 11 12 12	25 46 8 29	35.33 42.33 31.57 38.57 27.80	0 0 0 0	1 1 1 1 1	24.50 27.10 29.79 32.40 35.08	0 0 0 0	0 0 0 0	49.52 51.04 52.62 54.14 55.72	0.06 0.06 0.06 0.07	115.840 119.407 123.094 126.662
February (March (April (CMay ) Unne (CMay ) (C		13 13 13 14 14 14	13 32 54 15 37 58	17.04 59.57 48.81 55.81 45.05 52.05	0 0 0 0 0 0 0	1 1 1 1 1	37.77 40.20 42.89 45.50 48.18 50.79	0 0 0 0 0 0	0 0 1 1 1 1	57.29 58.72 0.29 1.82 3.40 4.92	0.07 0.07 0.07 0.08 0.08 0.08	134.036 137.366 141.053 144.621 148.308 151.876
August 0 September 0 October 0 November 0 December 0		15 16 16 16	20 42 3 25 46	41.28 30.52 37.52 26.76 33.76	0 0 0 0 0	1 1 1 2 2	53.48 56.17 58.77 1.46 4.06	0 0 0 0	1 1 1 1 1	6.50 8.07 9.60 11.17 12.70	0.08 0.08 0.08 0.09 0.09	155.563 159.249 162.817 166.504 170.072

TABLE III.—Continued.													
	2	3	4	5	6	7	8	9					
Year 0	0.000	0.000			_	0	0.0	0					
January 0 February 0	0.000 1.123	0.000	0	0	0 1	1	0.0	2					
March 0	2.209	0.575	2	1	3	3	0.9	3					
April 0	3.259	0.872	2	1	4	4	1.3	5					
May 0	4.382	1.159	3	1	5	6	1.8	7					
June 0	5.505	1.457	. 4	1	7	7	2.2	8					
July 0	6.591 7.714	1.745 2.042	5 6	2 2	8 10	9 10	2.7	12					
Tragas -				2	11	12	3.6	13					
September 0 October 0	8.837 9.923	2.339 2.626	7	3	12	14	4.0	15					
November 0	11.046	2.923	8	3	14	15	4.5	17					
December 0	12.132	3.211	9	3	15	17	4.9	18					
Year 1		124	Sugar .	1387				1					
January 0	13.254	3.508	10	3	17	19	5.4	20					
February 0	14.377	3.805	11	4	18 19	20 22	5.9 6.3	22 23					
March 0 April 0	15.391 16.514	4.073	11 12	4 4	21	23	6.7	25					
	17.600	4.658	13	4	22	25	7.2	27					
May 0 June 0	18.723	4.055	14	5	24	27	7.6	28					
July 0	19.809	5.242	15	5	25	28	8.1	30					
August 0	20.932	5.539	15	5	26	30	8.5	32					
September 0	22.054	5.836	16	6	28	31	9.0	33					
October 0	23.140	6.124	17	6	29	33	9.4	35					
November 0	24.263	6.421	18	6	30 32	34 36	9.9	37 38					
December 0	25.349	6.709	19	0	- 02	00	10.5	00					
Year 2 January 0	26.472	7.006	20	7	33	37	10.8	40					
January 0 February 0	27.595	7.303	20	7	34	39	11.3	42					
March 0	28.609	7.571	21	7	36	40	11.7	43					
April 0	29.732	7.868	22	7	37	42	12.1	45					
May 0	30.818	8.156	23	8	38	44	12.6	47					
June 0	31.941	8.453	24	8	40	45 47	13.0 13.5	48 50					
July 0	33.027	8.741	25 25	8 9	41 43	48	13.9	52					
August 0	34.150	9.038		9	44	50	14.4	53					
September 0 October 0	35.272 36.358	9.335 9.622	26 27	9	44	51	14.8	55					
November 0	37.481	9.919	28	9	47	53	15.3	57					
December 0	38.567	10.207	29	10	48	55	15.7	58					
Year 3													
January 0	39.690	10.504	30	10	50	56	16.2	60					
February 0	40.813	10.801	30	10	51 52	58 59	16.7 17.1	63					
March 0	41.827 42.950	11.070 11.367	31 32	11 11	54	61	17.5	65					
April 0		The second second	33	11	55	62	18.0	67					
May 0 June 0	44.036 45.159	11.654 11.951	34	11	57	64	18.4	68					
July 0	46.245	12.239	35	12	58	65	18.9	70					
August 0	47.368	12.536	35	12	59	67	19.3	. 72					
September 0	48.490	12.833	36	12	61	68	19.8	73					
October .0	49.576	13.121	37	12	62	70	20.2	75					
November 0	50.699	13.418	38	13	64	72 73	20.7 21.1	77 78					
December 0	51.785	13.705	39	13	65	10	21.1	10					

	TABLE IV.—Motion of Arguments for Days.														
Days.	g	ω	0	1	2	3	4	5	6	7	8	9			
Days.  1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	9  ( 42.23 1 24.47 2 6.70 2 48.93 3 31.17 4 13.40 4 55.63 5 37.87 6 20.10 7 2.33 7 44.57 8 26.80 9 9.03 9 51.27 10 33.50 11 15.73 11 57.97 12 40.20 13 22.43 14 4.67 14 46.90 15 29.14 16 11.37 16 53.60 17 35.84 18 18.07	0.09 0.17 0.26 0.35 0.43 0.52 0.61 0.69 0.78 0.87 0.95 1.04 1.13 1.21 1.30 1.39 1.47 1.56 1.65 1.74 1.82 1.91 2.00 2.08 2.17 2.26	0.05 0.10 0.15 0.20 0.25 0.30 0.36 0.41 0.46 0.51 0.56 0.61 0.66 0.71 0.76 0.81 0.86 0.91 0.97 1.02 1.07 1.12 1.17 1.22 1.27 1.32	0.119 0.238 0.357 0.476 0.595 0.714 0.833 0.951 1.070 1.189 1.308 1.427 1.546 1.665 1.784 1.903 2.022 2.141 2.260 2.378 2.497 2.616 2.735 2.854 2.973 3.092	2 0.036 0.072 0.109 0.145 0.181 0.217 0.253 0.290 0.326 0.362 0.398 0.434 0.471 0.507 0.543 0.579 0.616 0.652 0.688 0.724 0.760 0.797 0.833 0.869 0.905 0.941	0.010 0.019 0.029 0.039 0.048 0.058 0.067 0.077 0.086 0.105 0.115 0.125 0.134 0.144 0.153 0.163 0.173 0.182 0.201 0.211 0.220 0.230 0.240 0.249	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		0 0 0 0 0 0 0 0 0 0 0 1 1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 1 1 1 1 1 1 1 1 1	0 0 0 0.1 0.1 0.1 0.1 0.1 0.2 0.2 0.2 0.2 0.2 0.2 0.3 0.3 0.3 0.3 0.3	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			
27 28 29	19 0.30 19 42.54 20 24.77 21 7.00	2.34 2.43 2.52	1.37 1.42 1.47	3.211 3.330 3.449	0.978 1.014 1.050	$0.259 \\ 0.268 \\ 0.278$	1 1 1	0 0 0	1 1 1	1 1 1 1	0.4 0.4 0.4	1 1 1			
30 31	21 49.24	2.60 2.69	1.52 1.57	3.568 3.687	1.086 1.123	$0.288 \\ 0.297$	1	0	1	1	0.4	1 1			

TABLE V.—Motion of g for Hours.														
Hours. g Hours. g Hours. g														
	11		"		"		"							
0	0.00	6	10.56	12	21.12	18	31.67							
1	1.76	7	12.32	13	22.88	19	33.43							
2	3.52	8	14.08	14	24.64	20	35.19							
3	5.28	9	15.84	15	26.40	21	36,95							
4 5	7.04	10	17.60	16	28.16	22	38.71							
5	8.80	11	19.36	17	29.92	23	40.47							
6	10.56	12	21.12	18	31.67	24	42.23							

The period of arguments 1 to 9 is 600.

In January and February of those years which, though divisible by 4, are not leap years, namely, 1700, 1800, 1900, 2100, etc., Table IV must be entered with a number 1 greater than the real day of the month.

	TABLE VI.—Corrections of Arguments for Terms of Long Period.  Year.													
Year.	g	1	2	3	Year.	g	1	2	3					
1000 1010 1020 1030 1040	+36 51.00 36 6.49 35 22.14 34 37.97 33 54.00	-0.614 0.621 0.629 0.638 0.648	1.003 0.983 0.962 0.942	+1.792 1.756 1.720 1.684 1.649	1550 1560 1570 1580 1590	4 49.70 4 30.32 4 11.57 3 53.48	-0.200 0.153 0.106 0.060 -0.013	-0.144 0.134 0.125 0.117 0.108	+0.252 0.236 0.219 0.205 0.189					
1050 1060 1070 1080 1090	+33 10.25 32 26.71 31 43.41 31 0.37 30 17.61	$\begin{array}{c} -0.659 \\ 0.672 \\ 0.686 \\ 0.702 \\ 0.718 \end{array}$	-0.922 $0.902$ $0.882$ $0.862$ $0.842$	+1.614 1.579 1.544 1.509 1.474	1600 1610 1620 1630 1640	+3 36.03 3 19.26 3 3.14 2 47.69 2 32.83	+0.034 0.078 0.120 0.162 0.203	0.092 0.085 0.078 0.071	+0.175 0.161 0.148 0.135 0.123					
1100 1110 1120 1130 1140	+29 35.15 28 53.01 28 11.20 27 29.71 26 48.56	-0.735 0.752 0.770 0.790 0.809	-0.822 0.803 0.783 0.764 0.745	+1.439 1.405 1.370 1.337 1.304	1650 1660 1670 1680 1690	+2 18.77 2 5.32 1 52.55 1 40.46 1 29.05	+0.242 0.278 0.312 0.345 0.375	-0.064 0.058 0.052 0.046 0.041	+0.112 0.101 0.091 0.081 0.072					
1150 1160 1170 1180 1190	+26 7.74 25 27.27 24 47.16 24 7.42 23 28.06	-0.829 0.848 0.866 0.883 0.899	-0.726 0.707 0.689 0.670 0.652	+1.270 1.237 1.206 1.172 1.141	1700 1710 1720 1730 1740	†1 18.32 1 8.28 0 58.92 0 50.24 0 42.26	+0.403 0.429 0.452 0.472 0.489	-0.036 0.031 0.027 0.023 0.019	+0.063 $0.054$ $0.046$ $0.039$ $0.032$					
1200 1210 1220 1230 1240	+22 49.09 22 10.51 21 32.34 20 54.57 20 17.23	-0.914 0.927 0.939 0.950 0.960	-0.634 0.616 0.598 0.581 0.564	+1.110 1.073 1.046 1.017 0.986	1750 1700 1770 1780 1790	+0 34.96 0 28.36 0 22.44 0 17.22 +0 12.68	+0.508 0.514 0.522 0.527 0.529	-0.015 0.012 0.009 0.007 0.005	+0.026 0.021 0.017 0.013 0.010					
1250 1260 1270 1280 1290	+19 40.31 19 3.83 18 27.80 17 52.21 17 17.09	-0.967 0.972 0.975 0.977 0.977	-0.547 0.530 0.513 0.497 0.481	+0.957 0.928 0.898 0.870 0.842	1800 1801 1802 1803 1804	+8.84 8.4935 8.15 · .34 7.82 · .33 7.50 · .32	+0.528 0.528 0.528 0.527 0.527	-0.004 0.004 0.004 0.004 0.004	+0.007 0.007 0.007 0.007 0.007					
1300 1310 1320 1330 1340	+16 42.43 16 8.25 15 34.55 15 1.34 14 28.63	0.974 0.967 0.959 0.948 0.936	-0.465 0.449 0.433 0.417 0.402	+0.814 0.786 0.758 0.730 0.704		+7.18 6.87 31 6.57 30 6.27 30 5.98 29	+0.527 0.526 0.526 0.525 0.525	0.003 0.003 0.003 0.003	+0.006 0.006 0.006 0.006 0.006					
1350 1360 1370 1380 1390	+13 56.44 13 24.76 12 53.61 12 22.99 11 52.90	-0.921 0.903 0.883 0.861 0.837	-0.387 0.372 0.358 0.344 0.330	+0.677 0.651 0.626 0.602 0.578	1810 1811 1812 1813 1814	+5.69 5.4128 5.14 .27 4.88 .26 4.62 .26 .25	+0.524 0.523 0.523 0.522 0.522	-0.003 0.003 0.003 0.003 0.002	+0.005 0.005 0.005 0.005 0.005					
1400 1410 1420 1430 1440	+11 23.35 10 54.35 10 25.92 9 58.04 9 30.74	-0.810 0.780 0.748 0.714 0.678	-0.317 0.303 0.290 0.277 0.264	+0.555 0.530 0.508 0.485 0.462	1815 1816 1817 1818 1819	+4.37 4.1324 3.89 .24 3.66 .23 3.44 .22 .21	+0 521 0.520 0.520 0.519 0.518	-0.002 0.002 0.002 0.002 0.002	+0.004 0.004 0.004 0.004 0.004					
1450 1460 1470 1480 1490	+ 9 4.01 8 37.88 8 12.34 7 47.39 7 23.04	-0.641 0.601 0.560 0.518 0.475	-0.252 0.240 0.228 0.216 0.205	+0.441 0.420 0.399 0.378 0.359	1820 1821 1822 1823 1824	+3.23 3.0221 2.82 .20 2.63 .19 2.44 .49 1.18	+0.517 0.516 0.515 0.514 0.513	-0.002 0.002 0.002 0.002 0.002	+0.003 0.003 0.003 0.003 0.003					
1500 1510 1520 1530 1540	+ 6 59.29 6 36.14 6 13.61 5 51.69 + 5 30.40	-0.431 0.386 0.340 0.293 -0.247	-0.194 0.183 0.172 0.162 -0.153	+0.340 0.322 0.303 0.284 +0.268	1825 1826 1827 1828 1829	$\begin{array}{c} +2.26 \\ 2.09 \\ 1.92 \\ 1.76 \\ 1.76 \\ -1.5 \end{array}$	0.511 0.510 0.509 -0.508	-0.001 0.001 0.001 0.001 0.001	$\begin{array}{c} +0.002\\ 0.002\\ 0.002\\ 0.002\\ +0.002\\ \end{array}$					

	TABLE VI.—Continued.           Year.         g         1         2         3         Year.         g         1         2         3													
Year	.   g	1	2	3	Year.	g	1	2	3					
1830 1831 1832 1833	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{r} +0.507 \\     -0.506 \\     0.505 \\     0.503 \\ \end{array} $	-0.001 0.001 0.001 0.001	$\begin{array}{ c c c } +0.002 \\ 0.002 \\ 0.002 \\ 0.002 \\ \end{array}$	1885 1886 1887 1888	$ \begin{array}{c}     " \\     +4.06 \\     4.30 \\     4.54 \\     4.79 \end{array} $	$\begin{vmatrix} +0.404 \\ 0.402 \\ 0.399 \\ 0.397 \end{vmatrix}$	0.002	$\begin{array}{c} +0.003 \\ 0.004 \\ 0.004 \\ 0.004 \end{array}$					
1834 1835 1836 1837 1838	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{r} 0.502 \\ +0.501 \\ 0.500 \\ 0.498 \\ 0.497 \end{array} $	0.001 0 0 0	+0.002 +0.001 0.001 0.001 0.001	1889 1890 1891 1892 1893	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{r} 0.394 \\ +0.391 \\ 0.388 \\ 0.386 \\ 0.383 \end{array}$	0.002 -0.003 0.003 0.003 0.003	$\begin{array}{c} 0.004 \\ +0.004 \\ 0.005 \\ 0.005 \\ 0.005 \end{array}$					
1839 1840 1841 1842 1843	$\begin{array}{c ccccc} 0.47 & .08 \\ +0.39 & .07 \\ 0.32 & .06 \\ 0.20 & .06 \end{array}$	$\begin{array}{c c} 0.495 \\ +0.494 \\ 0.493 \\ 0.491 \\ 0.490 \end{array}$	0 0 0 0	0 0 0 0 0 0	1894 1895 1896 1897 1898	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c c} 0.380 \\ +0.377 \\ 0.374 \\ 0.372 \\ 0.369 \end{array}$	0.003 -0.003 0.003 0.004 0.004	0.005 +0.006 0.006 0.006 0.006					
1844 1845 1846 1847 1848	$ \begin{array}{c ccccc} 0.15 & .05 \\ +0.11 & .04 \\ 0.07 & .04 \\ 0.04 & .03 \\ 0.02 & .02 \end{array} $	$\begin{array}{c} 0.488 \\ +0.487 \\ 0.485 \\ 0.483 \\ 0.482 \end{array}$	0 0 0 0	0 0 0 0	1899 1900 1901 1902 1903	8.02 · 33 +8.35 · 33 +8.35 · 35 9.03 · 35 9.38 · 35	$\begin{array}{c} 0.366 \\ +0.363 \\ 0.360 \\ 0.357 \\ 0.353 \end{array}$	0.004 -0.004 0.004 0.004 0.005	0.007 +0.007 0.007 0.008 0.008					
1849 1850 1851 1852 1853	0.00 .02 0.00 .00 0.00 .00	$\begin{array}{c c} 0.481 \\ +0.479 \\ 0.477 \\ 0.476 \\ 0.474 \end{array}$	0 0 0 0 0 0	0 0 0 0 0 0	1904 1905 1906 1907 1908	$\begin{array}{r} 9.75 & .37 \\ +10.12 & .38 \\ 10.50 & .38 \\ 10.88 & .38 \\ 11.27 & .39 \end{array}$	0.350 + 0.347	0.005 -0.005 0.005 0.005 0.096	0.008 +0.009 0.009 0.010 0.010					
1854 1855 1856 1857 1858	$ \begin{vmatrix} 0.03 & .02 \\ +0.06 & .03 \\ 0.10 & .04 \\ 0.14 & .04 \\ 0.19 & .05 \end{vmatrix} $	$ \begin{array}{c c} 0.472 \\ +0.471 \\ 0.469 \\ 0.467 \\ 0.465 \end{array} $	0 0 0	0 0 0 0 0 0	1909 1910 1920 1930 1940	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	0.334 $-0.331$ $0.298$ $0.264$ $0.229$	0.006 -0.006 0.008 0.010 0.012	9.010 +0.010 0.013 0.017 0.021					
1859 1860 1861 1862 1863	0.24 .05 .06 +0.30 0.37 +.07 0.45 .08 0.53	0.463 $+0.461$ $0.459$ $0.457$	0 0 0 0 0 0	0 0 0	1950 1960 1970 1980	$\begin{array}{c} 0 \ 33.71 \\ +0 \ 40.79 \\ 0 \ 48.53 \\ 0 \ 56.93 \end{array}$	0.193 $+0.155$ $0.115$ $0.074$	0.015 -0.018 0.022 0.026	$\begin{array}{c} 0.026 \\ +0.032 \\ 0.039 \\ 0.046 \end{array}$					
1864 1865 1866 1867	0.62 .09 +0.71 +.10 0.81 +.11 0.92 .11	0.455 $0.453$ $+0.451$ $0.449$ $0.446$	0 0 0 0	$0 \\ 0 \\ +0.001 \\ 0.001 \\ 0.001$	1990 2000 2010 2020 2030	+1 26.03 1 37.03 1 48.67	$0.032 \\ +0.010 \\ -0.053 \\ 0.096 \\ 0.140$	$\begin{array}{c} 0.030 \\ 0.035 \\ -0.040 \\ 0.045 \\ 0.050 \\ \end{array}$	$0.053 \\ 0.061 \\ +0.069 \\ 0.078 \\ 0.088$					
1868 1869 1770 1871 1872	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$0.444 \\ 0.442 \\ +0.440 \\ 0.438 \\ 0.436$	$ \begin{array}{c} -0.001 \\ 0.001 \\ -0.001 \\ 0.001 \\ 0.001 \end{array} $	0.001 $0.001$ $+0.001$ $0.001$ $0.001$	2040 2050 2060 2070 2080	$ \begin{array}{c cccc} 2 & 0.94 \\ 2 & 13.85 \\ +2 & 27.38 \\ 2 & 41.53 \\ 2 & 56.29 \end{array} $	0.183 $0.226$ $-0.268$ $0.309$ $0.349$	0.056 $0.062$ $-0.068$ $0.075$ $0.082$	0.098 $0.108$ $+0.119$ $0.130$ $0.142$					
1873 1874 1875 1876 1877	2.21 +.17	0.433 $0.431$ $+0.429$ $0.426$ $0.424$	0.001 0.001 -0.001 0.001 0.001	$\begin{array}{c} 0.001 \\ 0.002 \\ +0.002 \\ 0.002 \\ 0.002 \end{array}$	2090 2100 2110 2120	3 11.65 3 27.61 +3 44.17 4 1.32	$0.388 \\ 0.427 \\ -0.464 \\ 0.499$	0.089 0.096 0.104 0.112	$0.155 \\ 0.168 \\ + 0.182 \\ 0.196$					
1878 1879 1880 1881	$ \begin{array}{c cccc} 2.57 & .18 \\ +2.76 & .19 \\ +2.96 & .20 \\ +2.96 & +.20 \\ 3.16 &20 \end{array} $	$ \begin{array}{c c} 0.422 \\ +0.419 \\ +0.417 \\ 0.414 \end{array} $	$ \begin{array}{c c} 0.001 \\ -0.001 \\ -0.002 \\ 0.002 \end{array} $	$     \begin{array}{r}       0.002 \\       0.002 \\       +0.002 \\       +0.003 \\       0.003     \end{array} $	2130 2140 2150 2160 2170	4 19.07 4 37.40 4 56.31 +5 15.74 5 35.72	$0.532 \\ 0.563 \\ 0.593 \\ -0.620 \\ 0.645$	0.120 $0.128$ $0.137$ $0.146$ $0.156$	$\begin{array}{c c} 0.210 \\ 0.225 \\ 0.240 \\ +0.256 \\ 0.273 \end{array}$					
1882 1883 1884	3.59 .22	$0.412 \\ 0.409 \\ +0.407$	0.002 0.002 -0.002	$0.003 \\ 0.003 \\ +0.003$	2180 2190 2200	5 56.24 6 17.29 +6 38.88	0.668	0.165 0.175 -0.184	0.289 $0.306$ $+0.322$					

	TAB	LE VII	.—Equa	TION (	OF CENT	TRE A	ND	PRI	INCIPAL	TERM (	F Log. 2		
g	E		Log.	r		g			E		Log	r	
00	0 0 00.00	59.81	1.26 18915		360°	10°	0	, 59	26.71	11	1.26 22488		350°
10'	0 0 59.81	59.81	18916	3	50'	10'	1	0	25.41	58.70	22608	120	50'
20	0 1 59.62	59.80	18919	5	40	20	1	1	24.08	58.63	22729	123	40
30	0 2 59.42	59.81	18924	7	30	30	1	2	22.71	58.59	22852	125	30
40 50	0 3 59.23 0 4 59.03	59.80	18931 18940	9	20	40 50	1	3	21.30 19.85	58.55	22977 23104	127	20 10
		59.79		II			1	*		58.52		130	-
1°	0 5 58.82	59.79	18951	13	359°	11°	1	5	18.37	58.48	23234	131	349°
10'	0 6 58.61	59.78	18964	15	50'	10'	1	6	16.85	58.43	23365	133	50'
20	0 7 58.39	59.79	18979	17	40	20	1	7	15.28	58.40	23498	135	40
30	0 8 58.18 0 9 57.96	59.78	18996 19015	19	30 20	30	1	8	13.68 12.04	58.36	23633	137	30 20
50	0 10 57.74	59.78	19036	21	10	50	1		10.36	58.32	23909	139	10
		59.77		23						58.27		142	
20	0 11 57.51	59.76	19059	25	358°	12		11	8.63	58.23	24051	143	348°
10	0 12 57.27	59.75	19084	27	50'	10'	1	12	6.86	58.18	24194	145	50'
20 30	0 13 57.02 0 14 56.76	59.74	19111	29	40 30	20 30	1	13 14	5.04	58.14	24339 24485	146	40 30
40	0 14 56.46	59.73	19171	31	20	40	1	15	1.28	58.10	24633	148	20
50	0 16 56.22	59.73	19204	33	10	50	-	15	59.33	58.05	24784	151	10
		59.71		34						58.00		153	
3° 10'	0 17 55.93	59.70	19238	37	357°	13°	1	16	57.33	57.96	24937 25091	154	347° 50′
20	0 18 55.63 0 19 55.33	59.70	19275 19314	39	50' 40	20	1	17 18	55.29 53.20	57.91	25247	156	40
30	0 20 55.01	59.68	19355	41	30	30	_		51.06	57.86	25405	158	30
40	0 21 54.68	59.67	19397	42	20	40	î		48.87	57.81	25566	161	20
50	0 22 54.34	59.66	19442	45	10	50	1	21	46.63	57.76	25728	162	10
40	10/10/2019	59.64		47	356°	14°	,			57.72		164	346°
10	0 23 53.98 0 24 53.61	59.63	19489	49	50'	10'	1	22 23	44.35	57.66	25892 26057	165	50'
20	0 25 53.22	59.61	19589	51	40	20	1	24	39.63	57.62	26225	168	40
30	0 26 52.81	59.59	19642	53	30	30	i	25	37.19	57.56	26395	170	30
40	0 27 52.39	59.58	19697	55	20	40	î		34.70	57.51	26566	171	20
50	0 28 51.95	59.56	19754	57	10	50	1	27	32.16	57.46	26740	174	10
5°	0 29 51.49	59-54	19812	58	355°	15°	1	28	29.57	57.41	26916	176	345°
10	0 30 51.01	59.52	19872	60	50'	10'	1	29	26.92	57-35	27093	177	50'
20	0 31 50.52	59.51	19934	62	40	20	i	30	24.22	57.30	27271	178	40
30	0 32 50.01	59.49	19999	65	30	30	i	31	21.47	57.25	27451	180	30
40	0 33 49.48	59.47	20065	66	20	40	1		18.67	57.20	27634	183	20
50	0 34 48.93	59.45	20134	69	10	50	1	33	15.80	57.13	27819	185	10
6,	0 35 48.36	59.43	20205	71	354°	16	1	34	12.88	57.00	28007		344°
10'	0 36 47.77	59.41	20278	73		10'			9.90	57.02	28196	189	50'
20	0 37 47.15	59.38	20352	74	40	20	1	36	6.87	56.97	28386	190	40
30	0 38 46.51	59.36	20428	76	30	30		37	3.77	56.90	28578	192	30
40	0 39 45.84	59.33	20507	79	20	40	1	38	0.62	56.85	28772	194	20
50	0 40 45.15	59.31	20588	82	10	50	1	38	57.41	56.73	28968	199	10
73	0 41 44.44	59.29	20670		353°	17°	1	30	54.14		29167		343°
10'	0 42 43.70	59.26	20755	85	50'	10'			50.81	56.67	29367	200	50'
20	0 43 42.94	59.24	20841	86 88	40	20		41	47.43	56.62	29568	201	40
30	0 44 42.15	59.21	20929		30	30	1		43.98	56.55	29771	203	30
40	0 45 41.33	59.18	21020	91	20	40		-	40.46	56.43	29976	207	20
50	0 46 40.48	59.15	21112	94	10	50	1	44	36.89	56.36	30183	200	10
83	0 47 39.61		21206		352°	18°	1	45	33.25		30392		342°
10'	0 48 38.71	59.10	21302	96	50'	10'	1	46	29.55	56.30	30603	211	50'
20	0 49 37.78	59.07	21400	98	40	20		47	25.78	56.23	30816	213	40
30	0 50 36.82	59.04	21499	99	30	30	1		21,95	56.10	31030	216	30
40	0 51 35.83	58.98	21601	104	20	40	1		18.05	56.04	31246	219	20
50	0 52 34.81	58.95	21705	106	10	50	1	50	14.09	55.97	31465	221	10
9°	0 53 33.76		21811		351°	19°	1	51	10.06		31686		341°
- 10	0 54 32.67	58.91	21919	108	50'	10'	1	52	5.96	55.90	31908	222	50'
20	0 55 31.55	58.88	22029	110	40	20	1	53	1.80	55.84	32132	224	40
30	0 56 30.39	58.84	22140	114	30	30	4		57.57	55·77 55·70	32358	227	30
40	0 57 29.20	58.77	22254	116	20	40	1		53.27	55.64	32585	229	20
50	0 58 27.97	58.74	22370	118	10	50	1	55	48.91	55-56	32814	231	.10
10°	0 59 26.71	0 , ,	22488		350°	20°	1	56	44.47		33045		340°
			1.26		9						1.26		9

			7		TAB	LE VI	1.—0	ontin	ued.				
	g	E		Log	;. r	2	g		E		Log	. r	
	20°	1 56 44.47	"	1.26 33045		340°	30°	2 49	51.28	"	1.26 50121	226	330°
ı	10'	1 57 39.96	55·49 55·43	33278	<sup>2</sup> 33 <sup>2</sup> 35	50'	10'	2 50		50.35	50457	336 338	50'
	20 30	1 58 35.39 1 59 30.74	55.35	33513	236	40 30	20 30	$\begin{vmatrix} 2 & 51 \\ 2 & 52 \end{vmatrix}$		50.14	50795	339	40 30
	40	2 0 26.02	55.28	33987	238	20	40	2 53	12.06	50.05	51475	341	20
	50	2 1 21.23	55.21	34227	240 24I	10	50	2 54	2.00	49.94	51818	343	10
	21°	2 2 16.36		34468	243	339°	31°	2 54		49.73	52162	345	329°
1	10' 20	2 3 11.42	55.06	34711 34956	245	50' 40	10' 20	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$		49.62	52507 $52854$	347	50' 40
۱	30	2 4 6.41 2 5 1.33	54.92	35204	248	30	30	2 57	20.70	49.52	53203	349	30
ı	40	2 5 56.17	54.84 54.76	35454	250 251	20	40	2 58		49.42	53553	35° 35°	20
1	50	2 6 50.93	54.68	35705	252	10	50	2 58	59.43	49.20	53905	353	10
1	22°	2 7 45.61	54.61	35957	254	338°	32°	2 59	48.63	49.10	54258	355	328°
ı	10' 20	2 8 40.22 2 9 34.76	54.54	$36211 \\ 36467$	256	50' 40	10' 20	$\begin{bmatrix} 3 & 0 \\ 3 & 1 \end{bmatrix}$	37.73 26.73	49 00	54613 54970	357	50' 40
ı	30	2 10 29.22	54.46	36726	259	30	30	3 2	15.62	48.89 48.79	55329	359	30
	40	2 11 23.60	54.38	36986	260	20	40	3 3	4.41	48.68	55689	361	20
	50	2 12 17.90	54.22	37248	263	10	50	3 3	53.09	48.57	56050	363	10
ı	23°	2 13 12.12	54.14	37511	265	337°   50′	33° 10′	3 4 3 5	41.66	48.46	56413 56777	364	327° 50′
ł	10' 20	2 14 6.26 2 15 0.32	54.06	37776 38043	267	40	20	3 5 6	18.47	48.35	57143	366	40
ł	30	2 15 54.30	53.98	38311	268	30	30	3 7	6.72	48.25	57510	367 369	30
ı	40	2 16 48.20	53.90	38581	270	20	40	3 7	54.85	48.02	57879	370	20
۱	50	2 17 42.02	53.73	38853	275	10	50	3 8	42.87	47.91	58249	372	10
ı	24° 10′	2 18 35.75	53.65	39128	276	336,	34	3 9	30.78	47.80	58621 58994	373	326°
ı	20	2 19 29.40 2 20 22.97	53.57	39404 39681	277	50' 40	$\begin{vmatrix} 10 \\ 20 \end{vmatrix}$	3 10 3 11	$18.58 \\ 6.26$	47.68	59369	375	50' 40
ı	30	2 21 16.46	53.49	39960	279	30	30	3 11	53.83	47.57	59746	377 378	30
I	40	2 22 9.87	53.41	40241	283	20	40	3 12	41.29	47.46 47.35	60124	379	20
ı	50	2 23 3.19	53.23	40524	284	10	50	3 13	28.64	47.23	60503	381	10
ŀ	25° 10′	2 23 56.42 2 24 49.57	53.15	40808	286	335°   50′	35° 10′	3 14 3 15	15.87 2.99	47.12	$60884 \\ 61266$	382	325° 50′
ı	20	2 25 42.63	53.06	41382	288	40	20	3 15	50.00	47.01	61650	384	40
1	30	2 26 35.61	52.98	41671	289	30	30	3 16	36.89	46.89	62035	385 387	30
ı	40 50	2 27 28.50 2 28 21.30	52.80	41962	293	20	40	3 17	23.67	46.66	$62422 \\ 62810$	388	20
			52.71	42255	295	10	50	3 18	10.33	46.55		390	10
1	26°	2 29 14.01 2 30 6.63	52.62	$42550 \\ 42846$	296	334° 50′	36°		56.88	46.43	$63200 \\ 63592$	392	324° 50′
ı	20	2 30 59.16	52.53	43144	298	40	20		43.31 29.63	46.32	63985	393	40
ı	30	2 31 51.60	52.44	43444	300	30	30	3 21	15.83	46.20	64380	395 396	30
ı	50	2 32 43.95 2 33 36.21	52.26	43745 44048	303	20	40	3 22	1.91	45.97	64776 65173	397	20
	27°		52.17		305	10	50	3 22	47.88	45.84		399	10
1	10'	2 34 28.38 2 35 20.46	52.08	44353 44659	306	333° 50′	37°	3 23 3 24	33.72 19.44	45.72	65572 65972	400	323° 50′
	20	2 36 12.44	51.98	44967	308	40	20	3 25	5.04	45.60	66373	401	40
	30 40	2 37 4.34	51.90	45277	310	30	30		50.53	45·49 45·36	66776	403	30
	50	2 37 56.14 2 38 47.85	51.71	45588 45901	313	20 10	40 50	3 26 3 27	35.89 21.13	45.24	67180 67585	405	20 10
	28°	2 39 39.46	51.61	46216	315					45.12	67992	407	ALC: UNK
	10'	2 40 30.98	51.52	46532	316	332° 50′	38°   10′	3 28 3 28	$6.25 \\ 51.25$	45.00	68400	408	322° 50′
1	20	2 41 22.40	51.42 51.32	46850	318	40	20	3 29	36.13	44.88	68810	410	40
1	30 40	2 42 13.72 2 43 4.95	51.32	47170	320	30	30	3 30	20.90	44.77	69221	411	30
	50	2 43 4.95 2 43 56.08	51.13	47491 47814	323	20 10	40 50	3 31	5.54 50.05	44.52	69633 70047	414	20 10
1	29°	2 44 47.12	51.04	48138	324	331°	39°			44.40	70463	416	321°
1	10'	2 45 38.06	50.94	48464	326	50'	10'		$34.45 \\ 18.72$	44.27	70880	417	50'
	20	2 46 28.90	50.84	48792	328	40	20	3 34	2.86	44.14	71298	418	40
1	30 40	2 47 19.64 2 48 10.29	50.65	49122 49453	331	30 20	30		46.88	44.02	71717 72138	419	30 20
1	50	2 49 0.83	50.54	49786	333	10	40 50		30.78 14.55	43.77	72560	422	10
	30°	2 49 51.28	50.45	50121	335	330°	40°		58.19	43.64	72984	424	320°
				1.26		<i>g</i>	10	0 00	00.10		1.26		g g
	- 1						-						

TABLE VII.—Continued.												
g	E	Log. r		g	E	Log. r						
40°	3 36 58 19	1.26 72984	320°	50°	0 / " " 1 4 16 34.27 00	.27						
10' 20	3 37 41.71 43·5 <sup>2</sup> 3 38 25.10 43·39	73409 425 73835 426	50' 40	10'	4 17 44 89 35.20 01	183 496 50' 681 498 40						
30	3 39 8.37 43.27	74262 427	30	30	4 18 19.88 35.00 02	2180 499 30						
40 50	3 39 51.51 43.14 3 40 34.52 43.01 42.88	74691 43° 75121 43°	20 10	40 50	2 10 04.00 24 77 02	2680 501 20 3181 501 10						
41°	3 41 17.40	75553 75986 433	319° 50′	51°	4 20 4.19 03	3683 309°						
10' 20	3 42 0.16 42.63 3 42 42.79 42.50	76420 434 76956 436	40	20	4 21 13.00 34.33 04	1690 504 40						
30 40	3 43 25.29 42.37 3 44 7.66 42.37	77293 437	30	30	4 21 41.18 34.04 05	5195 5°5 80 5701 5°5 20						
50	3 44 49.91 42.25	77731 438	10	50	22 80	3207 5°6 10						
42°	3 45 32.02 41.99	78171 440	318°	52° 10′	4 23 28.85	3714 508 308° 50′						
20	3 46 55.86 41.85	79053 442	40	20	4 24 35.88 33.44 07	1732 510 40						
30	3 41 31.35 41.59	79941 445	30 20	30 40	4 25 42 32 33.14 08	8754 511 90						
50	3 49 0.63 41.40	80387 446	10	50	32.84	266 514 10						
43°	3 49 41.96 3 50 23.16 41.20	80835 81284 449	317° 50′	53°		9780 9294 514 <b>307°</b> 5094 50'						
20	3 51 4.22 41.06	81733 449	40	20 30	4 27 53.39 32.54 10	0809 515 40 1325 516 30						
30 40	3 59 95 94 40.79	82635 452	30 20	40	4 28 58.03 32.24 11	1842 517 20						
50	3 53 6.60 40.66	83089 454 455	10	50	31.94	2361 519 10						
44°	3 54 27.52 40.39	83544 84000 456	316° 50′	54° 10′	1 30 33 85 31.79 15	2881 520 306° 50′						
20 30	3 55 7.78 40.26 3 55 47.90 40.12	84457 457 84914 457	40 30	20 30	27 40	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$						
40	3 56 27.89 39.99	85373 459	20	40	4 32 8.31 31.33 14	4966 522 20						
50	39.72	463	10	50 55°	31.03	525						
45°	3 58 27.05 39.58	86297 86760 463	315° 50′	10'	4 33 41.41 30.88 10	6540 525 50'						
20	3 59 6.50 39·45 3 59 45.81 39·31	87224 464 87690 466	40 30	20 30	20 57	7505 528 20						
40	4 0 24.98 39.17	88156 468	20	40	4 35 13.13 30.42 18	8123 528 20						
50 46°	38.89	88624 469	10 314°	50 56°	30.12	9182 53° 10 9182 53° 304°						
10'	4 2 21.65 38.75	89564 471	50'	10'	4 36 43.48 29.90 1	9712 530 50'						
20 30	1 9 99 75 38.48	90507 472	40 30	20 30	4 37 42 94 29.65 20	0776 533 30						
40 50	4 4 17.09 30.34	90980 473 91455 475	20 10	40 50	20 21	1309 533 20 1842 533 10						
47°	4 5 33.36 38.06	91931 476	313°	57°	4 39 10 96 29.19	9376 534 3030						
10'	4 6 11.29 37.78	92408 477	50' 40	10' 20	4 39 39.99 29.03 2	2911 535 50'						
30	4 7 26.72 37.65	93365 479	30	30	4 40 37.59 28.72 2	3986 538 80						
40 50	4 8 4.22 37.50 4 8 41.58 37.36	93845 482	20	40 50	4 41 0.10 28.41	5063 539 10						
48	0 4 9 18 80	94810	312°	58°	4 42 2.83	5603 540 302°						
10'		95294 484 95779 485	50'	10'	07.04	6143 54° 50′ 6684 54 <sup>1</sup> 40						
30	4 11 9.60 36.79	96265 486	30	30	4 43 26.66 27.79 2	7226 542 30						
50	4 12 22 76 36.51	97240 488	20 10	40 50	4 44 21.76 27.47 2	8311 543 10						
49	o 4 12 59.12 36.30	97730 490	311°	59°		8855 544 301° 50′						
10'	4 13 35.34 36.22 4 14 11.41 36.07	98220 49° 98711 491	50' 40	10'	4 45 43 99 26.99 9	9944 545 40						
30	4 14 47.34 35.93	99203 492	30	30	4 46 10.06 26.84 3	0491 547 30 1038 547 20						
50	4 15 58.77 35.64	*00191 495	20 10	40 50	4 40 30.10	1587 549 10						
50	2 4 16 34.27	*00687	310°	60°	4 47 29.64 3	2137						
1	00 Tuna 1979	*1.27	9		-	1.27 g						

Г				TAB	LE <sub>.</sub> VI.	I.— <i>C</i>	ontin	ued.			•	
g	E		Log	. r		g		E		Log	. r	
60°	1	26.21	1.27	550	300° 50′	70°		, , ,, 8 57.01	16.47	1.27 66156	582	290°
10' 20	4 47 55.85 4 48 21.90	26.05	32687 33237	550	40	20		9 13.48 9 29.79	16.31	66738	582	50' 40
30 40	4 48 47.79 4 49 13.53	25.89 25.74	33787	55° 551	30 20	30 40	5 1	9 45.93 1.91	15.98	67903	583 584	30 20
50	4 49 39.10	25.57	34890	552	10	50		17.72	15.81	69071	584	10
61°	4 50 4.52	25.42	35443	553	299°	71°	5 10	33.36	15.64	69655	584	289°
10' 20	4 50 29.78	25.26 25.10	35996	553 554	50'	10' 20	5 10		15.48	70239	584 585	50'
30	4 50 54.88 4 51 19.82	24.94	36550 37105	555	30	30	5 11 5 11		15.15	70824	585	30
40	4 51 44.60	24.78	37660	555 556	20	40	5 11		14.98	71994	585 585	20
50	4 52 9.22	24.46	38216	557	10	50		49.09	14.65	72579	586	10
62°	4 52 33.68 4 52 57.98	24.30	38773 39330	557	298° 50′	72°	5 19 5 19		14.49	73165	586	288° 50′
20	4 53 22.11	24.13	39888	558	40	20	5 19	32.55	14.32	74337	586 587	40
30 40	4 53 46.09 4 54 9.90	23.98 23.81	40446	558 559	30 20	30	5 13 5 13		13.99	74924	587	30
50	4 54 33 56	23.66	41565	560	10	50	5 13		13.82	75511 76098	587	20
63°	4 54 57.05	23.49	42126	561	297°	73°	5 18		13.66	76685	587	287°
10'	4 55 20.38	23.33	42687	561 562	50'	10'	5 18	41.66	13.49	77273	588 588	50'
20 30	4 55 43.56 4 56 6.57	23.01	43249	562	30	20 30	5 13		13.32	77861 78450	589	30
40	4 56 29.42	22.85	44374	563	20	40		21.12	12.99	79039	589	20
50	4 56 52.11	22.53	44938	564 565	10	50	5 14	33.94	12.82	79628	589 589	10
64° 10′	4 57 14.64	22.37	45503	565	296°	74°		46.60	12.49	80217	590	286°
20	4 57 37.01 4 57 59.21	22.20	46068	565	50'	10' 20	5 14 5 15	59.09	12.32	80807	590	50' 40
30	4 58 21.25	22.04	47199	566 567	30	30	5 15	23.57	12.16	81987	590	30
40 50	4 58 43.13 4 59 4.84	21.71	47766	567	20	40 50	5 15		11.99	82577	59°	20
65°	4 59 26.40	21.56	48333	568	10		5 15		11.66	83168	591	10
10'	4 59 47.79	21.39	48901 49469	568	295° 50′	75°	5 15 5 16		11.49	83759 84350	591	285° 50′
20	5 0 9.02	21.23	50038	569 569	40	20		21.87	11.33	84941	591	40
30	5 0 30.09 5 0 50.99	20.90	50607 51177	570	30 20	30	5 16 5 16		11.00	85532	591 592	30 20
50	5 1 11.73	20.74	51747	570	10	50		44.03 54.86	10.83	86124	591	10
66°	5 1 32.31	20.58	52318	571	294°	76°	5 17	5.52	10.66	87307	592	284°
10' 20	5 1 52.72	20.41	52889	571 572	50'	10'	5 17	16.02	10.50	87899	592 592	50'
30	5 2 12.97 5 2 33.06	20.09	53461 54033	572	40 30	$\begin{vmatrix} 20 \\ 30 \end{vmatrix}$	5 17 5 17		10.16	88491 89084	593	40 30
40	5 2 52.98	19.92	54606	573	20	40		46.51	10.00	89677	593	20
50	5 3 12.74	19.60	55179	573 574	10	50	5 17	56.34	9.83 9.66	90270	593 593	10
67° 10′	5 3 32.34 5 3 51.77	19.43	55753	574	293°	77°	5 18	6.00	9.50	90863	593	283°
20	5 4 11.04	19.27	56327 56901	574	50' 40	10' 20		15.50 24.82	9.32	91456 92049	593	50' 40
30	5 4 30.15	19.11	57476	575 575	30	30	5 18	33.99	9.17 8.99	92643	594	30
40 50	5 4 49.09 5 5 7.87	18.78	58051 58627	576	20 10	40 50	5 18 5 18	42.98 51.81	8.83	93237	594 593	20
68°	5 5 26.49	18.62	59204	577	292°	78°			8.66	93830	594	10
10	5 5 44.94	18.45	59781	577	50'	10'	5 19 5 19	0.47 8.97	8.50	94424 95018	594	282° 50′
20 30	5 6 3.23 5 6 21.35	18.29	60358	577 578	40	20	5 19	17.30	8.33 8.16	95612	594	40
40	5 6 39.30	17.95	60936 61514	578	30 20	30	5 19 5 19	25.46 33.46	8.00	96206 96800	594 594	30 20
50	5 6 57.09	17.79	62093	579	10	50		41.29	7.83	97395	595	10
69°	5 7 14.72	17.46	62673	579	291°	79°		48.95	7.66	97990	595	281°
10' 20	5 7 32.18 5 7 49.48	17.30	63252	579 580	50'	10'	5 19	56.45	7.50	98585	595	50'
30	5 8 6.61	17.13	63832 64412	580	40 30	20 30	5 20 5 20	$3.78 \\ 10.94$	7·33 7·16	99179 99774	594 595	40 30
50	5 8 23.57 5 8 40.37	16.96	64993	581 581	20	40	5 20	17.94	7.00	*00369	595	20
70°		16.64	65574	582	10	50		24.77	6.83	*00965	596	10
10	5 8 57.01		66156 1.27		290°	80°	5 20	31.44		*01560	0.0	280°
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Ī			-			TAR	ווע עו	I.—Con	tinna	,				
-	g		E		Log				linue	E E		Log		1
-	9	0 , ,		11	1.28			9	0 /		"		. r	
	80°	5 20 31.	44 6	.50	01560		280°	90°	5 29			1.28 37187		270°
1	10'	5 20 37.	102 6	-34	02155	595 595	50'	10'	5 25		3.37	37776	589	50
1	20 30	5 20 44. 5 20 50.	20 6	.17	02750 03346	596	30	20 30	5 22		3.53	38365	589	40
	40	5 20 56.	10 0	.01	03941	595	20	40	5 2		3.86	38954 39543	589	30
	50		20 5	.84	04536	595	10	50	5 2		4.01	40131	588	10
	81°	5 21 7.	96		05131	595	279°	91°	5 21	46.40		40719	588	269°
1	10'	5 21 13.	7 (1)	.50	05726	595 596	50'	10'	5 2		4-34	41307	588 587	50
ı	20 30	5 21 18.	07 5	.17	06322	595	30	20 30	5 2		4.66	41894	588	30
	40	5 21 28	97 5	.00	07512	595	20	40	5 2		4.82	42482	587	20
	50	5 21 33.	2	.84	08107	595	10	50	5 2		4.98	43655	586	10
	82°	5 21 38.	48		08702	595	278°	92°	5 21	17.97		44242	587	268°
	10'	5 21 42.	00	.51	09297	595 596	50'	10'	5 21	12.67	5.30	44828	586 586	50'
1	20 30	5 21 47. 5 21 51.	.00	.17	09893 10488	595	30	20 30	5 21		5.47	45414	586	30
1	40	5 21 55.	51 4	.01	11083	595	20	40	5 20		5.79	46585	585	20
	50	5 21 59.	30 3.	.85	11679	596	10	50	5 20			47170	585	10
1	83°		04		12274	595	277	93°	5 20	43.74		47755	585	267°
1	10'		00	35	12869	595	50'	10'	5 20	37.48	6.26	48339	584	50'
	20 30	5 22 9. 5 22 13.	09 3.	.18	13465	595	40 30	20 30	5 20		6.58	48923	584	40 30
	40	5 22 16.	11 3.	.02	14655	595	20	40	5 20	•	6.75	50090	583	20
П	50	5 22 18.	28 4	.86	15250	595 596	10	50	5 20	10.82	7.06	50673	583 583	10
	34°	5 22 21.	66		15846		276°	94°	5 20	3.76		51256	582	266°
Ш	10'	5 22 24.	10	53	16441	595 595	50'	10'	5 19		7.22	51838	582	50'
1	20 30	5 22 26. 5 22 28.	0.0	20	17036 17631	595	30	20 30	5 19		7.54	52420 53002	582	40 30
	40	5 22 30.	78 2.	.03	18226	595	20	40	5 19		7.69	53583	581	20
	50	5 23 32.	64 1.	70	18820	594	- 10	50	5 19		7.86	54163	580 580	10
1	35°	5 22 34.	34		19415	595	275°	95°	5 19		8.17	54743	580	265°
	10'	5 22 35.	O 8	53	20010	595 594	50'	10'	5 19		8.33	55323	579	50'
	20 30	5 22 37. 5 22 38.	44 I.	20	20604 21198	594	40 30	20 30	5 19 5 18		8.50	55902	579	40 30
	40	5 22 39.	48 1.	87	21792	594	20	40	5 18		8.64	57060	579	20
	50	5 22 40.		71	22386	594 594	10	50	5 18	35.61	8.81	57638	578 578	10
1	36°	5 22 41.	0.6	54	22980	594	274°	96°	5 18	26.65	0.12	58216	578	264°
	10' 20	5 22 41.	00	39	23574	593	50'	10'	5 18		9.27	58794	577	50' 40
_	30	5 22 41. 5 22 42.	91 0.	22	24167 24761	594	40 30	20 30	5 18 5 17		9.43	59371 59948	577	30
	40	5 22 42.	26	05	25354	593	20	40	5 17	49.24	9.59	60525	577	20
	50	5 22 42.	0.	27	25948	594 593	10	50	5 17		9.74	61101	576	10
	37°	5 22 41.5	38	43	26541		273°	97°	5 17	29.60	10.06	61677		263°
_	10' 20	5 22 41.4 5 22 40.8	25 0.1	60	27134 27726	593 592	50' 40	10'	5 17 5 17	19.54 9.33	10.21	62252 62827	575 575	50' 40
	30	5 22 40.0	10 0.	76	28319	593	30	30	5 16		10.37	63401	574	30
	10	5 22 39.	16	93	28911	592	20	40	5 16	48.44	10.52	63975	574	20
	50	5 22 38.0	74 I.:	25	29504	593 592	10	50	5 16		10.84	64548	573 572	10
	80	5 22 36.8	32	42	30096	592	272°	98°	5 16	26.92	10.99	65120	572	262°
	10' 20	5 22 35.4 5 22 33.8	10	58	30688 31280	592	50' 40	10' 20	5 16 5 16	15.93	11.15	65692 66264	572	50′ 40
	30	5 22 32.0	93 I.		31872	592	30	30	5 15	53.48	11.30	66836	572	30
	40	5 22 30.1		91	32464	59 <sup>2</sup> 59 <sup>1</sup>	20	40	5 15		11.46	67407	571	20
	50	5 22 28.1	2.	24	33055	592	10	50	5 15	30.41	11.77	67977	570	10
	9°	5 22 25.8		39	33647	591	271°	99°	5 15 5 15	18.64	11.92	68547	570	261° 50′
	20	5 22 23.4 5 22 20.9	1 2.	56	34238 34828	590	50' 40	10' 20	5 14		12.08	69686	569	40
	30	5 22 18.1	19 2.	72	35418	590	30	30	5 14	42.41	12.23	70255	569	30
	10	5 22 15.3	31	88	36008	589	20	40	5 14		12.38	70823	568	20 10
	50	5 22 12.9	3.	21	36597	590	10	50	5 14	17.49	12.69	71391	567	
9	0,	5 22 9.0	05		37187 1 28		270°	100°	5 14	4.80		71958 <b>1.28</b>	4.7	260°
-		TO COLI			1 20	-	9					1.20		9

1					TAB	LE VI	I.—Cor	ntinued.				
	g			Log	. r		g			Log.	r	
		0 / //	"	1.23				0 / //	11	1.29		
1	100°	5 14 4.80		71958	567	260°	110°	4 56 49.88	21.68	04888	528	250°
1	10'	5 13 51.96 5 13 38.96	7	72525	566	50'	10' 20	4 56 28.20 4 56 6.39	21.81	05416	528	50'
1	30	5 13 25.81	13.15	73656	565	30	30	4 55 44.44	21.95	06471	527	30
1	40	5 13 12.51	13.30	74221	565	20	40	4 55 22.34	22.10	06997	526 525	20
1	50	5 12 59.06	13.61	74785	563	10	50	4 55 0.10	22.38	07522	525	10
1	101° 10′	5 12 45.45 5 12 31.69	T 2 70	75348	563	259° 50′	111° 10′	4 54 37.72 4 54 15.21	22.51	08047	524	249°
I	20	5 12 17.78	13.91	76474	563	40	20	4 54 15.21 4 53 52.55	22.66	08571	523	50' 40
1	30	5 12 3.72	14.00	77036	562 562	30	30	4 53 29.76	22.79	09616	522	30
1	40 50	5 11 49.50 5 11 35.14	T4 26	77598	561	20	40 50	4 53 6.83	23.07	10137	521	20
1			14.52	78159	561	10	11 11 11	4 52 43.76	23.21	10658	520	10
1	102°	5 11 20.62 5 11 5.95	14.67	78720 79280	560	258° 50′	112° 10′	4 52 20.55 4 51 57.20	23.35	11178	519	248° 50′
	20	5 10 51.13	14.82	79839	559	40	20	4 51 33.72	23.48	12215	518	40
	30	5 10 36.16	14.97	80398	559 558	30	30	4 51 10.10	23.62	12732	517	30
	40 50	5 10 21.04 5 10 5.77	15.27	80956 81514	558	20 10	40 50	4 50 46.34 4 50 22.44	23.90	13248 13764	516	20
ı			15.42	10.79	557				24.03		515	
	103° 10′	5 9 50.35 5 9 34.78	15.57	82071 82628	557	257° 50	113° 10′	4 49 58.41 4 49 34.24	24.17	14279	514	247° 50′
ı	20	5 9 19.06	15.72	83184	556	40	20	4 49 9.94	24.30	15306	513	40
П	30	5 9 3.19 5 8 47.17	15.87	83739	- 555 555	30	30	4 48 45.50	24.44	15818	512	30
ı	40 50	5 8 47.17 5 8 31.01	16.16	84294 84849	555	20 10	40 50	4 48 20.92 4 47 56.21	24.71	16329	511	20 10
ı	104°	5 8 14.69	16.32	85403	554	256°	114°		24.85		510	
П	104	5 7 58.22	16.47	85956	553	50'	10'	4 47 31.36 4 47 6.38	24.98	17350 17859	509	246° 50′
1	20	5 7 41.61	16.61	86508	552 551	40	20	4 46 41.26	25.12	18367	508	40
ı	30 40	5 7 24.85 5 7 7.94	16.91	87059 87610	551	30 20	30 40	4 46 16.00	25.26 25.39	18874	507 506	30
П	50	5 6 50.88	17.06	88160	550	10	50	4 45 50.61 4 45 25.09	25.52	19380 19886	506	20
L	105°	5 6 33.67	17.21	88709	549	255°	115°	4 44 59.44	25.65	20391	505	245°
F	10'	5 6 16.32	17.35	89258	549	50'	10'	4 44 33.66	25.78	20391	504	50'
ı	20	5 5 58.82	17.50	89806	548 548	40	20	4 44 7.74	25.92 26.05	21398	503	40
ı	30 40	5 5 41.17 5 5 23.37	17.80	90354	548	30 20	30 40	4 43 41.69 4 43 15.50	26.19	21900 22401	501	$\begin{array}{c c} 30 \\ 20 \end{array}$
F	50	5 5 5.42	17.95	91449	547	10	50	4 42 49.19	26.31	22901	500	10
	106°	5 4 47.33	18.09	91995	546	254°	116°	4 42 22.74	26.45	23401	500	244°
Ŀ	10'	5 4 29.10	18 23 18.38	92540	545	50'	10'	4 41 56.16	26.58	23899	498	50'
ı	20 30	5 4 10.72 5 3 52.19	18.53	93085 93629	545	40	20	4 41 29.45	26.71 26.85	24397	498 497	40
ı	40	5 3 33.52	18.67	93629	543	30 20	30 40	4 41 2.60 4 40 35.62	26.98	24894 25390	496	30 20
ı	50	5 3 14.70	18.82	94715	543	10	50	4 40 8.52	27.10	25885	495	10
1	107°	5 2 55.74		95257	542	253°	117°	4 39 41.28	27.24	26380	495	243°
	10' 20	5 2 36.63	19.11	95798	541	50'	10'	4 39 13.91	27.37	26874	494 492	50'
	30	5 2 17.38 5 1 57.99	19.39	96338 96878	540	40 30	20 30	4 38 46.41 4 38 18.78	27.50 27.63	27366	491	40 30
	40	5 1 38.45	19.54	97417	539	20	40	4 37 51.02	27.76	27857 28348	491	20
	50	5 1 18.77	19.83	97955	538 538	10	50	4 37 23 13	27.89	28837	489	10
1	.08°	5 0 58.94	19.97	98493		252°	118°	4 36 55.12		29325	487	242°
	10' 20	5 0 38.97 5 0 18.86	20.11	99030 99566	537 536	50'	10'	4 36 26.98	28.14 28.27	29812	487	50'
	30	4 59 58.60	20.26	*00101	535	40 30	20 30	4 35 58.71 4 35 30.31	28.40	30299 30785	486	40 30
	40	4 59 38.21	20.39	*00636	535	20	40	4 35 1.78	28.53	31270	485	20
	50	4 59 17.67	20.69	*01170	534 533	10	50	4 34 33.13	28.65 28.78	31754	483	10
1,	09°	4 58 56.98 4 58 36.15		*01703	533	251°	119°	4 34 4.35	28.91	32237	482	241°
	20	4 58 36.15	20.97	*02236 *02768	532	50' 40	10' 20	4 33 35.44 4 33 6.41	29.03	32719	481	50'
	30	4 57 54.07	21.11	*03299	531	30	30	4 32 37.25	29.16	33200 33681	481	30
	40 50	4 57 32.81 4 57 11.42	27 22	*03829	530	20	40	4 32 7.96	29.29	34161	480	20
1.			21.54	*04359	529	10	50	4 31 38.55	29.41	34640	477	10
1	10°	4 56 49.88		*04888 *1.29		250°	120°	4 31 9.01		35117		240°
_				1.20		g			(See all	1.29		g

	TABLE VII.—Continued.											
g	E		Log.	r		g		E		Log.	r	
120°	4 31 9.01		1.29		240°	130°	3 57	57.75		1.29 61903		230°
10'	4 30 39.35	29.66	35593	476	50'	10'	3 57	21.10	36.65	62317	414	50'
20	4 30 9.56	29.79	36069	476	40	20	3 56	44.35	36.75	62729	412	40
30	4 29 39.65	30.04	36544	475	30	30	3 56	7.48	36.87	63140	411	80
40	4 29 9.61	30.16	37018	473	20	40	3 55	30.51	37.08	63550	400	20
50	4 28 39.45	30.29	37491	472	10	50		53.43	37.18	63959	407	10
121°	4 28 9.16	30.41	37963	471	239°	131°		16.25	37.28	64366	407	229°
10'	4 27 38.75	30.53	38434 38904	470	50' 40	10' 20	3 53 3 53	38.97	37.39	64773	406	50'
20 30	4 27 8.22 4 26 37.56	30.66	39372	468	30	30		24.08	37.50	65583	404	40 30
40	4 26 6.78	30.78	39840	468	20	40	3 51	46.48	37.60	65987	404	26
50	4 25 35.88	30.90	40306	466 465	10	50	3 51	8.78	37.70 37.81	66389	402	10
122°	4 25 4.85	33	40771		238°	132°	3 50	39.97	31.01	66790	401	228°
10'	4 24 33.71	31.14	41236	465	50'	10'	3 49	53.06	37.91	67190	400	50'
20	4 24 2.44	31.27	41700	464	40	20	3 49	15.04	38.02	67588	398	40
30	4 23 31.05	31.39	42163	462	30	30		36.92	38.22	67985	397 397	80
40 50	4 22 59.54 4 22 27.91	31.63	42625 43086	461	20 10	40 50	3 47	58.70 20.38	38.32	68382 68777	395	20
		31.75		460					38.43		394	
123°	4 21 56.16 4 21 24.29	31.87	43546	459	237° 50'	133°	3 46	41.95 3.42	38.53	69171	393	227° 50′
10'	4 21 24.29 4 20 52.29	32.00	44463	458	40	20		24.79	38.63	69955	391	40
30	4 20 20.18	32.11	44919	456	30	30		46.06	38.73	70345	390	30
40	4 19 47.94	32.24	45375	456	20	40	3 44	7.23	38.83	70734	389	20
50	4 19 15.59	32.35	45829	454	10	50	3 43	28.30	38.93	71122	388	10
124°	4 18 43,12	32.47	46282		236°	134°	3 42	49.27		71509		226°
10'	4 18 10.53	32.59	46735	453	50'	10'	3 42	10.14	39.13	71895	386	50'
20	4 17 37.83	32.70	47186	451	40	20	3 41	30.91	39.23	72279	384	40
30	4 17 5.01	32.94	47636	450	30 20	30		51.58	39.43	72662	382	30 20
40 50	4 16 32.07 4 15 59.01	33.06	48086 48534	448	10	40 50		12.15 32.62	39-53	73044	381	10
	1990 C. C.	33.17		447		S. Galler			39.62		380	
125°	4 15 25.84 4 14 52.55	33.29	48981 49428	447	235° 50°	135°		53.00 13.28	39.72	73805	379	225° 50′
- 20	4 14 19.14	33.41	49873	445	40	20		33.46	39.82	74561	377	40
30	4 13 45.62	33.52	50317	444	30	30		53.54	39.92	74937	376	30
40	4 13 11.98	33.64	50761	444	20	40		13.52	40.02	75312	375	20
50	4 12 38.22	33.76 33.87	51204	443	10	50	3 35	33.41	40.20	75686	374	10
126°	4 12 4.35		51645		234°	136°	3 34	53.21	40.31	76059		224°
10'	4 11 30.37	33.98	52085	440	50'	10'		12.90	40.40	76430	37I 370	50'
20	4 10 56.27	34.21	52524	439	40	20		32.50	40.49	76800	369	40
30	4 10 22.06 4 9 47.73	34-33	52962 53399	437	30 20	30		52.01 11.42	40.59	77169	368	30
50	4 9 13.29	34-44	53834	435	10	50		30.73	40.69	77903	366	10
1270		34-55	54268	434	233°	137°	3 30	49.95	40.78	78268	365	223°
10'	4 8 38.74	34.67	54702	434	50'	19'	3 30	9.08	40.87	78632	364	50'
20	4 7 29.29	34.78	55134	432	40	20	3 29		40.97	78995	363	40
30	4 6 54.40	34.89	55565	431	30	30	3 28	47.05	41.06	79356	361 360	30
40	4 6 19.40	35.00	55995	430	20	40	3 28	5.90	41.15	79716	359	20
50	4 5 44.29	35.23	56424	428	10	50	3 27	24.66	41.34	80075	358	10
128°	4 5 9.06		56852	427	232°	138°	3 26	43.32	41.43	80433	356	222°
10'	4 4 33.72	35·34 35·45	57279	426	50'	10'	3 26	1.89	41.52	80789	355	50
20 30	4 3 58.27 4 3 22.72	35.55	57705	425	40 30	20 30	3 25 3 24	20.37 38.76	41.61	81144 81498	354	40 30
40	4 3 22.12	35.67	58554	424	20	40		57.05	41.71	81851	353	20
50	4 2 11.27	35.78	58977	423	10	50			41.79	82202	351	10
129°	4 1 35.38	35.89	59399	422	231°	139°	3 22		41.88	82552	350	221°
10'	4 0 59.38	36.00	59820	421	50	10'	3 21		41.97	82901	349	50'
20	4 0 23.27	36.11	60239	419	40	20	3 21	9.35	42.06	83249	348	40
30	3 59 47.05	36.22 36.32	60657	418	30	30	3 20		42.15	83595	346	30
40	3 59 10.73	36.44	61074	417	20	40	3 19		42.24	83940	344	20
50	3 58 34.29	36.54	61489	414	10	50	3 19	2.63	42.41	84284	343	
130°	3 57 57.75		61903		230°	140°	3 18	20.22		84627		220°
	D. P.		1.29		9			152	EL.	1.29		$\mid g \mid$

						TAB	LE VI	l.—Còn	ıtinu	ed.				
1	g		E		Log	. r		g		E		Log	. r	
1		0	1 11	"	1.29		4		0	" '	"	1.30		
1	40°	3 18		42.50	84627	341	220°	150°		33 26.93	AM TA	02798	262	210°
	10'	3 17		42.59	84968	340	50'	10'		32 39.79 $31 52.59$	48 00	03060	260	50'
	20 30	3 16		42.68	85308 85647	339	30	30	1 -	$51 \ \ 52.59$	47 07	03320	259	40
	40		29.68	42.77	85985	338	20	40	1	30 17.98	47 24	03837	258	30 20
-	50		46.83	42.85	86321	336	10	50		29 30.58	47.40	04093	256	10
				42.94	-	335					47.47		255	
	41°	3 14		43.02	86656	334	219° 50′	151° 10′		28 43.11		04348	254	209°
	10' 20	3 12		43.11	86990 87322	332	40	20		$\frac{27}{7}, \frac{55.58}{7.98}$	AM 60	04602	252	50'
	30		54.56	43.20	87653	331	30	30		26 20.32	47 55	04854	251	40 30
	40		11.28	43.28	87983	330	20	40	1	25 32.59	17 77	05355	250	20
	50	3 10		43.36	88312	329	10	50		4 44.80	47.79	05604	249	10
Ι,	42°			43.45		327					47.85		247	
	10'	3 9 3	44.47	43.53	88639 88965	326	218° 50′	152° 10′		3 56.95 3 9.04	47.91	05851	245	208°
	20	3 8		43.62	89290	325	40	20		$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	47.98	06096	244	50'
	30	3 7	33.62	43.70	89614	324	30	30		1 33.02	48.04	06583	243	40 30
	40	3 6	49.83	43.79	89936	322	20	40		0 44.92	48.10	06824	241	20
	50	3 6	5.97	43.86	90257	321	10	50		9 56.76	48.16	07064	240	10
1.	400			43.95		320					48.22		238	
	43°   10′	3 5 3 4	22.02 $37.99$	44.03	90577	318	217°	153°		9 8.54	48.28	07302	237	207°
	20	3 3	53.88	44.11	90895	317	50'	10'		8 20.26	48.34	07539	236	50'
	30	3 3	9.69	44.19	91212 91528	316	30	20 30		7 31.92 6 43.51	48.41	07775	234	40
	40	3 2	25.42	44.27	91842	314	20	40		5 55.05	48.46	08009 08242	233	30 20
	50	3 1	41.08	44.34	92155	313	10	50	2 1		48.52	08242	231	10
				44.43	-	311					48.58		230	
	44°	3 0	0000	44.51	92466	410	216°	154°		4 17.95	48.64	08703	228	206°
	10'	3 0	12.14	44.59	92776	310	50'	10'		3 29.31	48.69	08931	227	50'
	20	2 59	27.55	44.66	93085	309	40	20		2 40.62	48.76	09158	226	40
	30 40	2 58 2 57		44.75	93393	307	30	30	2 1		48.81	09384	224	30
	50	2 57	58.14 13.32	44.82	93700	305	20	40	2 1		48.87	09608	223	20
				44.90	94005	304	10	50	2 1	0 14.18	48.92	09831	222	10
	15°	2 56	28.42	44.98	94309	1 61	215°	155°	2	9 25.26		10053	000	205°
	10		43.44	45.05	94612	303	50'	10'	2	8 36.28	48.98	10273	220	50'
	20		58.39	45.13	94913	301	40	20	2	7 47.24	49.04	10492	219	40
	30		13.26	45.21	95213	300	30	30	2	6 58.15	49.09	10709	216	30
	40	2 53	28.05	45.28	95511	298	20	40	2	6 9.01	49.14	10925	214	20
	50	2 52	42.77	45.36	95808	297	10	50	2	5 19.81	49.20	11139	213	10
14	16°	2 51	57.41		96104	4.0	214°	156°	2	4 30.55		11352		204°
1	10'	2 51	11.97	45.44	96398	294	50'	10'	2	3 41.24	49.31	11564	212	50'
	20	2 50	26.46	45.51	96691	293	40	20	2	2 51.88	49.36	11774	210	40
_	30		40.87	45·59 45.66	96983	292	30	30	2	2 2.47	49.41	11983	209	30
	40		55.21	45.73	97273	290	20	40		1 13.00	49.47	12191	208	20
1	50	2 48	9.48	45.73	97562	289 288	10	50		0 23.48	49.52	12397	206	10
	17°	2 47	23.67		97850		213°	157°	1 5		49.57	12602	205	203°
]	10'	2 46	37.79	45.88	98136	286	50'	10'	1 5		49.62	12805	203	50'
	20		51.83	45.96	98421	285	40	20		7 54.61	49.68	13007	202	40
	30	2 45	5.80	46.03	98705	284	30	30	1 5		49.73	13207	200	30
	10		19.70	46.17	98988	283	20	40		6 15.10	49.78	13405	198	20
1	50	2 43	33.53	46.24	99269	281	10	50		5 25.28	49.82	13602	197	10
14	18°	2 42	47.29		99549	9.11	212°	2			49.88	1	196	100
1	10'	2 42	0.98	46.31	99827	278	50'	158° 10′		4 35.40 3 45.47	49.93	13798 13992	194	202° 50′
	20		14.59	46.39	*00104	277	40	20		2 55.50	49.97	14185	193	40
	30	2 40	28.14	46.45	*00380	276	30	30	1 5		50.02	14103	192	30
•	40		41.61	46.53	*00654	274	20	40		1 15.41	50.07	14567	190	20
1	50		55.01	46.66	*00926	272	10	50	1 5		50.12	14756	189	10
14	19°	2 38	8.35			271					50.17		188	
	10'	2 37	21.62	46.73	*01197 *01467	270	211°	159°	1 4		50.21	14944	186	201°
	20		34.81	46.81	*01467	269	50'	10'		8 44.91	50.26	15130	185	50'
	30		47.94	46.87	*02004	268	40	20		7 54.65	50.31	15315	183	40
	10	2 35	1.01	46.93	*02270	266	30	30	1 4		50.36	15498	182	30
	50		14.00	47.01	*02535	265	20 10	40 50		3 13.98	50.40	15680	180	20 10
15	oo°	2 33	26.93	47.07		263					50.44	15860	179	
1	,0	2 00	20.93		*02798		210°	160°	1 4	33.14		16039	45 6	200°
_			100		*1.30		g				All and	1.30		

			,	TABL	E VII	.—Cont	inuec	<i>l</i> .				
9	E		Log.	r		9		E		Log.	r	
	0 1 11	"	1.30				0 1	"	11	1.30		
160°	1 44 33.14	50.40	16039	1 77 77	200°	170°	0 52	57.32	C2 C1	24087	89	190°
10'	1 43 42.65	50.49	16216	177	50'	10'	0 52		52.51	24176	88	50'
20	1 42 52.11	50.58	16392	174	40	20	0 51		52.56	24264	86	40
30	1 42 1.53	50.62	16566	173	30	30	0 50		52.58	24350	84	30
40	1 41 10.91	50.67	16739 16910	171	20 10	40 50	0 49		52.60	24434 24517	83	20
50	1 40 20.24	50.71		170					52.62		82	10
161°	1 39 29.53	50.75	17080	168	199°	171°	0 47		52.64	24599	80	189°
10'	1 38 38.78	50.80	17248	167	50'	10'	0 46		52.66	24679	79	50'
20	1 37 47.98	50.84	17415	166	40	20	0 45		52.69	24758	77	40
30	1 36 57.14 1 36 6.25	50.89	17581 17745	164	30	30		11.23	52.70	24835	75	30
40 50	1 35 15.33	50.92	17908	163	10	50		18.51	52.72	24984	74	10
		50.96		162					52.74		73	
162°	1 34 24.37	51.00	18070	160	198°	172°	0 45		52.76	25057	71	188°
10'	1 33 33.37	51.04	18230	158	50'	10'		33.01	52.77	25128	70	50'
20	1 32 42.33	51.09	18388	157	40 30	20 30		40.24	52.79	25198 25267	69	40 30
30	1 31 51.24	51.12	18545 18700	155	20	40		54.64	52.81	25334	67	20
40 50	1 30 8.96	51.16	18854	154	10	50	0 38		52.82	25399	65	10
		51.20		153					52.84	1	64	
163°	1 29 17.76	51.24	19007	151	197°	173°	0 37		52.86	25463	62	187°
10'	1 28 26.52	51.27	19158	150	50'	10'	0 30		52.87	25525 25586	61	50'
20	1 27 35.25	51.32	19308	148	40	20	0 35	30.36	52.89	25645	59	30
30	1 26 43.93 1 25 52.58	51.35	19456	147	30	30 40		37.45	52.91	25703	58	20
40 50	1 25 32.35	51.39	19749	146	10	50		44.53	52.92	25759	56	10
		51.42		144	100				52.93	10000	55	
164°	1 24 9.77	51.46	19893	142	196°	174°		51.60	52.94	25814	53	186°
10'	1 23 18.31	51.50	20035	141	50'	10'		58.66	52.96	25867	52	50'
20	1 22 26.81	51.53	20176	140	40	20	0 30		52.97	25919	50	40
30	1 21 35.28	51.57	20316	138	30	30		12.73	52.98	25969	48	30
40	1 20 43.71	51.60	20454 20590	136	20	40 50		3 19.75 26.76	52.99	26017	47	20
50	1 19 52.11	51.64	20590	135	10		0 2		53.00		46	
165°	1 19 0.47	51.67	20725	100	195°	175°	0 20		53.01	26110	44	185°
10'	1 18 8.80	51.70	20858	133	50'	10'	0 23		53.03	26154	43	50'
20	1 17 17.10	51.74	20990	131	40	20		47.72	53.04	26197	42	40
30	1 16 25.36	51.77	21121	129	30	30	0 23		53.04	26239	40	30 20
40	1 15 33.59	51.80	21250	127	20	40	0 23		53.06	26318	39	10
50	1 14 41.79	51.83	21377	126	10	50			53.07		37	
166°	1 13 49.96	51.86	21503	125	194°	178°		15.51	53.08	26355	35	184
10'	1 12 58.10	51.90	21628	123	50'	10'		22.43	53.08	26390	34	50'
20	1 12 6.20	51.93	21751	122	40	20		29.35	53.10	26424	32	40
30	1 11 14.27	51.96	21873	120	30	30		36.25 43.15	53.10	26456 26486	30	30 20
40	1 10 22.31	51.98	21993	119	20	40		50.03	53.12	26515	29	10
50	1 9 30.33	52.02	22112	118	10	50			53.12	La Charles	28	
167°	1 8 38.31	52.04	22230	116	193°	177°		56.91	53.13	26543	26	183°
10'	1 7 46.27	52.08	22346	114	50'	10'	0 1		53.13	26569	25	50'
20	1 6 54.19	52.11	22460	113	40	20		10.65	53.14	26594	23	30
30	1 6 2.08	52.14	22573	111	30	30		3 17.51 2 24.36	53.15	26639	22	20
40	1 5 9.94 1 4 17.78	52.16	22684 22793	109	10	40 50		31.21	53.15	26659	20	10
50		52.19	8/4	108		N. Carrie			53.15	1000000	19	234
163°	1 3 25.59	52.22	22901	107	192°	178°		38.06	53.16	26678	17	182
10'	1 2 33.37	52.24	23008	107	50'	10'		3 44.90 3 51.74	53.16	26695 26711	16	50'
20	1 1 41.13	52.27	23113	104	40	20		3 51.74 7 58.58	53.16	26711	15	30
30	1 0 48.86	52.29	23217 23320	103	30	30 40		5.41	53.17	26739	13	20
40	0 59 56.57	52.32	23320	101	10	50		6 12.24	53.17	26750	II	10
50		52.35		100					53.17		10	1
169°	0 58 11.90		23521	98	191°	179°		5 19.07	53.18	26760	8	181
10'	0 57 19.53	52.37	23619		50'	10'		4 25.89	53.17	26768	7	50'
20	0 56 27.13	52.40	23716	97 95	40	20		32.72	53.18	26775	5	40
30	0 55 34.71	52.44	23811	93	30	30		2 39.54	53.18	26780	4	30
40	0 54 42.27	52.46	23904	92	20	40	1 -	1 46.36 0 53.18	53.18	26784 26786	2	10
50	0 53 49.81	52.49	23996	91	10	50			53.18		I	
170°	0 52 57.32		24087		190°	180°	0	0.00		26787		180
	The state of the s		1.30		g		1			1.30		9

			TA	ABLE VI	II, Arg.	1.—Асті	ON OF JUP	TER.		
A	rg.	(v.c.0)	Diff.	(v.s.1)	(v.c.1)	(v.s.2)	(v.c.2)	(ρ.c.0)	(ρ.8.1)	(p.c.1)
	0	55.03 55.58	" + 0.55	0.14 0.13	4.42 4.42	0.10 0.10	0.11 0.12	2331 2331	164 166	134 134
	2 3	56.13 56.68	0.55	0.12	4.41	0.10 0.10	0.12 0.12	2330 2330	167 169	134 134
133	4	57.23	0.55	0.11	4.41	0.10	0.12	2330	171	135
	5 6	00.04	0.54	0.10 0.09	4.40 4.40	0.10 0.11	0.13 0.13	2329 2328	172 174	135 135
	7 8	58.87 59.42	0.55	0.09 0.08	4.39 4.39	0.11 0.11	0.13 0.13	2328 2327	176 177	135 135
1	9	59.97	0.55	0.08	4.38	0.11	0.14	2326	179	136
1	1	01.00	0.55	0.08	4.38	0.11	0.14	2324 2323	180 182	136 136
1:	3	61.60 62.15	0.55	$0.07 \\ 0.07$	4.37 4.36	0.11 0.11	0.15 0.15	2321 2320	184 185	137 137
14		62.69 63.23	0.54	0.08	4.36 4.35	0.11	0.15 0.15	2318 2316	187 188	137 137
10	6	63.78 + 64.32	0.55	0.08	4.35	0.11	0.16 0.16	2314 2312	190	137
18	3	64.86 65.40	0.54	0.09	4.34	0.11 0.11 0.11	0.16	2310	191 193	138 138
20	0	65.03	0.53	0.11	4.33	0.11	0.17 0.17	2308 2305	194 196	138 138
21 22		66.47 + 67.00	0.53	$0.12 \\ 0.13$	4.32 4.32	0.11 0.11	0.17 0.17	2303 2300	198 199	139 139
23		67.54 68.07	0.54	0.14 0.15	4.31 4.30	0.11 0.11	0.18 0.18	2297 2294	200 202	139 140
25 26		68.60 69.14 +	0.53	0.16	4.30	0.10	0.18	2291	203	140
27		69.66	0.52	0.18 0.20	4.29	0.10 0.10	0.19	2288 2284	205 206	140 140
28 29		70.19 $70.72$	0.53	$\begin{array}{c} 0.21 \\ 0.23 \end{array}$	4.28 4.28	0.10 0.10	$0.19 \\ 0.20$	2281 2277	208 209	140 141
30 31			0.52	$0.25 \\ 0.27$	4.27	0.10 0.10	0.20 0.20	2274 2270	210 212	141 141
32 33		72.28	0.52	0.29 0.31	4.26	0.10	0.21	2266 2262	213 214	141 142
34		73.32	0.52	0.33	4.25	0.10	0.21	2258	214	142
35 36		$\frac{73.83}{74.34} +$	0.51	0.35 0.38	4.25 4.24	0.10 0.10	0.22	2254 2249	217 218	142 142
37 38		74.85 75.36	0.51	0.40 0.43	4.24 4.23	0.10	0.22 0.23	2245 2240	219 221	143 143
39 40			0.50	0.46	4.23	0.09	0.23	2236	222	143
41 42		76.87 +	0.50	0.49	4.22	0.09	0.23 0.23	2231 2226	223 224	143 144
43		77.87	0.50	0.55	4.22	0.09	0.24 0.24	2221 2216	225 227	144 144
44		78.86	0.49	0.61	4.21	0.09	0.24	2210 2205	228	144 144
46 47			0.49	0.68	4.20	0.09	0.25 0.25 0.25	2200	230	145
48		80.32 80.80	0.48	0.75	4.20 4.20 4.20	0.09	0.26	2194 2188	231	145 145
50		81.28	0.48	0.82	4.20	0.09	0.26	2182	233	145 146
51 52		82.23	0.47	0.86 0.90	4.19 4.19	0.08	0.26 0.26	2170 2164	235	146 146
53 54		83.17	0.47	0.94 0.98	4.19 4.19	0.08	0.27 0.27	2158 2151	237 238	146 146
55 56		83.63 84.10 +	0.46	1.02	4.19	0.07	0.27	2145	239	146
57 58		84.55	0.45	1.07	4.19	0.07 0.07	0.28 0.28	2138 2132	240 241	146 146
59		85.46	0.45	1.16 1.20	4.19	0.07	0.28 0.28	2125 2118	242 243	147 147
60		85.91	,5	1.25	4.19	0.07	0.29	2111	244	147

60         85.91         "         "         "         "         "         "         244         61         86.36         +0.45         1.25         4.19         0.07         0.29         2111         244         244         62         86.80         0.44         1.30         4.19         0.07         0.29         2104         244         244         63         87.24         0.44         1.39         4.20         0.06         0.29         2090         246         64         87.68         0.43         1.44         4.20         0.06         0.29         2090         246         64         87.68         0.43         1.44         4.20         0.06         0.29         2090         246         65         88.11         1.49         4.20         0.06         0.30         2057         248         66         88.58         4.42         1.60         4.21         0.06         0.30         2059         249         68         89.38         0.42         1.65         4.21         0.06         0.30         2059         249         68         89.38         0.42         1.65         4.21         0.06         0.30         2059         249         69         29.29         2.01	
60	.c.1)
61 86.36 + 0.45 1.30 4.19 0.07 0.29 2104 244 624 63 86.80 0.44 1.34 4.20 0.06 0.29 2097 245 63 87.24 0.44 1.39 4.20 0.06 0.29 2090 246 64 87.68 0.43 1.44 4.20 0.06 0.29 2082 247 65 88.11 + 0.42 1.54 4.21 0.06 0.30 2075 248 66 88.53 + 0.42 1.54 4.21 0.06 0.30 2075 248 67 88.96 0.43 1.60 4.21 0.06 0.30 2067 248 68 89.38 0.42 1.65 4.21 0.05 0.30 2059 249 68 89.80 0.42 1.70 4.22 0.05 0.31 2044 250 0.41 1.81 4.23 0.05 0.31 2044 250 0.41 1.81 4.23 0.05 0.31 2044 250 0.41 1.81 4.23 0.05 0.31 2028 252 73 91.03 0.41 1.86 4.23 0.05 0.31 2028 252 73 91.03 0.40 1.92 4.24 0.05 0.31 2012 253 74 91.83 0.40 1.92 4.24 0.05 0.31 2012 253 74 91.83 0.40 1.92 4.24 0.05 0.31 2012 253 75 93.22 + 0.45 2.09 4.24 0.04 0.32 2003 253 75 93.38 0.38 2.21 4.27 0.04 0.32 1995 254 77 93.00 0.33 2.15 4.26 0.04 0.32 1996 255 77 93.36 0.38 2.21 4.27 0.04 0.32 1996 255 0.38 99.37 6 0.38 2.21 4.27 0.04 0.32 1996 255 0.38 99.37 6 0.38 2.27 4.28 0.04 0.32 1960 256 88 94.14 2.30 0.30 0.30 0.33 1948 257 94.87 0.36 2.45 4.31 0.03 0.33 1948 257 94.87 0.36 2.45 4.31 0.03 0.33 1948 257 94.87 0.36 2.45 4.31 0.03 0.33 1948 257 94.87 0.36 2.45 4.31 0.03 0.33 1948 257 94.87 0.36 2.51 4.32 0.03 0.33 1948 257 95.95 0.36 2.51 4.32 0.03 0.33 1948 257 95.95 0.36 2.51 4.32 0.03 0.33 1948 257 95.95 0.36 2.57 4.33 0.03 0.33 1945 258 95.95 0.36 2.57 4.33 0.03 0.33 1945 257 95.57 95.95 0.36 2.57 4.33 0.03 0.33 1945 257 95.57 95.95 0.36 2.57 4.33 0.03 0.33 1945 257 95.95 0.36 2.57 4.33 0.03 0.33 1945 257 95.95 0.36 2.57 4.33 0.03 0.33 1945 258 95.95 0.36 2.57 4.33 0.03 0.33 1945 257 95.95 0.36 2.57 4.35 0.03 0.33 1859 259 97.32 0.34 2.89 4.38 0.02 0.33 1869 259 97.32 0.34 2.89 4.38 0.02 0.33 1869 259 97.32 0.34 2.89 4.38 0.02 0.33 1869 259 97.32 0.34 2.89 4.38 0.02 0.33 1869 259 97.32 0.34 2.89 4.39 0.02 0.33 1869 259 97.32 0.33 2.99 4.42 0.02 0.33 1850 260 99.97 97.65 99.97 97.65 99.97 97.65 99.97 9	
61 86.36 +0.445	147
62 86.80 0.44 1.34 4.20 0.06 0.29 2097 245 63 87.24 0.44 1.39 4.20 0.06 0.29 2090 246 64 87.68 0.44 1.44 4.20 0.06 0.29 2090 246 66 87.68 0.43 1.44 4.20 0.06 0.29 2082 247 665 88.11 0.42 1.44 4.20 0.06 0.30 2075 248 66 88.53 0.42 1.54 4.21 0.06 0.30 2067 248 67 88.96 0.43 1.60 4.21 0.06 0.30 2059 249 68 89.38 0.42 1.54 4.21 0.05 0.30 2059 249 68 89.38 0.42 1.70 4.22 0.05 0.31 2044 250 0.41 1.70 4.22 0.05 0.31 2044 250 0.41 1.70 4.22 0.05 0.31 2044 250 0.41 1.81 4.23 0.05 0.31 2028 252 72 91.03 0.41 1.81 4.23 0.05 0.31 2028 252 73 91.43 0.40 1.92 4.24 0.05 0.31 2020 252 73 91.83 0.40 1.92 4.24 0.05 0.31 2020 253 74 91.83 0.40 1.92 4.24 0.05 0.31 2012 253 0.39 1.93 4.24 0.04 0.32 2003 253 0.39 0.33 2.15 4.26 0.04 0.32 1995 254 76 92.62 0.42 2.09 4.26 0.04 0.32 1995 254 76 92.62 0.42 2.09 4.26 0.04 0.32 1995 255 79 93.76 0.38 2.27 4.28 0.04 0.32 1995 255 79 93.76 0.38 2.27 4.28 0.04 0.32 1960 255 88 80 94.14 81 94.51 0.37 2.39 4.30 0.03 0.33 1916 258 80 94.14 0.37 2.39 4.30 0.03 0.33 1925 257 82 94.87 0.36 2.45 4.31 0.03 0.33 1925 257 82 94.87 0.36 2.45 4.31 0.03 0.33 1925 257 82 94.87 0.36 2.45 4.31 0.03 0.33 1925 257 82 94.87 0.36 2.51 4.32 0.03 0.33 1925 257 84 95.59 0.36 2.51 4.32 0.03 0.33 1925 257 88 95.23 0.36 2.51 4.32 0.03 0.33 1925 257 88 95.23 0.36 2.51 4.32 0.03 0.33 1925 257 88 96.30 0.34 2.83 4.37 0.03 0.33 1916 258 88 96.93 0.34 2.83 4.37 0.03 0.33 1888 259 97.32 0.32 0.33 2.96 4.39 0.02 0.33 1889 259 259 99 97.65 0.32 2.96 4.39 0.02 0.33 1869 259 99 97.65 0.32 2.96 4.39 0.02 0.33 1869 259 99 97.65 0.32 2.96 4.39 0.02 0.33 1859 260 99 97.65 0.32 2.96 4.39 0.02 0.33 1859 260 99 97.65 0.32 2.96 4.39 0.02 0.33 1840 260	147
63 87.24 0.44 1.39 4.20 0.06 0.29 2090 246 87.68 0.44 1.44 4.20 0.06 0.29 2082 247 65 88.11 - 0.42 1.44 4.20 0.06 0.30 2067 248 66 88.53 + 0.42 1.54 4.21 0.06 0.30 2067 248 667 88.96 0.43 1.60 4.21 0.06 0.30 2059 249 68 89.38 0.42 1.65 4.21 0.05 0.30 2059 249 69 89.80 0.42 1.70 4.22 0.05 0.31 2044 250 71 90.21 1.75 4.22 0.05 0.31 2044 250 71 90.62 + 0.41 1.81 4.23 0.05 0.31 2028 251 71 90.62 + 0.41 1.81 4.23 0.05 0.31 2028 251 72 91.03 0.41 1.86 4.23 0.05 0.31 2020 252 73 91.43 0.40 1.92 4.24 0.05 0.31 2020 252 73 91.43 0.40 1.92 4.24 0.05 0.31 2020 253 74 91.83 0.40 1.98 4.24 0.04 0.32 2003 253 75 92.22 + 0.42 2.09 4.26 0.04 0.32 1995 254 76 92.62 + 0.42 2.09 4.26 0.04 0.32 1996 255 79 93.76 0.38 2.21 4.27 0.04 0.32 1996 255 79 93.76 0.38 2.21 4.27 0.04 0.32 1969 255 79 93.76 0.38 2.27 4.28 0.04 0.32 1969 255 81 94.51 + 0.37 2.39 4.30 0.03 0.33 1934 257 82 94.87 0.36 2.51 4.32 0.03 0.33 1934 257 88 94.87 0.36 2.45 4.31 0.03 0.33 1925 256 84 95.59 0.36 2.51 4.32 0.03 0.33 1925 257 84 95.59 0.36 2.51 4.32 0.03 0.33 1925 257 88 99.87 0.36 2.45 4.31 0.03 0.33 1934 257 88 99.87 0.36 2.45 4.31 0.03 0.33 1934 257 88 99.87 0.36 2.45 4.31 0.03 0.33 1925 256 88 99.87 0.36 2.45 4.31 0.03 0.33 1925 257 88 99.87 0.36 2.45 4.31 0.03 0.33 1934 257 88 99.87 0.36 2.45 4.31 0.03 0.33 1934 257 88 99.87 0.36 2.45 4.31 0.03 0.33 1934 257 88 99.87 0.36 2.45 4.31 0.03 0.33 1935 258 88 96.93 0.34 2.89 4.38 0.02 0.33 1888 259 88 96.93 0.34 2.89 4.38 0.02 0.33 1888 259 99.89 0.36 0.34 2.89 4.38 0.02 0.33 1888 259 99.89 0.36 0.34 2.89 4.38 0.02 0.33 1869 259 99 97.65 0.32 0.32 2.96 4.39 0.02 0.33 1859 260 99 97.65 0.32 2.96 4.39 0.02 0.33 1840 260	148
64 87.68 8.44 0.43 1.44 4.20 0.06 0.29 2082 247 65 88.11 1.49 4.20 0.06 0.30 2075 248 66 88.53 +0.42 1.54 4.21 0.06 0.30 2067 248 67 88.96 0.43 1.60 4.21 0.06 0.30 2059 249 68 89.38 0.42 1.65 4.21 0.05 0.30 2052 250 69 89.80 0.42 1.70 4.22 0.05 0.31 2044 250 0.41 1.70 4.22 0.05 0.31 2044 250 0.41 1.70 4.22 0.05 0.31 2028 252 73 91.03 0.41 1.81 4.23 0.05 0.31 2028 252 73 91.03 0.41 1.81 4.23 0.05 0.31 2028 252 73 91.43 0.40 1.92 4.24 0.05 0.31 2020 252 73 91.83 0.40 1.98 4.24 0.04 0.32 2003 253 0.39 0.39 0.39 1.98 4.24 0.04 0.32 2003 253 0.39 0.39 0.39 1.98 4.24 0.04 0.32 1995 254 76 92.62 +0.42 2.09 4.26 0.04 0.32 1995 254 77 93.00 0.33 2.15 4.26 0.04 0.32 1978 255 79 93.76 0.38 2.21 4.27 0.04 0.32 1969 255 0.38 2.21 4.27 0.04 0.32 1969 255 0.38 2.21 4.27 0.04 0.32 1969 255 0.38 2.21 4.27 0.04 0.32 1969 255 0.38 2.21 4.27 0.04 0.32 1969 255 0.38 2.21 4.27 0.04 0.32 1969 255 0.38 2.27 4.23 0.04 0.32 1969 255 0.38 2.21 4.27 0.04 0.32 1969 255 0.38 2.21 4.27 0.04 0.32 1969 255 0.38 2.27 4.23 0.04 0.32 1969 255 0.38 2.27 4.23 0.04 0.32 1969 255 0.38 2.27 4.23 0.04 0.32 1969 255 0.38 2.27 4.23 0.04 0.32 1969 255 0.36 2.57 4.33 0.03 0.33 1916 258 85 95.59 0.36 2.57 4.33 0.03 0.33 1934 257 82 94.87 0.36 2.45 4.31 0.03 0.33 1934 257 82 94.87 0.36 2.45 4.31 0.03 0.33 1934 257 88 95.23 0.36 2.51 4.32 0.03 0.33 1936 258 85 95.95 0.36 2.57 4.33 0.03 0.33 1916 258 85 95.95 0.36 2.57 4.33 0.03 0.33 1889 259 88 96.93 0.34 2.83 4.37 0.03 0.33 1888 259 97.32 0.34 2.89 4.38 0.02 0.33 1889 259 97.32 0.34 2.89 4.38 0.02 0.33 1869 259 97.32 0.34 2.89 4.38 0.02 0.33 1859 260 91 97.65 0.32 0.32 3.09 4.42 0.02 0.33 1840 260	148
65 88.11 +0.42	148
66 88.53	148
67	143
68         89.38	148
69         89.80	148
70         90.21         1.75         4.22         0.05         0.31         2036         251           71         90.62 + 0.41         1.81         4.23         0.05         0.31         2028         252           72         91.03         0.40         1.86         4.23         0.05         0.31         2020         252           73         91.43         0.40         1.92         4.24         0.05         0.31         2012         253           74         91.83         0.40         1.92         4.24         0.04         0.32         2003         253           75         92.22         0.03         4.25         0.04         0.32         1995         254           76         92.62         0.42         2.09         4.26         0.04         0.32         1996         254           77         93.00         0.33         2.15         4.26         0.04         0.32         1978         255           78         93.38         0.38         2.21         4.27         0.04         0.32         1969         255           79         93.76         0.38         2.27         4.28         0.04         0.32	148
71	149
72         91.03         0.44         1.86         4.23         0.05         0.31         2020         252           73         91.43         0.40         1.92         4.24         0.05         0.31         2012         253           74         91.83         0.40         1.98         4.24         0.04         0.32         2003         253           75         92.22         0.23         4.25         0.04         0.32         1995         254           76         92.62         0.42         2.09         4.26         0.04         0.32         1986         254           77         93.00         0.33         2.15         4.26         0.04         0.32         1969         255           78         93.38         0.38         2.21         4.27         0.04         0.32         1969         255           79         93.76         0.38         2.27         4.28         0.04         0.32         1969         256           80         94.14         0.32         1960         256           81         94.51         0.37         2.39         4.30         0.03         0.32         1943         257	149
73         91.43         0.40         1.92         4.24         0.05         0.31         2012         253           74         91.83         0.40         1.98         4.24         0.04         0.32         2003         253           75         92.22         2.03         4.25         0.04         0.32         1995         254           76         92.62         2.03         4.26         0.04         0.32         1986         254           77         93.00         0.33         2.15         4.26         0.04         0.32         1986         254           77         93.06         0.38         2.21         4.27         0.04         0.32         1969         255           78         93.76         0.38         2.27         4.28         0.04         0.32         1969         256           80         94.14         2.33         4.29         0.04         0.32         1960         256           81         94.51         0.37         2.39         4.30         0.03         0.32         1943         257           82         94.87         0.36         2.45         4.31         0.03         0.33         1	149
74         91.83         0.45         1.98         4.24         0.04         0.32         2003         253           75         92.22         -0.40         2.09         4.26         0.04         0.32         1995         254           76         92.62         -0.40         2.09         4.26         0.04         0.32         1986         254           77         93.00         0.33         2.15         4.26         0.04         0.32         1986         254           77         93.03         0.38         2.21         4.27         0.04         0.32         1969         255           78         93.76         0.38         2.27         4.28         0.04         0.32         1969         255           79         93.76         0.38         2.27         4.28         0.04         0.32         1960         256           80         94.14         2.33         4.29         0.04         0.32         1952         256           81         94.51+0.37         2.39         4.30         0.03         0.33         1934         257           82         94.87         0.36         2.45         4.31         0.03	149
75         92.22         92.62         92.55         92.52         92.52         92	149
76         92.62 + 0.45         2.09         4.26         0.04         0.32         1986         254           77         93.00         0.33         2.15         4.26         0.04         0.32         1978         255           73         93.38         0.38         2.21         4.27         0.04         0.32         1969         255           79         93.76         0.38         2.27         4.28         0.04         0.32         1969         256           80         94.14         2.33         4.29         0.04         0.32         1952         256           81         94.51 + 0.37         2.39         4.30         0.03         0.32         1943         257           82         94.87         0.36         2.45         4.31         0.03         0.33         1934         257           83         95.23         0.36         2.51         4.32         0.03         0.33         1945         258           84         95.59         0.36         2.57         4.33         0.03         0.33         1916         258           85         95.95         0.36         2.57         4.35         0.03         0.33	149
77         93.00         0.38         2.15         4.26         0.04         0.32         1978         255           78         93.38         0.38         2.21         4.27         0.04         0.32         1969         255           79         93.76         0.38         2.27         4.28         0.04         0.32         1960         256           80         94.14         0.38         2.27         4.28         0.04         0.32         1952         256           81         94.51         0.36         2.45         4.31         0.03         0.32         1943         257           82         94.87         0.36         2.45         4.31         0.03         0.33         1934         257           83         95.23         0.36         2.51         4.32         0.03         0.33         1934         257           84         95.59         0.36         2.57         4.33         0.03         0.33         1916         258           85         95.95         0.36         2.57         4.35         0.03         0.33         1897         258           86         96.30         0.34         2.76         4	149
78         93.38         0.38         2.21         4.27         0.04         0.32         1969         255           79         93.76         0.38         2.27         4.28         0.04         0.32         1960         256           80         94.14         2.33         4.29         0.04         0.32         1952         256           81         94.51         0.36         2.39         4.30         0.03         0.32         1943         257           82         94.87         0.36         2.45         4.31         0.03         0.33         1934         257           83         95.23         0.36         2.51         4.32         0.03         0.33         1925         257           84         95.59         0.36         2.57         4.33         0.03         0.33         1916         258           85         95.95         2.64         4.34         0.03         0.33         1906         258           86         96.30         +0.35         2.70         4.35         0.03         0.33         1897         258           87         93.64         0.34         2.76         4.36         0.03	149
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	149
80 94.14 0.37 2.33 4.29 0.04 0.32 1952 256 81 94.51 0.36 2.35 4.30 0.03 0.32 1943 257 82 94.87 0.36 2.45 4.31 0.03 0.33 1934 257 83 95.23 0.36 2.51 4.32 0.03 0.33 1925 257 84 95.59 0.36 2.57 4.33 0.03 0.33 1916 258 85 95.95 0.36 2.57 4.34 0.03 0.33 1916 258 86 96.30 0.35 2.70 4.35 0.03 0.33 1897 258 87 93.64 0.34 2.76 4.36 0.03 0.33 1888 259 88 96.98 0.34 2.83 4.37 0.03 0.83 1878 259 89 97.32 0.34 2.89 4.38 0.02 0.33 1869 259 90 97.65 0.32 2.96 4.39 0.02 0.33 1859 260 91 97.97 0.32 3.02 4.41 0.02 0.33 1850 260 92 93.29 0.32 3.09 4.42 0.02 0.33 1840 260	149
81       94.51 + 0.37	149
82         94.87         0.36         2.45         4.31         0.03         0.33         1934         257           83         95.23         0.36         2.51         4.32         0.03         0.33         1925         257           84         95.59         0.36         2.57         4.33         0.03         0.33         1916         258           85         95.95         0.36         2.64         4.34         0.03         0.33         1906         258           86         96.30         0.34         2.76         4.35         0.03         0.33         1897         258           87         93.64         0.34         2.76         4.36         0.03         0.33         1888         259           88         96.93         0.34         2.83         4.37         0.03         0.83         1878         259           89         97.32         0.34         2.89         4.38         0.02         0.33         1869         259           90         97.65         0.32         3.02         4.41         0.02         0.33         1850         260           91         97.97         0.32         3.09         4	149
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	149
85	149
85         95.95         2.64         4.34         0.03         0.33         1906         258           86         96.30 + 0.35         2.70         4.35         0.03         0.33         1897         258           87         93.64  0.34         2.76         4.36         0.03         0.33         1888         259           88         96.98  0.34         2.83         4.37         0.03         0.83         1878         259           89         97.32  0.34         2.89         4.38         0.02         0.33         1869         259           90         97.65  0.32         2.96         4.39         0.02         0.33         1859         260           91         97.97  0.32         3.02         4.41         0.02         0.33         1850         260           92         98.29  0.32         3.09         4.42         0.02         0.33         1840         260	149
86         96.30 + 0.35         2.70         4.35         0.03         0.33         1897         258           87         93.64  0.34         2.76         4.36         0.03         0.33         1888         259           88         96.98  0.34         2.83         4.37         0.03         0.83         1878         259           89         97.32  0.34         2.89         4.38         0.02         0.33         1869         259           90         97.65  0.32         2.96         4.39         0.02         0.33         1859         260           91         97.97 + 0.32         3.02         4.41         0.02         0.33         1850         260           92         98.29  0.32         3.09         4.42         0.02         0.33         1840         260	149
87         93.64         0.34         2.76         4.36         0.03         0.33         1888         259           88         96.93         0.34         2.83         4.37         0.03         0.83         1878         259           89         97.32         0.34         2.89         4.38         0.02         0.33         1869         259           90         97.65         0.32         2.96         4.39         0.02         0.33         1859         260           91         97.97         0.32         3.02         4.41         0.02         0.33         1850         260           92         93.29         0.32         3.09         4.42         0.02         0.33         1840         260	149
89     97.32     0.34     2.89     4.38     0.02     0.33     1869     259       90     97.65     2.96     4.39     0.02     0.33     1859     260       91     97.97 + 0.32     3.02     4.41     0.02     0.33     1850     260       92     93.29     0.32     3.09     4.42     0.02     0.33     1840     260	149
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	149
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	149
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	148
92   98.29 0.32   3.09   4.42   0.02   0.33   1840   260	148
02 00 61 0.32 0 15 1 4 49 0 00 0 00 1000 000	148
95   95.01   3.15   4.45   0.02   0.55   1550   200	148
94 98.92 0.31 3.22 4.45 0.02 0.33 1820 260	148
	148
96 99.53 +0.30 3.35 4.48 0.09 0.34 1800 261	148
97   99.83   3.42   4.49   0.02   0.34   1790   261	148
95 100.12 0.20 3.49 4.51 0.01 0.54 1780 261	147
0.29 0.30 1.02 0.01 0.01	147
100 100 70 000 454 001 004 1700 001	147
	147
102   101.25   3.76   4.57   0.01   0.34   1739   261	147
103   101.52   3.83   4.59   0.01   0.34   1729   261	146
0.20	146
	146
100 102.29 025 4.04 4.05 0.01 0.54 1051 201	145
101 102.04 4.11 4.01 0.01 0.04 1000 201	145
108 102.78 24 4.18 4.09 0.01 0.34 1076 201	45
0.23	
110 103.25 4.32 4.73 0.01 0.34 1654 261	44
	44
112 103.10 4.40 4.11 0.01 0.34 1032 201	44
114 104.13 0.21 4.60 4.81 0.01 0.34 1611 260 1	43
0.21	-
	42
116 104.54 +0.20 4.74 4.85 0.01 0.33 1588 260 1 117 104.74 0.20 4.81 4.87 0.01 0.33 1577 260 1	42
111 104.14 4.81 4.81 0.01 0.33 1311 200 1	41
119 105 11 0.18 4.95 4.92 0.01 0.33 1555 259 1	41
0.10	
120         105.29         5.01         4.94         0.02         0.33         1544         259         1	40

		TABLE	VIII, A	.RG. 1.—(	Continued.			
Arg.	(v.c.0) Diff.	(v.s.1)	(v.c.1)	(v.s.2)	(v.c.2)	(p.c.0)	(p.s.1)	(p.c.1)
120 121 122 123 124	105.29 105.46 + 0.17 105.63 0.17 105.79 0.16 105.95 0.16	5.01 5.08 5.15 5.22 5.29	4.94 4.97 4.99 5.01 5.04	" 0.02 0.02 0.02 0.02 0.02 0.02	" 0.33 0.33 0.33 0.33 0.33 0.33	1544 1533 1521 1510 1499	259 259 258 258 258 258	140 140 139 139 138
125 126 127 128 129	106.10 106.25 + 0.15 106.25 + 0.15 106.39 0.14 106.53 0.14 106.65 0.12	5.36 5.43 5.50 5.57 5.64	5.06 5.09 5.11 5.14 5.16	0.02 0.02 0.02 0.02 0.02	0.33 0.33 0.33 0.33 0.33	1487 1476 1464 1453 1441	257 257 257 257 256 256	138 137 137 136 135
130 131 132 133 134	106.78 106.89 + o.11 107.01 o.12 107.11 o.10 107.22 o.11	5.71 5.78 5.85 5.91 5.98	5.19 5.21 5.24 5.26 5.29	0.02 0.03 0.03 0.03 0.03	0.32 0.32 0.32 0.32 0.32	1430 1418 1407 1395 1384	256 255 255 254 254	135 134 134 133 132
135 136 137 138 139	107.31 107.40 +0.09 107.49 0.09 107.57 0.08 107.64 0.07 0.06	6.05 6.11 6.18 6.25 6.31	5.32 5.34 5.37 5.40 5.42	0.03 0.04 0.04 0.04 0.04	0.32 0.32 0.32 0.32 0.32	1372 1360 1349 1337 1325	254 253 253 252 252	132 131 131 130 129
140 141 142 143 144	107.70 107.76 + 0.06 107.82	6.38 6.44 6.51 6.57 6.64	5.45 5.48 5.51 5.53 5.56	0.04 0.05 0.05 0.05 0.05	0.32 0.31 0.31 0.31 0.31	1314 1302 1290 1278 1267	251 251 250 250 249	129 128 127 126 126
145 146 147 148 149	107.95 107.98 +0.03 108.01 0.03 108.03 0.02 108.05 0.02	6.70 6.76 6.83 6.89 6.95	5.59 5.61 5.64 5.67 5.69	0.05 0.06 0.06 0.06 0.06	0.31 0.31 0.31 0.31 0.31	1255 1243 1231 1220 1208	249 248 248 247 247	125 124 123 123 122
150 151 152 153 154	108.05 108.06 + 0.01 108.05 - 0.01 108.04 0.01 108.03 0.02	7.01 7.08 7.14 7.20 7.25	5.72 5.75 5.78 5.80 5.83	0.07 0.07 0.07 0.07 0.08	0.31 0.31 0.31 0.30 0.30	1196 1184 1172 1161 1149	246 246 245 244 244	121 120 119 118 118
155 156 157 158 159	108.01 107.98 — 0.03 107.95 — 0.04 107.91 — 0.04 107.87 — 0.04 0.05	7.31 7.37 7.43 7.49 7.54	5.86 5.88 5.91 5.94 5.97	0.08 0.08 0.09 0.09 0.09	0.30 0.30 0.30 0.30 0.30	1137 1126 1114 1102 1090	243 243 242 241 241	117 116 115 114 113
160 161 162 163 164	107.82 107.77	7.60 7.66 7.71 7.77 7.82	5.99 6.02 6.04 6.07 6.10	0.10 0.10 0.10 0.11 0.11	0.30 0.30 0.30 0.30 0.29	1079 1067 1055 1044 1032	240 240 239 238 238	112 112 111 110 109
165 166 167 168 169	107.49 107.40 — 0.09 107.31 0.09 107.22 0.09 107.11 0.10	7.87 7.93 7.98 8.03 8.08	6.12 6.15 6.17 6.20 6.22	0.11 0.12 0.12 0.12 0.13	0.29 0.29 0.29 0.29 0.29	1020 1009 997 986 974	237 236 236 235 234	108 · 107 106 105 104
170 171 172 173 174	107.01 106.89 — 0.12 106.77 0.12 106.65 0.12 106.52 0.13 0.14	8.13 8.18 8.23 8.28 8.33	6.25 6.27 6.29 6.32 6.34	0.13 0.14 0.14 0.14 0.15	0.29 0.29 0.29 0.29 0.29	963 951 940 928 917	234 233 232 232 231	103 102 101 100 99
175 -176 177 178 179	106.3814 106.24 - 0.14 106.10	8.37 8.42 8.46 8.51 8.55	6.36 6.39 6.41 6.43 6.45	0.15 0.15 0.16 0.16 0.17	0.29 0.29 0.29 0.29 0.29	906 894 883 872 861	230 230 229 228 228	98 97 96 95 94
180	105.62	8.60	6.47	0.17	0.29	850	227	93

		TABLE	VIII, A	RG. 1.—C	ontinued.			
Arg.	(v.c.0) Diff	(v.s.1)	(v.c.1)	(v.s.2)	(v.c.2)	(p.c.0)	(p.s.1)	(p.c.1)
	" "	"	"	"	"			
180	105.62	8.60	6.47	0.17	0.29	850	227	93
181	105.45 -0.17	8.64	6.50	0.17	0.29	839	226	92
182	105 97 0.18	8.68	6.52	0.18	0.29	828	226	91
183	105 09 0.18	8.72	6.54	0.18	0.29	816	225	90
184	104 90 0.19	8.76	6.56	0.19	0.29	805	224	89
	0.19					The state of the s		
185	104.710.20	8.80	6.57	0.19	0.29	794	224	88
186	104.51 0.20	8.84	6.59	0.19	0.29	784	223	87
187	104.31 0.21	8.88	6.61	0.20	0.29	773	222	86
188	104.10	8.92	6.63	0.20	0.29	762	222	85
189	103.89 0.22	8.96	6.65	0.21	0.29	751	221	84
190	103.67	8.99	6.67	0.21	0.29	740	221	83
191	103.44 -0.23	9.03	6.68	0.21	0.29	730	220	82
192	103.21 0.23	9.07	6.70	0.22	0.29	719	219	81
193	109 98 0.23	9.10	6.71	0.22	0.29	708	219	80
194	100 74 0.24	9.13	6.73	0.22	0.29	698	218	79
	100 10							
195	102.490.25	9.17 9.20	6.74	0.23 0.23	0.29	688 677	217 216	78 77
196	102.24 0.26	9.20	6.76	0.23	0.29	667	216	
197	101.98 0.26 101.72 0.26	9.23	6.77 6.78	0.24	0.29	657	215	76 75
198		9.26	6.79	0.24	0.29	646	215	74
199	101.45 0.27	No. of the last				AND THE REAL PROPERTY.		
200	101.18	9.32	6.81	0.25	0.29	636	214	73
201	100.90	9.35	6.82	0.25	0.29	626	213	72
202	100.62 0.28	9.38	6.83	0.25	0.29	616	213	71
203	100.33 0.29	9.41	6.84	0.26	0.29	606	212	70
204	100.04 0.29	9.43	6.85	0.26	0.29	596	211	69
205	00 71	9.46	6.86	0.26	0.29	586	211	68
206	99.44 -0.30	9.48	6.86	0.27	0.29	577	210	67
207	99.13 0.31	9.51	6.87	0.27	0.29	567	210	66
208	98.82 0.31	9.53	6.88	0.27	0.29	557	209	65
208	98 50 0.32	9.55	6.88	0.28	0.29	548	208	64
	0.32					THE PARTY OF THE P		
210	98.18	9.58	6.89	0.28	0.29	538	208	63
211	01.00	9.60	6.89	0.28	0.29	529	207	62
212	01.04	9.62	6.90	0.29	0.29	520	206	61
213	01.10	9.64	6.90	0.29	0.29	510	206	60
214	96.84 0.35	9.66	6.90	0.29	0.29	501	205	59
215	00 10	9.68	6.91	0.30	0.29	492	205	58
216	96 14 -0.35	9.70	6.91	0.30	0.29	483	204	57
217	95 79 0.35	9.71	6.91	0.30	0.29	474	204	56
218	95 43 0.30	9.73	6.91	0.31	0.29	464	203	55
219	95 06 0.37	9.75	6.91	0.31	0.30	456	202	54
	0.37					448	202	53
220	94.69	9.76	6.91	0.31 0.31	0.30	439	202	52
221	94.02 0 28	9.78			0.30	439	201	51
222	93.94 0.28	9.79 9.81	6.90	0.32	0.30	422	200	50
223	90.00 0.20		6.90	0.32	0.30	413	200	49
224	95.11 0.39	9.82			The second	01 3000		
.225	92.78 20	9.83	6.89	0.33	0.30	405	199	48
226	92 39 -0.39	9.85	6.88	0.33	0.30	398	198	47
227	91.99 0.40	9.86	6.88	0.33	0.30	390	198	46
228	91.59 0.41	9.87	6.87	0.33	0.30	382	197	46
229	91.18 0.41	9.88	6.86	0.34	0.30	374	197	45
230	90 77	9.89	6.85	0.34	0.30	365	196	44
231	90.36 -0.41	9.90	6.84	0.34	0.30	357	196	43
232	89.94 0.42	9.91	6.83	0.34	0.30	349	195	42
233	89.51 0.43	9.91	6.82	0.34	0.30	342	194	41
234	89.09 0.42	9.92	6.81	0.35	0.30	334	194	41
	. 0.44	The second second						
235	88.65	9.93	6.80	0.35	0.30	327	194	40
236	88.22 -0.43	9.94	6.79	0.35	0.30	320	193	39
237	01.10	9.94	6.78	0.35	0.30	312	192	88
238	01.04	9.95	6.76	0.35	0.30	305	192	38
239	86.89 0.45	9.95	6.74	0.36	0.30	298 -		37
240	86.44	9.96	6.73	0.36	0.31	291	191	36
240	00.44	0.00	0.10	0.00	0.51			

Г			TABLE	VIII, A	RG. 1.—C	ontinued.			
	Arg.	(v.c.0) Diff.	(v.s.1)	(v.c.1)	(v.s.2)	(v.c.2)	(ρ.c.0)	(ρ. ε.1)	(p.c.1)
	240 241 242 243 244	86.44 85.99—0.45 85.53 0.46 85.08 0.45 84.61 0.47	9.96 9.96 9.96 9.97 9.97	6.73 6.71 6.69 6.67 6.66	" 0.36 0.36 0.36 0.36 0.36 0.37	0.31 0.31 0.31 0.31 0.31	291 284 278 271 265	191 190 190 189 189	36 35 35 34 33
	245 246 247 248 249	84.15 83.68 -0.47 83.21 0.47 82.73 0.48	9.97 9.97 9.98 9.98 9.98	6.64 6.61 6.59 6.57 6.55	0.37 0.37 0.37 0.37 0.37	0.31 0.31 0.31 0.31 0.31	258 252 246 240 234	188 188 187 187 186	33 32 31 31 30
	250 251 252 253 254	81.77 81.28—0.49 80.80 0.48 80.30 0.50 79.81 0.49 0.50	9.98 9.98 9.98 9.97 9.97	6.53 6.51 6.48 6.46 6.43	0.37 0.38 0.38 0.38 0.38	0.31 0.31 0.31 0.31 0.31	228 222 216 211 205	186 185 185 184 184	29 29 28 28 27
	255 256 257 258 259	79.31 78.82—0.49 78.31 0.51 77.81 0.50 77.30 0.51	9.97 9.97 9.96 9.96 9.96	6.40 6.37 6.34 6.31 6.28	0.38 0.38 0.38 0.38 0.38	0.31 0.30 0.30 0.30 0.30	200 195 190 184 179	183 183 182 182 181	27 26 26 25 25
	260 261 262 263 264	76.79 76.28—0.51 75.77 0.51 75.25 0.52 74.73 0.52	9.95 9.95 9.95 9.94 9.94	6.25 6.22 6.19 6.16 6.13	0.38 0.38 0.38 0.38	0.30 0.30 0.30 0.30 0.30	175 170 165 161 156	181 180 180 179 179	24 24 24 23 23
	265 266 267 268 269	74.21 73.69—0.52 73.16 0.53 72.64 0.52 72.11 0.53	9.93 9.93 9.92 9.92 9.91	6.10 6.06 6.03 5.99 5.96	0.38 0.38 0.38 0.38 0.38	0.30 0.30 0.30 0.30 0.30	152 148 144 140 137	178 178 177 177 176	22 22 22 21 21
	270 271 272 273 274	71.57 71.04 —0.53 70.51 0.53 69.97 0.54 69.43 0.54	9.90 9.90 9.89 9.88 9.88	5.92 5.88 5.85 5.81 5.77	0.39 0.39 0.39 0.39 0.39	0.30 0.30 0.30 0.30 0.30	133 129 126 122 119	176 175 175 174 174	21 20 20 20 20 20
	275 276 277 278 279	68.89 68.35 — 0.54 67.81 0.54 67.26 0.55 66.72 0.54	9.87 9.86 9.85 9.84 9.84	5.73 5.69 5.65 5.61 5.57	0.39 0.39 0.39 0.39 0.39	0.30 0.29 0.29 0.29 0.29	116 113 110 107 105	174 173 172 172 171	20 19 19 19 19
	280 281 282 283 284	66.17 65.620.55 65.07 0.55 64.52 0.55 63.97 0.55	9.83 9.82 9.81 9.80 9.79	5.52 5.48 5.44 5.40 5.35	0.39 0.39 0.39 0.39 0.39	0.29 0.29 0.29 0.29 0.29	102 .100 .97 .95 .93	171 170 170 169 169	19 19 18 18
	285 286 287 288 289	63.41 62.86 — 0.55 62.31 0.55 61.75 0.56 61.19 0.56	9.78 9.77 9.77 9.76 9.75	5.31 5.26 5.22 5.17 5.13	0.39 0.39 0.39 0.39 0.38	0.28 0.28 0.28 0.28 0.28	91 90 88 86 85	168 168 167 167 166	18 18 18 18 18
	290 291 292 293 294	60.64 60.08 -0.56 59.52 0.56 58.96 0.56 58.40 0.56	9.74 9.73 9.72 9.71 9.70	5.08 5.03 4.99 4.94 4.89	0.38 0.38 0.38 0.38 0.38	0.28 0.27 0.27 0.27 0.27	84 82 81 80 80	166 165 164 164 163	18 19 19 19
	295 296 297 298 299	57.84 57.280.56 56.72 0.56 56.16 0.56 55.60 0.56	9.69 9.68 9.67 9.66 9.65	4.84 4.80 4.75 4.70 4.65	0.38 0.38 0.38 0.38 0.38	0.27 0.27 0.26 0.26 0.26	79 78 78 77 77	163 162 162 161 161	19 19 19 20 20
	300	55.04	9,64	4.60	0.38	0.26	77	160	20

		TABLE	VIII, A	RG. 1.—	Continued.			
Arg.	(v.c.0) Diff.	(v.s.1)	(v.c.1)	(v.s.2)	(v.c.2)	(p.c.0)	(p.8.1)	(p.c.1)
	" "	11	"	"	"			
300	55.04	9.64	4.60	0.38	0.26	77	160	20
301	54.48 -0.56	9.63	4.55	0.38	0.26	77	159	20
302	59 00 0.50	9.62	4.50	0.38	0.25	77	159	20
303	59 98 0.50	9.61	4.45	0.38	0.25	77	158	21
304	50 00 0.50	9.60	4.40	0.38	0.25	78	158	21
	0.50					The same of the same of the	S. Property of	
305	52.240.56	9.59	4.35	0.38	0.25	78	157	21
306	01.08	9.58	4.30	0.38	0.25	79	156	22
307	01.12	9.57	4.25	0.38	0.24	80	156	22
308	50.50 0 56	9.56	4.20	0.38	0.24	81	155	22
309	50.00 0.56	9.55	4.15	0.38	0.24	82	154	23
310	10 11	9.54	4.10	0.38	0.24	83	154	23
311	48.88 -0.56	9.53	4.05	0.38	0.23	84	153	24
	48 99 0.55		4.01		0.23	85	152	- 24
312	20.00	9.52		0.38		00		
313	21.11	9.51	3.94	0.38	0.23	87	152	24
314	47.22 0.55	9.50	3.89	0.38	0.23	88	151	25
315	10 00	9.49	3.84	0.38	0.23	90	150	25
316	46.11 -0.55	9.48	3.79	0.38	0.22	92	150	26
317	45.56 0.55	9.47	3.74	0.38	0.22	94	149	26
318	45.01 0.55	9.46	3.69	0.38	0.22	96	148	27
	20.01	9.45	3.63	0.38	0.22	98	148	27
319	0.55				A STATE OF THE PARTY OF THE PAR	7- 11-		
320	43.91	9.44	3.58	0.38	0.21	100	147	28
321	43.36 -0.55	9.43	3.53	0.38	0.21	103	146	28
322	42.81 0.55	9.42	3.48	0.38	0.21	105	146	29
323	42.27 0.54	9.41	3.43	0.38	0.21	108	145	29
324	41 79 0.55	9.40	3.38	0.38	0.20	111	144	30
	0.54						100	W. 1. W. 1.
325	41.18	9.40	3.33	0.38	0.20	114	144	30
326	40.64 -0.54	9.39	3.28	0.38	0.20	117	143	31
327	40.10 0.54	9.38	3.23	0.38	0.20	120	142	32
328	39.56 0.54	9.37	3.18	0.38	0.19	123	141	32
329	39.03 0.53	9.36	3.14	0.37	0.19	127	140	33
	0.54		The state of the s	The state of the s	0.10	130	140	34
330	38.49	9.35	3.07	0.37	0.19		139	34
331	01.00	9.34	3.02	0.37	0.19	134	139	
332	37.43 0.53	9.33	2.98	0.37	0.18	138	138	35
333	36.90 0.53	9.32	2.93	0.37 •	0.18	141	137	36
334	36.37 0.53	9.31	2.88	0.37	0.18	145	136	36
335	35.85	9.30	2.83	0.37	0.18	150	136	37
		9.29	2.78	0.37	0.17	154	135	38
336	00.00					100000000000000000000000000000000000000		38
337	04.01	9.29	2.73	0.37	0.17	158	134	39
338	04.29	9.28	2.69	0.37	0.17	162	133	40
339	33.78 0.51	9.27	2.64	0.37	0.17	167	132	4 3 7 7
340	33 26	9.26	2.59	0.37	0.17	172	132	41
341	32 75 -0.51	9.25	2.54	0.37	0.16	176	131	42.
342	32 24 0.51	9.24	2.50	0.37	0.16	181	130	42
343	31.74 0.50	9.23	2.45	0.37	0.16	186	129	43
344	31.23 0.51	9.22	2.41	0.37	0.16	191	128	44
/	0.50					The second second	The state of the s	- 12
345	00 40	9.21	2.36	0.37	0.15	197	127	45
346	30.24 -0.49	9.20	2.31	0.37	0.15	202	126	46
347	99 74 0.50	9.20	2.27	0.37	0.15	207	126	46
348	99 95 0.49	9.19	2.23	0.37	0.15	213	125	47
349	98 76 0.49	9.18	2.18	0.37	0.15	218	124	48
	0.49					The state of the s		49
350	28.27	9.17	2.14	0.37	0.14	224	123	
351	27.79 -0.48	9.16	2.09	0.37	0.14	230	122	50
352	27 31 0.40	9.15	2.05	0.37	0.14	236	121	51
353	26.83 0.48	9.14	2.01	0.37	0.14	242	120	51
354	26.36 0.47	9.13	1.97	0.37	0.14	248	119	52
	0.47	No. of the last of				255	118	53
355	25.89	9.12	1.93	0.37	0.14			54
356	25.42 -0.47	9.12	1.89	0.37	0.13	261	117	
357	24.96	9.11	1.85	0.37	0.13	268	116	55
358	24.00 0 16	9.10	1.81	0.37	0.13	274	115	56
359	24.04 0.46	9.09	1.77	0.37	0.13	281	114	57
					and the second second second second	288	113	58

		TABLI	E VIII, A	RG. 1.—	Continued.			
Arg.	(v.c.0) Diff.	(v.s.1)	(v.c.1)	(v.s.2)	(v.c.2)	(p.c.0)	(µ.s.1)	(p.c.1)
360 361 362 363	23.58 23.13 -0.45 22.69 0.44 22.24 0.45 21.80 0.44	9.08 9.07 9.06 9.05	1.73 1.70 1.66 1.62	0.38 0.38 0.38 0.38	0.13 0.13 0.13 0.13	288 294 301 308	113 112 111 110	58 58 59 60
364 365 366 367 368 369	21.37	9.04 9.03 9.02 9.01 9.00 8.99	1.59 1.55 1.52 1.48 1.45 1.42	0.38 0.37 0.37 0.37 0.37 0.37	0.12 0.12 0.12 0.12 0.12 0.12 0.11	316 323 330 338 345 353	109 108 107 106 105 104	61 62 63 64 65 66
370 371 372 373 374	19.24 19.24 18.83 — 0.41 18.42 0.41 18.02 0.40 17.62 0.40 0.40	8.98 8.97 8.96 8.95 8.94	1.39 1.36 1.32 1.29 1.27	0.37 0.37 0.37 0.37 0.37	0.11 0.11 0.11 0.11 0.11	361 369 377 385 393	103 102 101 100 99	66 67 68 69 70
375 376 377 378 379	17.22 16.83 — 0.39 16.44 0.39 16.06 0.38 15.68 0.38	8.93 8.92 8.91 8.89 8.88	1.24 1.21 1.18 1.16 1.13	0.37 0.37 0.37 0.37 0.37	0.11 0.11 0.11 0.11 0.11	401 410 418 426 435	98 97 96 95 94	71 72 73 74 75
380 381 382 383 384	15.30 14.93 0.37 14.57	8.87 8.86 8.85 8.83 8.82	1.11 1.08 1.06 1.04 1.02	0.37 0.37 0.37 0.37 0.37	0.10 0.10 0.10 0.10 0.10	444 452 461 470 479	93 92 91 90 89	76 77 78 78 78
385 386 387 388 389	13.50 13.15 — 0.35 12.80	8.81 8.79 8.78 8.77 8.75	1.00 0.98 0.96 0.94 0.92	0.37 0.37 0.37 0.37 0.37	0.10 0.10 0.10 0.10 0.10	488 497 506 514 525	88 87 86 85 84	80 81 82 83 84
390 391 392 393 394	11.81 11.48 -0.33 11.16 0.32 10.85 0.31 10.54 0.31 0.31	8.74 8.72 8.71 8.70 8.68	0.90 0.88 0.87 0.85 0.84	0.37 0.37 0.37 0.36 0.36	0.10 0.10 0.10 0.10 0.10	534 544 554 564 573	82 81 80 79 78	85 86 86 87 88
395 396 397 398 399	10.23 9.93 —0.30 9.64 0.29 9.35 0.29 9.07 0.28	8.67 8.65 8.63 8.62 8.60	0.83 0.82 0.80 0.79 0.78	0.36 0.36 0.36 0.36 0.36	0.10 0 10 0.10 0.10 0.10	583 593 603 613 623	77 76 75 74 73	89 90 91 92 93
400 401 402 403 404	8.79 8.52 — 0.27 8.25	8.58 8.57 8.55 8.53 8.51	0.77 0.76 0.76 0.75 0.74	0.36 0.36 0.36 0.36 0.35	0.10 0.10 0.10 0.10 0.10	633 643 653 664 674	72 71 70 69 68	93 94 95 96 97
405 406 407 408 409	7.47 7.22 —0.25 6.98 0.24 6.75 0.23 6.51 0.24 0.22	8.49 8.47 8.46 8.44 8.42	0.74 0.74 0.73 0.73 0.73	0.35 0.35 0.35 0.35 0.34	0.10 0.10 0.10 0.10 0.10	. 684 695 706 716 727	67 66 65 64 63	98 98 99 100 101
410 411 412 413 414	6.29 6.07 — 0.22 5.85 0.22 5.64 0.20 5.44 0.20	8.39 8.37 8.35 8.33 8.31	0.73 0.73 0.73 0.73 0.73	0.34 0.34 0.34 0.34 0.34	0.10 0.10 0.10 0.10 0.10	737 748 759 770 781	62 61 60 59 58	101 102 103 104 104
415 416 417 418 419	5.24 5.04 —0.20 4.86 0.18 4.67 0.19 4.50 0.17	8.28 8.26 8.24 8.21 8.19	0.73 0.74 0.74 0.74 0.75	0.34 0.33 0.33 0.33 0.33	0.10 0.10 0.10 0.10 0.10	792 803 814 825 836	57 56 55 54 53	105 106 107 107 108
420	4.33	8.17	0.76	0.33	0.10	847	52	109

		TABLE	VIII, A	RG. 1.—C	ontinued.			
Arg.	(v.c.0) Diff.	(v.s.1)	(v.c.1)	(v.s.2)	(v.c.2)	(p.c.0)	(p.8.1)	(p.c.1)
100000	11 11	"	"	"	"			
420	4.33	8.17	0.76	0.33	0.10	847	52	109
421	4.16 -0.17	8.14	0.76	0.32	0.10	858	51	110
422	4 00 0.10	8.11	0.77	0.32	0.11	870	50	110
423	3 85 0.15	8.09	0.78	0.32	0.11	881	50	111
424	9 70 0.15	8.06	0.79	0.32	0.11	892	49	111
	0.14		M. Commercial			1 . V . V . V . V . V . V . V . V . V .		
425	3.56_0.14	8.04	0.80	0.32	0.11	904	48	112
426	5.42	8.01	0.81	0.31	0.11	916	47	113
427	0.20 0 72	7.98	0.82	0.31	0.11	927	46	113
428	5.10	7.95	0.83	0.31	0.11	938	45	114
429	3.04 0.11	7.92	0.85	0.31	0.11	950	44	114
430	2 93	7.89	0.86	0.31	0.11	961	44	115
431	2.82-0.11	7.86	0.87	0.30	0.11	973	43	116
432	2.72 0.10	7.83	0.89	0.30	0.11	984	42	116
433	2.62 0.10	7.80	0.90	0.30	0.11	996	41	117 .
434	2 53 0.09	7.77	0.92	0.29	0.11	1008	40	118
	0.08							118
435	2.45	7.74	0.94	0.29	0.11	1019	40 39	119
436	2.01	7.71	0.95	0.29	0.12	1031		119
437	2.29	7.67	0.97	0.29	0.12	1043	38	120
438	2.20	7.64	0.99	0.28	0.12	1054	38	120
439	2.16 0.07	7.60	1.01	0.28	0.12	1066	37	
440	0 11	7.57	1.03	0.28	0.12	1078	36	121
441	2.06 -0.05	7.54	1.05	0.28	0.12	1089	35	121
442	2.02 0.04	7.50	1.07	0.27	0.12	1100	35	122
443	1.98 0.04	7.47	1.09	0.27	0.12	1113	34	122
444	1.95 0.03	7.43	1.11	0.27	0.12	1124	33	122
445	0.03	7.39	1.14	0.26	0.12	1137	33	123
	1.92	7.36	1.14	0.26	0.12	1149	32	123
446	1.90 -0.02	7.32	1.18	0.26	0.12	1160	32	124
447	1.88 0.02	7.28	1.21	0.26	0.12	1172	31	124
448	1.81	7.24	1.21	0.25	0.12	1184	30	125
449	1.87							
450	1.87	7.20	1.26	0.25	0.12	1196	30	125
451	1.88 +0.01	7.16	1.28	0.25	0.12	1208	30	125
452	1.90	7.12	1.31	0.24	0.12	1220	29	126
453	1.92 0.02	7.08	1.33	0.24	0.12	1232	28	126
454	1.95 0.03	7.04	1.36	0.24	0.12	1243	28	127
455	1.98	7.00	1.39	0.23	0.12	1255	28	127
456	9 01 +0.03	6.96	1.42	0.23	0.12	1267	27	127
	2 06 0.05	6.91	1.45	0.23	0.12	1279	27	128
457 458	2.11 0.05	6.87	1.47	0.23	0.12	1291	26	128
459	0 10 0.05	6.83	1.50	0.22	0.12	1302	26	128
	0.07						Service Control	128
-460	2.23 +0.06	6.78	1.53	0.22	0.12	1314	26	128
461.	2.23 +0.06	6.74	1.56	0.21	0.12	1326	25	129
462	2.37	6.69	1.59	0.21	0.12	1338	25 25	129
463	2.44 0.00	6.65	1.62	0.21	0.12	1350	25	130
464	2.53 0.09	6.60	1.65	0.20	0.12	1361		1
465		6.56	1.68	0.20	0.12	1373	24	130
466	9 71 +0.09	6.51	1.72	0.20	0.12	1385	24	130
467	0 90	6.46	1.75	0.19	0.13	1396	24	130
468	2 92 0.10	6.41	1.78	0.19	0.13	1408	24	130
469	2 04 0.12	6.37	1.81	0.19	0.13	1420	23	131
	0.11		18 13 13 13	0.18	0.13	1431	23	131
470	3.15	6.32	1.84 1.88	0.18	0.13	1443	23	131
471		6.27			0.13	1455	23	131
472	0.41	6.22	1.91	0.18	0.12	1466	23	131
473	0.00	6.17	1.94	0.17		1478	23	132
474	3.69 0.14	6.12	1.98	0.17	0.12			ALL PROPERTY.
475	9 00	6.07	2.01	0.17	0.12	1489	23	132
476	3.98+0.15	6.02	2.04	0.16	0.12	1501	23	132
477	4.14	5.96	2.07	0.16	0.12	1512	23	132
478	4.31 0.17	5.91	2.11	0.16	0.12	1524	23	132
		5.86	2.14	0.15	0.12	1535	23	132
479		0.00	-	The second second				
	4.48 0.17	5.81	2.18	0.15	0.12	1546	23	132

		TABLE	VIII, A	rg. 1.—C	Continued.			
Arg.	(v.c.0) Diff.	(v.s.1)	(v.c.1)	(v.s.2)	(v.c.2)	(p.c.0)	(p.8.1)	(p.c.1)
480 481 482 483 484	4.65 4.83 + 0.18 5.02 0.19 5.21 0.19 5.40 0.19	5.81 5:75 5.70 5.65 5.59	2.18 2.21 2.24 2.28 2.31	0.15 0.15 0.15 0.14 0.14	0.12 0.12 0.12 0.12 0.12 0.12	1546 1558 1569 1580 1591	23 23 23 23 23 23	132 132 132 132 132 133
485 486 487 488 489	5.61 5.81 +0.20 6.03 0.22 6.24 0.23 6.47 0.23	5.54 5.48 5.43 5.37 5.32	2.35 2.38 2.42 2.45 2.48	0.14 0.13 0.13 0.13 0.12	0.12 0.12 0.12 0.11 0.11	1602 1613 1624 1635 1646	24 24 24 24 25	133 133 133 134 134
490 491 492 493 494	6.70 6.93 + 0.23 7.17 0.24 7.41 0.24 7.66 0.25 0.26	5.26 5.20 5.15 5.09 5.03	2.52 2.55 2.59 2.62 2.66	0.12 0.12 0.12 0.11 0.11	0.11 0.11 0.11 0.11 0.11	1657 1668 1679 1690 1700	25 25 25 25 26	133 133 133 133 133
495 496 497 498 499 500	7.92 8.18+0.26 8.44 0.26 8.71 0.27 8.99 0.28 0.27	4.98 4.92 4.86 4.80 4.75	2.69 2.72 2.76 2.79 2.83	0.11 0.11 0.10 0.10 0.10	0.11 0.11 0.11 0.11	1711 1721 1732 1742 1753	27 27 28 28 28	133 133 133 133 133
500 501 502 503 504	9.26 9.55 +0.29 9.84 0.29 10.13 0.29 10.43 0.30 0.31 10.74	4.69 4.63 4.57 4.51 4.44	2.86 2.89 2.93 2.96 2.99	0.10 0.10 0.09 0.09 0.09	0.11 0.11 0.10 0.10 0.10	1763 1774 1784 1794 1804	29 30 30 31 31	133 133 133 133 133
506 507 508 509	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	4.39 4.33 4.28 4.22 4.16	3.02 3.06 3.09 3.12 3.15	0.09 0.09 0.08 0.08 0.08	0.10 0.10 0.10 0.10 0.10	1814 1824 1834 1844 1853	32 32 33 34 35	133 133 133 133 133
510 511 512 513 514	12.33 12.66 +0.33 13.00 0.34 13.34 0.34 13.68 0.34 0.35	4.10 4.04 3.98 3.92 3.86	3.18 3.21 3.25 3.28 3.31	0.08 0.08 0.07 0.07 0.07	0.09 0.09 0.09 0.09 0.09	1863 1873 1882 1892 1901	35 36 37 38 39	133 133 133 133 133
515 516 517 518 519	14.03 14.39 + 0.36 14.75	3.80 3.74 3.68 3.62 3.56	3.34 3.37 3.40 3.43 3.46	0.07 0.07 0.07 0.07 0.07	0.09 0.09 0.09 0.09 0.08	1910 1920 1929 1938 1947	40 40 41 42 43	133 133 133 133 133
520 521 522 523 524	15.85 16.23 + 0.38 16.61 0.38 16.99 0.38 17.38 0.39 0.39	3.50 3.44 3.38 3.32 3.27	3.49 3.51 3.54 3.57 3.60	0.06 0.06 0.06 0.06 0.06	0.08 0.08 0.08 0.08 0.08	1956 1964 1973 1982 1990	44 45 46 47 48	132 · 132 132 132 132
525 526 527 528 529	17.77 18.17 + 0.40 18.57 0.40 18.97 0.40 19.38 0.41 0.41	3.21 3.15 3.09 3.03 2.97	3.62 3.65 3.67 3.70 3.73	0.06 0.06 0.06 0.06 0.05	0.08 0.08 0.08 0.07 0.07	1999 2007 2016 2024 2032	49 50 51 52 53	132 132 132 132 132
530 531 532 533 534	19.79 20.21 + 0.42 20.62 0.41 21.05 0.43 21.47 0.42 0.43	2.91 2.86 2.80 2.75 2.69	3.75 3.77 3.80 3.82 3.84	0.05 0.05 0.05 0.05 0.05	0.07 0.07 0.07 0.07 0.07	2040 2048 2056 2063 2071	55 56 - 57 58 59	132 132 132 132 131
535 536 537 538 539	21.90 22.34+0.44 22.77 0.43 23.21 0.44 23.66 0.45 0.44	2.63 2.57 2.52 2.46 2.40	3.87 3.89 3.91 3.93 3.96	0.05 0.05 0.05 0.05 0.05	0.07 0.07 0.07 0.07 0.06	2079 2086 2094 2101 2108	61 62 63 64 66	131 131 131 131 131
540	24.10	2.35	3.98	0.05	0.06	2115	67	131

1	100		TABLE	VIII, A	RG. 1.—C	oncluded.	7		
١	Arg.	(v.c.0) Diff.	(v.s.1)	(v.c.1)	(v.s.2)	(v.c.2)	(p.c.0)	(ρ.8.1)	(p.c.1)
ı		" "	"	"	- 11_	"			
ı	540	24.10 94.56+0.46	2.35	3.98	0.05	0.06	2115	67	131
ı	541 542	24.56 +0.46 25.01 0.45	2.29 2.24	4.00	0.05 0.05	0.06	2122 2129	. 68	131
1	543	95 47 0.40	2.18	4.04	0.05	0.06	2135	70 71	131 130
1	544	95 09 0.40	2.13	4.06	0.05	0.06	2142	73	130
1		0.40	2.08	4.07	0.05	0.06	2149	74	No. of Contract of
ı	545 546	26 85 +0.40	2.03	4.07	0.05	0.06	2149	75	130 130
1	547	97 39 0.47	1.97	4.11	0.05	0.06	2162	77	130
1	548	97 79 0.47	1.92	4.13	0.05	0.06	2168	78	130
ı	549	28.27 0.48	1.87	4.14	0.05	0.06	2174	80	130
ı	550	00 45	1.82	4.16	0.05	0.06	2180	81	130
1	551	29 23 +0.48	1.77	4.17	0.05	0.06	2186	83	130
1	552	29.71 0.40	1.72	4.19	0.06	0.06	2191	84	130
1	553	30.20 0.49	1.67	4.20	0.06	0.06	2197	86	130
1	554	30.69 0.49	1.62	4.22	0.06	0.06	2203	87	130
1	555	31.18	1.57	4.23	0.06	0.06	2208	89	130
1	556	31.67 +0.49	1.52	4.25	0.06	0.06	2214	90	130
1	557	02.10	1.48	4.26	0.06	0.06	2219	92	130
1	558 559	32.66 0.50 33.16 0.50	1.43 1.38	4.27 4.28	0.06	0.06	2224 2229	94 95	130 130
1		0.51					No. of the last		The Ash In
1	560	33.67 34.17 +0.50	1.34	4.29	0.06	0.06	2234	97	130
1	561 562	34.68 0.51	1.29 1.25	4.31 4.32	0.06 0.07	0.06	2238 2243	98 100	130 130
1	563	35 19 0.51	1.20	4.32	0.07	0.06	2248	101	130
ı	564	35 70 0.51	1.16	4.33	0.07	0.06	2252	103	130
ı	565	0.51	1.12	4.34	0.07	0.06	2256	105	130
1	566	36 73 +0.52	1.08	4.35	0.07	0.06	2261	106	130
ı	567	87 95	1.03	4.36	0.07	0.06	2265	108	130
1	568	37.76 0.51	0.99	4.37	0.07	0.06	2269	110	130
1	569	38.29 0.53	0.96	4.38	0.07	0.06	2272	111	130
1	570		0.92	4.38	0.07	0.06	2276	113	130
ı	571	39.34 +0.53	0.88	4.39	0.07	0.06	2280	115	130
1	572	39.86	0.84	4.40	0.07	0.07	2283	116	130
1	573	40.00	0.80	4.40	0.08	0.07	2287	118	130
1	574	0.53	0.77	4.41	0.08	0.07	2290	120	131
1	575	41.45 41.98+0.53	0.73	4.41	0.08	0.07	2293	121	131
1	576	0.54	0.70	4.42	0.08	0.07	2296	123	131
1	577	42.02 0.52	0.67	4.42	0.08	0.07	2299	125	131
1	578 579	43.00 0.54	0.63	4.42 4.43	0.08	0.07	2302 2304	126 128	131 131
1		0.53						The late of the la	
1	580 581	44.12 44.66+0.54	0.57 0.54	4.43	0.08 0.08	0.07	2307 2309	130 132	131 131
1	581	45.20 0.54	0.54	4.45	0.08	0.08	2312	133	131
1	583	45.74 0.54	0.48	4.44	0.09	0.08	2314	135	131
1	584	46.28 0.54	0.46	4.44	0.09	0.08	2316	137	132
1	585	46.83	0.43	4.44	0.09	0.08	2318	138	132
1	586	47.37 +0.54	0.40	4.44	0.09	0.08	2319	140	132
1	587	47.91	0.38	4.44	0.09	0.09	2321	142	132
1	588	48.46 0.55	0.36	4.44	0.09	0.09	2322	144	132
1	589	49.00 0.54	0.33	4.44	0.09	0.09	2324	145	132
1	590	40 55	0.31	4.44	0.09	0.09	2325	147	132
1	591	50.10 +0.55 50.64 0.54	0.29	4.44	0.09	0.09	2326	149	132
1	592	50.64	0.27	4.44	0.10	0.09	2327	150	133
1	593 594	51.19 0.55 51.74 0.55	0.25 0.23	4.44	0.10	0.10 0.10	2328 2329	152 154	133 133
1		0.55							HALL ON THE
1	595	52.29 52.84 +0.55	0.22	4.43	0.10	0.10	2330 2330	155 157	133
1	596 597	53.38 0.54	0.20 0.18	4.43 4.43	0.10 0.10	0.10	2330	157	133 133
1	598	53.93 0.55	0.17	4.43	0.10	0.11	2331	161	134
1	599	54.48 0.55	0.16	4.42	0.10	0.11	2331	162	134
1	600	55.03	0.14	4.42	0.10	0.11	2331	164	134
1	600	55.05	0.14	4.42	0.10	0.11	2001	104	104

					TA	BLE	IX, Arc	a. 2.—	-Action	OF SAT	URN.				
	Arg.	(v.c. 0)	Diff.	(v.s.1)	Diff.	Sec.var.	(v.c.1)	Diff.	Sec.var	(v.s.2)	Diff.	Sec.var.	(v.c.2)	Diff.	Sec. var.
1	0	20.54	"	120.04	"	0 5 9	002 70	"	0.56	182.62	"	1 55	014.05	"	0.10
1	$\frac{0}{1}$	$\begin{vmatrix} 38.54 \\ 38.63 \end{vmatrix}$ +	-0.09	139.94 141.38	+1.44		293.78 293.81	+0.0	3 0.55	183.80	+1.18	1.77	$\begin{vmatrix} 244.67, \\ 244.10 \end{vmatrix}$	-0.57	$0.12 \\ 0.12$
1	2 3	38.72 38.81	0.09	142.82 $144.26$	1.44	2.00	293.83 293.83	0.00	0.54 $0.53$	184.96 186.12	1.16	1.74	243.52 242.93	0.58	0.12 0.11
1	4	38 00	0.09	145.70	1.44	2.48	293.82	-0.01 0.03	0.52	187.27	1.15	1.71	242.32	0.61	0.11
1	5	38.98	0.09	147.14 148.58		2.47	293.79	_0.04	0.51	188.42 189.56	_	1 70	241.71	_0.62	0.11
ı	6 7	39 16	0.09	148.58	1.43	$2.46 \\ 2.45$	293.75 $293.70$	0.05		189.56	1.13	1 67	$241.09 \\ 240.46$	0.63	0.11
ı	8 9	39.24	0.09	151.45 152.89	I.44 I.44	$\frac{2.44}{2.43}$	293.63 293.54	0.07	0.43	191.82 192.94	1.13		239.81 $239.15$	0.66	0.10 0.10
ı	10	39 41	0.08	154 32	1.43	2.42	293.44	0.10	0.46	194.05	1.11	1.63	238 48	0.67	0.10
	11 12		0.09	155.76 <sup>-</sup> 157.19	1.43	$\frac{2.41}{2.40}$	293.33	0.11	0.45	195.16 196.26	1.10	1.61	237.80	-0.68 0.69	0.10
L	13	39.67		154.19	1.43	2.39	293.20 $293.06$	0.14	0.43	197.35	1.09	1.58	237.11 $236.41$	0.70	$0.10 \\ 0.10$
	14	00.10	0.09	160.05	I.43 I.43	2.38	292.90	0.16	0.42	198.43	1.08	1.57	235.69	0.72	0.10
	15 16	$\frac{39.84}{39.92} +$	0.00	161.48 $162.90$	-1.42	$\frac{2.36}{2.35}$	292.73 292.55	-0.18	$0.42 \\ 0.41$	199.51 $200.58$	+1.07	1.55 1.53	234.96 234.22	_0.74	0.10
	17	40.01	0.00	164.32	I.42 I.42	2.34	292.34	0.21	0.40	201.64	1.06	1.52	233.48	0.74	0.09
	18 19	40.10	0.08	165.74 167.16	1.42	2.33 2.32	292.13 291.90	0.23	0.00	202.69 203.74	1.05	1.50	232.73 231.96	0.77	0.09
	20	40.27	1	168.58	1.42	2.31	291.65	0. 25 -0. 26	0.37	204.78	1.04	1.47	231.18	0.78	0.09
	21 22	40.44	0.09	169.99 <del> </del> 171.40	1.41	2.30 2.29	291.39 <sup>-</sup> 291.12	0.27	$0.36 \\ 0.35$	205.81 206.83	1.02	1.46	230.39 <sup>-</sup> 229.60	0.79	$0.09 \\ 0.09$
	23	40.59	0.00	172.81	1.41	2.27	290.83	0.29	0.35	207.84	1.01	1.43	228.80	0.80	0.10
1	24 25	40 51	0.09	174.22 $175.62$	1.40	2.26	290.53 290.22	0.31	0.34	208.85 209.85	1.00	1.41	227.98	0.83	0.10
1	26	40.80	0.09	177.02	1.40	2.24	289.89	-0.33	0.32	210.84	0.99	1.39	$\frac{227.15}{226.31}$ -	0.84	0.10
	27 28	40.89	0.09	$178.42 \\ 179.81$	1.39	$\begin{bmatrix} 2.23 \\ 2.21 \end{bmatrix}$	289.55 $289.19$	0.34	$0.31 \\ 0.30$	$211.82 \\ 212.79$	0.97		225.46 224.60	0.86	0.10
	29	41.07	0.00	181.20	1.39		288.82	0.37	0.30	213.76	0.97		223.74	0.86	0.11
	30	41.16 41.25	0.09	182.59 + 183.97 +	-1.38		288.44 288.04	-0.40	0.29	214.71 215.66	+0.95		222.87	-0.88	0.11
1	32	41.35	0.10	185.35	1.38	2.17	287.63	0.41	0.28	216.60	0.94	1.30	221.10	0.89	0.11
	33	41.44	0.10	$186.73 \\ 188.10$	1.37		287.20 286.76	0.44	$0.27 \\ 0.26$	217.53 218.44	0.93		220.20 $219.28$	0.90	0.12
:	35	41.64		100 48	1.37		996 90	0.46	0.26	910 95	0.91		019 96	0.92	0.12
	36	41.74		189.47 $190.83$ $192.19$	- 0		285.84 285.35	-0.46 0.49	$0.25 \\ 0.24$	220.25 221.14	0.89	1.25	217.43	0.93	0.12
3	38	41.93	0. 10	193.55	1.36	2.09	284.86	0.49	0.23	222.03	0.89	1.22	216.49 215.55	0.94	0.13
	39	42.03		194.90	1.35	2.07	284.35	0.51	0.23	222.90	0.86		214.59	0.97	0.13
4	41	42.13 42.24	), I () I	196.25 197.59+	1.34	2.05		-0.53	$0.22 \\ 0.22$	223.76 224.61	<b>+0.85</b>	1 18	$\frac{213.62}{212.65}$	-0.97	0.13
	42 43	42.34	0.10	198.93 200.26	1.34 1.33		282.76 282.20	0.55	$0.21 \\ 0.21$	225.45 226.28	0.84	1.16	211.67	0.98	0.14
	14	42.55	0.11	201.59	I.33 I.32		281.63	0.57	0.21	227.11	0.83		210.68 209.68	I.00 I.01	0.14
	15	42.66 42.77	0.11	$202.91 \\ 204.23 +$			281.04	0.59	0.20	227.92			208.67	-1.01	0.15
4	17	42.87	0.10	205.54	1.31	1.96	279.82	0.62	0.19	228.72 - 229.51	0.79		207.66 <sup>-</sup> 206.64	1.02	0.15
	18	42.98	0.11	206.85 208.15	1.31	1.94	279.20 278.56	0.62	0.18 0.18	230.29 231.07	0.78	1.07	205.61		0.15
	50	10.00		209 44	1.29		277 91	0.65	0.18	231 83	0.76		204.57 203.52	1.05	0.16
1	51	43.32+6	0.11	210.73+	1.28	1.91	277.24	0.68	0.17	232.58	-0.75 0.74	1.03	202.47		0.17
1	53	43.54	2.11	212.01 $213.29$	1.28	1.88	276.56 275.87	0.69	0.16	233.32 234.05	0.73		201.41 $200.34$	1.07	0.17 0.18
	54	43.65	0.12	214.57	1.28	1.87	275.17	0.70	0.16	234.77	0.72	0.99	199.26	1.08	0.18
	55	43.77	J. 14 6	$215.84 \\ 217.10 +$	-1.26		274.45 273.72	-0.73	0.15	235.48 236.18		0.97	$198.18 \\ 197.09$	-1.09	0.19
1	57	44 (11)	2 72	218.35 219.60	T 25	1.82	272.98	0.74	0.15	236.87	0.69	0.95	196.00	1.09	0.20
	59	44 94		219.60 $220.84$	1.24		272.23 271.46	0.77	0.15 0.14	237.54 238.20	0.66		$194.90 \\ 193.79$	1.11	0.21
1	60	44.35		222,07	1.23		270.69	0.77	0.14	238.85	0.65		192.67	1.12	0.22
-		-			-			-							

i				TABI	LE 1X,	Ang. 2	.—Con	tinued.				
	Arg.	(v.s.3)	(v.c.3)	(v.s.4)	(v.c.4)	(p.c.0)	(p.s.1)	(p,c,1)	(0.8.2)	(o.c.2)	(p.s.3)	(o.c.3)
		"	"	**	"				-			
	0	11.40	14.53	1.58	1.68	1678	182	1513	711	306	137	85
	1	11.52	14.48 14.43	1.59	1.66	1679	182	1526	711	302	137	85
	2 3	11.64	14.43	1.61	1.65	1680 1680	183 184	1539 1551	710	298 295	137 137	85 85
	4	11.87	14.33	1.62	1.63	1681	185	1564	703	291	137	85
	5	11.98	11.28	1.63	1.62	1682	187	1577	707	288	137	85
	6	12.10 12.21	14.22 14.16	1.64	1.61	1682 1683	188	1590	706	284	137	85
	7 8	12.21	14.10	1.65	1.50	1683	190 191	1603 1615	704	281 278	138 138	84
	9	12.43	14.04	1.66	1.58	1682	193	1628	701	274	138	84
	10	12.54	13.97	1.67	1.56	1682	195	1641	700	271	138	84
	11	12.65 12.76	13.91 13.84	1.68 1.69	1.55	1681 1680	197 199	1654 1666	699 693	267 264	138 138	84
	13	12.87	13.77	1.69	1.53	1679	201	1679	696	260	138	84
	14	12.97	13.70	1.70	1.52	1678	203	1691	695	257	137	83
	15	13.07	13.63	1.71	1.50	1677	206	1704	691	253	137	83
	16 17	13.18 13.28	13.56 13.49	1.71 1.72	1.49	1675 1674	208 211	1716 1729	692 691	250 246	137 137	83 83
	18	13.38	13.41	1.73	1.47	1672	214	1741	689	243	137	82
	19	13.48	13.33	1.74	1.45	1670	217	1754	687	239	137	82
	20	13.58	13.25	1.74	1.44	1668	220	1766	685	236	137	82
	21 22	13.68 13.78	13.17	1.75 1.75	1.43	1666 1664	223 227	1778 1790	683 681	233 230	137 137	82 81
	23	13.87	13.01	1.76	1.40	1662	230	1802	679	226	137	81
1	24	13.97	12.92	1.76	1.39	1660	234	1814	677	223	137	81
	25	14.06	12.83	1.77	1.37	1658	237	1826	675	220	137	81
	26 27	14.15	12.74 12.65	1.78 1.78	1.36 1.35	1656 1653	241 245	1838 1850	673 671	217 214	137 137	81 80
	28	14.33	12.56	1.79	1.34	1651	249	1862	668	211	137	80
	29	14.41	12.47	1.79	1.32	1648	253	1874	666	208	137	80
	30	14.50	12.37	1.79	1.31	1645	258 262	1886 1898	664 662	205 202	137 137	79 78
	31 32	14.58 14.66	12.28 12,19	1.80 1.80	1.30	1642 1638	262	1910	659	199	137	78
	33	14.74	12.09	1.80	1.27	1635	272	1922	657	196	137	78
	34	14.82	11.99	1.81	1.25	1631	277	1934	654	193	137	78
	35	14.90	11.89 11.79	1.81	1.24	1627 1623	282	1946 1958	652 650	190 187	137 137	77
	36 37	14.97 15.05	11.69	1.81	1.21	1619	292	1970	647	184	137	77
	38	15.12	11.59	1.82	1.20	1615	297	1982	645	181	137	76
	39	15.19	11.49	1.82	1.13	1611	302	1993	642	179	137	76
	40	15.26 15.33	11.38	1.82 1.82	1.17	1608 1602	308	2005 2016	640 637	176 173	137	76
	41	15.39	11.17	1.82	1.14	1597	319	2028	635	171	137	76
1	43	15.46	11.06	1.82	1.13	1592	325	2039	632	168	137 137	75 74
	44	15.52	10.95	1.82	1.11	1587	331	2051	630	166 163		74
	45 46	15.58 15.64	10.84	1.82 1.82	1.10	1582 1577	337 343	2062 2073	627 624	160	137 137	74
	47	15.70	10.62	1.82	1.07	1572	349	2084	621	158	137	73
1	48	15.76	10.51	1.82 1.82	1.06	1566 1561	355 362	2095 2106	619 616	155 153	137 137	73
	49	15.81	10.40	1.82	1.04	1556	368	2117	613	150	137	72
	50 51	15.86 15.91	10.28	1.82	1.03	1550	375	2128	610	148	137	72
	52	15.96	10.05	1.82	1.00	1545	381	2138	607	145	137	72
	53 54	16.01 16.05	9.94 9.82	1.81 1.81	0.98	1539 1533	388 394	2149 2159	604	143 140	137 137	72 72
	55	16.09	9.70	1.81	0.96	-1527	401	2170	598	138	137	71
	56	16.13	9.59	1.81	0.94	1521	408	2180	595	135	137	71
	57	16.17	9.47	1.80	0.93	1515	415	2191 2201	592 589	133 131	137 137	71
	58 59	16.20 16.23	9.35 9.23	1.80 1.80	0.92	1509 1502	422	2212	586	129	137	71
	60	16.26	9.11	1.80	0.89	1496	437	2222	583	127	137	71
	,	0.20										

,				TAB	LE IX,	ARG.	2.— <i>Co</i>	ntinued.					
	Arg.	(v.c.0) Diff.	(v.s.1) Diff.	Sec.var.	(v.c.1)	Diff.	See.var.	(v.s.2)	Diff.	See.var.	(v.c.2)	Diff.	See.var.
N		" "	" "	"	"	"	"	"	"	"	"	"	"
	60	44.35 +0.12		1.78	$\begin{vmatrix} 270.69 \\ 269.89 \end{vmatrix}$	_0.80	0.13	238.85 239.49	+0.64	$0.91 \\ 0.90$	192.67 191.55	I.I2	0.23
	62	44.59 0.12	224.52	1.75	269.09	0.80	0.15	240.12	0.63	0.98	190.42	1.13	0.23
ı	63	44.71	226.73	1.79	$\begin{vmatrix} 268.28 \\ 267.45 \end{vmatrix}$	0.83	0.15	$\begin{vmatrix} 240.74 \\ 241.35 \end{vmatrix}$	0.61	0.87	189.29 188.14	1.15	$0.24 \\ 0.25$
1	65	44 95	1.20	1 70	266.61	0.84 -0.85	0.10	041 05	0.60	0.04	186.99	1.15	0.25
	66	45.07 +0.12	$\begin{vmatrix} 228.14 \\ 229.33 \\ 1.18 \end{vmatrix}$	1.69	265.76 264.89	0.87	0.12	241.95 $242.53$ $243.10$	0.57	0.83	185.83	_1.16 1.16	0.26
	68	45.19 0.12	231.69 1.18	1.66	264.02	0.87	0.12	243.10	0.57	0.82 0.81	184.67 183.51	1.16	$0.27 \\ 0.28$
	69	45.44 0.13	232.86 1.17	1.64	263.13	0.89	17. 1 1	244.22	0.55	0.79	182.34	1.17	0.28
1	70	$\frac{45.56}{45.68}$ + 0.12	234.02 +1.15	$\frac{1.63}{1.62}$	262.23 $261.32$	_0.91	$0.11 \\ 0.11$	244.76 245.28	+0.52	0.78	181.16 179.97	_1.19	$0.29 \\ 0.30$
1	72	45.80 0.12	236.31	1.60	260.39	0.93	0.11	245.79	0.51	0.75	178.78	1.19	0.31
1	73	46.92 0.12	238 58 1.13	1.59 1.57	259.46 $258.52$	0.93	0 0 20 2	246.29 246.78	0.49	0.74 0.73	177.59 176.40	1.19	0.32 0.33
ı	75	0.12	020 70	1.56	257.56	0.96	0.11	247 26	0.48	0.71	175.20	1.20	0.34
1	76	46.29 +0.13	240.81	1.55	256.59	-0.97 0.98	0.11	247.73	1-0.47	0.70	173.99	-I.2I I.2I	0.34
1	77	46.41 0.12	241.91 243.00 1.09	1.53 1.52	255.61 254.62	0.99	V. J. L	248.18 248.62	9.44		172.78 171.56	1.22	0.35
1	79	46.65 0.12	244.09 1.08	1.50	253.62	1.00		249.05	0.43		170.34	I.22 I.23	0.37
ı	80	46.77 46.89 0.12	245.17 + 1.07	1.49	252.61	_1.02	0.11	249.47		0.65	169.11		0.38
1	81 82	47.01 0.12	246.24 1.06 247.30 1.05	1.48 1.46	251.59 <sup>-</sup> 250.56	1.03	0.11	249.87 - 250.26	0.39		167.88 <sup>-</sup> 166.65	1.23	0.39
ı	83 84	47.13 0.11 47.24 0.11	248.35	1.45 1.43	249.51	1.05	0.11	250.64	0.38	0.62	165.41	I. 24 I. 24	0.41
١	85	47 36	249.38 I.03 250.41	1.42	248.45 247.38	1.07	0.11	251.01	0.36		164.17	1.25	0.42
1	86	47.48 +0.12	251.43 +1.02	1.40	246.30	-1.08	0.12	251.37 $251.71$	-0.34		$\frac{162.92}{161.67}$	-1.25	0.43
١	87 88	47.59 O.11 47.71 O.12	252.44 I.or 253.44 I.oo	1.39 1.38	245.21 $244.12$	1.09	$0.12 \\ 0.12$	252.04 252.36	0.33		160.42	1.25	0.44
	89	47.82 0.11	254.43 0.99	1.36	243.01	I.II I.I2	0.12	252.56	0.31		159.16 157.90	1.26	0.45
1	90	47.94 48.05 +0.11	255.41	1.35	241.89		0.12	252.96	0.29		156.63	1.27	0.47
1	91 92		256.38 +0.97 257.34 0.96		240.76 <sup>-</sup> 239.62	1.14	$0.12 \\ 0.12$	253.24 253.50	0.26		155.36 <sup>-</sup> 154.09	I.27	0.48   0.49
١	93	48.27	258.29 0.95	1.30	238.48	1.14	0.13	253.75	0.25	0.51	152.82	I.27 I.27	0.50
ı	94 95	40.55 0.11	0.93	1	237.33	1.17	0.13	253.98	0.23		151.55	1.28	0.51
	96	48.59 +0.10	260.16 261.08 +0.92	1.26	236.16 234.98	-1.18	0 19	254.21 254.43	-0.22	0.49 0.48	150.27 - 148.99	_1.28	$0.52 \\ 0.54$
ı	97 98	48.70	261.99 0.89	1.25	233.79	1.19	0.13	254.63	0.20	0.47	147.71	1.28	0.55
I	99		263.76 0.88 0.87		232.60 $231.39$	1.21		254.82 254.99	0.17		146.42 145.13	1.29	0.56 0.57
ı	100	49.01	264 63	1.20	230.18	1.21		955 15	0.16	100000	143.84	1.29	0.58
ı	101 102	49 21 0.10	265.49 0.85		228.96 <b>-</b> 227.73	1.23		255.30 <sup>7</sup> 255.43	0.13		142.55 <sup>-</sup> 141.26	1.29	0.59
1	103	49.31	267.18 0.82	1.16	226.50	1.23	0.15	255.55	0.12		139.97	1.29	0.60 0.61
1	104	0.10	268.00 0.81		225.25	I.25 I.26		255.66	0.09		138.67	1.30	0.62
1	105 106	49 50 70.09	268.81 269.61 +0.80		223.99 $222.73$	-1.26	0.16	255.75 255.83 +	-0.08	0.39	137.37. 136.07	-1.30	0.63
۱	107	49.68	270.41	1.10	221.46	I.27 I.28	0.17	255.90	0.07	0.38	134.77	1.30	0.66
ı	109		271.19 0.77 271.96 0.77		220.18 $218.88$	1.30		255.95 255.99	0.05		133.47 132.17	1.30	0.67
	110	49.94	272 71	1.06	217.58	1.30		256.02	0.03		130.87	1.30	0.69
1	111 112	50 11 0.09	273.45 +0.74 274.18 0.73	1.05	216.28 -	1.31	0.18	256.04	0.00	0.34	$129.57^{-}$	1.30	0.70
1	113	50.19	274.90 0.72	1.02	214.97 213.65	1.32	0.19	$\frac{256.04}{256.03}$	-0.01		$128.26 \\ 126.96$	1.30	0.71   0.73
	114	0.08	275.60 0.70 0.69	1.00	212.33	I.32 I.34	0.20	256.00	0.03		125.66	1.30	0.74
1	115	50.41 +0.07	276.29 276.97 +0.68		$\frac{210.99}{209.65}$ $-$	-1.34		255.96	-0.05		124.36	-1.31	0.75
1	117	50.48	277.63	0.97	208.31	1.34	0.21	255.91 <sup></sup> 255.84	0.07		123.05 - 121.75	1.30	0.76
	118	50.62 0.07	978 09 0.64		$206.96 \\ 205.60$	1.35 1.36		255.76 255.67	0.08		120.45 $119.15$	1.30	0.78
	120	0.07	279.55 o.63		204.23	1.37		255.56	0.11		117.85	1.30	0.81
L						11.00	0.20	m00.00		0.21	111.00	a line	0.01

-				TABI	E IX,	ARG. 2	.—Cont	tinued.				
	Arg.	(v.s.3)	(v.c.3)	(v.s.4)	(v.c.4)	(p.c.0)	(p.s.1)	(p.c.1)	(p. 8.2)	(p.c.2)	(p.s.3)	(p.c.3)
		"	"	"	"							
	60 61	16.26 16.29	9.11	1.80 1.79	0.89	1496 1489	437 445	2222 2233	583 580	127 125	137 137	71
İ	62	16.32	8.88	1.79	0.87	1483	453	2243	577	123	137	70
	63	16.35	8.76	1.78	0.85	1477	460	2254	574	121	137	70
	64	16.38	8.64	1.78	0.84	1470	468	2264	570	119	137	69
	65	16.41	8.52	1.78	0.83	1464	476	2275	567	117	136	69
-	66	16.43	8.40	1.77	0.81	1457	484	2285	564	115	136	68
	67 68	16.45 16.47	8.28 8.16	1.77 1.76	0.80	1451 1444	492 501	2295 2306	560 557	113 112	136 136	68 67
-	69	16.49	8.04	1.75	0.78	1438	509	2316	553	110	136	67
	70	16.50	7.91	1.75	0.76	1431	518	2326	550	108	136	66
	71	16.51	7.79	1.74	0.75	1424	527	2336	546	107	136	66
	72	16.52	7.67	1.74	0.74	1417	536	2346	543	105	136	66
	73	16.53	7.55	1.73	0.73	1410	545	2356	540	103	135	65
	74	16.54	7.43	1.72	0.71	1403	554	2365	536	102	135	65
	75 76	16.54 16.54	7.31 7.19	1.72	0.70	1396	563 572	2375	533	100	135	64
	77	16.54	7.07	1.70	0.68	1389 1382	581	2384 2394	530	99 98	135	64 64
	78	16.54	6.95	1.70	0.67	1374	590	2403	523	96	135	63
	79	16.53	6.83	1.69	0.65	1367	599	2413	519	95	135	63
	- 80	16.53	6.71	1.68	0.64	1360	608	2422	516	94	135	62
	81	16.52	6.60	1.67	0.63	1353	618	2431	512	93	135	62
	82 83	16.52 16.51	6.48	1.66 1.65	0.62	1346 1339	627	2440	508 505	92 91	134 134	61
	84	16.50	6.24	1.64	0.60	1332	646	2457	501	89	134	60
	85	16.48	6.13	1.63	0.59	1325	656	2466	498	88	134	60
	86	16.46	6.01	1.62	0.58	1318	664	2475	494	87	134	59
	87	16.44	5.89	1.61	0.57	1311	676	2483	490	86	134	59
	88	16.42	5.78	1.60	0.56	1304	684	2492	487	85	134	58
	89	16.40	5.66	1.59	0.55	1296	696	2500	483	84	133	58
	90	16.38	5.55	1.58	0.54	1289	706	2509	480	84	133	57
	91 92	16.35 16.33	5.44 5.32	1.57 1.56	0.53 0.52	1281 1273	717	2517 2525	476 472	83 82	133	57 56
	93	16.30	5.21	1.55	0.51	1266	738	2534	469	82	132	56
	94	16.27	5.09	1.54	0.50	1258	749	2542	465	81	132	55
	95	16.24	4.98	1.53	0.50	1250	760	2550	461	81	132	55
	96	16.20	4.87	1.52	0.49	1242	771	2558	457	80	131	54
	97 98	16.17 16.13	4.76 4.64	1.51 1.50	0.48	1234 1226	782	2566 2574	454 450	80	131	54 53
	99	16.13	4.54	1.49	0.47	1218	804	2582	446	79	130	53
	100	16.05	4.44	1.48	0.46	1210	815	2590	442	79	130	52
	101	16.01	4.33	1.46	0.46	1202	826	2598	438	79	130	51
	102	15.96	4.23	1.45	0.45	1194	838	2605	435	79	129	51
	103	15.92	4.13 4.02	1.44 1.43	0.44	1186	849 861	2613 2620	431 428	78 78	129	50 50
	104	15.87	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		1000000	1178		1-11	-	- 98-		
	105	15.83 15.78	3.92 3.82	1.42	0.43 0.43	1170 1162	872 883	2627 2634	424	78	128 128	49
	107	15.73	3.72	1.39	0.43	1154	895	2641	416	78	128	48
	108	15.68	3.62	1.38	0.42	1146	907	2647	413	78	127	48
	109	15.62	3.52	1.37	0.41	1138	919	2654	409	78	127	47
	110	15.56	3.43	1.36	0.41	1130	931	2661	405	78	126	46
	111 112	15.51 15.45	3.34 3.24	1.34	0.40	1122	943 955	2668	402 398	78	126 125	46 45
	113	15.45	3.15	1.32	0.40	1106	967	2681	394	79	125	45
	114	15.33	3.06	1.31	0.39	1098	979	2687	391	79	124	44
	115	15.27	2.97	1.29	0.39	1090	991	2693	387	80	124	44
1	116	15.21	2.88	. 1.28	0.38	1082	1003	2699	383	80	123	44
	117	15.14	2.80	1.26 1.25	0.38	1074	1016	2705	380 376	80	122	48
	118	15.08 15.01	2.71 2.62	1.23	0.38	1059	1028	2716	373	81	121	42
	120	14.94	2.54	1.23	0.37	1051	1053	2722	370	82	120	42
1	120	21.01	2.01			2002		-,	7.0			

	l In			TABI	LE IX,	ARG.	2.— <i>C</i>	ontinued.					
	Arg	. (v.c.0) Diff	f.(v.s.1) Diff	Sec.var.	(v.c.1)	Diff.	Sec.var	(v.s.2)	Diff.	Sec.var.	(v.c.2)	Diff.	Sec.var.
		" "	" "	"	"	"	"	"	"	"	"	11	11
	120 121	50.69	$\begin{vmatrix} 279.55 \\ 280.16 \end{vmatrix} + 0.0$	0.93 $0.92$	$\begin{vmatrix} 204.23 \\ 202.86 \end{vmatrix}$	_1.37	$0.23 \\ 0.24$	255.56 255.44	_0.I2	$0.27 \\ 0.26$	117.85	-1.30	0.81
	121	50.82	280.76	0.90	201.48	1.30	0.24	255.31	0.13	0.26	116.55 115.25	1.30	0.82
	123	50.88 0.00	281.35	9 0.89	200.10	1.38	0.25	255.16	0.15	0.25	113.95	1.30	0.85
	124	0.05	0.1		198.71	1.39	)	254.00	0.17	0.25	112.65	1.30	
	125	50.98 51.03+0.05	282.48 +0.5	0.87	197.31 195.91	_1.40	0.26	254.83	-0.19	0.24	111.36	—I.29	0.88
	$\frac{126}{127}$	51.08	283.02 +0.5		193.91	1.41	$0.27 \\ 0.27$	254.64 254.44	0.20	$0.23 \\ 0.23$	110.07	1.30	U. OH
	128	51.13	284.07	$^{2}$ 0.83	193.09	1.41	0.28	254.23	0.21	0.22	107.48	1.29	0.92
	129	51.17	1284.51		191.67	I.42	0.40	254.00	0.23	0.22	106.19	1.29	
	130	51.22 51.26+0.04	285.06	0.80	190.25	Y 40	0.29	253.76	0.25	0.21	104.91		0.95
1	131 132	51.30 0.04	285.53 +0.4 285.99 0.4	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	188.82 187.39	1.43	0.00	253.51 253.24	0.27	$0.21 \\ 0.20$	103.63	_1.28	
	133	51.34 0.04	286.44 0.4	5 0.76	185.95	1.44	0.32	252.96	0.28	0.20	102.35	1.28	0.00
	134	51.37 0.03			184.51	1.44	U. UU	252.67	0.29	0.19	99.79	1.28	1.01
	135	51.40	00H 00	0.74	183.07		0.33	252.36		0.19	98.52	1.27	1 02
ı	136 137	51.43 0.02	287.69 +0.4 288.08 0.3		101.02	—1.45 1.45	0.01	252.04	0.33	0.18	97.25	-I.27 I.26	1.03
	138	51.47 0.02	288 45 0.3	0 . 1	180.17 178:72	1.45		$\begin{vmatrix} 251.71 \\ 251.36 \end{vmatrix}$	0.35	$0.18 \\ 0.17$	95.99 $94.73$	1.26	1.05 1.06
ı	139	51.49 0.02	288.81 0.3	0.69	177.26	1.46	0.37	251.00	0.36	0.17	93.47	1.26	1.08
4	140	51.51	289.16	0.68	175.80	1.46	0.38	250.63	0.37	0.16	92.21	1.26	1.09
1	141	51.52 +0.01 51.53 0.01			174.33	-1.47 1.47		250.24	0.40	0.16	90.96	-1.25	1.10
	142 143	51.54 0.01	289.80 °.3 290.10 °.3		172.86 171.39	1.47	$0.40 \\ 0.41$	249.84 249.43	0.41	0.15 0.15	89.71 88.46	1.25	1.12 1.13
1	144	51.55 0.01	290.39 0.2	9 0.63	169.92	1.47	0.42	249.01	0.42	0.14	87.22	1.24	1.15
1	145	51.55	290.66	0.69	168.44	1.48	0.42	248.57	0.44	0.14	85.98	1.24	1.16
1	146	51.55 0.00	290.92 +0.2	0.61	166.96	-1.48 1.48	0.43	248.12	0.45	0.14	84.75	-I.23	1.17
1	147 143	51.55 0.00	291.16 0.2 291.38 0.2	0.00	165.48 164.00	1.48	$0.44 \\ 0.45$	247.66	0.48	0.13 0.13	83.52	1.23	1.19
ı	149	51.53 0.01	291.59 0.2	0.57	162.52	1.48	0.46	247.18 246.69	0.49	0.13	82.29 81.07	1.22	$\frac{1.20}{1.22}$
1	150	51.52	291.79	0.56	161.03	1.49	0.47	246.19	0.50	0.12	79.85	1.22	1.23
1	151	51.50 -0.02	291.97 +0.1		159.54	-1.49	0.48	245.68	_0.51	0.12	78.64	-1.21	1.24
ı	152 153	51.49 0.01	292.13 O.16 292.28 O.15	U. 0 T	158.05 156.56	1.49	0.49 0.50	245.15	0.53	0.12	77.44	1.20	1.26
1	154	51.45 0.02	292.42 0.1	0.52	155.07	1.49	0.51	244.61 244.06	0.55	0.11	76.24 75.04	1.20	1.27 1.29
ı	155	51.43	292.54	0.51	153.58	1.49	0.52	243.50	0.56	0.11	79 05	1.19	1.30
ı	156	51.40 -0.03 51.37 0.03	292.64+0.10	0.50	152.09	-1.49	0.54	242.92	-0.58	0.11	72.67	-1.18	1.31
	157 158	51.37 o.o3 51.34 o.o3	292.73 0.00 292.80 0.07			1.49	0.55	242.33		0.11	71.49	1.18	1.33
	159	51 30 0.04	292.86 0.06	0.10	149.11 $147.62$	1.49		241.73 241.12	0.61	0.10	70.32 69.15	1.17	1.34 1.36
ı	160	51.26	292.90		146.12	1.50	1000	240.49	0.63	0.10	67.99	1.16	
П	161	51.22 <sup>-0.04</sup> 51.17 0.05	292.93+0.03	0.45	144.63	-1.49	0.59	239.85	-0.64	0.10	66.84	-1.15	1.37
	$\begin{array}{c c} 162 \\ 163 \end{array}$	51.17 0.05	292.94 0.01 292.94 0.00	0.44	143.13	1.50	0.60	239.20		0.10	65.69	1.15	1.40
	164	51.07 0.05	292.92 -0.02	0.42	141.63 140.14	1.50		238.54 237.87		0.10	64.55 ·63.41	I. I4 I. I4	1.42
	165	51 01	292 88	0.41	138.64	1.50		237.18	0.69	0.09	62.28	1.13	
1	166	50.95 -0.06	292.83 -0.05	0.40	37.15	-1.49	0.65	236.48 -	-0.70	0.09	61.16	-I.I2	1.45
	167 168	50.89 0.00	292.76 0.07 292.68 0.08	0.40	35.66		0.66	235.77	0.71	0.09	60.05	I.II	1.48
	169	50 76 0.06	292.68 0.08 292.58 0.10	0.00	134.17 132.68		1	$235.05 \\ 234.32$		0.09	58.94 57.84		1.50
	170	50.69	292.47		131.20	1.48		233.58	0.74	0.09		1.09	1.51
L	171	50.62 -0.07	292.34 -0.13	0.36 1	29.71	-1.49		232.82 -	-0.76	0.09	56.75 55.67	80.1	1.53
	172 173	50.54 0.08	292.19 0.15 292.03 0.16	0.35	28.23	1.48	0.71	232.05	0.77	0.09	54.59	1.00	1.56
	174	50.37 0.09	291.86 0.17		26.75 25.27		- 1	231.27 $230.48$		0.10	53.52 52.45		1.57
	175	50.09	291.67		23.79	1.48			0.80		0	1.05	1.59
	176	50.19 -0.09	291.46 -0.21	$0.33   1 \\ 0.32   1$	$\frac{23.19}{22.32}$	-1.47	$ \begin{array}{c cccc} 0.75 & 5 \\ 0.76 & 5 \end{array} $	$\frac{229.68}{228.87}$ $-$	0.81	$\begin{bmatrix} 0.10 \\ 0.10 \end{bmatrix}$	$\frac{51.40}{50.35}$		$\begin{bmatrix} 1.60 \\ 1.61 \end{bmatrix}$
	177	50.10	291.24 °.22 291.01 °.23	0.31 1	20.85	1.47	0.77   9	228.05	0.02	0.10	49.31	1.04	1.63
	178 179	49 91 0.10	291.01 °.23 290.76 °.25		19.38						10.40	1.03	1.64
	180	0.10	290.49	2000		1.46	73.00	220.01	0.86	0.11	41.20	1.01	1.66
1_	00	10.01	200.40	0.29 1	16.45		0.81	225.51		0.11	46.25		1.67

1				TABI	LE IX,	ARG. 2	.—Con	tinued.				
	Arg.	(v.s.3)	(v.c.3)	(v.s.4)	(v.c.4)	(p.c.0)	(p.s.1)	(p.c.1)	(p.s.2)	(p.c.2)	(p.8.3)	(p.c.3)
1		".	"	"	"		11	- 11				No.
1	120	14.94	2.54	1.23	0.37	1051	1053	2722	370	82	120	42
1	121	14.87	2.46	1.22	0.37	1043	1065	2727	366	82	120	42
	122	14.80	2.38	1.20	0.37	1035	1078	2732	362	83	120	41
1	123	14.73	2.30	1.19	0.37	1028	1090	2737	359	83	119	41
1	124	14.66	2.22	1.18	0.37	1020	1103	2742	355	84	119	40
1	125	14.59	2.15	1.17	0.37	1012	1116	2747	352	85	119	40
1	126	14.52	2.07	1.15	0.37	1004	1129	2751	348	85	118	39
1	127	14.44	2.00	1.14	0.37	996	1141	2756	344	86	118	39
	128	14.37	1.93	1.13	0.37	989	1154	2760	341	87	117	38
	129	14.29	1.86	1.11	0.37	981	1167	2765	337	88	117	38
1	130	14.21	1.79	1.10	0.37	973	1180	2769	334	89	116	37
	131	14.13	1.72	1.09	0.37	965	1193	2773	330	90	115	37
	132	14.06	1.66	1.07	0.37	958	1206	2777	327	91	115	36
1	133	13.98	1.59	1.06	0.37	950	1219	2781	324	92	114	36
1	134	13.90	1.53	1.05	0.38	942	1232	2785	321	93	113	35
	135	13.82	1.47	1.04	0.38	935	1245	2789	318	94	112	35
	136	13.74	1.41	1.02	0.38	927	1258	2793	314	95	112	35
1	137	13.66	1.35 -	1.01	0.38	920	1271	2796	311	96	111	34
	138	13.57	1.30	1.00	0.39	912	1284	2800	308	97	110	34
1	139	13.49	1.24	0.99	0.39	905	1298	2803	305	99	109	33
	140	13.40	1.19	0.97	0.39	897	1311	2806	302	100	108	33
1	141	13.32	1.14	0.96	0.40	889	1325	2809	298	101	108	33
1	142	13.24	1.09	0.95	0.40	882	1338	2811	295	103	107	32
ı	143	13.15	1.04	0.94	0.41	875	1352	2814	292	104	106	32
ı	144	13.07	0.99	0.93	0.41	867	1366	2816	289	106	105	32
1	145	12.98	0.94	0.91	0.41	859	1379	2819	286	107	105	31
	146	12.90	0.90	0.90	0.42	852	1393	2821	282	109	104	31
١	147	12.81	0.86	0.89	0.42	844	1407	2823	279	110	103	31
1	148	12.73	0.82	0.88	0.43	837	1420	2825	276	112	102	30
	149	12.64	0.78	0.87	0.44	829	1433	2826	273	113	101	30
	150	12.55	0.74	0.86	0.44	822	1447	2828	270	115	100	30
1	151	12.46	0.70	0.85	0.45	815	1461	2829	267	117	99	30
1	152	12.38	0.67	0.84	0.46	807	1474	2831	264	118	98	29
1	153	12.29	0.64	0.83	0.46	800	1488	2832	261	120	97	29
1	154	12.20	0.61	0.82	0.47	793	1502	2834	258	122	96	29
1	155	12.11	0.58	0.81	0.48	786	1515	2835	256	124	95	28
1	156	12.11	0.55	0.80	0.49	778	1529	2836	253	126	- 94	28
1	157	11.94	0.52	0.79	0.49	771	1543	2837	250	128	93	28
1	158	11.86	0.50	0.78	0.50	764	1556	2837	247	129	92	28
1	159	11.77	0.47	0.77	0.51	756	1569	2838	244	131	91	27
1					0.52	749	1583	2838	242	133	90	27
1	160 161	11.68 11.59	0.45 0.43	0.76 0.75	0.52	749	1597	2838	239	135	90	27
1	162	11.59	0.45	0.74	0.53	735	1611	2838	236	137	89	27
1	163	11.42	0.40	0.73	0.54	728	1624	2837	233	139	88	27
1	164	11.33	0.38	0.72	0.55	721	1638	2837	230	141	87	27
1	The state of			A DESCRIPTION OF THE PERSON OF	0.56	714	1652	2836	228	143	86	27
-	165	11.24 11.16	0.37 0.36	0.71	0.56	707	1665	2835	228	143	85	27
-	166 167	11.16	0.35	0.71	0.58	700	1679	2834	222	147	84	27
1	168	10.99	0.34	0.69	0.59	693	1693	2833	219	149	83	27
1	169	10.91	0.33	0.68	0.60	686	1706	2833	216	151	82	27
1			The state of the s		100000000000000000000000000000000000000	20.2		2831	214	153	82	27
	170	10.82	0.32	0.68	0.61	679 672	1720 1734	2831	214	156	82	27
1	171 172	10.74 10.66	0.32	0.66	0.62	665	1747	2829	208	158	80	27
	173	10.57	0.31	0.66	0.64	659	1761	2826	206	160	79	27
	174	10.49	0.31	0.65	0.65	652	1775	2824	204	162	78	28
1			ST STA		The second		Contract of		202		77	28
	175	10.41	0.31	0.65	0.66	645	1788 1802	2822 2820	199	165 167	76	28
	176	10.33 10.25	0.31	0.64 0.63	0.67	632	1802	2820	199	170	75	28
1	177 178	10.25	0.31	0.63	0.69	625	1819	2815	195	173	74	28
1	178	10.17	0.32	0.63	0.00	618	1842	2812	192	175	73	28
	180	10.01	0.33	0.62	0.71	611	1855	2810	190	178	72	28
				48 85 35			1 12000	1 22111				

			TAB	LE IX,	ARG.	2.— <i>Ca</i>	ntinued.					1
Arg.	(v.c.0) Diff.	(v.s.1) Diff.	Sec.var.	(v.c.1)	Diff.	Sec.var	(v.s.2)	Diff.	Sec.var.	(v.c.2)	Diff.	Sec.var
100	// //	" "	0.90	110 45	"	0.01	995 51	"	0.11	11	"	"
180 181	49.81	1290.20	0.20	116.45 114.99	-1.46	$0.81 \\ 0.82$	$\begin{vmatrix} 225.51 \\ 224.64 \end{vmatrix}$	-0.8	11 11	46.25	_1.01	1.67 $1.68$
182	49.60 0.11	289.90 0.30	0.28	113.53	1.46	0.84	223.77	0.88	0.11	44.24	1.00	1.70
183 184	49.49	239.09	0.44	112.08 110.63	1.45	0.00	222.89 221.99	0.90	0.12	43.25	0.99	1.11
	49.37 0.12	0.3	5 0.20	100000	1.45	0.00		0.91		42.28	0.9	1.15
185 186	49.25 49.13 —0.12	$\begin{vmatrix} 288.91 \\ 288.55 \end{vmatrix}$ -0.36	11 20	109.18 107.74	-I.44	11.031	221.08 220.16	-0.92	0.12	41.31 40.35	-0.96	1.74
187	49.00 0.13	288.17	0.24	106.30	I.44	0.90	219.23	0.93	0.12	39.40	0.95	1 77
188 189	48.87 0.13	287.78 0.41	0.24	104.87	1.43	0.01	218.29	0.94	0.13	38.46	0.92	1.10
	0.13	0.42		103.44	1.42	0.00	217.34	0.96	0.13	37.53	0.92	1.00
190 191	48.61	286.95	. 11 21	$102.02 \\ 100.60$	1.42	17. 27.3	216.38 215.41	-0.97	0 3	36.61 35.70	-0.91	1.81
192	48.33	286 05 0.40	0.21	99.19	1.41	0.97	214.44	0.97	0.14	34:80	0.90	1 94
193	48.19 0.14	285.58 0.48	0.20	97.78	1.41	0.98	213.46	1.00	0.14	33.91	0.89	1.85
194	48.05 0.15	285.10 0.50		96.38	1.40		212.46	1.01		33.02	0.87	1.87
195 196	47.90 47.75 -0.15	284.60 284.09 —0.51	0.19	94.98 93.59	_1.39	$\frac{1.01}{1.02}$	211.45 210.43	_1.02	0.15	32.15	<b>-0.86</b>	1.88
197	47.60 0.15	283.56 0.53	0.13	92.20	1.39	1.04	209.40	1.03	0.15	31.29	0.85	1.91
198	47.44 0.16	283.01 0.55 282.45 0.56	0.18	90.82	1.38	1.00	208.37	1.03	0.15	29.60	0.84	1 93
199	0.16	0.57	0.17	89.44	1.37	1.07	207.33	1.05	0.16	28.77	0.82	1.94
200 201	47.12 46.95 —0.17	281.88 281.29 —0.59	0.17	88.07 86.71	_1.36	1.08	206.28 205.22	_1.06	0.16	27.95	-0.8I	1.96
202	46.78 0.17	280 68 0.01	0.16	85.36	1.35	1.11	203.22	1.07	$0.17 \\ 0.17$	27.14 26.34	0.80	1.97 1.99
203	46.61 0.17	280.06 0.62	0.16	84.01	I.35 I.35	1.12	203.07	1.08	0.18	25.55	0.79	2.00
204	0.18	0.65	0.16	82.66	1.34	1.14	201.98	1.09	0.18	24.78	0.77	2.01
205 206	46.26 46.08 -0.18	278.78 278.12—0.66	0.15	81.32 79.99		1.15	200.89 199.79	_I.IO	0.19	24.01	-0.75	2.03
207	45.90 0.18	277.44 0.68	0.15	78.67	1.32	1.16	199.79	1.11	$\begin{bmatrix} 0.20 \\ 0.20 \end{bmatrix}$	$23.26 \\ 22.52$	0.74	$\begin{array}{c c} 2.04 \\ 2.05 \end{array}$
208	45.71 0.19	276.75 0.69	0.14	77.36	1.31	1.19	197.56	1.12	0.21	21.79	0.73	2.06
209	0.19	276.04 0.71	0.14	76.05	1.31	1.21	196.43	1.13	0.21	21.07	0.72	2.08
210 211		275.32 274.58 -0.74	0.14	74.75	_1.29	1.22	195.30	-1.14	0.22	20.36	-0.70	2.09
212	44.94 0.20	273.83 0.75	0.13	73.46 <sup>-</sup> 72.18	1.28	1.23 1.25	194.16 193.01	1.15	0.23	19.66 18.97	0.69	$\begin{bmatrix} 2.10 \\ 2.12 \end{bmatrix}$
213		273.06 0.77	0.13	70.91	1.27	1.26	191.85	1.16	0.24	18.30	0.67	2.13
214	0.20	0.79	0.13	69.64	1.27	1.28	190.69	1.16	0.25	17.64	0.66	2.14
215 216	44.34	271.49 270.68 —0.81	0.12	68.37 - 67.12	-1.25	1.29	189.52	-1.18	0.26	17.00_	-0.63	2.16
217	43.92	000 000	$0.12 \\ 0.12$	65.88	1.24	1.31 1.32	188.34 <sup>-</sup> 187.15	1.19	$0.27 \\ 0.28$		0.63	2.17 2.18
218	43.71	269.03	0.12	64.65	1.23	1.34	185.96	1.19	0.28	15.13	0.61	2.19
219	0.22	0.86	0.12	63.42	I.23 I.22		184.76	I.20 I.20	0.29	14.53	0.60	2.21
220 221	43.28 -0.22	267.32 266.44 — 0.88	0.11	62.20	-1.21		183.56	-1.21	0.29	13.95	-0.57	2.22
222	49.84	265.55	0.11	60.99 $59.80$	1.19		182.35 T 181.14	1.21	0.30 0.31	13.38 12.82	0.56	2.23
223	42.62	264.65 0.90	0.11	58.61	1.19	1.41	179.92	I.22	0.31	12.82	0.55	2.26
224	42.40	263.73 0.92 0.93	0.11	57.43	1.17	1.43	178.69	1.23	0.33	11.73	0.54	2.27
225 226		262.80 261.85 —0.95	0.11	$\frac{56.26}{55.10}$		1.44	177.46		0.34	11.21	3100	2.29
227	41.71 0.23 9	260.89 0.96	0.11	55.10 T	1.14		176.22 - 174.97	1.25	0.34	10.10	0.50	2.30
228	41.48 0.23	259.92 0.97	0.11	52.82	1.14	1.48	173.72	1.25	0.35	$10.20 \\ 9.72$	0.48	2.31
229	0.24	258.94 0.98	0.11	51.69	1.13	1.50	172.46	1.26	0.37	9.25	0.47	2.34
230 231	41.00	257.94 256.93 —1.01	0.11	50.57		1.51	171.19		0.38	8.79		2.35
232	40.52 0.24 2	255.92 1.01	0.11	49.46 - 48.37	1.09		169.92 - 168.65	1.27	0.39	8.35 <sup>-</sup> 7.92	0.44	2.36 2.37
233	40.28 0.24 2	254.89 1.03	0.11	47.28	1.09	1.55	167.37	1.28	0.40	7.50	0.42	2.37
234	0.25	253.85 1.04	0.11	46.20	1.08		166.09	1.28	0.42	7.09	0.41	2.39
235 236	39.78	252.79 251 79 —1.07	0.11	45.13	-1.05		164.80		0.42	6.70		2.41
237	39.28 0.25 9	250 64 1.08	0.11	44.08	1.03		1000.01	1.29	0.43	6.32	0.36	2.42
233	39.03	249.55 1.09	0.12	42.02	1.03	1.63	160.92	1.30	0.44	5.96 5.61	0.35	2.43
259	0.26	248.45 1.10	0.12	41.00	I.02		159.62	1.30	0.46	5.27	0.34	2.45
240	38.51	247.33	0.12	39.98		1.66	158.31	3-	0.47	4.95	0.32	2.46
									-		-	

				TABI	LE IX,	Arg. 2	.—Cont	tinued.				
	Arg.	(v.s.3)	(v.c.3)	(v.s.4)	(v.c.4)	(p.c.0)	(ρ.8.1)	(p.c.1)	(p.s.2)	(p.c.2)	(p.s.3)	(p.c.3)
	180 181 182 183	10.01 9.93 9.85 9.78	0.33 0.34 0.35 0.36	0.62 0.62 0.61 0.61	0.71 0.72 0.73 0.75	611 604 598 591	1855 1869 1882 1895	2810 2807 2804 2801	190 188 186 184	178 180 183 185	72 71 70 69	28 28 28 28
	184 185 186 187 188 189	9.70 9.63 9.55 9.47 9.40 9.33	0.37 0.38 0.39 0.41 0.42 0.44	0.61 0.60 0.60 0.60 0.60 0.59	0.76 0.77 0.78 0.79 0.80 0.81	584 577 571 564 557 551	1908 1921 1935 1948 1961 1974	2798 2794 2791 2787 2783 2779	182 180 178 176 174 172	190 192 195 197 200	68 67 66 65 64 63	28 29 29 29 29 29
	190 191 192 193 194	9.26 9.19 9.12 9.05 8.98	0.45 0.47 0.50 0.52 0.54	0.59 0.59 0.59 0.59 0.59	0.83 0.84 0.85 0.86 0.87	544 538 531 525 519	1987 2000 2013 2025 2038	2775 2771 2766 2762 2757	171 169 167 165 163	202 205 207 210 212	62 61 60 59 58	30 30 30 31 31
	195 196 197 198 199	8.91 8.84 8.78 8.71 8.65	0.56 0.59 0.61 0.64 0.66	0.59 0.59 0.59 0.59 0.59	0.88 0.90 0.91 0.92 0.93	512 506 500 494 488	2051 2064 2076 2089 2101	2752 2747 2742 2737 2731	161 159 157 156 154	215 218 220 223 225	57 56 55 54 53	32 32 32 33 33
	200 201 202 203 204 205	8.59 8.53 8.47 8.41 8.36	0.69 0.72 0.75 0.78 0.81	0.59 0.59 0.59 0.59 0.60	0.94 0.95 0.97 0.98 0.99	482 476 470 464 459	2113 2126 2138 2150 2162	2726 2720 2714 2708 2702	152 151 150 148 147	228 231 233 236 239	52 51 50 49 48	34 35 35 36
	206 207 208 209 210	8.30 8.25 8.19 8.14 8.08 8.03	0.84 0.87 0.90 0.93 0.96	0.60 0.60 0.61 0.61	1.00 1.01 1.02 1.03 1.04	453 447 441 436 430	2174 2186 2198 2210 2222	2695 2689 2682 2675 2668	146 144 142 141 140	242 244 247 250 253 256	47 47 46 45 44 43	36 37 37 38 39
	211 - 212 - 213 - 214 - 215	7.98 7.93 7.88 7.84 7.79	1.00 1.03 1.06 1.10 1.13	0.62 0.62 0.63 0.63 0.63	1.05 1.06 1.07 1.08 1.09	425 419 413 408 402 397	2234 2245 2257 2268 2280 2291	2661 2654 2646 2639 2631 2624	138 137 135 134 133	259 262 265 268 271	43 42 41 40 39	40 41 42 43
	216 217 218 219 220	7.74 7.70 7.65 7.61	1.17 1.21 1.24 1.28 1.32	0.64 0.65 0.66 0.66	1.10 1.11 1.12 1.13 1.14	392 386 380 375	2302 2313 2324 2335 2346	2616 2608 2600 2592 2584	130 129 128 127	274 277 280 283 286	39 38 37 36	44 44 45 46
	221 222 223 224 225	7.53 7.49 7.45 7.41 7.38	1.39 1.43 1.46 1.50	0.68 0.69 0.69 0.70	1.15 1.16 1.17 1.18 1.19	364 359 354 349	2357 2357 2367 2378 2389	2575 2567 2558 2550 2541	125 125 124 123	289 292 295 298	35 34 33 32 32	47 47 48 49 50
-	226 227 228 229 230	7.34 7.31 7.28 7.25	1.54 1.58 1.62 1.66 1.70	0.71 0.72 0.73 0.74	1.20 1.21 1.22 1.23 1.24	339 334 329 324 319	2409 2420 2430 2440 2450	2532 2523 2513 2504 2494	121 121 120 119	304 307 310 313	31 30 30 29 28	50 51 52 53
	231 232 233 234 235	7.19 7.17 7.14 7.11	1.74 1.78 1.81 1.85 1.89	0.75 0.76 0.77 0.78 0.79	1.24 1.25 1.25 1.26	314 310 305 300 296	2450 2460 2470 2480 2489 2499	2484 2484 2474 2464 2454	118 117 116 116	318 321 324 327 330	28 27 27 26 25	54 55 56 57 58
	236 237 238 239 240	7.07 7.05 7.03 7.01 6.99	1.97 2.00 2.04 2.08 2.12	0.80 0.81 0.82 0.83	1.27 1.28 1.28 1.29 1.30	291 287 283 278	2508 2518 2527 2536 2545	2433 2423 2412 2401 2390	114 114 113 113	333 336 339 342	25 24 23 22	59 60 61 62 63
1		21 July		0.04	1.00	217	2010	2000	1.0	0.20		

31 July, 1873.

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							ntinued.			1		
Arg.	(v.c.0) Diff.	(v.s.1) Diff.	Sec.var.	(v.c.1)	Diff.	Sec.var.	(v.s.2)	Diff.	Sec.var.	(v.c.2)	Diff.	Sec.var.
	" "	" "	"	"	"	"	"-	"	"	"	"	"
240	38.510.26	247.33 246.20—1.13	$0.12 \\ 0.12$	39.98 38.98		1.66	$\begin{vmatrix} 158.31 \\ 157.00 \end{vmatrix}$	_1.31	0.47	4.95		2.46
241 242	37 99 0.26	245.06 1.14	0.19	38.00	0.98	1.69	155.69	1.31	0.49	4.64 4.34	0.30	2.41
243	37.73	243.91	0.13	37.03	0.97	1.70	154.37	1.32	0.50	4.06	0.28	2.49
244	37.46 0.27	242.75 1.18		36.07	0.95		153.05	I.32	0.51	3.79	0.27	2.00
245	37.20	241.57	0.13	35.12	_0.93	1.73	151.73		0.53	3.54	0.24	2.51
246	36.93 0.27	240.39 I.19 239.20 I.19	17. 10	34.19 33.27	0.92	1.14	150.40 149.07	1.33		3.30	0.23	2.52
247 248	36.39	237.99 1.21	0.14	32.36	0.91	1 76	147.74	1.33	0.56	3.07 2.86	0.21	2 33
249	36.12 0.27	236.77 1.22	0.14	31.46	0.90	1 70	146.41	1.33	0.57	2.66	0.20	9 55
250	35.85	235.54	0.14	30.57	_0.87	1 70	145.07		0.58	2.48		0.50
251	35.58 -0.27	234.30 -1.24	0.14	29.70	0.86	1.80	143.73	—1.34 1.34	0.59	2.31	-0.17 0.15	2.57
252 253	35.31 0.28	233.05		28.84 27.99	0.85	1.82	142.39 141.05	1.34	0.00	2.16	0.14	2.58
254	34.75 0.28	990 54 1.20	0.18	27.15	0.84	1 05	139.71	1.34	$0.61 \\ 0.62$	$ \begin{array}{c c} 2.02 \\ 1.89 \end{array} $	0.13	
255	34 47	229.26	0.16	00 22		1 00	138.36	1.35	0.64	1.78	0.11	2.61
256	34.19 -0.28	227.98 -1.28	0.16	25.52	0.81	1.88	137.01	-1.35	0.65	1.68	-0.10	2 61
257	33.91 0.28	226.68 I.30 225.37 I.31	0.1	24.73	0.79	1.89	135.66	1.35	0.66	1.60	0.08	2.62
258 259	33.63 0.29 33.34 0.29	225.37 1.31 224.06 1.31	0.17 0.18	23.95 23.18	0.77	1.01	134.31 132.96	1.35	0.67	1.53 1.47	0.06	2.63
	33.06	222.74	0.18		0.75			1.35	0.00		0.04	
260 261	32.78-0.28	221.41 -1.33	0.18	22.43 21.69	-0.74		131.61 130.26	<b>—1.35</b>	$0.69 \\ 0.70$	1.43	-0.03	2.65 2.66
262	32.49 0.29	220.07 1.34	0.19	20.97	0.72	1 97	128.90	1.30	0.71	1 20	-0.01	0 67
263	02.21	218.72 1.35 217.36 1.36	0.19	20.26	0.71	1.00	127.55	1.35	0.73	1.40	+0.01	
264	0.29	1.37	0.20	19.56	0.68	1.99	126.20	1.35	0.74	1.42	0.03	2.68
265 266	31.630.29	$\begin{vmatrix} 215.99 \\ 214.62 - 1.37 \end{vmatrix}$	$\begin{array}{c} 0.20 \\ 0.21 \end{array}$	18.88 18.21	_0.67	2.01	124.85	_1.35	0.75	1.45	+0.05	2.69
267	31 05 0.29	213.24 1.38	0.21	17.56	0.65		123.50 122.14	1.36	$0.76 \\ 0.77$	1.50 1.56	0.06	$2.70 \\ 2.71$
268	30.76	211.85 1.39	0.22	16.92	0.64	0.04	120.79	1.35	0.79	1.63	0.07	2.71
269	30.47 0.29	210.45 1.40	0.22	16.29	0.61		119.44	1.35	0.80	1.72	0.09	2.72
270	30.18	209 05	0.23	15.68	_0.60	2.07	118.09	-1.35	0.81	1.82	+0.12	2.73
271 272	29.88 0.29	207.64 —1.41 206.22 1.42	$\begin{array}{c c} 0.24 \\ 0.24 \end{array}$	15.08 14.50	0.58	2.08	116.74	1.35	0.82	1.04	0.13	2.74
273	29.29 0.30	204.79 1.43	0.25	13.94	0.56	2.10	115.39 $114.04$	1.35	0.84 0.85	$\frac{2.07}{2.21}$	0.14	2.74 2.75
274	29.00 0.29	203.36 1.43	0.25	13.39	0.55	0 10	112.70	1.34	0.87	2.37	0.16	2.75
275	00 74	201 92	0.26	12.85		0 11	111.35	1.35	0.88	2.55	. 0.10	
276	28.41 —0.30 28.41 —0.29	200.48 — 1.44 199.03 — 1.45	0.27	12,00	-0.52 0.50	2.15	110.01	1.34	0.89	2.74	+0.19	
277 278	97 99 0.29	197 57 1.46	$0.27 \\ 0.28$	11.83 11.34	0.49	2.17 2.18	108.67	1.34	0.91	2.95	0.22	2.77
279	27 54 0.29	196.11 1.46	0.28	10.86	0.48		107.33 105.99	1.34	$0.92 \\ 0.94$	3.17 3.40	0.23	2.78 2.78
280	27.25	194.64	0.29	10.40	0.46	2.21	104.66	1.33	0.95	9.05	0.25	
281	26.95 -0.30	193.17 -1.47	0.30	9.95	-0.45		103.33	-1.33	0.96	$\frac{3.65}{3.91}$	+0.26	$   \begin{array}{c c}     2.79 \\     2.79   \end{array} $
282	26.00 0.30	191.69 1.48 190.20 1.49	0.31	9.52	0.43	2.23	102.00	1.33	0.98	4.19	0.28	2.80
283 284	26.07 0.29	199 71 1.49	0.32	9.10 8.70	0.40	2.24 2.25	100.67	1.33	0.99	4.48	0.30	2.80
285	0.29	187.22	0.34	8.31	0.39		99.34	1.32	1.01	4.78	0.32	2.81
286	25.48 -0.30	185.72-1.50	0.34	8.31 7.94	-0.37	2.27 2.28	98.02 96.70	1.32	1.02	5.10 5.43	-0.33	2.81
287	25.19 0.29	184.21 1.51	0.35	7.59	0.35	2.29	95.39	1.31	1.05	5.78	0.35	2.82 2.82
288 289	0 20	182.70 I.51 181.19 I.51	0.36	7.25	0.34	2.30	94.08	1.31	1.06	6.14	0.36	2.83
	0.29	1.52	0.37	6.93	0.30	2.31	92.77	1.31	1.08	6.51	0.37	2.83
290 291	24.02 -0.29	179.67 $178.15$ $-1.52$	0.38	6.63 6.34		2.32	91.47	-1.30	1.09	6.90	-0.40	2.84
292	23.73	176.63 1.52	0.40	6.07	0.27	2.33	90.17 <sup>-</sup> 88.87	1.30	1.10	7.30 7 7.72	0.42	2.84 2.85
293	09 15 0.29	175.10 1.53 173.57 1.53	0.41	5.81	0.26	2.36	87.58	1.29	1.13	8.15	0.43	2.85
294	23.13 0.29	1.53	0.42	5.57	0.23	2.37	86.29	1.29	1.15	8.59	3.44	2.86
295 296	99 57 -0.29	172.04 $179.50$ $-1.54$	0.43	5.34	-0.21	2.38	85.01		1.16	9.05		2.86
297	00 00 0.20	168.96 I.54	0.43	5.13 <del>-</del> 4.93	0.20	$\begin{array}{c c} 2.39 \\ 2.40 \end{array}$	83.74	1.27	1.17	0.02	0.49	2.86
298	22.00 0.29	167.42 1.54	0.45	4.75	0.18	2.40	82.47 81.20	1.27	1.19	10.01 10.51	0.50	2.87
299	21.11 0.29	165.88 I.54 I.55	0.46	4.59	0.16	2.43	79.93	1.27	1.22	11.02	0.51	2.88
300	21.42	164.33	0.47	4.44	-3	2.44	78.67	1.20	1.23	11.55	0.53	2.88
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[				TABI	Æ 1X,	Arg. 2	.—Cont	inucd.				
-	Arg.	(v.s.3)	(v.c.3)	(v.s.4)	(v.c.4)	(p.c.0)	(p.s.1)	(p.c.1)	(p.s.2)	(p.c.2)	(p.8.3)	(p.c.3)
	240 241 242 243	6.99 6.97 6.96 6.94	2.12 2.16 2.20 2.24	0.84 0.85 0.86 0.87	1.30 1.31 1.31 1.31	274 270 265 261	2545 2554 2562 2571	2390 2379 2368 2357	113 113 113 112	345 348 350 353	21 21 20 19	63 64 65 66
	244 245 246	6.92 6.90 6.88	2.24 2.28 2.31 2.35	0.88 0.90 0.91	1.31 1.32 1.32	257 253 249	2579 2587 2595	2346 2384 2822	112 112 112	356 359 362	19 18 18	67 68 69
	247 248 249	6.87 6.85 6.84	2.38 2.42 2.45	0.92 0.93 0.94	1.32 1.32 1.33	245 242 238	2603 2611 2618	2311 2299 2287 2275	112 112 111	365 368 371 374	17 16 16	70 72 73
	250 251 252 253 254	6.83 6.82 6.82 6.81 6.80	2.48 2.52 2.55 2.55 2.61	0.95 0.96 0.97 0.98 0.99	1.33 1.33 1.33 1.34	234 230 227 223 219	2626 2633 2641 2648 2656	2215 2263 2251 2239 2226	111 111 111 111 111	377 380 383 386	15 14 14 13	75 76 77 78
	255 256 257 258 259	6.79 6.79 6.78 6.78 6.77	2.64 2.67 2.70 2.73 2.76	1.00 1.02 1.03 1.04 1.05	1.34 1.34 1.34 1.34	215 212 208 204 201	2663 2670 2677 2684 2691	2214 2201 2189 2176 2164	111 111 112 112 112	389 392 395 898 401	13 13 12 12 12	79 80 82 83 84
	260 261 262 263 264	6.77 6.77 6.77 6.77 6.77	2.79 2.82 2.85 2.88 2.90	1.06 1.07 1.09 1.10 1.11	1.34 1.34 1.33 1.33	198 195 192 189 186	2698 2704 2711 2717 2723	2151 2138 2125 2112 2098	112 112 113 113 113	404 407 410 413 416	11 11 11 11 11	85 86 87 89 90
	265 266 267 268 269	6.77 6.77 6.77 6.77 6.77	2.93 2.95 2.98 3.00 3.03	1.12 1.13 1.14 1.15 1.16	1.33 1.32 1.32 1.32 1.32	183 180 177 174 172	2729 2735 2740 2745 2751	2085 2072 2058 2045 2031	114 114 115 115 116	419 422 425 427 430	11 11 11 11 11	91 92 93 94 96
	270 271 272 273 274	6.77 6.77 6.77 6.78 6.78	3.05 3.07 3.09 3.11 3.13	1.17 1.18 1.20 1.21 1.22	1.31 1.31 1.31 1.30 1.30	169 166 164 161 159	2756 2761 2766 2771 2776	2018 2004 1990 1977 1963	116 117 117 118 119	433 436 439 442 444	11 11 10 10 10	97 98 99 100 102
	275 276 277 278 279	6.78 6.79 6.79 6.80 6.81	3.15 3.17 3.19 3.20 3.22	1.23 1.24 1.25 1.26 1.27	1.29 1.28 1.28 1.27 1.27	156 154 151 149 146	2781 2785 2790 2794 2798	1949 1935 1921 1907 1892	119 120 121 121 121 122	447 450 452 455 457	10 10 10 10 10	103 104 105 106 107
	280 281 282 283 284	6.81 6.82 6.83 6.83 6.84	3.23 3.25 3.26 3.27 3.28	1.28 1.28 1.29 1.30 1.31	1.26 1.25 1.25 1.24 1.23	144 142 139 137 135	2802 2806 2809 2813 2816	1878 1864 1849 1835 1820	123 124 124 125 126	460 463 465 468 471	10 10 10 10 11	108 110 111 112 113
	285 286 287 288 289	6.84 6.85 6.85 6.86 6.86	3.29 3.30 3.31 3.32 3.32	1.32 1.33 1.34 1.34 1.35	1.22 1.22 1.21 1.20 1.19	133 131 129 127 126	2819 2822 2825 2828 2830	1805 1791 1776 1761 1746	127 127 128 129 130	474 476 479 482 484	11 11 11 11 11	115 116 117 118 120
	290 291 292 293 294	6.87 6.88 6.88 6.89 6.89	3.33 3.33 3.34 3.34 3.35	1.36 1.37 1.38 1.38 1.39	1.18 1.17 1.16 1.15 1.14	124 123 121 119 118	2833 2835 2837 2838 2840	1731 1716 1702 1686 1671	131 132 133 134 136	487 490 492 495 497	12 12 12 13 13	121 122 123 125 126
	295 296 297 298	6.90 6.90 6.90 6.91	3.35 3.35 3.35 3.35	1.40 1.40 1.41 1.42	1.13 1.12 1.11 1.10 1.09	116 115 114 112 111	2841 2843 2844 2845 2847	1656 1641 1626 1611 1596	137 138 139 141 142	500 503 505 508 510	13 13 14 14 14	127 128 130 131 132
-	299 300	6.91	3.35	1.42	1.08	1110	2848	1581	143	512	15	133

1.   1.   1.   1.   1.   1.   1.   1.					ŢABL	E IX,	A RG.	2.—Con	tinued.					
14.2		Arg.	(v.c.0) Diff.	(v.s.1) Diff. S	Sec.var.	(v.c.1)	Diff.	Sec.var.	(v.s.2)	Diff. S	ec.var.	(v.c.2)	Diff.	Sec.var.
Section   Sect			11 11	" "			"						"	"
900 2 90.85 0.28 161.93 1.55 0.49 4.19 0.12 9.46 76.17 1.5 1.26 19.64 0.55 9.1 9.30 20.07 0.28 165.12 1.55 0.51 4.01 0.28 18.70 1.23 1.29 18.70 0.55 9.1 9.1 9.2 9.1 1.55 0.51 4.01 0.28 18.70 1.23 1.29 18.70 0.55 9.2 9.01 1.25 0.28 165.07 1.56 0.51 4.00 0.28 1.25 0.00 1.25 0.20 18.70 0.25 18.70 0.							_0.13			_1.25		11.55	+0.54	2.88
20.57	ì		21.10	TOM. TO			0.12	2.46		_			0.55	2.88
304 20.29 0.28 158.12 1.59 0.51 4.01 c.c. 2.48 73.70 -3 1.29 13.79 c.59 2.4 3			90 57 0.28	159 68 1.55	0.50	11 11 11 11 11 11 11		2.47	74.93		1.27	13.21		2.89
306   90.01   306   56.57   30.53   3.94   3.95			20 29 0.28		0.51	4.01		7. 4.8	73.70		1.29	13.79	_	4-03
19.46		305	20.01	156.57			_0.0			_I.22		14.38		0 00
19.30   19.30   19.30   19.30   19.5			19.10	155.01				2.00				14.99	0.62	$\frac{2.89}{2.89}$
18.90   0.27   16.034   1.55   0.57   3.84   -0.01   2.53   67.62   1.20   1.35   1.			19.45	151 90 1.56				2.52						2 90
18.63			18 90 0.27	150 34 1.50	0.57	3.84			67.62		1.36	16.88		
311 18.90 0.27 144.07 1.56 0.60 3.93 0.04 2.96 64.05 1.18 1.40 18.00 0.69 2.31 313 17.82 0.27 144.12 1.56 0.61 3.98 0.08 2.57 62.87 1.17 1.42 19.60 0.72 2.53 1.54 1.55 0.21 4.56 1.56 0.62 4.06 0.10 2.58 61.10 1.17 1.42 19.60 0.72 2.53 1.54 1.55 0.21 4.56 1.56 0.62 4.06 0.10 2.58 61.70 1.17 1.42 19.60 0.72 2.53 1.54 1.55 0.61 4.56 1.56 0.65 4.06 0.10 2.58 1.56 1.70 1.17 1.42 19.60 0.72 2.53 1.54 1.55 0.65 4.00 0.10 2.58 1.54 1.55 1.47 2.55 1.55 1.55 1.55 1.55 1.55 1.55 1.55	- 1	310	18.63	140 70		3.85		2.54	66.42					2.90
18-18   18-1	ı		18.30	141.20 1 56				4 2.00	65.23	1.18		10.41		2.00
14			10.00	144 19 1.55				9 57					0.70	2.90
Since   17.28	Н		17 55 0.27	140 50 1.50				2.58					-	2 90
Since   17, 09 - 0.26   130, 14 - 1.56   0.66   4.27 + 0.11   2.59   50.39 - 1.15   1.47   21, 746 + 73   2.48   2.51   0.75   2.52   2.55   0.51   0.58   0.71   0.50   0.50   0.75			17.28	141 00	0.64			2.59	60.54		1.45	21.03		2 91
18		316	17.02 -0.26	139.44-1.56	0.65	4.27		2.59	59.39		1.47	21.76	+0.73	2.91
10.28			10.10	101.00 T CC				4.00		_				#. U L
15.97			10.40	134.77 1.56			0.10	2.62						4.01
Second Color			0.20	1.55		1 00		9.69		1.12		24 82	•	2 91
322         16.46			15.71-0.26	131.67 -1.55	0.70	5.08	+0.19	2.64	53.74	-1.11		25.62	+0.80	2.91
324   14.96			15.46 0.25	100.12				4.00			-			4.01
12.5   14.71			10.21					2.00						$2.90 \\ 2.90$
326	н		0.25	1.54		0.00		9.67		1.08				2.00
327			14.47 -0.24	123.94 -1.54		6.27	+0.27	2.68	48.30	-1.07		29.77	+0.85	2.90
13.28	1	327	14.23 0.24	122.11	0.77	6.56	0.20	2.69	47.23	1.07	1.63	30.63	0.86	2.90
330   13.51   0.24   117.82   1.53   0.81   7.52   0.84   7.57   0.85   7.57   0.85   116.30   1.67   33.30   13.28   0.23   116.30   1.52   0.84   8.24   0.37   2.72   43.07   1.70   35.13   0.92   2.8   33.31   12.81   0.23   113.26   1.52   0.85   8.62   0.38   2.73   41.06   1.00   1.70   35.13   0.92   2.8   33.31   12.81   0.23   113.26   1.52   0.85   8.62   0.38   2.73   41.06   1.00   1.71   36.06   0.93   2.8   33.31   12.81   0.23   113.26   1.52   0.85   8.62   0.38   2.73   41.06   1.00   1.71   36.06   0.93   2.8   33.31   11.31   0.22   105.72   1.50   0.88   9.44   0.42   2.75   38.10   0.99   1.74   37.97   2.8   33.31   11.91   0.22   105.73   1.49   0.91   10.78   0.42   2.75   38.10   0.95   1.78   40.89   0.98   2.8   33.31   11.05   0.22   104.24   1.49   0.93   11.26   0.49   2.77   36.19   0.95   1.78   40.89   0.98   2.8   34.30   11.05   0.21   101.27   1.48   0.95   12.26   0.49   0.94   1.05   0.94   1.05   0.94   1.07   0.95   1.84   44.95   1.00   2.8   34.30   1.04   0.20   98.33   1.47   0.98   13.33   0.54   2.79   31.57   0.99   1.84   44.95   1.00   2.8   34.41   0.05   0.19   98.35   1.47   0.98   13.33   0.54   2.79   31.57   0.99   1.84   44.95   1.00   2.8   34.9   4.95   0.94   1.05   0.94   1.05   0.94   1.05   0.94   1.05   0.94   1.05   0.94   1.05   0.94   1.05   0.94   1.05   0.94   1.05   0.94   1.05   0.94   1.05   0.94   1.05   0.94   0.94   1.05   0.94   0.	H		10.00	120.00				2.00						2.00
331			0.24	1.53				3 2.10					,	2.00
332							+0.35		44.10	-1.03		33.30	+0.91	2.89
12.58			13.04 0.24	114.78 1.52				2.72		1.01			0.92	2.89
335			12.01	110.40 T F2		1	-	4.10						20.00
336	d		0.23	1.51			0.42	2.14						2.88
11.91   0.22   107.22   107.23   0.90   10.32   0.745   2.76   37.14   0.90   1.77   39.91   0.97   2.8   33.9   11.47   0.22   104.24   1.49   0.93   11.26   0.49   2.77   35.24   0.95   1.80   41.89   1.00   2.8   1.01   10.27   11.05   0.49   1.75   0.49   2.77   35.24   0.95   1.80   41.89   1.00   2.8   1.01   10.27   11.05   0.49   2.78   35.24   0.95   1.80   41.89   1.00   2.8   1.01   10.27   10.27   1.48   0.95   1.26   0.49   2.77   35.24   0.95   1.80   41.89   1.00   2.8   1.01   10.27   1.48   0.95   1.26   0.49   2.78   35.24   0.95   1.80   41.89   1.00   2.8   1.01   10.27   1.48   0.95   1.26   0.49   2.78   35.24   0.95   1.80   41.89   1.00   2.8   1.01   10.27   1.48   0.95   1.26   0.49   2.78   35.24   0.95   1.80   41.89   1.00   2.8   1.01   10.27   1.48   0.95   1.26   0.49   2.78   35.24   0.95   1.80   41.89   1.00   2.8   1.01   10.27   1.49   0.93   11.75   0.53   2.79   35.24   0.95   1.80   41.89   1.00   2.8   35.24   0.95   1.80   41.89   1.00   2.8   35.24   0.95   1.80   41.89   1.00   2.8   35.24   0.95   1.80   41.89   1.00   2.8   35.24   0.95   1.80   41.89   1.00   2.8   35.24   0.95   1.80   41.89   1.00   2.8   35.24   0.95   1.80   41.89   1.00   2.8   35.24   0.95   1.80   41.89   1.00   2.8   35.24   0.95   1.80   41.89   1.00   2.8   35.24   0.95   1.80   41.89   1.00   2.8   35.24   0.95   1.80   42.90   1.81   42.90   2.8   35.24   0.95   1.80   1.81   42.90   2.8   35.24   0.95   1.80   1.81   42.90   2.8   35.24   0.95   1.80   1.81   42.90   2.8   35.24   0.95   1.80   1.81   42.90   2.8   33.38   0.99   1.82   43.92   1.00   2.8   33.38   0.99   1.82   43.92   1.00   2.8   33.38   0.99   1.82   43.92   1.00   2.8   33.38   0.99   1.82   43.92   1.00   2.8   33.38   0.99   1.82   43.92   1.00   2.8   33.38   0.99   1.82   43.92   1.00   2.8   33.38   0.99   1.82   43.92   1.00   2.8   33.38   0.99   1.82   43.92   1.00   2.8   33.38   0.99   1.82   43.92   1.00   2.8   33.38   0.99   1.82   43.92   1.00   2.8   33.38   0.99   1.82   43.92   1.00   2.8   33.3			19 19 -0.22	110.23		9.44	+0.43	2.75	39.07	-0.97		37.97	40.97	2.88
11.47			91	11/17/99	0.90	10.32	0.4	2.76	37.14	0.96			0.97	2.88
340			11.09	100.10				4.11						2.01
340       11.26       0.21       102.75       1.48       0.94       11.75       2.78       34.30       0.91       1.81       42.90       2.8         341       11.05       0.21       10.27       1.48       0.95       12.26       -0.53       2.78       33.38       0.92       1.82       43.92       1.02       43.92       1.02       10.02       98.83       1.47       0.97       12.79       0.53       2.79       32.47       0.91       1.84       42.90       2.8         344       10.44       0.20       98.83       1.47       1.00       13.89       0.56       2.80       30.68       0.89       1.87       44.95       1.03       2.8         345       10.24       98.50       1.46       1.00       13.89       0.56       2.80       30.68       0.89       1.87       47.03       1.04       2.8         347       9.85       0.20       1.45       1.02       15.05       0.60       2.81       28.93       0.87       1.90       49.15       1.06       2.8         348       9.66       0.19       91.06       1.44       1.05       16.26       0.61       2.82       27.23       0.85       <			0.21	1.49				2.11						2.01
10.42				101 97 -1.48		11.75	+0.5		34.30			42.90	+1.02	2.87
343         10.64         0.20         98.33         1.47         0.98         13.33         0.54         2.79         31.57         0.90         1.85         45.99         1.04         2.80           345         10.24         95.40         1.01         14.46         2.80         29.80         1.88         48.09         2.80           347         9.85         0.20         92.50         1.45         1.04         15.65         0.60         2.81         28.08         0.85         1.90         49.15         1.06         2.80           348         9.66         0.19         91.06         1.44         1.05         16.26         0.61         2.82         28.08         0.85         1.91         50.22         1.07         2.8           349         9.47         0.19         89.63         1.43         1.07         16.89         0.63         2.82         26.39         0.84         1.94         50.22         1.07         2.8           351         9.10         88.21         1.08         17.54         0.65         2.83         25.57         1.96         23.90         53.50         53.50         52.40         1.10         53.50         54.61         1.11			10.84	99.80 1.47		14.40	0.53	3 2 79		0.91			1.03	2.86
344         10.44         0.20         36.86         1.46         1.00         13.89         0.57         2.80         30.68         0.83         1.87         47.03         10.6         2.80         1.01         14.46         1.00         2.80         29.80         29.80         29.80         48.09         49.15+1.06         2.8         28.93         0.87         1.90         49.15+1.06         2.8         28.93         0.87         1.90         49.15+1.06         2.8         28.93         0.87         1.90         49.15+1.06         2.8         28.93         0.85         1.91         50.22         1.07         2.8         28.93         0.85         1.91         50.22         1.07         2.8         28.93         0.85         1.91         50.22         1.07         2.8         28.93         0.85         1.91         50.22         1.07         2.8		343	10.64 0.20	98.33		13.33		2.79	31.57		1.85	45.99		2.86
345         10.24         95.40         1.01         14.46         -59         2.80         29.80         29.80         48.09         49.15+1.06         2.80           347         9.85         0.20         92.50         1.45         1.04         15.65         0.60         2.81         28.93         -0.87         1.90         49.15+1.06         2.8           348         9.66         0.19         91.06         1.44         1.05         16.26         0.61         2.82         27.23         0.85         1.91         50.22         1.07         2.8           350         9.28         9.63         1.43         1.07         16.89         0.63         2.82         26.39         0.84         1.94         50.22         1.07         2.8           351         9.10         0.18         89.63         1.43         1.07         16.89         0.65         2.82         26.39         0.84         1.94         52.40         1.10         2.8           351         9.10         0.18         86.79         1.42         1.09         18.20         40.66         2.83         25.57         1.96         53.50         53.50         54.61         1.11         2.8         55.73 <th></th> <th></th> <th>10.44 0.20</th> <th>1.46</th> <th></th> <th></th> <th>0.5</th> <th>7 4.00</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>4.00</th>			10.44 0.20	1.46			0.5	7 4.00						4.00
347         9.85         0.20         92.50         1.45         1.04         15.65         0.60         2.81         28.08         0.85         1.91         50.22         1.07         2.8           349         9.66         0.19         91.06         1.44         1.05         16.26         0.61         2.82         27.23         0.85         1.91         50.22         1.08         2.8           350         9.28         0.19         89.63         1.43         1.07         16.89         0.63         2.82         26.39         0.84         1.94         52.40         1.10         2.8           351         9.10         0.18         86.79         1.42         1.09         18.20         40.66         2.83         25.57         0.82         1.10         25.40         1.10         2.8           352         8.92         0.18         86.79         1.41         1.11         18.88         0.68         2.84         23.97         0.79         1.99         55.73         1.12         2.8           353         8.74         0.18         83.98         1.40         1.12         19.57         0.62         2.84         23.18         0.79         2.00         5							300	2.80		-0.87		48.09		9 95
348         9.66         0.19         91.06         1.44         1.05         16.26         0.01         2.82         27.23         0.85         1.93         51.30         1.08         2.8           350         9.28         89.63         1.43         1.07         16.89         0.65         2.82         26.39         0.84         1.94         52.40         1.10         2.8           351         9.10         88.21         1.08         17.54         2.83         25.57         1.96         53.50         2.8           352         8.92         0.18         86.79         1.42         1.09         18.20         40.66         2.83         24.76         0.81         1.97         54.61         1.11         2.8           353         8.74         0.18         83.98         1.40         1.12         18.88         0.69         2.84         23.97         0.79         1.99         55.73         1.12         2.8           354         8.57         0.17         82.58         1.40         1.14         1.957         0.69         2.84         23.18         0.79         2.00         55.73         1.12         2.8           355         8.40         0.17<			9.85 0.20	92.50 1.45		40.00	0.60	2.81		0.85		50.22	1.07	2.85 2.85
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	i	348	9.66 0.19	91.06 1.44	1.05	16.26		2.82	27.23		1.93	51.30		2.85
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			0.10	1.42				2.02	26.39	0.82	1.94	52.40		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			9.28	88 91		17.54		0 09		- 0-		53.50		284
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			8.93 0.18	85 38 1.41		18.20	0.00	981				55 73	1.12	2.83 2.83
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		353	8.74 0.18	83.98 1.40	1.12	19.57		2.84	23.18	0.79	2.00	56.86		2.82
$ \begin{bmatrix} 355 \\ 356 \\ 357 \\ 8.07 \\ \hline 0.16 \\ \hline 359 \\ \hline 7.75 \\ \hline 0.16 \\ \hline 0.15 \\ \hline \end{bmatrix} \begin{bmatrix} 81.19 \\ 79.81 \\ \hline -1.38 \\ 1.16 \\ 1.16 \\ \hline 21.00 \\ 21.74 \\ \hline +0.74 \\ 2.85 \\ 22.49 \\ \hline 0.75 \\ 2.85 \\ \hline 2.85 \\ 20.16 \\ \hline 0.75 \\ 2.85 \\ \hline 20.16 \\ \hline 0.73 \\ 2.05 \\ \hline 20.16 \\ \hline 0.73 \\ 2.05 \\ \hline 0.73 \\ 2.05 \\ \hline 0.73 \\ 2.05 \\ \hline 0.18 \\ \hline 0.29 \\ \hline 1.15 \\ 2.8 \\ \hline 0.29 \\ \hline 1.16 \\ 2.8 \\ \hline 0.70 \\ 2.85 \\ \hline 19.43 \\ 0.72 \\ 0.70 \\ \hline 0.72 \\ 2.08 \\ \hline 0.73 \\ 2.06 \\ \hline 0.20 \\ \hline 0.16 \\ \hline 0.29 \\ \hline 1.16 \\ 2.8 \\ \hline 0.29 \\ \hline 1.16 \\ 2.8 \\ \hline 0.29 \\ \hline 1.17 \\ 2.7 \\ \hline 0.70 \\ \hline 0.15 \\ \hline 0.18 \\ \hline 0.18 \\ \hline 0.18 \\ \hline 0.18 \\ \hline 0.29 \\ \hline 0.70 \\ \hline 0.70 \\ \hline 0.18 \\ \hline 0.18 \\ \hline 0.70 \\ 0.70 \\ \hline 0.70 \\ $			0.17	1.39	1.14	20.28			22.40	0.78			1.13	2.82
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			8.40	81.19				2.85	21.64			59.14		2.81
358 7.91 0.16 77.07 1.37 1.19 23.25 0.76 2.85 19.43 0.73 2.06 62.62 1.17 2.7	1		8.07 0.16	78 44 1.37		WY. IX		4.00		0.73		60.29	1.16	2.80
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		358	7.91	77.07 1.37	1.19	23.25	0.76	2.85		0.73			1.17	2.80
			0.15		1.21	24,03		2.86						2.79
		360	7.60	74.36	1.22	24.82	ST.		18.01		2.09	64.98		2.78

				TABI	E IX,	Aro. 2	.—Cont	inued.					
1	lrg.	(v.s.3)	(v.c.3)	(v.s.4)	(v.c.4)	(p.c.0)	(p.s.1)	(p.c.1)	(p.s.2)	(p.c.2)	(p.s.3)	(p.c.3)	
-		"	"	11									
	300	6.92	3.35	1.43	1.08	110	2848	1581	143	512	15	133	ŀ
	301	6.92	3.35 3.35	1.43 1.44	1.07	109	2849 2849	1566 1551	144 146	515 517	15 15	134 135	ŀ
	303	6.93	3.34	1.44	1.05	107	2850	1535	147	519	16	137	
	304	6.93	3.34	1.45	1.04	106	2850	1520	149	522	16	138	
	305	6.94	3.34	1.45	1.03	105	2850	1505	150	524	17	139	
	306	6.94	3.33	1.46	1.01	104	2850	1490	152	526	17	140	ŀ
	307	6.94	3.33	1.46	1.00	103	2850	1474	153	528	18	141	ì
	308	6.94	3.32	1.47	0.99	103	2850	1459	154	531	18	142	ı
1	309	6.95	3.31	1.47	0.98	102	2849	1444	156	533	19	143	l
	310	6.95	3.31	1.47	0.96	102	2849	1429	157	535	20	144	ŀ
	311	6.95 6.95	3.30 3.29	1.47 1.48	0.95	101 101	2848 2847	1413 1398	158 160	538 540	20 21	145 146	
	313	6.95	3.28	1.48	0.93	100	2847	1383	162	542	22	147	
	314	6.94	3.27	1.48	0.92	100	2846	1368	163	545	23	148	
	315	6.94	3.26	1.48	0.90	99	2845	1352	165	547	24	149	١
	316	6.94	3.25	1.48	0.89	99	2843	1337	167	549	24	150	
	317	6.94	3.23	1.48	0.88	99	2842	1322	168	551	25	151	
	318	6.93	3.22	1.48	0.86	98	2840	1307	170	554	26	152 153	
	319	6.93	3.21	1.48	0.85	98	2838	1291	171	556	27		ı
	320	6.92	3.20	1.48	0.84	98	2836	1276	173	558	27 28	154 155	l
	321 322	6.92	3.18	1.48	0.83	98 98	2834 2831	1261 1246	175 176	560 562	29	156	ı
	323	6.91	3.15	1.48	0.80	98	2828	1231	178	564	29	157	ı
	324	6.90	3.14	1.48	0.79	99	2825	1216	180	566	30	158	ı
	325	6.89	3.12	1.48	0.77	99	2822	1202	181	568	31	159	ı
	326	6.88	3.11	1.48	0.76	99	2819	1187	183	570	32	159	ı
	327	6.87	3.10	1.47	0.75	100	2815	1172	185	572	33	160	ı
	328	6.86	3.08	1.47	0.74	100	2812	1157	186	573	33	16I 162	ı
	329	6.85	3.06	1.47	0.72	101	2808	1143	188	575			ľ
	330	6.83	3.04	1.46	0.71	101	2804	1128	190	577 579	35	163 164	ı
P	331	6.82 6.81	3.03	1.46	0.70	102	2800 2796	1113 1098	192 193	581	37	165	ı
	333	6.79	2.99	1.45	0.67	103	2792	1084	195	583	38	165	ı
	334	6.77	2.97	1.45	0.66	104	2788	1069	197	585	39	166	١
	335	6.75	2.96	1.44	0.65	105	2784	1054	199	587	40	167	١
	336	6.74	2.94	1.44	0.64	106	2779	1039	201	589	41	168	ı
	337	6.72	2.92	1.43	0.63	107	2775	1025	203	591	42	169	l
	338	6.70	2.90	1.43	0.61	108	2770 2765	1010	204	592 594	43	169 170	ı
	339	6.68									45	171	۱
	340 341	6.66	2.87 2.85	1.42	0.59	110	2760 2755	981 967	208	596 598	46	171	
	342	6.62	2.83	1.40	0.57	112	2750	953	212	599	47	172	۱
	343	6.59	2.81	1.40	0.56	114	2744	938	214	601	48	173	ı
	344	6.57	2.79	1.39	0.55	115	2739	924	217	603	49	173	ı
	345	6.55	2.78	1.38	0.53	116	2733	910	219	605	50	174	ı
	346	6.52	2.76	1.37	0.52	117	2727	896	221	606	51	174	ł
	347	6.50	2.74	1.36	0.51	119	2721 2715	882 868	223 226	608	52 53	176	ł
	348	6.47	2.72 2.70	1.36 1.35	0.50	121 122	2709	855	228	611	54	176	ı
	350	6.41	2.69	1.34	0.48	124	2703	841	230	613	55	177	1
	351	6.37	2.67	1.33	0.45	124	2696	828	232	614	57	177	
-	352	6.34	2.65	1.32	0.46	128	2689	814	235	616	58	178	
	353	6.31	2.64	1.31	0.45	130	2682	801	237	617	59	178	
	354	6.28	2.62	1.30	0.44	132	2675	788	239	619	60	178	
	355	6.24	2.60	1.29	0.43	134	2668	775	241	620	61	179	
	356	6.21	2.59	1.28	0.42	136	2660 2653	762	244	621	62	179	1
	357 358	6.18	2.57	1.26 1.25	0.41	141	2645	736	248	624	64	180	1
	359	6.10	2.54	1.24	0.39	144	2637	723	250	626	65	180	
	360	6.07	2.53	1.23	0.38		2629	710	252	627	67	181	
	000	0.01	2.00	1.20	0.00	1	1						4

		TABI	LE IX, ARG	. 2.— <i>Co</i>	ntinued.			
Arg.	(v.c.0) Diff.	(v.s.1) Diff. See.var.	(v.c.1) Diff.	Sec.var.	(v.s.2) Diff.	Scc. var.	(v.c.2)	Diff. Sec.va
	" "	" " "	" "	"	" "	"	"	" "
360	7.60	$\begin{bmatrix} 74.36 \\ 73.02 \\ \end{bmatrix}$	24.82 25.63 0.8	$\frac{2.86}{2.86}$	18.01 17.33 — 0.68	2.09	64.98 66.17	LI.19 2.78
361 362	7.45 0.15	73.02 1.34 1.23 71.69 1.33 1.25	06 45	- 0 07	16.66 0.67	$2.10 \\ 2.12$	67.37	1.20 2.77
363	7.15 0.15	70.37 1.32 1.26	27 29 0.8	4 2.87	16 00 0.00	2 13	68.58	1.21 2.76
364	7 01 0.14	69 05 1.32 1 28	28.14 0.8	5 9 87	15 35 0.05	2 15	69.79	2.75
365	6.87	67.75 1.29	00 00	0.00	14.71	2.16	71.01	2.74
366	6.74 -0.13	66 46 -1.29 1 31	29.88 +0.8	2.88	14 00 -0.02	2.17	72.23	2.74
367	6 61 0.13	65.18 1.28 1.32	30.78	2.88	13.48 0.60	9.18	73.46	1.23 972
368	6.48 0.13	63.90 1.34	31.69 0.9	2.00	12.88	2.19	74.70	1.24 2.72
369	6.36 0.12	62.63 1.25 1.35	32.61 0.9	2 09	12.29 0.57	2.21	75.95	1.26 2.71
370	6.24	61.38 1.37	99 54	0 00	11.72	2.22	77.21	1.26 2.71
371	6.12 -0.12	60.14 1.23 1.38	34.49 +0.9	6 2.89	1111 0 54	2.23	10.41	T 27 4.10
372	0.00	58.91 T.23 1.40	35.45 0.9 36.42 0.9	2.89	10.00	4.20	79.74	T 27 2.69
373 374	5.89 0.11	57.68 1.23 1.41 56.46 1.22 1.43	37.40 0.9	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10.10 0.51	$\frac{2.26}{2.27}$	81.01 82.28	1.27 2.68 1.27 2.67
	0.10	1.20	1.0	0	0.50			1.20
375 376	5.68 5.57—0.11	55.26 54.07 —1.19 1.44	$\frac{38.40}{39.41} + 1.0$	$\frac{2.89}{2.89}$	$\frac{9.09}{8.60}$ -0.49	2.29 2.30	83.56 84.85	2.66
377	5.47 0.10	52.89 1.18 1.47	40.43	2 2.89	8.12 0.48	2.31	86.14	$\begin{array}{ccc} 1.29 & 2.66 \\ 1.29 & 2.65 \end{array}$
378	5.38 0.09	51.72 1.17 1.48	41.47 1.0	4 2.89	7.66 0.40	2.32	87.43	1.29 2.64
379	5.30 0.08	50.57 1.15 1.50	42.52 1.0	5 2.89	7.21 0.45	2.34	88.73	1.30 2.63
380	5.22	49 49 1 51	43 58	2.80	6.78	2.35	90.04	2.62
381	5.14-0.08	$48.29^{-1.13}$ 1.52	44.65+1.0	7 2.89	6.36 - 0.42	2.36	91.35	-1.31 2.61
382	5.07	47.17 1.12 1.54	45.74	9 2.89	5.96 0.40	2.37	92.67	1.32 2.60
383   384	4.00	40.00	40.04	2.09	0.01	4.00	93.99	1.32 2.59 1.32 9.58
	0.07	44.96 1.09 1.01	1.1	2 2.09	5.19 0.36	2.39	95.31	1.33
385	4.84	43.87 1.07 1.58	$\frac{49.07}{50.20} + 1.1$	2.89	4.83	2.40	96.64	2.57
386 387	2.11	42.80	51.34		4.70	2.42	01.01	T 22 2.01
388	4.71 0.00	41.74 40.69 1.05 1.61	52.50 1.1	2.08	4.15 0.33 3.83 0.32	2.43 2.44	99.30 100.64	1.33 2.56 1.34 2.55
389	4.60 0.05	39 65 1.04 1 64	53 67 I.I	7 9.80	3 59 0.31	2.45	101.98	1.34 2.54
390	4.56	38.63 1.66	54.85	9.80	3.23	2.46	102 22	1.35
391	4.52 -0.04	37.62 -1.01 1.67	56.04 + 1.1	9 2.88	2.96 -0.27	2.47	103.33 104.68	$-1.35$ $\begin{array}{c} 2.53 \\ 2.52 \end{array}$
392	4.48 0.04	36.63 0.99 1.69	57.25	2.88	2.70 0.20	2.48	106.03	2.51
393	4.45 0.03	35.65 0.98 1.70	58.46 I.2	2.87	2.45 0.25	2.49	107.38	1.35 2.50
394	4.41 0.03	34.67 0.96 1.71	59.68 1.2	7. X7	2.22 0.23	2.50	108.74	1.36 2.49
395	4.38	33.71 -0.94 1.73	00 01	0 01.	2.01	2.51	110.10	0 14
396	T.00	02.11	62.15 +1.2 63.40 1.2	4 2.87	1.81 -0.20	2.52	111.46	1.36 2.46
398	4.33 0.02	31.85 0.92 1.75 30.94 0.91 1.76	63.40 1.2 64.67 1.2	, 4.01	1.02 O TH	2.53	112.82	1.36 2.45 1.36 2.44
399	4 30 0.01	20.02 0.91 170	65 95 1.2	8 2.00	1.40 0.16	2.54	114.18 115.55	1.37 2.43
400	4.00	0.09	1.2	0 00	0.15			1.37
401	4.28-0.01	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	67.23 + 1.2 $68.52 + 1.2$	$\frac{2.86}{2.86}$	$\frac{1.14}{1.01}$ -0.13	2.56 2.57	116.92 118.29	$-1.37$ $\begin{array}{c} 2.42 \\ 2.41 \end{array}$
402	4.28	07 40 0.05 1 00	69.82 ***3	2.85	0.90 0.11	2.58	119.66	9 40
403	4.28	26.57	71.13	2.85	0.80	2.59	121.03	1.37 2.39
404	4.28 +0.01	25.73 0.82 1.85	72.45 1.3	3 2.84	0.72 0.08	2.60	122.41	1.38 2.38 1.37 2.38
405	1 00	24.91	73.78	9 84	0.65	2.60	123.78	0.00
406	4.29 +0.01	24.11 0.78 1.88	75.12 + 1.3 76.47 1.3	- 2.04	0.60 -0.05	0 01	125.16	2.35
407 408	4.32	20.00 0 77 1.09	10. TI	6 4.00	0.00	2.02	126.53	7 20 4.04
409	4.34 0.02	91 90 0.76 1.91	77.83	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.53 0.52 0.61	4.00	127.91 $129.28$	1.38 2.33 1.37 2.32
410	0.03	0.74	1.3	7 4.02	0.00			1.37
411	$^{4.39}_{4.42}$ +0.03	21.06 $20.33$ $-0.73$ $1.94$ $1.95$	80.56 $81.94 + 1.3$	$8 \begin{array}{c} 2.82 \\ 2.82 \end{array}$	$0.52 \\ 0.54 + 0.02$	2.65	130.65 132.02	2.31
412	4.46 0.04	19 62 0.71 1 97	83.33	9 2.81	0.54	$\frac{2.66}{2.67}$	133.40	$\begin{array}{ccc}  & 1.37 & 2.30 \\  & 1.38 & 2.29 \end{array}$
413	4.50 0.04	18.93 0.09 1.98	84.73	0 2.81	0.62 0.05	2.67	134.77	1.37 2.27
414	4.54 0.04	18.25 0.67 1.99	86.14	2.80	0.68 0.00	9.68	136.14	1.37 2.26
415	1 # 0	1 to 0 0 0 1	87.55	9 80	0.00	0.00	137 51	2 95
416	4.64 +0.05	16.93 -0.05 2.02	88.97 +1.4	2 2.79	0.85 +0.09	2.70	138.88	-1.37 2.24
417 418	4.70	16.30 2.03	90.39	2 2.79	0.96	2.71	140.25	1.37 2.22
419	4.76 0.06	10.01 0.61 2.04	01.02 T	1 2.10	1.08 0.12	2.11	141.62	1.37 2.21 1.37 2.20
420	4.82 0.06	0.59 2.06	1.4	5	0.15	4.12	142.99	1.36
	4 00	14.47 2.07	94.71	2.77	1.37	2.73	144.35	2.19

				TAB	LE įX,	ARG. 2	.—Con	tinued.				
I	Arg.	(v.s.3)	(v.c.3)	(0.8.4)	(v.c.4)	(p.c.0)	(ρ.ε.1)	(p.c.1)	(ρ.ε.2)	(p.c.2)	(p.s.3)	(p.c.3)
	360 361 362 363 364	6.07 6.02 5.98 5.94 5.90	2.53 2.51 2.50 2.49 2.48	1.23 1.22 1.21 1.20 1.19	0.38 0.38 0.37 0.36 0.35	146 148 151 153 156	2629 2621 2613 2605 2596	710 697 685 672 660	252 254 256 259 261	627 628 629 631 632	67 68 69 70	181 181 182 182 182
	365	5.85	2.46	1.17	0.35	159	2588	647	263	633	72	183
	366	5.81	2.45	1.16	0.34	162	2579	635	265	634	74	183
	367	5.76	2.44	1.15	0.34	164	2570	623	267	635	75	183
	368	5.72	2.44	1.14	0.33	167	2562	610	270	636	76	183
	369	5.67	2.43	1.12	0.32	170	2563	598	272	638	77	184
	370	5.63	2.42	1.11	0.32	173	2544	586	274	639	78	184
	371	5.58	2.41	1.10	0.31	176	2535	574	276	640	79	- 184
	372	5.53	2.41	1.08	0.31	180	2526	562	279	641	80	- 184
	373	5.48	2.40	1.07	0.30	183	2516	550	281	642	81	- 184
	374	5.43	2.39	1.05	0.30	186	2507	539	283	643	82	- 184
	375	5.38	2.39	1.04	0.29	190	2498	528	285	645	83	184
	376	5.33	2.39	1.03	0.29	194	2488	517	288	646	84	184
	377	5.28	2.38	1.01	0.29	197	2479	506	290	647	85	184
	378	5.22	2.38	1.00	0.28	201	2469	495	292	648	86	184
	379	5.17	2.38	0.98	0.28	205	2460	485	294	649	87	184
	380	5.12	2.38	0.97	0.28	208	2450	474	297	650	88	184
	381	5.07	2.38	0.96	0.28	212	2440	463	299	651	89	184
	382	5.01	2.38	0.94	0.27	216	2429	453	302	652	90	184
	383	4.96	2.39	0.93	0.27	220	2419	443	304	653	91	184
	384	4.90	2.39	0.91	0.27	224	2408	433	306	654	92	184
	385	4.84	2.39	0.90	0.27	228	2397	423	309	655	94	184
	386	4.79	2.40	0.88	0.27	232	2386	413	312	656	95	184
	387	4.73	2.40	0.86	0.27	236	2374	404	314	657	96	184
	388	4.67	2.41	0.85	0.27	240	2363	394	317	657	97	183
	389	4.61	2.42	0.84	0.27	245	2351	384	319	658	98	183
	390	4.55	2.43	0.82	0.27	249	2340	375	322	659	99	183
	391	4 49	2.44	0.81	0.27	253	2328	366	324	660	100	183
	392	4.43	2.46	0.79	0.27	258	2316	357	327	661	102	183
	393	4.37	2.47	0.78	0.27	262	2305	348	329	662	103	182
	394	4.31	2.48	0.76	0.27	266	2293	339	332	662	104	182
	395	4.24	2.49	0.75	0.27	271	2281	330	334	663	105	182
	396	4.18	2.51	0.73	0.28	276	2269	322	336	664	106	182
	397	4.12	2.53	0.72	0.28	280	2257	313	339	665	107	182
	398	4.06	2.55	0.70	0.28	285	2245	304	341	666	109	181
	399	4.00	2.57	0.69	0.28	290	2232	296	344	667	110	181
	400 401 402 403 404	3.93 3.87 3.80 3.74 3.68	2.59 2.62 2.64 2.66 2.69	0.67 0.66 0.65 0.63 0.62	0.29 0.29 0.30 0.30 0.31	294 299 304 309 314	2220 2207 2195 2182 2170	288 280 273 265 258	346 348 351 353 355	667 668 669 669	111 112 113 114 115	181 181 180 180 180
	405 406 407 408 409	3.62 3.55 3.49 3.43 3.36	2.72 2.75 2.78 2.81 2.84	0.60 0.59 0.57 0.56 0.55	0.31 0.31 0.32 0.33 0.33	320 325 331 337 342	2157 2144 2131 2119 2106	251 244 237 230 224	358 361 363 365 368	669 669 670 670	116 116 117 118 119	179 179 179 178 178
	410	3.30	2,88	0.53	0.34	348	2093	217	371	670	120	178
	411	3.24	2,92	0.52	0.35	354	2080	211	373	670	121	177
	412	3.17	2,95	0.50	0.36	359	2066	205	376	670	122	177
	413	3.11	2,99	0.49	0.36	365	2053	199	378	671	122	176
	414	3.04	3,03	0.48	0.37	371	2039	193	381	671	123	176
	415	2.98	3.07	0.46	0.38	377	2026	187	382	671	124	175
	416	2.92	3.11	0.45	0.38	383	2012	181	386	671	125	174
	417	2.85	3.15	0.44	0.39	389	1998	176	388	671	126	174
	418	2.79	3.20	0.42	0.40	395	1985	170	391	671	126	173
	419	2.73	3.24	0.41	0.41	401	1971	165	393	672	127	173
	420	2.67	3.29	0.40	0.42	407	1957	160	396	672	128	172

			TABLE IX	, Arg.	2.— <i>Con</i>	ntinued.				
Arg.	(v.c.0) Diff.	(v.s.1) Diff. S	ec.var. (v.c. 1	) Diff.	Sec.var.	(v.s.2) D	iff. Sec.var.	(v.c.2)	Diff. S	Sec. var.
400	" "	14.47	2.07 94.7	1	2.77	1.37	2.73	144.35	"	2.19
420 421	4.88	13.90 -0.57	2.08 96.1	6+1.45	2.76	1.54	2.74	145.72	+1.37	2.18
422 423	5.02 0.07 5.10 0.08	13.35 °.55 12.81 °.54	$ \begin{array}{c cccc} 2.10 & 97.6 \\ 2.11 & 99.0 \end{array} $	Z T AT	2.10	1.72	2.74 0.20 2.75	147.09 148.45	1.36	$\frac{2.16}{2.15}$
424	5.18 0.08	12.28 0.53	2.11 100.5		9.75	2 13	0.21 2.75	149.80	1.35	2.13
425	5.26	11.77	2.14 102.0		O FA	2.35	2.76	151.15	+1.35	2.12
426 427	5.44 0.09	10.80 0.48	$\begin{array}{c cccc} 2.15 & 103.5 \\ 2.17 & 105.0 \end{array}$	$\frac{4}{2}$ + 1.48		2.84	0.25 2 77	152.50 153.84	1.34	2.11 2.09
428	5.53	10.34 0.45	2.18 106.5	0 1.49	2.72	3.11	28 2.78	155.19	1.35	2.08
429	5.63 0.10	0.43	2.20 108.0	1.51	4.64	3.39	0.30 2.18	156.54	1.34	2.06
430 431	5.73 5.83 +0.10	9.46 -0.41	2.21   109.5 2.22   111.0	2+1.21			$0.31  \begin{array}{c} 2.79 \\ 2.79 \end{array}$	157.88 159.22	+1.34	$\frac{2.05}{2.04}$
432	5.94	8.66 0.39	2.23 112.5	3 1.51	2.09	4.00	0.33 2.80 0.34 2.80	160.55	1.33	2.02
433	6.05 6.17 0.12	7 91 0.37	2.24 114.0 2.25 115.5	g 1.52	9.67		0.35 2.80 2.35 2.81	161.88 163.20	1.32 1.32	$\frac{2.01}{1.99}$
435	e 90	7.56	9 97 117 0	a 33	2 66	5.39	2.81	164.52		1.98
436	6.41 +0.12	7.23 -0.33 6.92 0.31	2.28 118.6 2.29 120.1	2+1.53 6 1.54	$2.66 \\ 2.65$		0.38 2.82 0.40 2.82	165.84 167.15	1.31	1.97 1.95
437 438	6.67 0.13	6.62 0.30	2.30 121.7	0 1.54	2.64	6.58	2.83	168.46	1.31	1.94
439	6.80 0.13	6.34 0.28 0.27	2.31 123.2	1.54	2.00	1.00	2.83	169.76	1.30	1.92
440	6.94 7.08+0.14	$\frac{6.07}{5.82}$ -0.25	2.32   124.7 2.33   126.3		$\frac{2.62}{2.61}$	$\frac{7.44}{7.89} + c$	2.84 2.84	171.06 172.35	+1.29	1.91 1.90
442	7.22 0.14	5.59 0.23	2.34 127.8	8 1.55	2.60	8.36	2.85	173.64	I.29 I.29	1.88
443	7.37 0.15 7.52 0.15	5.38 0.21 5.18 0.20	2.36   129.4 2.37   130.9	g 1.55		9 33 0	0.49 2.86	174.93 176.21	1.28	1.87 1.85
445	0.15	5.00	2.38 132.5	1.50	9 57	0.84	9.51	177 49	1.27	1.84
446	7.83+0.10	4.83 -0.17	2.39   134.1	0+1.50	2.57	10.36 +0	2.86	178.75	1.27	1.83
447	8.15 0.16	4.68 0.13	$ \begin{array}{c cccc} 2.40 & 135.6 \\ 2.42 & 137.2 \end{array} $	0 1.56	2.55	11.44	0.55 2.87	180.01 181.26	1.25	1.81 1.80
449	8.31 0.16	4.43 0.12	2.43 138.7		2.54	12 00 C	0.56 0.57 2.88	182.51	I.25 I.24	1.78
450	8.48 8.65 +0.17	4.33	2.44 140.3	$\frac{5}{2} + 1.57$	0.52	12.57	2.88	183.75 184.99	·	1.77
451 452	8 82 0.1/	4 19 0.06	2.45   141.9 2.46   143.4	9 31	2.51	13.76	0.60 2.88	184.99	1.25	1.76 1.74
453	9.00 0.18	4.14 0.05	2.47 145.0	6 1.57	2,50	14.37	62 2.89	187.44	I.22 I.22	1.73
454 455	9.18 o.18 9.36	4.10 0.01	2.48 146.6	1.57			0.64 2.89	188.66 189.87	1.21	1.71
456	9 54 +0.18	4 00 0.00	2.49   148.2 2.50   149.7	7 + 1.57	2.47 2.46	$\frac{15.63}{16.28} + c$	0.65 2.89 6- 2.89	191.07	1.20	1.70 1.69
457 458	9.73 o.19 9.92 o.19	4.11 +0.02 4.14 0.03	2.51 151.3 2.52 152.9	1.57	2.45 2.44	10 05	0.67 2.89 0.68 2.90	192.27 193.46	1.20	1.67
459	10.11 0.19	4.18 0.04	2.53 154.4	0 1.57	9 42	19 29	0.69 2.90 0.70 2.90	194.64	1.18	1.66 1.64
460	30.00	4.25	2.54 156.0		2.42	19.02	2.90	195.81	1.17	1.63
461 462	$\begin{array}{c} 10.30 \\ 10.50 \\ 10.70 \end{array} + 0.20 \\ 0.20 \end{array}$	4 43 0.10	2.55   157.6 2.56   159.1	0 1.57	2.41 2.40	20.45	0.72 2.90	196.98° 198.14	1.16	1.61 1.60
463	10.90 0.20	4.55	2.57 160.7	6 1.57	2.39	21.19	75 2.90	199.29	1.15	1.58
464	0.21	0.15	2.58 162.3	1.56		21.34 C	.77 2.30	200.43	1.13	1.57
465 466	11.31 11.52 +0.21	4.83	2.59 163.8 2.59 165.4	5 + 1.50	2.36 $2.35$	$\frac{22.71}{23.48} + 0$	$0.77 \begin{array}{c} 2.91 \\ 2.91 \end{array}$	201.56 202.68	1.12	1.55 1.53
467	11.73	5.17	2.60   167.0	1 1.50	2.34	24.27	2.91	203.79	1.11	1.52
468 469	12.15 0.21	5.59 0.22	2.61 168.5 2.62 170.1	3 1.56	2.32	25.88	0.81 2.91	204.90 206.00	1.10	1.50
470	12.37	5 89	2 63 171 6	2 1.55	2 31	96 70	0.82	207 09	1.09	1.47
471	12.59 +0.22 12.81 0.22	6.07 +0.25 6.34 0.27	2.64 173.2 2.65 174.7	3 + 1.55	2.30 2.29	27.53 +0	0.84 2.91	208.17	1.08	1.46
473	13.03	6.62 0.28	2.65 176.3	3 1.55	2.27	29.22	0.85 2.90	210.30	1.06	1.43
474	0.23	6.91 0.29	2.66 177.8	1.54		30.03	0.88 2.90	211.36	1.06	1.41
475 476	13.49 13.72+0.23	7.22	2.67 179.4 2.68 180.9	$\frac{1}{5} + 1.54$	9 95	$\frac{30.97}{31.86} + 6$	$0.89 \begin{array}{c} 2.90 \\ 2.90 \end{array}$	212.40 213.43	+1.03	1.40 1.39
477	13.95	7.90 0.35	2.69   182.4	8 1.53	2.23	32.76	2.90	214.45	I.02 I.02	1.37
478 479	14 41 0.23	8 63 0.37	2.69 184.0 2.70 185.5	4 1.53	2 20	34.50	0.92 9 90	215.47 216.48	1.01	1.36 1.34
480	14.65	9.02	2.71 187.0	1.52	2.19	35.52	2.89	217.47	0.99	1.33
			1201.0	1//-	2.10	00.02	2.00	221.71	17.75	1.00

			P1 4 vs 4	42 437							
					ARG. 2						
Arg.	(v.s.3)	(v.c.3)	(0.8.4)		(p.c.0)	(p.s.1)	(p.c.1)	(p.s.2)	(p.c.2)	(p.8.3)	(p.c.3)
420	2.67	3.29	0.40	0.42	407	1957	160	396	672	100	150
421	2.61	3.34	0.39	0.43	413	1943	155	399	672	128 129	172 172
422	2.55	3.39	0.38	0.44	419	1930	150	402	673	129	171
423 424	2.49 2.43	3.44	0.36	0.45	425 431	1916 1903	146 141	405	673 673	130 131	171 171
425	2.37	3.55	0.34	0.47	437	1889	136	410	673	132	170
426	2.31	3.61	0.33	0.49	443	1875	132	413	673	133	170
427	2.25	3.66	0.32	0.50	450	1862	128	416	673	133	169
428 429	2.20 2.14	3.72 3.78	0.31	0.51 0.52	456 463	1848 1834	124 120	418 421	673 673	134 135	169 168
430	2.08	3.84	0.29	0.53	469	1820	117	424	673	136	167
431	2.03	3.90	0.28	0.54	476	1806	114	426	673	136	167
432	1.97	3.96	0.27	0.55	482	1791	111	429	673	137	166
433	1.92	4.03	0.26	0.57	489	1777 1762	108	432	673	138	165
434	1.86	4.10	0.25	0.58	3300	1762	105	434	673	139	165
435 436	1.81 1.76	4.16 4.23	0.24 0.23	0.59	503 510	1748	102 100	437	672 672	139 140	164 163
437	1.70	4.30	0.22	0.62	517.	1719	98	442	672	141	163
438	1.65	4.37	0.22	0.63	524	1704	96	445	671	142	162
439	1.60	4.45	0.21	0.64	531	1690	94	447	671	142	161
440	1.55 1.50	4.59	0.20 0.19	0.66	539 546	1675 1660	92 91	450 453	671 670	143	160 159
442	1.46	4.67	0.13	0.68	553	1645	90	455	670	144	159
443	1.41	4.75	0.18	0.70	560	1631	89	458	669	145	158
444	1.37	4.83	0.17	0.71	567	1616	88	460	669	145	157
445	1.32	4.91	0.17	0.73	574	1601 1586	87	463	669	146 146	156 156
446	1,28 1,24	4.99 5.07	0.16 0.16	0.74 0.75	582 589	1571	87 86	466	668	147	155
448	1.20	5.15	0.15	0.77	596	1557	86	471	667	147	154
449	1.16	5.24	0.14	0.79	603	1542	86	473	667	147	153
450	1.12	5.32	0.14	0.80	610	1527	86	476	667	148	152
451 452	1.08 1.04	5.40 5.49	0.13 0.13	0.82	618 625	1512 1497	87 87	479 481	666	148 149	152 151
453	1.01	5.57	0.12	0.85	633	1483	88	484	665	149	150
454	0.97	5.66	0.12	0.86	640	1468	88	486	665	149	149
455	0.94	5.75	0.12	0.88	648	1453	89	489	664	150	148
456 457	0.91 0.88	5.84 5.94	0.11	0.89	656	1438	90	492	664	150 150	148 147
458	0.85	6.03	0.11	0.92	671	1409	93	497	662	151	146
459	0.82	6.13	0.10	0.94	679	1394	95	499	661	151	145
460	0.80	6.23	0.10	0.95	687	1379	96	502	661	151	144
461	0.77 0.75	6.32	0.10 0.10	0.97	695 703	1364 1349	98 100	505 507	660	151 152	144 143
463	0.73	6.51	0.10	1.00	711	1335	102	510	659	152	142
464	0.71	6.61	0.10	1.02	719	1320	105	512	658	152	142
465	0.69	6.71	0.09	1.03	727	1305	108	515	657	152	141
466	0.68	6.81	0.09	1.05	735	1290 1275	110	517 520	657 656	153 153	140 139
468	0.64	7.01	0.09	1.08	751	1261	116	523	655	153	139
469	0.63	7.11	0.09	1.10	759	1246	119	525	654	154	138
470	0.62	7.21	0.09	1.11	767	1232	123	528	653	154	137
471	0.62	7.31	0.10	1.13	775 784	1217 1203	127	531 533	652 651	154 155	136 136
473	0.60	7.52	0.10	1.16	792	1189	135	536	649	155	135
474	0.60	7.62	0.10	1.18	800	1175	139	539	648	155	134
475	0.60	7.72	0.10	1.19	809	1161	143	542	647	156	133
476	0.60	7.83	0.11	1.21	817 826	1147	148	545 548	646	156 156	133
477	0.60	8.04	0.11	1.23	834	1119	158	551	643	156	131
479	0.61	8.15	0.12	1.25	843	1105	163	551	642	156	130
480	0.61	8.26	0.12	1.27	851	1091	168	556	640	156	130

32 July, 1873.

			TAB	LE IX,	ARG.	2.— <i>Co</i>	ntinued.					
Arg	(v.c.0) Diff.	(v.s.1) Diff.	Sec.var	(v.c.1)	Diff.	Sec.var.	(v.s.2)	Diff.	Sec.var.	(v.c.2)	Diff.	Sec.var.
480	14.65	9.02	2.71	187.06	"	2.19	35.52	"	2.89	217.47	11	1.33
481	14.89 +0.24	9.43 +0.41	2.72	188.57	+1.51	2.18	36.46	十0.94 0.95	2.89	218.46	+0.99	1.39
482 483	15.13 0.24	9.85 0.42	2.72 $2.73$	190.08 191.59	1.51	2.15	37.41 38.37	0.96	2.88	219.44 220.40	0.96	. 130
484	15.61 0.24	10.74 0.45	2.74	193.09	1.50	2 14	39.35	0.98	9.88	221.35	0.95	1.27
485	15.85 16.09 +0.24	11.21	2.74	194.59	_	0 10	40.33	+0.99	2.88	222.29		1.26
486 487	16 33 0.24	12 19 0.50	$2.75 \\ 2.76$	194.59 196.08 197.57		9 10	41.32	1.00	2.88	223.22 224.13	0.91	1.25
488	16.58 0.25	12.71 0.52	2.77	199.05	1.48	2.09	43.33	I.01 I.02	2.87	225.04	0.91	1.22
489	10.00 0.25	0.55	2.77	200.53	1.47	2.01	44.35	1.03	2.87	225.94	0.89	1.20
490 491	17.08 17.33+0.25	13.79 $14.35 + 0.56$	$\frac{2.78}{2.79}$	202.00 203.46	+1.46	$2.06 \\ 2.05$	45.38 46.42	+1.04	2.87 $2.87$	226.83 227.71	+0.88	1.19
492	17.58 0.25	14.93 0.58	2.79	204.92	1.46	2.03	47.46	1.04	2.86	228.58	0.87	1.16
493	17.83 0.25 18.09 0.26	16 13 0.61	$\frac{2.80}{2.80}$	206.37 207.81	1.44	$\frac{2.02}{2.00}$	48.51 49.58	1.07	$\frac{2.86}{2.86}$	229.43 230.27	0.85	1 19
495	18.34	16 75	2.81	209 24	1.43	1.99	50.65	1.07	2.85	931 10	0.83	1 10
496	18.60 +0.26	17.39 +0.64	2.81	210.67	<b>1.43 1.42</b>	1.98	51.73	+1.08	2.85	231.92	+0.82 0.81	1.10
497	18.85 0.25 19.11 0.26	18 71 0.67	$\frac{2.82}{2.82}$	212.09 $213.50$	1.41	1.96 1.95	52.82 53.92	1.10	2.85 2.85	232.73 233.52	0.79	1.09
499	19.36 0.25	19.39 0.68	2.83	214.90	1.40	1.93	55.03	1.11	2.84	234.30	0.78	1.06
500	19.62 19.88+0.26	$\frac{20.09}{20.80}$ +0.71	2.83	216.30 217.69		1.92	56.14 57.26		2.84	235.07		1.04
501 502	20.14 0.20	21.52	2.83 $2.84$	217.69	1.38	1.91 1.89	57.26 58.38	1.12	$\frac{2.83}{2.83}$	235.83 236.58	0.75	1.03
503	20.40 0.26 20.66 0.26	22.26 0.74	2.84	220.44	1.37	1.88	59.52	1.14	2.82	237.31	0.73	1.00
504	20.00 0.26	0.76	2.84	221.81 223.17	1.36	1.86	60.67	1.15	2.82	238.03	0.71	0.99
506	21.18+0.26	24.55 + 0.78	2.85 2.85	224.52	-1.35	1.85 1.84	$\frac{61.82}{62.98}$	+1.16	$\frac{2.81}{2.80}$	238.74 239.44	+0.70	$0.97 \\ 0.96$
507 508	21.44 0.26 21.69 0.25	\$25.34 0.79 26.15 0.81	2.85	225.85 $227.18$	I.33	1.82	64.14	1.16	2.80	240.12	0.68	0.95
509	21.95 0.26	26.13 26.97 0.82 0.84	$\frac{2.85}{2.86}$	228.50	1.32	1.81 1.79	65.31 66.49	1.18	$\begin{bmatrix} 2.79 \\ 2.79 \end{bmatrix}$	240.79 241.45	0.66	$0.94 \\ 0.92$
510	22.21	27.81	2.86	229.81	1.31	1.78	67.68	1.19	2.78	040 10	0.65	0.91
511 512	22.47 +0.26 22.72 0.25	28.66 To.85 29.52 o.86	2.86 2.87	231.11 + 232.39	1.28	1.77 1.75	68.87 70.07	1.19	2.77	242.73	+0.63	0.90
513	22.98 0.26	30.40	2.87	233.67	1.28	1.74	71.28	1.21	2.77 2.76	243.36 $243.98$	0.62	0.88
514	0.25	51.28 0.90	2.87	234.94	1.27	1.72	72.49	I.21 I.22	2.75	244.58	0.60	0.86
515 516	23.49 23.75+0.26	$\frac{32.18}{33.09} + 0.91$	2.88	236.20 237.45	-1.25	1.71	73.71 74.93	-I.22	2.74 2.74	245.16	-0.55	0.84
517	24.00 0.25	34.01	2.88	238.69	I.24 I.23	1.68	76.16	1.23	2.73	245.71 246.26	0.55	0.83
518 519	24.20	25 00 0.95	2.88	239.92 241.13	I.2I	1.66	77.39 78.63	1.23	2.72 2.72	246.80 247.33	0.54	0.81 0.79
520	24 76	0.90	9 80	949 22	1.20	1.63	79.87	1.24	2.71	247.84	0.51	0.78
521	25.02+0.20	37.83 +0.97	2.89	243.52	1.19	1.62	81.12	1.25	2.70	248.34	0.49	0.77
522 523	25 52 0.25	39.82 1.00	2.89	244.70 245.87	1.17	1.60 1.59	82.37 83.62	1.25		248.83 249.30	0.47	0.75
524	25.77 0.25	40.83 1.01	2.89	247.03	1.16	1.57	84.88	1.26		249.76	0.46	0.73
525 526	26.02 26.27 +0.25	41.85 42.88+1.03	2.89	248.18		1.56	86.14	-1.27	2.66	250.21		0.71
527	26.52 0.25	43 92 1.04		249.31 + 250.43	1.12	1.55 1.53	87.41 <sup>†</sup> 88.69	1.28		250.64 <del>1</del> 251.06	0.42	0.70
528	26.76 0.24	44.97 1.05	2.89	251.53	I.10 I.10	1.52	89.97	1.28	2.64	251.47	0.41	0.68
529 530	27.00 0.24	1.08		252.63	1.09	1.50	91.25	1.29		251.86	0.39	0.66
531	27.48 +0.24	47.12 48.21+1.09	2.89	253.72 + 254.79 +	1.07	1 49 1.48	$\frac{92.54}{93.83}$ +	-1.29	2.62 2.61	252.24 252.60	-0.36	0.65 0.64
532 533	27.72 0.24 27.96 0.24	49.31	2.89	255.85	1.06	1.46	95.12	1.29	2.60	252.95	0.35	0.63
534	28 19 0.23	51.53 1.11		256.90 257.93	1.03	1.45	96.42 97.72	1.30		253.29 253.61	0.32	0.62 0.61
535	28.42	52.66	2.88	258 95	1.02	1.42	99.02	1.30	0.50	052.00	0.31	0.60
536 537	28.65 +0.23 28.88 0.23	53.80 +1.14 54.95 1.15	2.88	259.96+	0.99	1.40	100.32+	1.31	2.57	254.22 →	0.28	0.58
538	29.11 0.23	56.11 1.16	2.88	260.95 261.93	0.98		101.63 102 94	1.31		254.50 254.77	0.27	0.57
539	0.22	57.27 1.16	2.88	262.90	0.97	1.36	104.25	1.31		255.02	0.25	0.55
540	29.55	58.45	2.88	263.85		1.34	105.56		2.53	255.26	HT 3	0.54

				TAR	LE IX,	ARG 9	- Cons	tinund			-	
	Arg.	(v.s.3)	(v.c.3)	(v.s.4)					(0.8.2)	(002)	(0.8.3)	(p.c.3)
H		"	"	"	"	(7:010)	(10.17)	(7.0.2)	(10.2)	(9.0.2)	(7.0.0)	(p.c.o)
	480	0.61	8.26	0.11	1.27	851	1091	168	556	640	156	130
	481	0.62	8.36 8.47	0.12	1.28	860	1076	173	559	639	156	129
	483	0.65	8.58	0.13	1.31	868 877	1063	179 184	561 564	637 636	156 156	128 128
	484	0.66	8.69	0.14	1.33	885	1035	190	566	634	156	127
	485	0.67	8.79	0.14	1.35	894	1021	196	569	633	156	126
9	486	0.69	8.90 9.01	0.15 0.15	1.36	902	1007	202	571	632	156	125
	488	0.73	9.11	0.15	1.37	911 919	994 980	208 214	574 576	630 629	156 156	124 124
	489	0.75	9.22	0.17	1.40	927	966	220	579	627	156	123
	490	0.77	9.33	0.17	1.42	936	953	227	581	626	156	122
	491	0.80	9.43 9.54	0.18	1.43	945 954	940 926	234	584	624	156	121
	493	0.85	9.65	0.19	1.44	963	913	241 249	586 589	623 621	156 156	120 120
	494	0 88	9.75	0.20	1.47	972	900	256	591	619	156	119
	495	0.91	9.86	0.21	1.49	981	887	264	594	618	156	118
	496	0.94	9.97	0.22 0.23	1.50 1.51	990	874 861	272 280	596 599	616	156 156	117
1	498	1.02	10.18	0.23	1.53	1008	848	288	601	613	155	116
	499	1.06	10.29	0.24	1.54	1017	835	296	604	611	155	115
1	500	1.10	10.39	0,25	1.55	1026	822	304	606	610	155	115
	501 502	1.14	10.50 10.60	0.26 0.27	1.57	1035 1044	810	312 321	608	608	155 155	114
	503	1.24	10.70	0.21	1.59	1053	785	329	611	606	154	113
	504	1.29	10.81	0.29	1.60	1063	772	338	615	602	154	113
	505	1.34	10.91	0.30	1.62	1072	760	346	617	600	154	112
	506 507	1.39 1.44	11.01 11.12	0.31 0.32	1.63	1081	748	355 364	620	598	154	112
1	508	1.50	11.22	0.33	1.65	1099	724	373	622 624	596 594	154	110
	509	1.56	11.32	0.34	1.66	1108	712	382	626	592	153	110
1	510	1.62	11.42	0.35	1.67	1117	700	391	628	590	153	109
	511 512	1.68	11.52 11.62	0.37	1.68	1126	688 677	401 410	631	588	153 153	109
	513	1.80	11.71	0.39	1.70	1144	666	420	635	585 583	153	108
1	514	1.87	11.81	0.40	1.71	1153	654	430	637	581	153	107
1	515	1.94	11 91	0.41	1.72	1162	643	440	639	578	153	106
1	516 517	2.01 2.08	12.00 12.09	0.42 0.43	1.73	1171	632	450 460	642	576 573	153 152	106
	518	2.16	12.19	0.45	1.75	1189	610	471	646	571	152	105
1	519	2.23	12.28	0.46	1.76	1197	599	481	648	569	152	105
	520	2.31	12.37	0.47	1.77	1206	588	492	650	566	152	104
1	521 522	2.39	12.46 12.55	0.49	1.78	1215 1224	577 567	503	652 654	564	152 151	104
	523	2.55	12.63	0.51	1.79	1233	557	525	656	558	151	103
-	524	2.63	12.72	0.52	1.80	1242	546	536	658	556	151	103
1	525	2.71	12.81	0.54	1.81	1250	536	548	660	553	151	102
	526 527	2.80 2.88	12.89	0.55	1.82	1259	526 517	559 571	662	550 548	151	102
1	528	2.97	13.06	0.58	1.83	1276	507	583	666	545	150	101
	529	3.06	13.14	0.60	1.84	1284	498	595	668	542	150	100
	530	3.15	13.22	0.61	1.85	1293	498	607	670	540	150 150	100 100
-	531 532	3.24	13.30 13.37	0.62	1.85	1301	479	618	672	537	149	99
-	533	3.43	13.45	0.65	1.86	1318	461	642	675	532	149	99
	534	3.53	13.52	0.67	1.87	1327	452	654	677	529	149	98
-	535	3.63	13.59	0.68	1.87	1335	443	666	678 680	527 524	149	98
	537	3. 73	13.66	0.69	1.88	1352	426	690	682	521	148	98
	538	3.93	13.80	0.72	1.89	1360	417	702	683	519	148	97
	539	4.03	13.87	0.74	1.89	1368	409	714	685	516	148	97
-	540	4.13	13.93	0.75	1.90	1376	401	726	686	513	147	97

				TABI	LE IX,	ARG.	2.— <i>Co</i>	ncluded.					
	Arg.	(v.c.0) Diff.	(v.s.1) Diff.	Sec.var	(v.c.1)	Diff.	Sec.var.	(v.s.2) I	)iff. Sec.v	ar. (v.	2.2)	Diff.	Sec.var.
		" "	" "	"	"	- 11	"	"	" "	1	,,	"	"
	540 541	29.55 29.77 +0.22	58.45 59.63+1.18	$\frac{2.88}{2.88}$	263.85 $264.79$	+0.94	1.34	$\frac{105.56}{106.88} +$	1.32 2.5	$\begin{vmatrix} 3 & 255 \\ 2 & 255 \end{vmatrix}$	.26	+0.23	$0.54 \\ 0.53$
	542	29.99 0.22	60.82	2.88	265.71	0.92	1.32	108.19	1.31 2.5	1 255	.70	0.21	0.52
1	543 544	30.21 0.22 30.43	62.02 1.20 63.24 1.22	2.87 $2.87$	$\begin{vmatrix} 266.62 \\ 267.52 \end{vmatrix}$	0.90	1.50		$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			0.20	0.51
١	545	0.21	CA AC 1.22	2.87	000 10	0.88	1 05	110 15	1.32	7 950	95	0.17	0.40
ı	546	30.85 +0.21	65.69 +1.23	2.87	269.27	+0.87	1 00	113.47	1.32 2.4	6 256	.41	+0.16	0.49 0.48
1	547 548	31.06 0.21 31.27 0.21	66.93 1.24 68.18 1.25	2.87	270.12	0.85	1.25	114.00 .	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	5 256	.55	0.14	0.47
1	549	31.47 0.20	69.43 1.25	$\frac{2.86}{2.86}$	270.96 $271.79$	0.83	1.25	117.45	$\begin{array}{cccccccccccccccccccccccccccccccccccc$			0.11	$0.46 \\ 0.45$
1	550	31.67	70.69	2.86	979 60		1 01	110 88	9.4	2 256	.89	0.10	044
I	551 552	01.01	71.96 +1.27 73.23 1.27	2.86	273.40	+0.80 0.78	1.20	120.09	$\begin{bmatrix} 1.32 & 2.4 \\ 2.4 & 2.4 \\ 3.3 & 9.4 \end{bmatrix}$	$ \begin{array}{c c} 1 & 256 \\ 0 & 257 \end{array} $	.987	0.07	
۱	553	32.06 32.25 0.19	74 51 1.20	$2.85 \\ 2.85$	274.18 $274.95$	0.77	1.18 1.17	19974	1.32 2.3			0.06	0.42
ı	554	32.44 0.19	75.80 1.29	2.84	275.70	0.75	1 15	104 07	1.33 2.3	8 257	.15	0.04	0.40
ı	555 556	$\frac{32.63}{32.81}$ +0.18	77.10 + 1.30	2.84 2.84	276.44 277.16		114	$\frac{125.39}{126.71} + 1$	2.3	6 257	18	-0.02	0.40
ı	557	32.99 0.10	79.71 1.31	2.83	277.86	0.70	1.12	128.03	.32 2.3		20	0.00	0.39
ı	558 559	33.17 o.18 33.35 o.18	81.03 1.32 82.35 1.32	2.83	278.55	0.69	1.09	120.00	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3 257.	13	0.03	0.37
ı	560	33.52	1.33	2.82	279.23	0.66		130.61	•34			0.04	0.36
	561	33.69 +0.17	$83.68 \\ 85.01 + 1.33$	$2.82 \\ 2.82$	279.89 280.54	+0.65	1.06	$\frac{132.01}{133.33} + 1$	$\begin{array}{ccc}  & 2.3 \\  & 2.3 \end{array}$			-0.05	0.35
ı	562 563	33.86 O.17 34.03 O.17	86.35 1.34 87.69 1.34	2.81	281.17	0.63	1.03	134.65	.32 2 2	9 257.		0.07	0.33
ı	564	34.19 0.10	90.04 1.35	2.81 2.80	281.78 282.38	0.60		137 98 I	.31 2.2			0.10	0.33   0.32
ı	565	34.35	90.40	2.80	999 97	0.59		138.60	2.2		71	0.11	0.31
ı	566 567	34.51 +0.16 34.67 0.16	91.76 +1.36 93.13 1.37	2.79	283.54	0.55	0.98	139.91	·31 2.2	256.	98	0.12	0.30
	568	34.82 0.15	94.50 1.37	2.79 2.78	284.09 284.63	0.54		141.22 149.54	.32 2.2			0.15	$0.29 \\ 0.29$
1	569	34.97 0.15	95.88 I.38	2.78	285.16	0.53		143 85	·31 2.20	256.		0.16	0.28
	570 571	35.12 35.27 +0.15	97.26 + 1.38 $98.64 + 1.38$	2.77 2.76	285.67 286.16		0.93	145.16	2.19			-0.19	0.27
П	572	35.41	100.03	2.76	286.64	0.40		147 76	.30 2 1			0.20	$0.26 \\ 0.26$
	573 574	25 60 0.14	101.42 1.39 102.82 1.40		287.10 287.55	0.46	0.89	149.05	·29 2.18 ·30 2.18			0.21	0.25
1	575	0.13	1.40	0 71	00 - 00	0.43		190.55	.29		00	0.24	$0.25 \\ 0.24$
ı	576	35.95 0.13	105.62 +1.40	2.73	288.40	-0.42	0.86	152.93 T	.29 2.1	254.	63	-0.26	0.23
	577 578	36.21 0.13	108 44 1.41	2.73	288.80 289.18	0.40	0.83	104.22	·29 2.08 ·28 2.08			0.27	0.23 0.22
	579		109.85 1.41		289.55	0.37		155.50 $156.77$ $1$	·27 2.06			0.29	0.22
	580	36.45	111.26	2.71	289.91		0.79	158 05	2.08		48_	-0.32	0.21
	581 582	36.69	114 10 1.42	2.70 2.69	290.25 <del> </del> 290.57				$\begin{array}{cccccccccccccccccccccccccccccccccccc$		10	0.33	0.21
L	583	36.81	115.52	2.68	290.88	0.31		167 95	.26 2.01	252.	48	0.35	0.20
	584	36.93 0.11	1.43		291.18	0 30	0.75		.26 1.99			0.37	0.19
	585 586	37.15 +0.11	118.38 $119.81 + 1.43$	2.67 2.66	$\frac{291.46}{291.72}$	-0.26	0.73	$\frac{164.37}{165.62} + 1$	.25 1.98			-0.39	0.19
	587	37.26 0.11	121.24 1.43	2.65	291.96	0.24	0.71	166.87	25 1.95	250.	96	0.40	0.18
1	588 589	37.48 0.11	124.11 1.44		292.19 292.41	0.23		100.11	·24 1.94 ·24 1.99			0.41	0.17
	590	37.58	125.54	2.62	292 61	0.20			1.91	_		0.44	0.16
	591 592	37.68 +0.10 37.78 0.10	126.98 +1.44	2.61	292.79	0.17	0.67	171.81 + 1	.23 1.90	249.	24	0.45	0.16
1	593	37.88 0.10	129.85	2.60 2.59	292.96 293.12	0.16			·22 1.88 ·22 1.8			0.47	0.15
	594	37.98 0.10	131.29 1.44	2.58	293.26	0.14		175 46 I	.21 1.88			0.48	0.13
	595 596	38.08 +0.10	132.73 $134.17 + 1.44$	2.58	293.38			176.67	1.8			-0.51	0.14
-	597	38.27	135.61 1.44	2.57 2.56	293.49 <sup>-</sup> 293.58	0.09			.20 1.85 .20 1.85		02	0.52	0.14 0.13
-	598 599	38.36 0.09 38.45 0.09	137.05 1.44 138.50 1.45	2.55	293.66	0.08	0.58	180.26 I	1.80	245.	77	0.53	0.13
1	600	0.09	1.44	2.54	293.73	0.05		101.44	.18	1		0.54	0.12
1	000	38.54	139.94	2.53	293.78		0.56	182.62	1.7	244.	67	1 11	0.12

			TABI	E IX,	ARG. 2	.—Conc	luded.				Legi-
Arg	. (v.s.3)	(v.c.3)	(v.s.4)	(v.c.4)	(p.c.0)	(ρ. ε. 1)	(p.c.1)	(p.s.2)	(p.c.2)	(p.8,3)	(p.c.3
		"	"	"							
54	0 4.13	13.93	0.75	1.90	1376	401	726	686	513	147	97
54		13.99	0.76	1.90	1384	393	738	688	510	147	97
54		14.05	0.78	1.90	1392	386	751	689	507	147	96
54		14.11	0.79	1,90	1400	378	763	691	503	146	96
54	4 4.56	14.17	0.81	1.91	1408	371	776	692	500	146	95
54	5 4.67	14.23	0.83	1.91	1416	363	788	693	497	146	95
54		14.28	0.84	1.91	1424	356	801	695	494	146	95
54		14.34	0.85	1.91	1431	349	813	696	491	146	94
54		14.39	0.87	1.92	1439	343	826	698	487	145	94
54		14.44	0.89	1.92	1446	336	838	699	484	145	94
55	0 5.24	14.49	0.90	1.92	1454	329	851	700	481	145	93
55		14.54	0.92	1.92	1461	323	864	702	478	145	93
55		14.58	0.93	1.92	1468	316	877	703	475	145	93
55		14.63	0.95	1.92	1475	310	890	704	471	144	93
55		14.67	0.96	1.92	1482	304	903	705	468	144	92
						19.00					
55		14.71	0.98	1.92	1489	298	916	706	465	144	92
55		14.75	0.99	1.92	1496	292	929	708	462	144	92
55		14.79	1.01	1.92	1502	287	943	709	458	144	92
55		14.82	1.02	1.92	1509	281	956	710	455	143	92
55	9 6.30	14.85	1,04	1.92	1515	276	970	711	452	143	91
56	0 6.42	14.88	1.05	1.92	1522	270	983	712	449	143	91
56		14.91	1.07	1.92	1528	265	996	713	445	143	91
56		14.93	1.08	1.92	1534	260	1010	714	442	143	91
56		14.96	1.10	1.91	1541	255	1023	715	438	142	91
56		14.99	1.11	1.91	1547	250	1036	716	435	142	90
56	5 7.04	15.01	1.13	1.91	1553	246	1049	716	431	142	90
56		15.01	1.13	1.91	1559	242	1063	717	428	142	90
56		15.05	1.16	1.90	1564	238	1076	717	424	142	90
56		15.06	1.17	1.90	1570	234	1089	717	421	141	90
56		15.08	1.18	1.90	1575	230	1102	718	417	141	89
57		15.09	1.20	1.89	1581	226	1116	718	413	141	89
57		15.09	1.21	1.89	1586	223	1129	718	410	141	89
57		15.10	1.23	1.89	1591	219	1142	718	40G	141	89
57		15.10	1.24	1.88	1596	216	1155	719	403	140	89
57	4 8.16	15.11	1.26	1.88	1601	213	1169	719	399	140	89
57	5 8.29	15.11	1,27	1.87	1605	210	1182	719	395	140	88
57		15,12	1.29	1.86	1610	207	1195	719	392	140	88
57		15.12	1 30				1208	719	388	140	88
57		15.11	1.32	1.85	1618	202	1221	719	385	140	88
57		15.10	1,33	1.84	1622	200	1234	719	381	139	88
			1.34	-	1626	198	1248	719	378	139	88
58 58		15.09 15.08	1.35	1.84	1630	196	1245	719	374	139	87
58		15.08	1.36	1.83	1634	194	1274	719	371	139	87
58		15.04	1.38	1.83	1637	192	1288	719	367	139	87
58		15.04	1.39	1.81	1641	191	1301	719	364	139	87
							0.13	1190,61			
58		15.02	1.40	1.81	1645	189	1315	718	360	139	87
58		.15.00	1.42	1.80	1648	188	1328	718	857	139	87
58		14.98	1.43	1.79	1651	186	1342	718	353	139	87
58		14.96	1.44	1.79	1654	185	1356	717	350	138	86
58	9 10.06	14.93	1.45	1.78	1657	184	1369	717	346	138	86
59	0 10.18	14.91	1.46	1.77	1660	183	1382	717	343	138	86
59		14.88	1,48	1.76	1662	182	1396	716	339	138	86
59		14.85	1,49	1.75	1665	182	1409	716	335	138	86
59		14.81	1.50	1.74	1667	181	1422	716	332	138	86
59		14.78	1.51	1.73	1669	181	1436	715	328	138	85
					1671	181	1448	715	324	138	85
59		14.74	1.52	1.72	1671	181	1445	714	321	138	85
59		14.71	1.53	1.71	1674	181	1474	714	317	137	85
59		14.67	1.55	1.71	1676	181	1487	713	313	137	85
59		14.63	1.56		1677	182	1500	712	310	137	85
59		14.58	1.57	1.69			100				100
	0 11.40	14.53	1.58	1.68	1678	182	1513	711	306	137	85

Γ			V T		TA	BLE 2	, Arc	a. 3.—	ACTIO	N OF	NEPTU	NE.			
	Arg.	(v.c.0)	Diff.	(v.s.1)	Diff.	(v.c.1)	Diff.	(v.s.2	2) Diff	(v.c.	2) Diff.	(v.s.3)	(v.c.3)	(v.s.4)	(v.c.4)
		"	" "	"	"	"	"	"	ii	"	"	"	"	"	"
	0	92.96 92.67	_0.29	0.87 0.98	+0.11	34.22 34.77	+0.55	7.42	_0.06		_0.13	0.80	1.15 1.16	-0.85 $0.86$	-1.13 1.14
	2	92.38	0.29	1.10		35.31	0.54	7.30	0.06	3.70	0.12	0.83	1.18	0.87	1.15
	3	92.07	0.30	1.23	0.15	35.85	0.54	1.40	0.07	0.00		0.84	1.20	0.89	1.16
	4	91.77	0.31	1.38	0.15	36.39	0.53	1.10	0.07	3.41	0.11	0.86	1.22	0.91	1.17
75	5 6	91.46 91.15	-0.31	1.53 1.70	+0.17	36.92 37.44	+0.52	$\begin{vmatrix} 7.09 \\ 7.01 \end{vmatrix}$	_0.08	$\begin{vmatrix} 3.36 \\ 3.25 \end{vmatrix}$		0.88	$\frac{1.23}{1.24}$	-0.93 $0.95$	1.18 1.18
	7	90.84	0.31	1.88	0.18	37.96	0.52	6.92	0.09	3.15	0.10	0.91	1.25	0.97	1.19
	8	90.52	0.32	2.08	0.21	38.48	0.52	6.82	0.10	3.05		0.93	1.26	1.00	1.19
	9	90.19	0.33	2.29	0.22	39.00	0.51	6.72	0.11	2.95	0.09	0.95	1.27	1.02	1.20
	10 11	89.86 89.53	-0.33	$\frac{2.51}{2.75}$	+0.24	39.51 40.02	+0.51	$\begin{vmatrix} 6.61 \\ 6.51 \end{vmatrix}$	-0.10	$2.86 \\ 2.77$		$\begin{bmatrix} 0.97 \\ 1.00 \end{bmatrix}$	1.28 1.28	-1.04 $1.06$	-1.20 $1.19$
1	12	89.18	0.35	2.99	0.24	40.52	0.50	6.40	0.11	2.69	0.08	1.02	1.29	1.08	1.19
	13	88.83	0.35	$3.26 \\ 3.54$	0.27	$41.01 \\ 41.50$	0.49	6.28	0.I2 0.I2	2.61	0.08	1.05	1.29	1.09	1.18
	14	88.47	0.38		0.29		0.49	6.16	0.12	2.54	0.07	1.07	1.29	1.11	1.18
	15	$\frac{88.09}{87.71}$	-0.38	3.83	+0.30	41.99 42.47	Fo.48	$\frac{6.04}{5.91}$	-0.13	2.47 $2.41$	_0.06	$1.09 \\ 1.12$	1.29	-1.12 1.13	-1.17 $1.15$
1	17	87.31	0.40	4.45	0.32	42.94	0.47	5.78	0.13	2.36	0.05	1.14	1.28	1.15	1.13
	18	86.90	0.41	4.78	0.33	43.40	0.46	5.64	0.14	2.31	0.05	1.17	1.27	1.16	1.12
	19	86.49	0.43	5.13	0.36	43.86	0.45	5.50	0.14	2.27	0.04	1.19	1.26	1.17	1.10
	20 21	$\frac{86.06}{85.62}$ $-$	-0.44	5.49	+0.38	44.31 44.74	-0.43	$\frac{5.36}{5.22}$	-0.14	2.23 $2.20$	_0.03	1.21 1.23	1.25 1.23	-1.18 - 1.19	$-1.08 \\ 1.06$
2	22	85.16	0.46	6.26	0.39	45.16	0.42	5.08	0.14	2.18	0.02	1.25	1.22	1.19	1.03
	23	84.69	0.47	6.67	0.41	45.58		4.93	0.15	4.10	0.00	1.27	1.20	1.20	1.00
	24	84.22	0.50	7.09	0.44	45.98	0.40	4.78	0.15	2.16	0.00	1.29	1.19	1.20	0.99
	25 26	$\frac{83.72}{83.22}$	-0.50	7.53	+0.45	46.38 46.77	-0.39	4.63		$\frac{2.16}{2.16}$	0.00	1.31	1.16 -	-1.20 - 1.19	-0.97 $0.95$
2	27	82.70	0.52	8.45	0.47	47.14	0.37	4.33	0.15	2.17	+0.01	1.35	1.12	1.19	0.93
	88	82.17	0.53	8.94	0.50	47.49		4.18		2.19	0.02	1.36	1.10	1.18	0.91
	29	81.62	0.57	9.44	0.51	47.83	0.33	4.02	0.15	2.22	0.04	1.37	1.07	1.17	0.90
	0 1	$\frac{81.05}{80.48}$	-0.57	9.95	1-0.53	48.16 48.47		$\frac{3.87}{3.72}$	-0.15	$\frac{2.26}{2.30}$	+0.04	1.38	1.05	-1.17 - 1.15	-0.89 $0.88$
3	2	79.89	0.59	11.02	0.54	48.76		3.58	0.14	2.35	0.05	1.39	1.00	1.13	0.86
	3	79.29	0.61	11.58	0.57	49.04	0 26	3.43		2.41	0.06	1.40	0.97	1.11	0.85
	4		0.63	12.15	0.58	49.30	0.25	3.28	0.14	2.48	0.07	1.40	0.94	1.09	0.84
	5 6	$\frac{78.05}{77.41}$	0.64	12.73 13.33	F0.60	49.55	-0.22	$\frac{3.14}{3.01}$ -	-0.13	2.55	+0.09	1.40	0.91 -	-1.09 - 1.07	-0.83 0.83
3	7	76.76	0.65	15.74	0.63	49.98	0.21	2 87	0.14	2.73	0.09	1.40	0.85	1.05	0.82
	8	76.10	0.68	14.57	0.64	50.16	0 16	2.74		2.83	0.10	1.39	0.82	1.03	0.82
	9	H / HO	0.69	15.21	0.65	50.32	0.14	2.61	0.12	2.94	0.11	1.38	0.79	0.99	0.81
	0		0.69	15.86 16.52	Ho.66	50.46 50.58	-0.12	$\frac{2.49}{2.38}$	-0.11	$\frac{3.05}{3.17}$	+0.12	1.37	0.76  -0.73  -	-0.99 - 0.97	$-0.81 \\ 0.81$
4	2	73.33	0.71	17.19	0.67	50.68	0.10	2.27	0.11	3.30	0.13	1.34	0.70	0.95	0.82
	3	71.01	0.73	17.87 18.56	0.69	50.76	0.05	2.17	0.10	3.44	0.14	1.32	0.67	0.93	0.82
	5	71.14	0.74	19.26	0.70	50.81	-0.02	2.07	0.10	3.58	0.14	1.30	0.65	0.91	0.83
	6	70.39	0.75	19.26	-0.7I	50.83 50.83	0.00	$\frac{1.97}{1.88}$	-0.09	$\frac{3.72}{3.87}$	+0.15	1.28	0.62   -	$\begin{bmatrix} -0.91 \\ 0.91 \end{bmatrix}$	-0.83 $0.84$
4	7	69.63	0.76	20.68	0.71	50.81	-0.02	1.81	0.07	4.03	0.16	1.23	0.58	0.87	0.86
	8		0.77	21.40 22.12	0.72	50.75 50.67		1.75		4.19	0.16	1.20	0.56	0.86	0.87
	0		0.78	22.12	0.73		0.10	1.69	0.05	4.36	0.17	1.17	0.54	0.85	0.88
	1	66.54	0.78	22.85	1-0.73	50.57 50.44	-0.13	$\frac{1.64}{1.61}$	-0.03	4.53 4.71	+0.18	1.14	0.52  -	$ \begin{array}{c c} -0.84 \\ 0.84 \end{array} $	$ \begin{array}{c c} -0.90 \\ 0.92 \end{array} $
5	52	65.75	0.79	24.32	0.74	50.29	0.15	1.58	0.03	4.89	0.18	1.07	049	0.83	0.94
	3	64.96 64.16	0.80	25.06 $25.79$	0.73	50.11 49.90	0 01	1.56 1.55		5.07	0.18	1.03	0.48	0.82	0.96
	55	00 05	0.81	26.53	0.74	49.66	0.24	1 55	0.00	5.25	0.18	1.00	0.47	0.81	0.98
5	66	$\frac{63.35}{62.54}$	-0.81	27.27	+0.74	49.86	-0.27	$\frac{1.55}{1.57} +$	-0.02	$5.43 \\ 5.62$	+0.19	$0.96 \\ 0.92$	0.47	-0.81 - 0.81	-1.00 $1.01$
	7	61.73	0.81	27.99	0.72	49 11	0.20	1.59	0.02	5.81	0.19	0.89	0.47.	0.82	1.03
	58	60.92 $60.11$	0.81	28.72 29.45	0.73	48.79 48.41	0.35	1.62 1.66	001	5.99 6.17	0.18	0.85	0.48	0.82	1.05
	30	59.30	0.81	30.17	0.72	48.07	0.37		0.06		0.19	0.81	0.48	0.83	1.07
		00.00		50.11		40.01		1.72		6.36		0.77	0 49  -	-0.83	-1.09

			TABLE X, A	RG. 3.—Con	tinued.			9-41	
Arg.	(v.c.0) Diff	(v.s.1) Diff.	(v.c.1) Diff.	(v.s.2) Diff.	(v.c.2) Diff.	(v.s.3)	v.c.3)	(v.s.4)	(v.c.4)
	11 11	" "	" "	" "	11 11	"	11	"	-11-
60	59.300.8	30.17	48.07	1.72 +0.06	6.36 6.54+0.18		0.49	-0.83	-1.09
61	57 67 0.8	31 59 0.71	47.66 0.42	1.78 0.08	6 71		0.50 0.52	0.84	1.10
63	56 96 0.0	20 00 0.70	46.79 0.45	1 95 0.09	6.89 0.18		0.54	0.87	1.13
64	56.05 0.8		46.31 0.48	2.05 0.10	7.06 0.17	0.62	0.56	0.88	1.14
65	55.24	33.64 . 66	45.81	2.16 2.28+0.12	7.23 10 16	0.59	0.59	-0.89	-1.15
66	52.61 0.8	0.65	44 73 0.55	0 41 "3	7.39 0.15	0.55	0.62	0.91	1.16
68	59.84 0.0	35.58	44 16 0.57	2.55	7.69		0.68	0.95	1.17
69	52.05 0.7	1000.21	43.56 0.60	2.70 0.15	7.83 0.14	0.47	0.71	0.97	1.18
70	51.26	36.82	42.93	2.85	7.96	0.45	0.75	-0.99	-1.19
71 72	50.47 0.7		42.28 0.66	3 19 0.17	8.08 0.12	0.43	0.78   0.82	1.00	1.19
73	18 98 0.7	38 53 0.55	10 01 0.00	3 37	8 31	0.39	0.87	1.04	1.18
74	48.17 0.7	39.06	40.23 0.71	3.56 0.19	8.40 0.00	0.38	0.91	1.06	1.18
75	47.43	39.56	39.51	2 75	8.49	0.37	0.96	-1.08	-1.18
76	46.69 -0.7	10.00	38.77 -0.74 38.01 0.76	3.96 +0.21	8.57 +0.08	0.36	1.00	1.10	1.17
77	45.96 0.7 45.24 0.7	40.02	37.23 0.78	4.37 0.21	8.69 0.05	0.36	1.10	1.12	1.15
79	44.52 0.7	41.38 0.42	36.44 0.79	4.59 0.22	8.73 0.04		1.14	1.13	1.13
*80	43.82	41.78	35.63	4 00	8.76		1.18	-1.14	-1.12
81	40.14	42.16 +0.38 42.51 0.35	29 00 0.83	5.02 +0.22	8.77 ±0.01 8.78 ±0.01	0.38	1.23	1.15	1.10
82	11 00 0.6	10 89 0.32	39 19 0.85	5.47 0.23	8.77 -0.01		1.32	1.17	1.06
84	41.15 0.6	43.12 0.29	32.28 0.85	5.69 0.22	8.75 0.02	0.43	1.36	1.17	1.04
85	40.52	43.38	31.42	F 01	8.72	0.46	1.41	_1.18	-1.02
86	39.90		30.55 -0.87	6.13 +0.22 6.35 0.22	8.68 0.06	0.49	1.45	1.18	1.01
87 88	39.30	44.00 0.18	29 80 0.88	6.57 0.22	8.55 0.07	0.55	1.52	1.17	0.97
89	38.14 0.5		27.91 0.89	6.79 0.22	8.47 0.08	0.59	1.56	1 16	0.95
90	37.58	44.28	27.01	7.00	8.38		1.59	1.16	-0.94
91	37.04 -0.5 36.52 0.5		26.12 0.89 25.23 0.89	7.21 +0.21	8.27 —0.11 8.15 0.12	0.66	1.61	1.15	0.92
93	36.02 0.5	44.48 +0.04	24.33 0.90	7.60 0.19	8.02 0.13	0.76	1.66	1.13	0.90
94	35,53 0.4		23.43 0.90	7.79 0.19	7.89 0.13	0.80	1.68	1.12	0.89
95	25.07	14 16	22.54 -0.89	7.97 8.14 +0.17	7.74 -0.16	0.85	1.70	-1.11	-0.88 0.87
96	34.62 -0.4 34.20 0.4	44 32	21.00 0.88	0 20	7 41 0.17	0.90	1.71 1.72	1.10	0.86
98	22 70 0.4	44.20 0.12	19.90 0.87	8.45	7.24 0.17	1.00	1.72	1.06	0.85
99	33.41 0.3	44.01	19.03 0.87	0.13	0.20		1.73	1.04	0.84
100	33.04	43.90 20	18.16 _0.85	8.73 +0.13	6.85 -0.20	1.10	1.72 1.72	-1.03 $1.02$	-0.83 0.83
101 102	32.10	43.10 0.23	11.31 0.85	0.80 0.11	R 44	1.13	1.70	1.00	0.83
103	32.08	43.21	15.62 0.82	9.06	6.23	1.26	1.69	0.98	0.83
104	31.80 0.2	0.31	14.80 0.81	9.15 0.08	6.01 0.22	1.31	1.67	0.96	0.83
105	31.540.2	42.61 -0.34	13.99 _0.79	9.23 +0.07	5.79 -0.22	1.35	1.65 1.63	-0.95 $0.94$	-0.83 0.84
106	31.31 0.2	41 89 0.38	13.20 0.78	9.30 0.05	5 21 0.25	1.44	1.60	0.92	0.85
108	30.92	41.49 0.40	11.66 0.70	9.39	0.10	1.48	1.56	0.90	0.86
109	30.76 0.1	41.08 0.44	0.73	9.42 0.01	4.81 0.23	1.53	1.53	0.89	0.87
110 111	30.62	40.64	10.19	9.43 9.44 +0.01	4.64	1.56	1.49	0.88 0.87	0.88 0.89
1112	30.42 0.0	39.68 0.49	8.80 0.09	9.42-0.02	4.17 0.23	1.62	1.41	0.86	0.91
113	30.35	00.10	8.14 0.00	9.40 0.02	0.04	1.65	1.37	0.86 0.85	0.93
114	_0.0	0.56	0.62	0.05	0.23	1.67			-0.96
115	30.28	38.05	6.880.60	9.31 -0.07	3.480.22	1.70	1.27	0.84 0.84	0.96
117	30 32	36.86 0.61	5.71 0.57	9.17	3.04 0.22	1.73	1.17	0.84	0.99
118	30.37	36.24	5.17 0.54	9.08 0.09	2.82 0.21	1.74	1.12	0.84	1.01
119	0.1	0.65	1.00 0.49	0.11	2.61 0.20	1.74	1.02	-0.84	
120	30.56	34.95	4.16	8.88	2.71	1.12	1.02	0.04	1.04

		# 10		TABLE X, A	RG. 3.—Co	ntinued.				
	Arg.	(v.c.0) Diff	(v.s.1) Diff.	(v.c.1) Diff.	(v.s.2) Diff	f. (v.c.2) Diff.	(v.s.3)	(v.c.3)	(v.s.4)	(v.c.4)
	to E	" "	" "	" "	" "	" "	"	††	"	"
	120	30.56	34.95 34.27 — 0.68	4.16 3.69—0.47	8.88	$\begin{vmatrix} 2.41 \\ 2.21 \end{vmatrix} = 0.20$	1.74	1.02	-0.84	-1.04
H	$\frac{121}{122}$	30.85 0.15	33 58 0.69	3 26 0.43	8 63 0.13	2 02 0.19	1.73	$0.97 \\ 0.91$	0.84	1.06 1.08
	123	31.03 0.18	32.88 0.70	2.85 0.41	8.49 0.14	1.84 0.18	1.72	0.86	0.86	1.09
1	124	31.23 0.20	1 00.2. 141	2.47 0.38	8.34 0.15		1.71	0.81	0.87	1.10
	125	31 46	31 49	2.13	8.18	11.51	1.70	0.77	_0.88	_1.11
1	126	31.71 +0.25	00.01	1.81 -0.32	8.02 -0.16	1.00	1.67	0.72	0.90	1.12
1	127	31.98 0.27 32.28 0.30	1 40.04	1.52 0.26 1.26 0.26	7.85 0.18		$1.65 \\ 1.62$	0.68	0 92	1.13
1	$\frac{128}{129}$	32.61 0.33	28 39 0.77	1.03	7.48 0.19	0 96 0.12	1.59	0.59	$0.93 \\ 0.94$	1. I3 1.14
1	130	20 06	97 60	0.20	7.29	0.84	1.56	0.55	0.95	_1.15
1	131	33.34 +0.38	26.82 -0.79	0.67 -0.10	7 09 -0.20	0.74 -0.10	1.53	0.51	0.96	1.15
1	132	33.74	26.03	0.54 0.13	6.88 0.21	0.65 0.09	1.49	0.48	0.98	1.15
Н	133	34.16 0.42 34.60 0.44	25.24 0.80 24.44 0.80	0.44 0.07 0.07	6.67	0.57 0.06	1.45	0.45	0.99	1.15
H	134	0.46	0.79	0.04	6.46 0.21	0.05		0.42	1.01	1.16
	135 136	$\frac{35.06}{35.54}$ +0.48	23.65	0.33	$\begin{vmatrix} 6.25 \\ 6.03 - 0.22 \end{vmatrix}$	$\begin{vmatrix} 0.46 \\ 0.41 - 0.05 \end{vmatrix}$	1.37	0.40 -	-1.03	_1.16
1	137	36.05 0.51	22.06 0.80	0 35 +0.03	5.81 0.22	0.03	1.28	0.37	1.05 1.06	1.15
ı	138	36.58	21.27 0.79	0.40	5.59 0.22	0.36 -0.02	1.23	0.35	1.07	1.13
ı	139	37.13 0.55	20.48 0.79	0.49 0.09	5.38 0.21	0.36 0.00	1.18	0.34	1.08	1.12
I	140	27 70	19.69	0.61	5.16	0.96	1.13	0.34 -	_1.09	_1.11
ŀ	141	38.30 +0.60 38.92 0.62	18.90 -0.79 18.13 0.77	0.76 +0.15 0.18	4.95 -0.21 4.73 0.22	0.38 +0.02 0.41 0.03	1.09	0.33	1.09	1.09
J.	142 143	39.55 0.63	17.36 0.77	1.15 0.21	4.13	0.45 0.04	1.00	0.34	1.10	1.07
	144	40.21 0.66	16.60 0.76	1.39 0.24	4.31 0.21	0.50 0.05	0.95	0.35	1.12	1.05
I	145	40.88	15.85	1.66	4.10	0.57	0.91	0.36	_1.13 _	_1.04
ı	146	41.56 +0.68	15.12 -0.73	1.95 +0.29	3.90 -0.20	0.65 +0.08	0.86	0.38	1.13	1.03
L	147	42.27 0.71	14.39 0.73 13.67 0.72	4.20	0.11	0.13	0.82	0.40	1.13	1.02
ı	148 149	43.75 0.75	12 97 0.70	3.01 0.38	3 33 0.19	0.93 0.11	0.78	0.41	1.13	1.01
ı	150	0.70	19 98 0.09	0.41	3.15	0.11	0.71	0.46	_1.14 _	_0.98
ı	151	45.30 +0.79	11.60 -0.08	3 86 +0.44	2.98 -0.17	1 16 +0.12	0.67	0.50	1.14	0.96
E	152	46.09 0.79	10.94 0.64	4.32	2.82 0.16	1.29 0.13	0.64	0.53	1.13	0.95
Е	153 154	46.90 0.83	9.68	7.00	2.00	1.40	0.62	0.56	1.13	0.94
Г		0.84	0.00	0.53	0.14	0.16	0.59	0.59	1.12	0.98
L	155 156	48 57 49.42 +0.85	9.08 8.49—0.59	6 26 +0.54	$\begin{bmatrix} 2.37 \\ 2.25 \end{bmatrix}$ $\begin{bmatrix} -0.12 \\ \end{bmatrix}$	1.74	0.57	0.63	$\begin{bmatrix} -1.11 \\ 1.10 \end{bmatrix}$	-0.92
L	157	50 29 0.0/	7 92 0.5/	6 00 0.50	2 13 0.12	2.07		0.70	1.09	0.91
П	158	51.17 0.88	7.37	7.51	2.01	2.24	0.52	0.74	1.08	0.89
ı	159	52.07 0.90	6.84 0.53	8.12 0.62	1.91 0.00	2.42 0.18	0.51	0.78	1.06	0.88
L	160	52.97 $53.89 + 0.92$	6.34	$\frac{8.74}{9.20} + 0.65$	1.82	2.60		0.82 -	-1.05	-0.87
L	161 162	54.82	5.39 0.46	10.05 0.66	1.66 0.08	0.19		0.86	1.04	0.87
ı	163	55.75 0.93	4 95 0.44	10 70 0.07	1 60 0.00	3 16 0.19		0.94	1.02	0.86
Ŀ	164	56.70 0.95	4.54 0.40		1.55 0.05	3.35 0.19		0.97	1.00	0.86
Н	165	57.66	4.14	12.10	1 51	3 55	0.52	1.01 -	-0.99 _	-0.86
Н	166	00.00	3.77 -0.37	12.80 +0.70	1.48-0.03	3.75 +0.20		1.05	0 97	0.87
ı	167	60.58 0.98	3.42 0.35 3.10 0.32	13.52 °.72 14.25 °.73	1.40	3.94 0.19 4.14 0.20		1.08	0.96	0.87
L	169	61.57 0.99	2.80 0.30	15 00 0.75	7 /5 0.001	4.34 0.20		1.11	0.94	0.88
L	170	62.56	2.52	15 74	+0.01	1.50	A 100 TO	1.18 -	-0.93	-0.89
	171	63.56 +1.00	2.27 -0.25	16.49 +0.75	1.48 +0.02	4.72 +0.19		1.21	0.92	0.91
	172 173	64.56 I.OO 65.57 I.OI	2.05 0.22	17.25	1.51	4.91	0.65 .	1.23	0.91	0.92
	174	66.58 1.01	1.67 0.17	18 78 0.76	1 33	0.00		1.25	0.90	0.93 0.94
	175	67.60	0.16	10.55	0.06	0.18		1.27		
	176	68.61 +1.01	1.51	20 33 +0.70	72 -0.07	5 64 +0.18		$\begin{bmatrix} 1.29 \\ 1.30 \end{bmatrix}$	-0.89 — 0.88	0.95
	177	69.63	1.27	21.09	81 0.00	5.81 0.17		1.31	0.88	0.97
	178 179	10.00	1.19 0.08	21.86	1.89	5.97	0.81	1.32	0.88	0.98
		11.01	0.05	0.77	0.10	0.15		1.33	0.88	0.99
L	180	72.69	1.08	23.40	2.08	6.27	0 88	1.34	-0.88	1.00

Arg.   (e.c. 0)   Diff.   (e.s. 1)   Diff.   (e.s. 2)   Diff.   (e.s. 2)   Diff.   (e.s. 3)   (e.s. 3)   (e.s. 4)   (e.s. 4)   (e.s. 4)				TABLE X,	Aro. 3.—Ce	ontinued.				
191   13.71   1.02   1.08   -0.01   24.11   0.77   2.90   0.12   0.15   0.15   0.15   1.31   0.88   1.03   1.05   1.05   1.05   0.05   1.13   0.05   1.05   0.05   1.05   0.88   1.03   0.15   1.05   1.05   1.05   0.05   1.05   0.05   1.05   0.88   1.03   0.15   1.05   0.05   0.05	Arg.	(v.c.0) Diff.	(v.s.1) Diff.	(v.c.1) Diff.	(v.s.2) Diff.	(v.c.2) Diff.	(v.s.3)	(v.c.3)	(v.s.4)	(v.c.4)
181   12.71   1.02   1.07   -0.01   24.17   -0.77   2.99   0.127   2.19   1.15   0.09   1.33   0.88   1.09   1.08   1.0		" "	" "	" "	11 H	11 11	"	"	11	11
18.11   1.00   1.00   0.01   2.11   1.07   0.02   0.13   1.31   0.88   1.03   1.03   1.03   1.03   1.03   0.88   1.03   1.03   1.03   1.03   1.03   0.89   1.04   1.05				23.40	2.08	6.27	0.88	1.34	0.88	_1.00
1.4.16		10.11	1.04	- W. W. C. C.	2.20 +0.12	6 49 +0.15				
184		14.15	1.00	24.02 0 06	2.31	0.00				
1.55   17.77   1.01   1.24   0.16   27.99   0.73   2.83   0.12   1.00   1.06   1.32   0.92   1.06   1.85   78.78   1.09   1.29   1.09   1.20		13.13	1.44	20.00	2.40	0.00				
185		1,01				10.01	1.00	1.33	0.89	1.05
187   10.18   1.00   1.46   0.11   28.63   0.73   2.05   0.14   1.28   0.09   1.00   1.01   1.28   0.09   1.01   1.28   0.09   1.14   0.17   30.05   0.70   3.15   0.15   1.29   0.09   1.11   1.29   0.94   1.08			1.24		2.69					
188		10.10	1,02 0 17	A 1 + 0/ U	2.83 O.13	1.04				
189   81.76   0.99   1.74   0.15   0.15   0.05   0.71   0.25   0.15   1.30   0.08   1.18   1.28   0.95   1.09     190   82.75   0.99   1.74   0.15   0.15   0.70   0.70   0.70     191   83.74   0.07   2.10   0.22   0.22   32.10   0.06   3.71   0.15   0.15   0.15   0.15   0.15   0.15     193   86.75   0.95   2.95   0.23   32.10   0.06   3.71   0.15   0.15   0.15   0.15   0.15   0.15     194   86.61   0.95   0.70   0.26   33.41   0.04   0.16   0.15   0.15   0.15   0.15   0.15   0.15     195   87.56   0.95   0.95   0.25   33.41   0.04   4.02   0.15   0.15   0.05   1.29   0.99   1.10     196   88.50   0.94   3.32   0.29   3.52   0.06   3.75   0.16   0.15   0.03   1.23   1.17   1.00   1.10     197   88.42   0.92   3.62   0.27   35.27   0.06   4.02   0.15   0.15   0.03   1.25   1.12   1.19   0.99   1.10     198   90.34   0.92   3.62   0.27   35.27   0.06   4.02   0.15   0.15   0.03   1.25   1.12   1.19   0.11     199   1.40   0.94   0.95   3.25   0.55   4.64   0.16   1.05   0.05   1.25   1.12   1.10   1.11     199   1.40   0.94   0.95   0.35   0.35   0.55   0.44   0.16   1.05   0.05   1.05   1.05     200   92.14   0.85   0.85   0.85   0.85   0.85   0.85   0.85   0.85   0.85   0.85   0.85   0.85   0.05   0.15   0.15   0.15   0.15   0.15     201   30.92   0.85			1,40	20.00	2.00	7.13				
190   82,75   4-0,99   1.91   4-0,10   30.75   4-0.86   3.40   4-0.75   7.87   4-0.66   1.16   1.26   -0.96   -1.10   1.91   88.561   -0.95   2.55   -0.24   32.10   -0.65   3.55   -0.15   7.48   +0.05   1.18   1.24   0.97   1.10   1.93   88.65   -0.95   2.55   -0.24   32.10   -0.65   3.55   -0.15   7.48   +0.05   1.18   1.24   0.97   1.10   1.93			1 74 0.15	30 05 0.71	2 95 0.15					
191   83.74   40.99   2.10   50.71   73.143   50.85   1.744   50.95   1.90	-	0.99	0.17	0.70	0.15	0.07				
192   84.71   0.97   9.33   0.22   32.16   0.67   3.71   0.16   7.48   0.05   1.29   1.29   0.99   1.10   1.10   1.10   85.61   0.95   2.79   0.26   33.41   0.65   4.02   0.16   7.57   0.04   1.23   1.17   1.00   1.10   1.10   1.11			0 10 +0.19	21 49 +0.03	2 55 +0.15					
193			0 90 0.22	20 10 0.07	3.71 0.10	7 10 0.05				
194		85.65 0.95	0.55	0.00	3 86 0.15	7 53				
195	194	86.61 0.95	9 70 0.24	99 41 0.05	4.02 0.10	7 57 0.04				
196	195	87.56	9.05	21.05	4 17	7 60			1.01	
198   90.34   0.92   3.02   0.29   3.5.27   0.60   4.49   0.16   1.63   1.00   1.26   1.01   1.02   1.11   1.10		88.50 - 0.94	3 33 +0.28	34.67 +0.02	4.33 +0.16	7 60 +0.02				
199   90.34   0.99   3.98   0.31   3.98   6.59   4.64   6.15   7.63   0.00   1.27   1.07   1.03   1.10		89.42 0.92	3.62 0.29	35.27	4.49	7.68 +0.01				
190		90.34 0.92	3.93 0.31	35.86 0.59	E-OE	7 63 0.00				
200 92.14	199	01.22			4.79 0.15	7.62 -0.01		1.04	1.04	1.10
201 93.02 + 0.88	200	00 14	4.58	36.99	14.94	7.60	1.28	1.02	1.05	_1.09
202 93.89 0.57   5.28 0.50   5.25 0.52   5.23 0.14   7.54 0.05   1.98 0.97   1.06 1.07   204 95.59 0.85   6.03 0.38   39.04 0.48   5.51 0.14   7.46 0.04   1.26 0.92   1.08 1.05   205 90.41   206 97.23 + 0.82   6.81 + 0.39   39.51   0.44   5.89 0.12   7.35 - 0.06   1.24   0.87   1.09 1.04   207 98.02 0.79   7.22 0.41   40.40 0.41   6.80 0.12   7.35 - 0.06   1.24   0.87   1.09 1.04   208 99.57 0.76   8.06 0.42   41.21 0.40   41.5   0.37   0.95   0.95   1.09   1.03   210 100.32 + 0.74   8.49 + 0.43   41.94 + 0.36   6.32 + 0.10   1.07   1.06   211 101.78 0.72   9.36 0.44   42.29 0.34   42.29 0.34   42.29 0.30   6.50 0.09   213 102.48 0.70   9.80 0.44   42.29 0.30   6.50 0.09   1.17   0.77   1.10   0.99   214 103.17 0.69   10.24 0.45   43.48 + 0.26   6.71 + 0.06   6.66 0.10   215 108.94   10.69   43.18 + 0.24   43.90 0.29   10.63   11.50   0.45   43.94   0.24   43.95   0.29   106.30   0.57   13.41 + 0.45   43.68   0.22   107.45 + 0.55   13.86   0.44   44.29 + 0.6   12.04   44.49 +	201	93.02+0.88	1 00 +0.34	27 52 +0.54		7.57 -0.03		1.00	1.05	1.08
204 95.59 0.85 6.03 0.39 39.60 0.48 3.51 0.14 1.40 0.04 1.21 0.05 1.05 1.05 1.05 1.05 1.05 1.05 1.0		93.89	0.20	01,00	0.20	1.01				
205 96.41 206 97.23 + 0.82 6.81 + 0.39 39.96 + 0.45 5.77 + 0.13 7.35 - 0.06 1.24 0.87 1.09 1.04 7.35 - 0.06 1.24 0.87 1.09 1.04 7.35 - 0.06 1.24 0.87 1.09 1.04 7.35 - 0.06 1.24 0.87 1.09 1.04 7.35 - 0.06 1.24 0.87 1.09 1.04 7.35 - 0.06 1.24 0.87 1.09 1.04 7.35 - 0.06 1.24 0.87 1.09 1.04 7.35 - 0.06 1.24 0.87 1.09 1.04 7.35 - 0.06 1.24 0.87 1.09 1.04 7.35 - 0.06 1.24 0.87 1.09 1.04 7.35 - 0.06 1.24 0.87 1.09 1.04 7.35 - 0.06 1.24 0.87 1.09 1.04 7.35 - 0.06 1.24 0.87 1.09 1.04 7.35 - 0.06 1.24 0.87 1.29 0.83 1.09 1.09 1.04 7.35 - 0.06 1.24 0.87 1.29 0.83 1.09 1.09 1.04 7.35 - 0.06 1.24 0.87 1.29 0.83 1.09 1.09 1.04 7.35 - 0.06 1.24 0.87 1.29 0.83 1.09 1.09 1.04 7.35 - 0.06 1.24 0.87 1.29 0.83 1.09 1.09 1.04 7.35 - 0.06 1.24 0.87 1.29 0.83 1.09 1.09 1.04 7.35 - 0.06 1.24 0.87 1.29 0.83 1.09 1.09 1.04 7.35 - 0.06 1.29 0.83 1.09 1.09 1.04 7.35 - 0.06 1.29 0.83 1.09 1.09 1.04 7.35 - 0.06 1.29 0.83 1.09 1.09 1.04 7.35 - 0.06 1.29 0.83 1.09 1.09 1.04 7.35 - 0.06 1.29 0.83 1.09 1.09 1.04 7.35 - 0.06 1.29 0.83 1.09 1.09 1.04 7.35 - 0.06 1.29 0.83 1.09 1.09 1.04 7.35 - 0.06 1.29 0.83 1.09 1.09 1.04 7.35 - 0.06 1.29 0.83 1.09 1.09 1.04 7.35 - 0.06 1.29 0.83 1.09 1.09 1.04 7.35 - 0.06 1.29 0.83 1.09 1.09 1.00 1.01 1.01 0.09 1.01 1.01		91.11	0.00	05.00	0.01	10				
205         96.41 - 0.82         6.81 + 0.39         39.51 + 0.45         7.41 - 0.13         7.43 - 0.66         1.24 + 0.87         1.09 - 1.04         1.04         0.81 + 0.45         5.64 + 0.12         7.35 - 0.66         1.24 + 0.87         1.09 - 1.04         1.04         0.41 + 0.40         0.41 + 5.89 - 0.12         7.35 - 0.67         1.24 + 0.87         1.09 - 1.04         1.00         1.00         2.00         9.57 - 0.76         8.06 - 0.42 + 40.81 - 0.44         6.01 - 0.11         1.01         1.00         0.85 - 1.09         1.03         1.09         1.03         1.09         1.03         1.09         1.09         1.03         1.09         1.09         1.09         1.00         1.00         1.00         1.00         0.44         4.12         0.40         0.44         4.29         0.34         6.22 + 0.10         6.32 + 0.10         6.32 + 0.10         1.17 - 0.77         1.10         0.09         1.10         0.09         1.17 - 0.77         1.10         0.09         1.10         0.09         1.10         0.09         0.09         0.09         1.17 - 0.72         0.09         1.17 - 0.72         0.09         0.09         1.17 - 0.72         0.09         0.09         1.10         0.09         0.09         0.09         0.09         0.09         0.09				0.47	0.13	1.40	1.26			
207 98.02 0.79 7.22 0.41 40.40 0.44 5.89 0.12 7.23 0.07 1.23 0.85 1.09 1.03 209 99.57 0.76 8 06 0.42 40.81 0.40 6.12 0.17 7.13 0.08 1.21 0.81 1.09 1.01 210 101.06 +0.74 8.92 0.43 41.58 +0.36 6.32 +0.10 6.93 0.44 42.29 0.34 6.41 0.09 6.86 0.10 1.17 0.77 1.10 0.99 213 102.48 0.70 9.80 0.44 42.29 0.34 6.40 0.09 6.76 0.10 1.13 0.75 1.09 0.98 213 102.48 0.70 10.69 0.45 43.18 0.26 6.50 0.09 6.76 0.10 1.11 0.73 1.09 0.97 215 103.84 2.10 10.40 0.45 43.18 0.26 6.77 0.06 6.45 0.10 1.11 0.73 1.09 0.97 215 103.84 0.45 43.89 0.22 6.80 0.07 6.76 0.10 1.11 0.73 1.09 0.97 216 104.49 -0.55 11.14 0.45 43.44 0.26 6.71 0.06 6.45 0.12 1.04 0.70 1.07 0.95 11.14 0.30 0.45 44.11 0.21 6.87 0.05 6.11 0.11 1.00 0.70 1.05 0.93 1.30 0.45 44.60 0.12 1.01 0.18 0.05 0.12 1.09 0.70 1.06 0.94 44.84 0.45 0.15 0.99 0.00 0.55 11.30 0.45 11.30 0.45 13.41 0.45 13.41 0.45 13.41 0.45 13.41 0.45 13.00 0.25 11.30 0.45 13.41 0.45 13		96.41	6.42	39.51	5 64					
208 93.81 0.79 7.64 40.81 0.41 6.01 0.12 7.21 0.08 1.09 1.01 2.09 99.57 0.76 8.69 0.43 41.91 0.45 6.12 0.17 7.13 0.08 1.29 0.83 1.09 1.01 1.02 0.11 101.06 0.75 8.49 0.43 41.94 0.36 6.32 0.10 6.12 0.17 7.13 0.08 1.29 0.81 1.09 1.01 0.99 0.10 1.01 0.00 0.12 101.78 0.79 9.80 0.44 42.98 0.34 6.41 0.09 6.86 0.10 1.15 0.76 1.09 0.98 0.44 42.98 0.34 6.41 0.09 6.86 0.10 1.15 0.76 1.09 0.98 0.44 42.98 0.35 6.58 0.05 6.66 0.10 1.15 0.76 1.09 0.98 0.44 42.98 0.39 0.30 0.57 0.00 6.76 0.10 1.11 0.75 1.09 0.97 0.97 0.11 0.00 0.99 0.99 0.70 1.00 0.99 0.99 0.70 1.00 0.99 0.99 0.70 1.00 0.90 0.99 0.70 1.00 0.90 0.99 0.70 1.00 0.90 0.99 0.70 1.00 0.90 0.99 0.70 1.00 0.90 0.99 0.70 1.00 0.90 0.99 0.70 1.00 0.90 0.70 0.70 0.70 0.90 0.70 0.70 0		97.23 +0.32	0.01	33.30 0 11	5.77 70.13	().)				
209   99.57   0.76   8.06   0.42   41.91   0.45   6.12   0.11   7.13   0.08   1.21   0.81   1.09   1.01		20.02	1.32 0 43	40.40	0.00	1.20				
210 100.32		00.01	8.06 0.42	11 91 0.40						
211 101.06 + 0.74		0.75	0.43	0.37	0.10	0.00				
212         101.78         0.72         9.36         0.44         42.28         0.31         6.50         0.99         6.86         0.10         1.15         0.76         1.09         0.98           214         103.17         0.69         10.24         0.44         42.99         0.30         6.58         0.00         6.76         0.10         1.13         0.75         1.09         0.97           215         103.84         10.69         0.44         42.89         0.30         6.58         0.66         0.10         1.11         0.73         1.09         0.97           216         104.49         -0.65         11.15         0.45         43.48         -0.26         6.71         -0.66         6.45         -0.11         1.09         0.72         -1.08         0.96           218         106.73         0.61         12.96         0.45         43.90         0.22         6.87         0.05         1.04         0.70         1.06         0.71         1.08         0.96           220         106.90         12.95         0.46         44.11         0.18         6.91         0.04         1.01         1.00         0.70         1.06         0.91		100.32			6 20 +0.10	7.05 _0.09				
213         102.48         0.70         9.80         0.44         42.59         0.30         6.50         0.09         6.76         0.10         1.13         0.75         1.09         0.97           214         103.17         0.69         0.44         42.59         0.30         6.58         0.88         6.66         0.10         1.11         0.73         1.09         0.97           215         103.84         0.67         10.69         0.44         42.89         0.29         6.58         0.86         6.66         0.10         1.11         0.73         1.09         0.97           216         104.49         -65         11.14         -0.45         43.18         +0.26         6.71         -0.66         6.71         0.06         0.71         1.08         0.96           218         106.73         0.61         12.04         0.46         43.90         0.22         0.56         6.92         0.01         1.06         0.71         1.08         0.96           220         106.30         0.50         13.86         0.45         44.81         0.15         6.91         0.04         1.09         0.70         1.06         0.72         1.00         0.92		101.78 0.72	9 36 0.44	47.04 0.34						
214 103.17 0.09 10.24 0.44 0.45 10.69 0.30 6.58 0.05 6.66 0.10 1.11 0.73 1.09 0.97 2.15 103.84 0.65 11.14 0.45 43.18 0.24 6.77 0.06 6.45 0.10 1.09 0.72 1.08 0.96 11.14 0.65 11.14 0.45 43.68 0.24 6.77 0.06 6.45 0.10 1.00 0.71 1.03 0.96 1.10 0.95 11.14 0.25 0.45 43.68 0.24 6.77 0.06 6.32 0.11 1.00 0.70 1.07 0.95 11.00 0.50 0.45 11.38 0.45 11.38 0.45 11.39 0.45 11		102 48 0.70	9.80 0.44	19 50 0.31	6.50 0.09	6.76 0.10				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	214		10 04 0.44	19 89 0.30	10.00	6.66 0.10	1.11		1.09	0.97
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	215	109 04		49 10	0.05		1 09	0.72	_1.08	-0.96
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	916	101 10 +0.65	11 14 +0.45	10 11 -0.20	6 71 +0.00	P 45 O. II		0.71	1.08	0.96
218 106.73	217	105.12	11 59	43 68		6.33	1.04	0.70	1.07	
220	218	106.73	12.04	43.90	0.00	0.22				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	219	L 1212 . 43 +3		44.11 0.18	0.04	0.11	1.00	0.70		1000
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		106 90	12.95 10.46	44.29 10.16	6 91	5.99				
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		107.45	13.41	44.40 0.15		5.81				
224         109.00         0.50         14.75         0.45         44.84         0.10         6.99 +0.01         5.53         0.12         0.88         0.71         1.01         0.92           225         109.48         15.19         44.94         45.02 +0.08         6.99 +0.01         5.53 &0.12         0.86         0.72         -1.00         -0.92           226         109.94 +0.46         15.63 +0.44         45.02 +0.08         45.02 +0.08         6.99 -0.01         5.31 -0.11         0.86         0.72         -1.00         -0.92           228         110.73         0.43         16.50 -0.43         45.12 -0.04         45.08 -0.01         6.96 -0.01         5.20 -0.11         0.81         0.73         1.00         0.92           229         111.18 -0.40         16.93 -0.42         45.14 -0.01         45.14 -0.01         6.94 -0.02         4.98 -0.11         0.77         0.76         0.98         0.92           230         111.55         17.76 +0.41         18.17 -0.41         45.15 -0.00         4.98 -0.01         4.98 -0.10         0.77 -0.76         0.98 -0.97         -0.93           231         112.83 -0.31         18.96 -0.39         45.04 -0.02         45.04 -0.02         4.98 -0.01         0.74 -0.79         0		101.33	13.50	44.00 0.12	0.00 0.02	D. (0 O TT				
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		109.00 0.50	14.30 0.45	44.13 0.11	6.99 +0.01	5 53 0.12				
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		0.48	0.44	0.10	0.00	0.11		1		
227       110.37       0.43       16.07       0.44       45.08       0.04       6.97       0.01       5.20       0.11       0.81       0.73       1.00       0.92         229       111.18       0.40       16.93       0.43       45.12       0.04       6.94       0.02       4.98       0.11       0.77       0.76       0.98       0.92         230       111.55       0.37       17.35       17.35       17.76       0.01       45.15       0.00       6.94       0.02       4.98       0.11       0.77       0.76       0.98       0.92         231       111.89       +0.34       18.17       0.41       45.15       0.00       6.88       0.03       4.88       0.76       0.78       -0.97       -0.93         232       112.23       0.34       18.17       0.41       45.13       -0.02       6.85       0.03       4.68       0.10       0.74       0.79       0.97       0.93         233       112.54       0.31       18.96       0.39       0.04       45.09       0.04       6.80       0.05       4.58       0.10       0.71       0.83       0.95       0.93         235       113.10		109.48	15.19	41.94	6.99 -0.01					
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		110.37 0.43	16.07 0.44	45 08 0.00		17.47 1				
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			16.50 0.43	45.12 0.04	6.96 0.01	5.09 0.11				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		111.18 0.40	16.93 0.43	45.14 0.02	6.94 0.02	4.98 0.11				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	230	111 55	17 95		6.91	1 99		0.78	-0.97	-0.93
232 112.23 0.34 18.17 0.40 45.13 0.04 45.09 0.04 4.58 0.10 0.71 0.83 0.95 0.95 0.95 0.27 113.10 0.236 113.35 0.22 0.09 0.37 113.57 0.20 0.37 113.57 0.22 0.09 0.37 113.57 0.22 0.09 0.37 113.57 0.22 0.09 0.37 113.57 0.22 0.09 0.37 113.57 0.22 0.09 0.37 113.57 0.22 0.09 0.37 113.57 0.22 0.09 0.37 113.57 0.22 0.09 0.37 113.57 0.22 0.09 0.37 113.57 0.22 0.09 0.37 113.57 0.22 0.09 0.37 113.57 0.22 0.09 0.37 113.57 0.20 0.06 0.36 0.06 0.91 0.93 0.98 0.93 0.99		111.89 +0.34	17.76 +0.41	45 15 0.00	6.88 -0.03	4.78 -0.10				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	232	112.23 0.34	18.17	45.13 -0.02	0.00	4.68	0.72			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		I I W. UT	15.01	45.09	0.00	4.00				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	234		18.96 0.39		6.75	4.40	0.69	0.85	0.94	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		113 10	10 91	1100	6 70	4.40				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			19.72 +0.38	44.91 -0.07	6.64 -0.06	4.01				
239 113.95 0.18 20.80 0.35 44.59 0.12 6.45 0.07 4.09 0.07 0.65 0.96 0.93 1.00		113.51	20.09	44.82	0.00	4.20				
0.16 20.30 0.35 44.00 0.12 0.40 0.07 0.07 0.07		110.11	0.70	44.11	6.45 0.06	4.10				
240 114.11 21.15 44.47 5.38 4.02 0.65 0.98 -0.93 -1.01		0.16	0.35	0.12	0.07	0.07		1000	10-35	
	240	114.11	21.15	44.47	6.38	4.02	0.65	0.98	-0.93	-1.01

33 August, 1873.

1				TABLE	X, A	RG. 3.—Con	itinued.				
	Arg.	(v.c.0) Diff.	(v.s.1) Diff.	(v.c.1)	Diff.	(v.s.2) Diff.	(v.c.2) Diff.	(v.s.3)	(v.c.3)	(v.s.4)	(v.c.4)
1		" "	" "	"	"	" "	" "	"	"	"	"
1	240	114.11	$\frac{21.15}{21.48} + 0.33$	44.47	-0.14	$\frac{6.38}{6.30}$ —0.08	$\frac{4.02}{3.96}$ —0.06	$0.65 \\ 0.65$	0.98	-0.93 $0.93$	$-1.01 \\ 1.01$
1	$\frac{241}{242}$	114.24 +0.13	21.48 +0.33 21.80 0.32	44.33 44.18	0.15	6 23 0.07	3 90 0.00	0.65	1.03	0.93	1.01
1	243	114 46 0.10	22.12 0.32	44.02	0.16	6.15 0.08	3.85 0.05	0.65	1.05	0.94	1.03
1	244	114.54 0.08	22.43 0.31	43.86	0.16	6.07 0.08	3.80 0.05	0.65	1.07	0.95	1.04
1	245	114.60	22.73	43.68	-0.19	5.99	3.75	0 65	1.10	-0.95	1.04
1	246	114.63 +0.03 114.65 +0.02	23.01 +0.28	43.49	0.19	5.91 0.08	3.71 0.03	0.65	1.12	$0.96 \\ 0.97$	1.04
ı	247 248	114 64 -0.01	93 56 0.27	43.30 43.10	0.20	5 74 0.09	9 05 0.03	0.66	1.14	0.97	1.05
ı	249	114.61 0.03	23.82 0.26	42.88	0.22	5.66 0.08	3.62 0.03	0.67	1.19	0.98	1.06
1	250	114 55	24.06	42.67	-0.22	5.58	3.60	0.69	1.21	-0.98	1.06
ı	251	114.48 0.09	24.30 +0.24	42.45	0.23	5.49	3.59	0.70	1.23	0.98	1.06
Н	252 253	114.39 0.10	21.75 0.22	42.22 41.98	0.24	5.41 0.08 5.33 0.08	3.580.01	$0.72 \\ 0.73$	1.24 1.26	$0.99 \\ 1.00$	1.06 1.07
ı	254	114 10 0.13	24.95 0.20	41.74	0.24	5.25 0.09	3.57 0.00	0.75	1.28	1.01	1.07
	255	114.16 0.15	25.15	41.49	0.25	5 16	3.57	0.77	1.30	-1.01	_1.07
	256	113.84 -0.17	25.34 +0.19	41.24	0.25	5.08 -0.08	3.57 0.00	0.78	1.31	1.01	1.07
1		113.66 0.10	25.52 0.18 25.70 0.18	40.98 $40.73$	0.25	5.01 0.07 4.93 0.08	3.57 0.00	$0.80 \\ 0.82$	$1.32 \\ 1.34$	$1.01 \\ 1.02$	$\frac{1.07}{1.06}$
ı	258 259	113.22 0.23	25.86 0.16	40.47	0.26	4.85 0.08	3.60 0.02	0.84	1.35	1.03	1.05
	260	112.98	96 09	40.21	0.26	4.78	9 69	0.87	1.36	-1.03	1.05
П	261	112.71-0.27	26.16 +0.14	39.95	-0.26	4.71 -0.07	3.64 +0.02	0.89	1.37	1.03	1.04
П		112.43 0.28	26.30 0.14 26.43 0.13	39.68	0.27	4.64 0.07	3.66	0.91	1.38	1.03	1.03
Н	263 264	112.14 0.29	26.43 0.13 26.55 0.12	39.41 39.13	0.28	4.57 0.06	3.69 0.03	$0.93 \\ 0.96$	1.38 1.39	1.04 1.05	$1.02 \\ 1.01$
Н	265	111.51	26.66	38.86	0.27	4.45	3.75	0.98	1.39	_1.05	1.01
ı	266	111.16 -0.35	26.77 +0.11	38.59	-0.27	1 39-0.00	3 79 +0.04	1.00	1.39	1.05	1.01
П	267	110.80 0.36	26.87	38.31	0.28	4.33	3.83 0.04	1.02	1.39	1.05	1.01
1	268	110.43 0.37	20.90	38.03	0.27	4.28 0.05	3.86 0.03	1.05	1.38	1.05	1.00
ı	269	0.41	0.08	37.76	0.27	4.22 0.05	0.04	1.07	1.38	1.05	0.99
ı	270 271	109.63 $109.21$ $-0.42$	$\frac{27.12}{27.19} + 0.07$	37.49 37.21	-0.28	4.17	$\frac{3.94}{3.99} + 0.05$	$\frac{1.09}{1.12}$	1.38 1.37	1.05 1.05	-0.99
1	272	108.77 0.44	27.26 0.07	36.93	0.28	1 07 0.05	4 03 0.04	1.14	1.37	1.05	0.98
1	273	108.32 0.45	27.32 0.06	36.65	0.28	4.02	4.08 0.05	1.16	1.36	1.04	0.98
ı	274	0.48	0.05	36.37	0.27	0.03	4.12 0.04	1.18	1.35	1.04	0.97
	275	$\frac{107.38}{106.90}$ -0.48	$\frac{27.42}{27.46}$ + 0.04	36.10	-0.28	$\frac{3.95}{3.92}$ -0.03	4.17	1.20	1.34	-1.04	-0.97
1	276 277	106.40 0.50	27 50 0.04	35.82 35.54	0.28	3.89	4.22 0.05	1.22	1.32 1.31	1.03	0.97
1	278	105.89	27.53	35.27	0.27	3.86	4.32 0.05	1.26	1.30	1.01	0.97
	279	0.53	0.03	35.00	0.27	3.83 0.03	4.37 0.05	1.28	1.28	1.00	0.96
	280	104.84	27.59	34.72	-0.28	3.80	4.42	1.29	1.26	-1.00	-0.96
	281 282	103 75 0.55	27 63 0.02	34.44	0.27	3.77 0.03	153 0.06	1.31 1.32	1.24	1.00	0.96
-	283	103.19	27.64	33.90	0.27	3.74	4.58 0.05	1.34	1.20	0.99	0.96
	284	0.58	0.00	33.63	0.27	3.72 0.02	4.64 0.05	1.35	1.18	0.98	0.95
1	285	102.04	27.65 0.00	33.36		3.71	1 00	1.36	1.16	-0.98	-0.95
1	286 287	101.46 -0.58 100.87 0.59	27 65 0.00	33.09 <sup>-</sup> 32.82	0.27	3.70 -0.01	4.74 +0.05	1.37	1.14	$0.98 \\ 0.98$	0.95
	288	100.27 0.60	27.64 -0.01	32.55	0.27	200 0.01	1 25 0.06	1.38	1.12	0.97	0.95
	289	99.67 0.60	27.63 0.01	32.29	0.26	3.67 -0.01	4.90 0.05	1.39	1.07	0.96	0.97
1	290	00 00	27.62	32.02	. ,	3.67	1 05	1.39	1.05	0.96	-0.98
	291 292	98.45—0.61 97.83 0.62	27.60 -0.02 27.58 0.02	31.76	0.26	3.67 0.00	5.00 +0.05	1.40	1.02	0.96	0.98
	293	97.21 0.62	27.56 0.02	31.50 31.23	0.27	0.00	5.11 0.05	1.40	1:00	0.95	1.00
	294	96.58 0.63	27.54 0.02	30.97	0.26	3 68 +0.01	5.16 0.05	1.40	0.95	0.95	1.01
	295	05 05	27.52	30.71		0.00	5.21	1.39	0.93	_0.95	-1.02
	296	95.31 -0.64 94.67 0.64	27.48 -0.04	30.45	-0.26 0.26	3.70 +0.01	5.26 +0.05	1.39	0.91	0.95	1.02
1	297 298	94.04 0.63	27.42 0.03	30.19 29.93	0.26	3.71 0.01 3.72 0.01	5.37 0.05	1.38	0.88	0.96	1.02 1.03
	299	93.40 0.64	27.38 0.04	29.67	0.26	3.74 0.02	5.49 0.05	1.37	0.84	0.97	1.03
	300	92.77	27.34	29.40	0.27	3.76	5.47	1.35	0.82	0.97	-1.03
									1		

1						TABLE	X, A	ко. 3	- Con	tinued.			-48		
i	Arg.	(v.c.0)	Diff.	(v.s.1)	Diff.	(v.c.1)	Diff.	(v.s.2)	Diff.	(v.c.2)	Diff.	(0.8.3)	(v.c.3)	(v.s.4)	(v.c.4)
ı		11	11	"	"	"	"	11	"	"	"	"	"	"	11
ı	300	92.77	_0.64	27.34	-0.04	29.40	-0.24	3.76	-0.01	5.47	0.04	1.35	0.82	0.97	_1.03
ı	301	92,13 91.50	0.63	27.30 27.26	0.04	29.16° 28.89	0.27	3.77 + 3.80	0.03	5.51	0.05	1.34	0.80	0.97	1.03
1	303	90.87	0.63	27.21	0.05	28.63	0.26	3.82	0.02	5.61	0.05	1.31	0.76	0.98	1.04
ı	304	90.24	0.63	27.16	0.05	28.37	0.26	3.85	0.03	5.66	0.05	1.30	0.74	0.99	1.04
ı	305	89.60		27.10		28,11		3.87		5.71		1.28	0.72	_0.99	_1.04
ı	306	88.97	0.63	27.05	0.06	27.86	0.25	9.91	0.03	9.19	0.05	1.27	0.71	1.00	1.04
ı	307	88.35 87.72	0.62	26.99 26.93	0.06	27.60 27.35	0.25	3.94	0.03	5.80	0.04	1.25 1.23	0.69	1.00	1,04 1.04
ı	309	87.10	0.62	26.86	0.07	27.10	0.25	4.01	0.04	5.88	0.04	1.21	0.66	1.01	1.04
ı	310	86.49	0.61	26.79	0.07	26.85	0.25	4.05	0.04	5,92	0.04	1.19	0.65	1.02	_1.04
ı	311	85.89	0.60	26.72	0.07	26.59	0.25	4.09	0.04	5.96+	0.04	1.17	0.64	1.02	1.04
ı	312	85.29	0.60	26.65	0.07	26.34	0.25	4.14	0.04	6.00	0.03	1.15	0.63	1.03	1.03 1.03
1	313	84.69	0.60	26.58 26.49	0.09	26.09 25.84	0.25	4.18	0.04	6.03	0.04	1.12	0.62	1.03	1.03
۱			0.58	26.40	0.09	25.59	0.25	4.27	0.05	6,10	0.03	1.08	0.61	_1.04	_1.03
1	315	83.51 82.93	-0.58	26.31	_0.09	25.39	_0.25	4.32	-0.05	6.14+	-0.04	1.05	0.61	1.04	1.02
1	317	82.37	0.56	26,22	0.09	25.10	0.24	4.37	0.05	6.17	0.03	1.03	0.61	1.04	1.02
ı	318	81.81	0.56	26.12	0.10	24.85	0.25	4.43	0.05	6.19	0.03	1.01	0.61	1.04	1.01
ı	319	81.27	0.54	26.02	0.11	24.60	0.25		0.06		0.03		TO SEE	_1.04	_1.00
ı	320 321	80.73 80.20	-0.53	25.91 25.80	_0.11	24.35 24.11	_0.24	4.54	10.06	6.25	-0.02	0.96	0.61	1.04	0.99
1	322	79.68	0.52	25.68	0.12	23.87	0.24	4.66	0.00	6.29	0.02	0.91	0.62	1.03	0.99
ı	323	79.17	0.51	25.56	0.12	23.63	0.24	4.72	0.06	6.30	0.01	0 89	0.62	1.03	0.98
1	324	78.68	0.49	25,44	0.13	23.39	0.23	4.78	0.07	6.32	0.02	0.87	0.63	1.03	0.98
ı	325	78.19	-0.47	25.31	-0.14	23.16	-0.24	4.85	-0.07	6.34	-0.01	0.85	0.64	1.03 1.03	-0.97 $0.97$
ı	326 327	77.72	0.46	25.17 25.02	0.15	22.92	0.23	4,92	0.07	6.35	0.00	0.83	0.66	1.02	0.96
ı	358	76.82	0.44	24.87	0.15	22.46	0.23	5.06	0.07	6.35	0.00	0.79	0.67	1.02	0.96
1	329	76.39	0.43	24.72	0.15	22.23	0.23	5.13	0.07	6.35	0.00	0.77	0.69	1.01	0.95
ł	330	75.97		24.56		22.00		5.20	-0.07	6.35	0.00	0.75	0.70	1.01	0.95
ı	331	75.57	0.39	24.00	0.17	21.78	-0.22 0.21	0.21	0.07	6.35	-0.01	0.73	0.72	1.00	0.95 0.95
ı	332 333	75.18	0.37	24.21 24.03	0.18	21.57	0.22	5.34 5.41	0.07	6.34	0.01	0.70	0.76	0.99	0.95
ı	334	74.45	0.36	23.84	0.19	21.14	0.21	5.48	0.07	6.32	0.01	0.69	0.78	0.99	0.95
1	335	74.11	0.34	23.65	0.19	20.94	0.20	5.56		6.30		0.68	0.80	0.99	0.95
ı	336	73.79	-0.32	23.45	-0.20 0.2I	20.73	-0.2I 0.20	5.63	0.07	6.28	0.03	0.67	0.82	0.98	0.95
ı	337	73.48	0.31	20.21	0.22	20.53	0.19	5.70	0.00	6.25	0.03	0.66	0.84	0.96	0.95 0.95
1	339 339	73.18	0.27	23.02 22.80	0.22	20.34	0.19	5.85	0.07	6.19	0.03	0.64	0.88	0.95	0.95
1	340	72.66	0.25	22.57	0.23	19.96	0.19	-	0.07		0.04	0.64	0.91	0.95	0.95
1	341	72.42	-0.24	22.33	-0.24	19.79	-0.17 0.17	5.98	0.07	6.11	0.04	0.63	0.93	0.95	0.96
1	342	72.20	0.22	22.09	0.24	19.62	0.17	6.05	0.07	6.07	0.05	0.63	0.95	0.94	0.96
1	343 344	72.00	0 18	21.84	0.26	19.45	0.15	6.12	0.07	6.02	0.05	0.63	1.00	0.93	0.97
1		100	0.16	100	0.27		0.15	0 05	0.06	5 01	0.06	0.63	1.02	0.93	_0.97
I	345 346	71.66	-0.14	21.31	_0.27	19.15	-0.15	6.31	10.06	5.86	-0.05	0.64	1.05	0.93	0.98
ı	347	71.39	0.13	20.75	0.29	18.87	0.13	6.37	0.06	5.80	0.06	0.64	1.07	0.94	0.99
	348	71.29	0.10	20.46	0.29	18.74	0.13	6.43	0.05	9.10	0.07	0.65	1.09	0.94	1.00
1	349	71.21	0.06	20.16	0.31	18.62	0.10	6.48	0.05	0.00	0.07			0.94	_1.02
	350	71.15	-0.05	19.85 19.54	_0.31	18.52 18.43	_0.09	6.53	10.05		_0.08	0.67	1.14	0.94	1.02
	351 352	71.08	-0.02	19.34	0.32	18.34	0.09	6.62	0.04	5.43	0.08	0.69	1.18	0.95	1.03
	353	m 1 00	0.00	10 00	0.32	18.26	0.08	6.66	0.04	0.00	0.08	0.11	1,20	0.95	
	354	71.08	0.05	1	0.34	10.10	0.05	6.70	0.03	0.21	0.09	0.12	1.22		1
	355	71.15		18.22		18.14	0.04	6.73		5.18 5.09	-0.00	0.74	1.23	0.95 0.96	
	356 357	71.21	0.08	17.88 17.53	0.35	10 07	0.03	6 70	0.03	5.00	0.09	0.78	1.26	0.97	
	358	71.40	0.11	17.17	0.36	18.05	-0.02	6.81	0.02	4.91	0.09	0.80	1.27	0.98	1.07
	359	71.52	0.12	16.80	0.37	18 05	0.00	6.83	0.02	4.81	0.10	0.02	1.28	0.99	
	360	71.67		16.43	31	18.06		6.84		4.71		0.84	1.29	-0.99	_1.07

						TABL	EX	Apa	3 .Cc	ntinu	ed.				
		14 0	73100	1, 1								14 00	1, 0	1.	1.
	Arg.			(v.s.1)				-							(v.c.4)
	360	71.67	"	16.43	"	18.06	"	6.84	"	4.71	"	0.84	1.29		
	361	71.84	0.17	16.05	-0.38 0.38	18.08	+0.02	6.84	0.00	4.61	_0.10	0.87	1.30	1.00	1.07
	362 363	72.02	0.22	15.67 15.28	0.39	18.12 18.17	0 0	10.04	0.00	4.51	0.10	0.89	1.31 1.31	1.01 1.02	1.07
1	364	72.48	0.24	14.89	0.39	18.24	0.07	6.83		4.31	0.10	0.94	1.32	1.02	1.07
ı	365	72.73	+0.27	14.50	0.39	18.32		6.81	0.03	4.21	0.10	0.96	1.32	_1.03	1.07
ı	366 367	73.00	0.30	14.11 13.71	-0.39 0.40	18.42 18.53	+0.10 0.11	6.79	0.03	4.11	0.10	0.98 1.01	$\frac{1.32}{1.32}$	1.03	1.06
1	368	73.62	0.32	13.31	0.40	18.66	0.13	6.73	0.03	3.90	0.11	1.01	1.32	1.04 1.05	1.06
ı	369	73.96	0.34	12.91	0.40	18.81	0.15	6.68	0.05	3.80	0.10	1.06	1.31	1.06	1.05
ı	370 371	74.33	+0.38	12.51 12.10	-0.41	18.97 19.15	+0.18	$6.63 \\ 6.58$	_0.05	3.70 3.60	_0.10	1.08	1.30	-1.07	_1.05
1	372	75.12	0.41	11.70	0.40	19.35	0.20	6.52	0.06	3.51	0.09	$\begin{array}{c c} 1.10 \\ 1.12 \end{array}$	$\frac{1.29}{1.28}$	$1.07 \\ 1.07$	$\frac{1.05}{1.04}$
1	373 374	75.54	0.45	11.30 10.90	0.40	19.57	0.23	6.46	0.07	$\frac{3.41}{3.32}$	0.10	1.14	1.27	1.08	1.04
1	375	76.45	0.46	10.50	0.40	19.80 20.04	0.24	6.39 6.32	0.07	3.23	0.09	1.16	1.25	1.08	1.03
1	376	76.94	-0.49	10.10	-0.40	20.30	+0.26	6.24	-0.08	3.15	-0.08	1.18	1.23 1.22	-1.08 $1.08$	-1.02 $1.00$
I	377 378	77.44	0.50	9.71 $9.32$	0.39	20.58 20.89	0.28	6.15	0.09	3.07 $2.99$	0.08	1.22	1.20	1.08	0.99
l	379	78.51	0.55	8.93	0.39	21.21	0.32	$6.06 \\ 5.96$	0.10	2.99	0.07	1.23 1.25	1.19	1.08	$0.98 \\ 0.97$
L	380	79.08	0.57	8.54	0.39	21.55	0.34	5.85	0.11	2.85	0.07	1.26	1.13	-1.08	_0.96
۱	381 382	79.66 + 80.27	0.01	8.16 <sup>-</sup> 7.79	-0.38	21.91 22.28	0.37	5.74	0.11	2.78 2.72	0.06	1.27	1.11	1.07	0.96
ı	383	80.90	0.63	7.43	0.36	22.23	0.39	5.63 5.51	0.12	2.67	0.05	1.28	1.09	1.07	0.95
ı	384	81.54	0.64	7.07	0.36	23.08	0.41	5,39	0.12	2.62	0.05	1.29	1.04	1.06	0.93
ı	385 386	82.19 82.87+	-0.68	6.73 6.39	-0.34	23.51 23.95	+0.44	5.27	-0.13	$\frac{2.58}{2.55}$	-0.03	1.29	1.01	-1.06	-0.92
ı	387	83.56	0.69	6.06	0.33	24.41	0.46	5.14 <sup>-</sup> 5.01	0.13	2.53 $2.53$	0.02	1.29	0.98	1.06	$0.92 \\ 0.92$
L	388 389	84.27 85.01	0.71	5.74	0.32	24.89	0.40	4.87	0.14	2.51	0.02	1.28	0.93	1.04	0.91
ı	390	05 55	0.74	5.42	0.30	25.38	0.51	4.73	0.14	4.40	0.00	1.28	0.91	1.03	0.91
ı	391	86.51 +	-0.76	4.84	-0.28	25.89 26.42	-0.53	4.59 4.45	-0.141	$\frac{2.49}{2.49}$	0.00	$\begin{bmatrix} 1.27 \\ 1.26 \end{bmatrix}$	0.88	$\begin{bmatrix} -1.02 \\ 1.01 \end{bmatrix}$	$-0.90 \\ 0.90$
L	392 393	27 90	0.78	4.56	0.28	26.96	0.54	4.31	0.14	2.49 2.50	0.02	1.25	0.83	1.00	0.90
	394	88 80	0.81	4.30	0.24	27.51 28.08	0.57	$4.16 \\ 4.02$	0.14	2.52 $2.55$	0.03	1.23 1.22	0.81 0.78	0.99	0.90
	395			3.83	0.23	00.07	0.59	0.05	0.15	0 50	0.03	1.20	0.76	-0.97	-0.90
	396 397	89.71 + 90.54 + 91.39		3.61	0.20	29.27	0.00	3.73	-0.14	$2.63^{+}$	0.05	1.17	0.74	0.95	0.91
	398	92.25	0.86	3.22	0.19	29.88 30.50	0.62	3.58 3.44	0.14	$2.68 \\ 2.74$	0.06	1.15	0.72	0.94	0.91 0.92
	399		0.89	3.06	0.16	31.14		3.30		2.81	0.07	1.10	0.69	0.92	0.92
	400 401	$94.02 \\ 94.92 +$	0.90	2.91 2.77	-0.14	31.79 32.45 +		3.16		2.88		1.08	0.68	-0.91 -	-0.93
	402	95.83	0.91	2.65	0.12	33.11	0.00	$\frac{3.02}{2.89}$	0.13	2.96+ 3.06		1.05	0.67	0.91	0.93
	403 404	96.75 97.68	0.92	2.56 2.48	0.09	33.79	0.08	2.76	0.13	3.16	0.10	0.99	0.65	0.90	0.95
	405	98 69	0.94	2.43	0.05	34.48 35.17	0.69	2.64	0.12	3.27	0.12		0.65	0.89	0.96
	406	99.57+	0.95	9 30 -	-0.04	35.87	-0.70	= . II	-O. II	$\frac{3.39}{3.51}$ +	-O. I 2		0.64	$ \begin{array}{c c} -0.89 \\ 0.89 \end{array} $	-0.97 $0.99$
1	407	100.00	0.96	2.37 - 2.37	0.00	36.58	0.71	2.31	0.10	3.64	0.13	0.87	0.65	0.89	1.01
	409	102.47	0.97	$\frac{2.37}{2.39} +$	-0.02	37.30 38.02	0.72	2.20 $2.10$	0.10	3.78 3.93	0.15		0.65	$0.90 \\ 0.90$	1.02
	410	103 46	0.99	2.44	0.05	38.74	0.72	2.01	0.09	1.08	0.15		0.67	-0.90	-1.04
	411 412	104.45 + 105.44	0.99	$\frac{2.52}{2.52} + \frac{2.61}{2.61}$	0.08	39.47	-0.73	1.93	-0.08	1.23+	0.15	0.74	0.69	0.91	1.05
	413	106.44	1.00	2.72	0.11	40.19 40.92	0.73	1.86	0.07	1.39	0.17		$0.70 \\ 0.72$	$0.91 \\ 0.92$	1.07
	414	101.44	1.00	2,00	0.13	41.66		1.73		1.73			0.74	0.92	1.09
	415	$\frac{108.44}{109.45}$ +	1.01	$\frac{3.00}{3.18} +$		42.39 43.12+		1.69		1.91 5.09+	0.78		0.77 -	-0.92 -	-1.10
	417	110.46	1.01	3.38	0.20	43.12	0.72	$1.65$ $^{-}$	0.03	$5.09^{+}$ $5.27^{-}$			$0.79 \\ 0.82$	0.93	1.10
	418 419	111.41	1.02		0.22	44.57	0.73	1,60	0.02	5.46	0.19	0.56	0.85	0.96	1.11
		113.51	1.02		0.27	45.29 46.01	0.72	1,59	0.00	6.65	0.19		0.88	0.97	1.12
				1.14		10.01		1,59		5.84		0.53	0.92  -	-0.98 -	-1.12

				TABLE X,	Ana. 3.—Con	stinued.				
A	rg.	(v.c.0) Diff.	(v.s.1) Diff.	(v.c.1) Di	ff. (v.s.2) Diff.	(v.c.2) Diff.	(v.s.3)	(v.c.3)	(0.8.4)	(v.c.4)
-		" "	" "	" "	" "	11 11	"	"	11	11
	20	113.51 114.53 +1.02	4.12	46.01 +0.	1.59	5.84	0.53	0.92	-0.98	-1.12
	22	115.55	1 72 0.31	17 11 0.	1 63 0.03	6.04 +0.20	0.52 0.51	0.95	0.99	1.12
	23	116.57 1.02	5.07	48.10	1.65	6.42 0.19	0.50	1.02	1.02	1.11
	24	114.39	0.38	45.19 0.0	0.06	0.19	0.49	1.06	1.03	1.11
	25 26	$\frac{118.59}{119.59 + 1.00}$	5.80 6.21 +0.41	49.48 50.15 +0.0	7 1.81 +0.06	6.80	0.49	1.10	-1.04 $1.06$	-1.11 1.10
	27	120.59 1.00	6.63 0.42	50.80 0.0	5 1.88 0.07	7.17 0.19	0.49	1.13	1.08	1.10
	28	121.60 1.01 122.59 0.99	7.07 0.44	51.44 o.6 52.06 o.6	. 1.00	7.35 0.18	0.50	1.22	1.09	1.10
	29	0.00	0.49	0.0	0.10	0.18	0.51	1.26	1.10	1.09
	30	123.58 124.57 +0.99	8.03 8.54 +0.51	52.67 53.27 +0.0	2.16 2.26 +0.10	7.70	0.53	1.30	-1.11 1.11	-1.09 $1.08$
4	32	125.55 0.98	9.08 0.54	53.85 °.	8 2.38 0.12	8.03 0.16	0.56	1.38	1.11	1.07
	33 34	126.52 0.97 127.48 0.96	9.62 0.54 10.18 0.56	54.41 °.5	2102	8.19 0.16	0.58	1.41	1.12 1.12	1.06 1.05
	35	0.96	10.76	55.48	1 20 0 0	8.48	0.64	1.48	-1.13	-1.04
	36	129.38 +0.94	11.37 +0.01	55.99 +0.	1 2.96 +0.15	8.62 +0.14	0.66	1.51	1.13	1.02
	37	130.31 0.93	11.99 0.02	56.48	( 0.10	8.74 0.12	0.70	1.54	1.13	1.00
	38	131.24 0.93	13 96 0.64	57.38	14 3.47 0.17	8.86 0.12	0.73	1.57	1.13	0.99
	40	199 06	13.93	57.80	2 0.18	9.07	0.82	1.61	_1.13	0.97
4	41	133.95 +0.89	14.61 +0.68	58.19 +0.	39 3.84 +0.19	9.16 +0.09	0.86	1.63	1.12	0.95
_	43	131.33 0.87	15.31 °.7° 16.01 °.7°	58.56 o.3	4.04	9.24 0.08	0.90	1.64	1.12 1.12	0.93
	44	134 55 0.85	16.73 0.72	59.22 0.3	2 4.44 0.20	9.37 0.06	0.99	1.66	1.11	0.91
4	45	137.39	17.45	59.51	4.65	9.42	1.04	1.67	_1,11	_0.90
_	46	138.21 +0.82	18.19 +0.74	59.78 +0.	1 1.00	9.45 +0.03	1.09	1.67	1.09	0.90
	47	139.81 0.79	18.93 0.74	60.02	0 5 99 0.21	9.49 +0.01	1.13	1.67	1.07	0.89
	49	140.59 0.78	20.45 0.77	60.40	8 5 10 0.21	9.49 0.00	1.23	1.65	1.05	0.87
_	50	141.36	21.22	60.55	E #1	9.48	1.28	1.64	-1.04	0.86
	51 52	142.11 +0.75 143.83 0.72	21.99 +0.77 22.77 0.78	60.67		9.45 -0.03	1.32	1.62	1.02	0.86
_	53	143.54 0.71	93 55 0.78	00 00 0.0	0.21	9.38 0.04	1.41	1.58	0.99	0.86
4	54	144.23 0.69	24.33 0.78 0.78	60.85 +0.0	6.55 0.21	9.32 0.06	1.45	1.55	0.98	0.86
	55	144.91	25.11 25.89 +0.78	60.85 -0.6	6.75 6.96 +0.21	9.25	1.49	1.52	-0.97	-0.86
	56	148 19 0.03	96 67 0.10	60.76	17.15	0.10	1.53	1.49	0.95	0.87
4	58	146.81 0.02	27.45	60.66	7.35 0.18	8.97	1.60	1.41	0 91	0.88
	59	0.58	0.77	60.54	16 1.33 0.17	0.12	1.63	1.37	0.90	0.88
	60	147.98 148.54 0.53	$\frac{28.99}{29.75}$ +0.76	60.38 -0.	18 7.70 +0.17	8.74	1.66	1.33	0.89 0.88	-0.89 0.90
4	62	149.07	30.51	59.98	8.04	8.46 0.14	1.70	1.24	0.87	0.91
	63	149.59 0.49	39 00 0.74	50 45 0.:	8 0.20 0.15	18 3	1.72	1.19	0.86	0.92
	65	150.54	32.73	50.14	0.14	7.97	1.74	1.09	_0.85	-0.94
	66	150 98 +0.44	22 15 70. 12	50 01	8.62 +0.13	7.79 -0.18	1.75	1.03	0.85	0.96
	67	151.40 0.42	34.16 0.69	58.44	O TI	7.61 0.10	1.75	0.98	0.85	0.98
	68	151.80 0.38	34.85 0.67	57 69 0.4	13 8 95 0.10	7.22 0.20	1.75	0.93	0.85 0.85	1.00
			90.10	0.,	0.00	7.01	1.73	0.82	-0.85	-1.03
4		152.53 152.87 0.31	36.83	56.69	0.00	6.81 -0.20	1.72	0.77	0.86	1.05
	72	153.18 0.28	31.40 0.61	55.18 0.1	4 0 00 0.05	6.60 0.22	1.70	0.72	0.86	1.07
	74	153.72 0.26	38.67 0.60	55.09	5 0 07 0.05	6.16	1.66	0.62	0.87	1.10
19.7	75	152 95	39.24	54.51	0.03	5.93	1.63	0.58	-0.88	-1.11
4	76	154.16 +0.21	39.79 +0.55	53.91 -0.0	3 0 00 +0.01	5.71 -0.22 5.48 0.23	1.60	0.54	0.90	1.12
	77	154.51 0.17	40.82 0.50	50.20 0.0	0 0 21 -0.01	5.25 0.23	1.56 1.53	0.50	0.91	1.13
	79	154.66 0.15	41.31 0.49	51.94 0.0	0.02	5.03 0.22 0.21	1.48	0.42	0.93	1.15
4	80	154.77	41.77	51.25	9.25	4.82	1.44	0.39	-0.94	-1.16

					ŋ	TABLE	X, A:	rg. 3.—	- Con	tinued.					
	Arg.	(v.c.0)	Diff.	(v.s.1)	Diff.	(v.c.1)	Diff.	(v.s.2)	Diff.	(v.c.2)	Diff.	(v.s.3)	(v.c.3)	(v.s.4)	(v.c.4)
	400	"	"	"	"	"	"	"	"	"	11	"	//	11	- "
	480 481	154.77 154.86	-0.09	41.77	+0.43	51.25 50.53	-0.72	$\frac{9.25}{9.20}$	-0.05	$\begin{vmatrix} 4.82 \\ 4.60 \end{vmatrix}$	-0.22	1.44	0.39	0.94	_1.16
	482	154.86	0.07	42.20	0.41	49.80	0.73	9.20	0.05	4.60	0.21	1.35	$0.36 \\ 0.34$	0.96	1.16
	483	174 00	0.05	42.99	0.38	49.04	0.76	9.08	0.07	4.17	0.22	1.30	0.31	1.00	1.16
	484	154.98	-0.01	43.34	0.35	48.28	0.76	9.00	0.08	3.96	0.2I 0.2I	1.25	0.30	1.01	1.16
	485	754 00	0.0.	43.67		47.49		8.90		3.75		1.20	0.28	_1.02	_1.16
	486 487	154.95	0.03	43.67	0.27	46.69	0.80	8.90	0.11	3.54	0.20	1 15	0.27	1.04	1.15
	488	154.90 154.82	0.08	44.25	0.24	45.88	0.83	8.69	0.12	3.34	0.19	1 10 1.04	0.26	1.06	1.15
	489	154.72	0.10	44.45	0.22	45.05 44.21	0.84	8.44	0.13	3.15 2.98	0.17	0.99	0.26	1.08	1.15
	490	154 59	0.13	44.90	0.19	12 27	0.84	8 30	0.14	2.81	0.17	0.94	0.27	_1.10	
1	491	154.45	-0.14	45.05	+0.15	42.51	_0.86	8.14	-0.16	$\begin{vmatrix} 2.61 \\ 2.64 - \end{vmatrix}$	-0.17	0.88	0.28	1.11	-1.14 $1.13$
	492	154.28	0.17	45.18	0.13	41.64	0.07	7.98	0.10	2.49	0.15	0.83	0.29	1.12	1.12
	493 494	154.08	0.21	45.28	0.10	40.77	0.87	1.01	0.17	W. U.	0.15	0.78	0.30	1.13	1.11
	495	153.87	0.24	45.35	0.03	39.90	0.89	7.64	0.19	2.20	0.13	0.74	0.32	1.14	1.10
	496	153.63 153.37	_o.26	45.38 45.39	+0.01	39.01 38.12	_0.80	$\begin{vmatrix} 7.45 \\ 7.26 \end{vmatrix}$	-0.10	$\begin{vmatrix} 2.07 \\ 1.95 \end{vmatrix}$	-0.12	0.69	0.35	-1.15	1.09
	497	153.09	0.28	45.37	-0.02	37.24	0.00	7.06	0.20	1.95	0.11	0.65	0.38	1.15 1.15	1.07
	498	152.79	0.30	45.32	0.05	36.35	0.89	6.86	0.20	1.74	0.10	0.56	0.44	1.16	1.03
	499	152.46	0.33	45.23	0.09	35.46	0.89	6.66	0.20	1.66	0.08	0.53	0.47	1.16	1.01
	500	152.11		45.12		34.57		6.45		1.59		0.49	0.51	-1.17	0.99
	$501 \\ 502$	151.74	0.38	44.00	0.14	33.68	0.88	6.23	0.21	1.54	0.05	0.46	0.55	1.17	0.97
	503	151.36 150.95	0.41	44.81	0.21	32.80 31.92	0.88	6.02 5.80	0.22	1.49	0.04	0.43	0.59	1.16	0.95
	504	150.52	0.43	44.38	0.22	31.04	0.88	5.59	0.21	1 49	0.03	0.39	0.64	1.16	0.93
	505	150.08	0.44	44.12	0.26	30.18	0.86	5.37	0.22	1.40	-0.02	0.37	0.73		
ä	508	149.61	-0.47	43.84	-0.28	29.32	-0.86	5.15	-0.22	1.40	0.00	0.36	0.78	-1.15 $1.13$	-0.90 $0.89$
	507 508	148.13	0.48	43.52	0.32	28.46	0.86	4.93	0.22	7 10	0.00	0.35	0.83	1.11	0.87
	509	148.63 148.11	0.52	43.18 42.82	0.36	27.62	0.82	4.72	0.21	1.40	0.03	0.34	0.87	1.10	0.86
	510		0.53		0.40	26.80	0.82	4.51	0.21	1.46	0.05	0.34	0.92	1.09	0.85
	511	147.58 147.03	-0.55	42.42 42.00	-0.42	25.98 25.17	_0.81	$\frac{4.30}{4.09}$	-0.21	$\begin{vmatrix} 1.51 \\ 1.57 \end{vmatrix}$ +	0.06	0.34	0.97	-1.08	0.84
	512	146.46	0.57	41.56	0.44	24.38	0.19	3.89	0.20	1.64	0.07	0.34 0.35	$1.02 \\ 1.06$	1 06 1.04	0.84
	513 514	145.87	0.59	41.09	0.47	23.61	0.77	3.69	0.20	1 72	0.08	0.36	1.11	1.02	0.83
		145.27	0.61	40.60	0.51	22.85	0.74	3.50	0.19		0.09	0.37	1.16	1.01	0.83
	515 516	144.66	-0.62	40.09 39.55	-0.54	22.11		3.32		$\frac{1.90}{2.01}$ +	0.77	0.39	1.20	-1.00	0.82
	517	144.04		39.55	0.50	21.38	0.70	3.14	0.16		0.11	0.41	1.24	0.00	
	518	142.74	0.66	38.41	0.58	19.99	0.69	$\frac{2.98}{2.82}$	0.16	2.12 2.25	0.13	0.43	$\frac{1.28}{1.32}$	$0.96 \\ 0.94$	0.82 0.83
	519	142.07	0.67	37.81	0.60	19.32	0.67	2.66	0.16	2.39	0.14	0.49	1.35	0.92	0.83
	520	141.39		37.19		18.68		2.51	0.15		0.14	0.52	1.39	-0.90	0.84
	$\frac{521}{522}$	140.70	0.70	36.56	0.65	10.00	-0.63 0.60	2.38	0.13	2.68	0.15	0.55	1.42	0.98	0.85
	523	$140.00 \\ 139.29$	0.71	35.91 35.25	0.66	17.45	0.58	2.25	0.13	2.84	0.16	0.58	1.44	0.97	0.87
	524	138.57	0.72	34.57	0.68	16.87 $16.32$	0.55	2.13 $2.03$	0.10	3.00 3.16	0.16	$0.62 \\ 0.66$	1.47	$0.96 \\ 0.95$	0.88
	525	137.84	0.73	33.87	0.70	15.79	0.53	1.94	0.09	2 22	0.17			1000	0.89
	526	137.10	-0.74	33.15	-0.72	15.28	-0.51	1.86	0.08	$\begin{vmatrix} 3.33 \\ 3.51 + \end{vmatrix}$	0.18	$0.70 \\ 0.74$	1.51 $1.53$	-0.94 $0.94$	-0.90 $0.91$
3	527 528	136.35	0.75	32.43	0.72	14.79	0.49	1.78	0.08	3 69	0.10	0.78	1.54	0.93	0.93
1	529	135.59 134.83	0.76	31.70 30.96	0.74	14.34	0.45	1.14	0.06	0.01	0.18	0.82	1.55	0.93	0.95
	530		0.76		0.74	13.91	0.40	1.01	0.04	4.06	0.19	0.86	1.55	0.92	0.97
	531	134.07 133.30	-0.77	30.22 29.46	-0.76	13.51 13.13	-0.38	$\frac{1.63}{1.60}$		4.25	0.19	0.90	1.56	-0.91	_0.99
	532 533	132.52	0.78	28.69	0.77	12.78	0.35	1 50	0.02		0.19	0.94	1.55	$0.91 \\ 0.92$	1.01
	534	131.73	0.79	27.92	0.77	12.46	0.32	1 57-	0.01	4.82	0.19	1.02	1.54	0.92	1.03 1.05
	535	130.94	0.79	27.15	0.77	12.16	0.30	1.58 +	0.01	5 00	0.18	1.06	1.54	0.93	1.07
A.	536	130.15 129.35		26.37	100	11.90		1 60		5 18		1.09	1.53	_0.93	_1.09
	537	129.35 $128.55$	0.00	25.58 <sup>-</sup> 24.81	0.77	11.66	0.21	1.62 +	0.02	5.36+	0.18	1.13	1.51	0.95	1.10
	538	127.75	0.80	24.03	0.78	11.45 11.26	0.19	1.65 1.70	0.05	0.04	0.18	1.17	1.50	0.96	1.12
	539	126.95	0.80	23.25	0.78	11.10	0.16	1.76	0.06	5.12	0.18	1.20 1.23	1.48	0.97	1.13 1.14
	540	126.15		22.48	0.77	10.98	0.12	1.82	0.06	6.07	0.17				
L						20.00		1.04		0.01	-	1.26	1.43	-0.99	-1.15

				Т	ABLE :	X, Are	3. 3.—	-Conti	nued.				45	
Arg.	(v.c.0)	Diff.	(v.s.1)	Diff.	(v.c.1)	Diff.	(v.s.2	) Diff.	(v.c.2)	Diff.	(v.s.3)	(v.c.3)	(v.s.4)	(v.c.4)
	11	19	"	"	11	11	"	"	"	"	"	99	"	"
540	126.15	-0.79	22.48	_0.78	10.98	-0.10	1.82 1.90	Lo.08	6.07	-0.16	1.26	1.43	_0.S9	_1.15
541	125.36° 124.56	0.80	21.70	0.77	10.88	0.08	1.90	0.08	6.23	0.16	1.28	1.41	0.91	1.15
542 543	123.76	0.80	20.16	0.77	10.75	0.05	2.08	0.10	6.54	0.15	1.33	1.36	0.95	1.16
544	122.96	0.80	19.40	0.76	101 4 25	-0.02 +0.01	2.18	0.10	6.69	0.15	1.35	1.33	0.96	1.17
545	122.17	_o.So	18.65	-0.75	10.74	+0.03	2.29		6.83	-0.13	1.37	1.30	0.97	_1.18
546	121.37	0.79	17.90	0.73	10.77	0.06	$\frac{2.40}{2.52}$	0.12	6.96 7 7.08	0.12	1.38	1.26	0.99	1.18
547 548	120.58 119.80	0.78	16.44	0.73	10.92	0.09	2.65	0.13	7.20	0.12	1.41	1.20	1.04	1.18
549	119.03	0.77	15.73	0.71	11.02	0.10	2.79	0.14	7.31	0.11	1.41	1.17	1.06	1.18
550	118.26	-0.76	15.03	_0.69	11.15		2.93	+0.15	7.41	-0.10	1.42	1.14	-1.08	-1.18
551	117.50	0.76	14.34	0.68	11.31	0.18	3.08	0.15	7.51	0.08	1.42	1.11	1.10	1.17
552 553	115.99	0.75	12.99	0.67	11.69	0.20	3.38	0.15	7.67	0.08	1.41	1.04	1.13	1.15
554	115.24	0.75	12.35	0.64	11.91	0.22	3.54	0.16	7.73	0.06	1.41	1.01	1.14	1.14
555	114.50		11.71	_0.62	12.16		3.70	+0.16	7.79	+0.04	1.41	0.98	-1.15	-1.13
556	113.77	0.73	11.09	0.61	12.43 12.71	0.28	3.86	0.16	7.83	0.04	1 40	0.95	1.15	1.11
557 558	113.05	0.70	9.89	0.59	13.02	0.31	4.19	0.17	7.90	0.03	1.38	0.90	1.17	1.07
559		0.70	9.32	0.57	13.35	0.33	4.35	0.16	7.92	0.02	1.36	0.87	1.18	1.05
560		- 60	8.76		13.69		4.51	+0.16	7.93	+0.01	1.34	0.85	-1.19	-1.03 1.01
561 562		0.66	8.23	-0.53 0.52	14.04	+0.35	4.67	0.17	7.94	-0.01	1.32	0.83	1.19	0.99
563		0.65	7.21	0.50	14.81	0.39		0.16	7.92	0.01	1.28	0.79	1.19	0.97
564		0.65	6.73	0.48	15.22	0.41	5.16	0.16	7.90	0.02	1.20	0.77	1.19	0.95
565		060	6.26	- 11	15.64	+0.43	5.32	+0.15	7.87	-0.04	1.24	0.76	-1.19 $1.17$	-0.93 $0.91$
560		0.60	5.82 5.39	0.43	A tra	0.45	5.47	0.15	7.78	0.05	1.20	0.73	1.16	0.89
568		0.00	4.98	0.41	16.98	0.46	5.77	0.15	7.73	0.05	ALAS	0.72	1.15	0.87
569		0.58		0.38	17.45	0.47	5.91	0.14	4 - 10 4	0.00	1.10	0.72	1.14	0.86
570		0.55	4.23	_0.36	17.93	+0.49	6.05	+0.14	7.60	-0.08	1.12	0.71	-1.13 1.11	-0.85 0.85
571			1 3.01	0.33	18.42	0.50	6.19	0.13	7.44	0.08	1.07	0.71	1.09	
578	103.13	0.52	3.22		19.42	0.50	6.44	0.12	1.00	0.09	A.UT	0.71	1.07	0.83
574	102.62	0.51	1 00 - 1/13	0.29	13.00	0.52	0.00	0.12	1.20	0.09	1.02	0.71	-1.04	1 200
575			2.65	-0.20	20.45	+0.52	6.68	+0.11	7.17	-0.11	1.00		1.02	
570		0.48	9 15	0.24	21.49	0.54	6 89	0.10	6.95	0.11	0.95	0.72	1.00	0.81
578	100.69	0.40	1.92	0.23	22.03	0.54	6.98	0.00	0.04	0.11	0.00		0.98	
579		0.44		0.18	22.00	0.54	1.01	0.00	6.13	0.12	0.01		-0.94	
580		-0.43	1.53	-0.10	23,12	+0.5	7.16	+0.08	6.61	_0.13	0.89		0.92	
583 583		0.41	1.19	0.16	24.21	0.55	7.30	0.06	6.35	0.13	0.85	0.78	0.90	
583	98.57	0.41	1.06	0.13	24.77	0.50	1.00	0.00	6,23	0.13	0.00		0.88	
58	-	0.38	3 0.00	0.11	25,00	0.55	1.72	0.05	6.10	0.13			-0.86	0.000
588	97.80	-0.37	0.82	0.00	25 88	+0.50	7.47	+0.00	5.97	_0.14	0.80		0.80	0.87
586 58'		0.30	0.65	0.08	27.00	0.50	7.55	0.0	5.69	0.13	0.10		0.85	
58	96.72	0.35	0.58	0.07		0.56	1,000	0.0		0.13	0.77		0.84	The second second
599		0.34	1	0.0	20.	0.50	7 00	0.01	5 00	0.13	0.76		-0.89	
590			0.50	0.0	28.68	+0.50	7.62	+0.01	5.14	-0.13	0.76	0.96	0.89	0.96
59		0.3	0 10	-0.01	90 79	0.5	7.63	0.00	5.01	0.13	4 0.10		0.82	
59	95.08	0 21	0.47	+0.0	30.35		7.63	-0.01	4.87	0.17	0.76		0.81	
59		0.31	0.40	0.0	30.01	0.5	7 60	0.0.	4 60	0.13	0.76		-0.81	
59 59		-0.31	0.52	+0.0	31.46	+0.5	7.58	-0.0	4.47	-0.1	0 77	1.06	0.89	1.06
59	7 93.85	0.30	0.63	0.00	32.50	0.5	7.55		4.34	0.1	0.10		0.83	
59			V . I V	0.01		0.50	7.46	0.0	4.08	0.1	3 0.79		0.85	
59		0.30	0.87	0.0	34.22	0.5	7.42	0.0	3.95	0.1	0.80		-0.85	1.13
60	0 92.96		0.31		04.22		1.72		10.00				1	1

ì				ŗ	FABLE	E X, A	RG. 3.—	Continued.				
	Arg.	(p.c.0)	(p.s.1)	(p.c.1)	(ρ.8.2)	(p.c.2	Arg.	(p.c.0)	(ρ. ε. 1)	(p.c.1)	(p.s.2)	(p.c.2)
	0 1 2 3 4	524 525 525 526 527	180 178 176 174 172	89 90 90 91 91	49 50 50 51 52	58 58 57 57 56	60 61 62 63 64	746 747 748 749 749	17 17 16 16 16	244 249 255 260 266	33 32 30 29 27	10 11 11 11 11
	5 6 7 8 9	528 529 531 533 535	170 168 165 163 161	92 92 92 93 93	53 54 55 55 56	56 55 55 54 53	65 66 67 68 69	750 750 750 750 750 749	16 16 17 17 18	271 277 282 287 293	26 24 23 22 20	12 13 13 14 14
	10 11 12 13 14	538 540 543 546 550	158 156 154 151 149	94 94 95 96	57 57 58 59 59	53 52 51 50 49	70 71 72 73 74	748 747 746 744 742	19 21 22 24 26	298 303 308 313 318	19 18 17 16 14	15 16 17 18 19
	15 16 17 18 19	553 557 560 564 568	146 144 141 138 135	97 98 99 100 101	60 60 61 61 62	48 47 46 45 44	75 76 77 78 79	740 787 734 731 728	29 31 34 37 40	323 327 332 336 340	13 12 11 10 09	20 21 22 23 24
	20 21 22 23 24	573 577 582 586 591	132 129 126 123 120	102 103 105 106 108	62 62 62 63 63	44 42 41 40 39	80 81 82 83 84	.724 721 717 713 708	43 47 51 55 59	344 348 352 355 359	09 08 07 07 06	26 27 28 30 31
	25 26 27 28 29	596 601 606 611 617	117 113 110 107 103	109 111 113 115 117	63 63 63 63 63	38 37 36 34 33	85 86 87 88 89	703 698 693 688 682	63 68 72 77 82	362 364 367 369 372	06 05 05 05 05	33 34 36 37 39
	30 31 32 33 34	622 627 633 638 643	96 93 90	119 121 123 126 129	62 62 62 62 61	32 31 30 29 28	90 91 92 93 94	676 670 663 657 650	87 92 97 102 108	373 375 376 378 378	05 05 05 05 05 06	41 42 44 45 47
	35 36 37 38 39	648 654 659 664 669	79 76 72	132 135 139 142 145	61 60 60 59 58	27 26 24 23 22	95 96 97 98 99	643 636 629 622 614	114 119 125 130 136	379 379 379 379 379	06 06 07 08 08	48 50 51 52 54
	40 41 42 43 44	674 680 685 689 694	62 58 55	149 152 156 160 164	58 57 56 55 54	21 20 19 18 18	100 101 102 103 104	606 598 590 582 574	141 147 153 159 164	378 377 376 374 373	09 10 11 12 13	55 56 57 58 60
	45 46 47 48 49	698 703 707 711 715	46 43 40 37	168 173 177 182 186	53 52 51 50 49	17 16 15 14 14	105 106 107 108 109	565 557 548 539 530	170 176 181 186 192	371 368 366 363 360	14 15 16 17 19	61 62 62 63 64
	50 51 52 53 54	719 722 726 729 732	32 30 28 26	191 196 201 206 211	47 46 45 43 42	13 13 12 12 11	110 111 112 113 114	521 512 503 494 484	197 202 207 212 217	357 353 350 346 342	20 21 23 24 25	64 65 65 66 66
	55 56 57 58 59	735 737 740 742 744	22 21 19 18	216 222 227 233 238	40 39 38 36 35	11 11 11 11 10	115 116 117 118 119	475 465 456 446 436	222 227 231 235 239	338 333 329 324 319	27 28 30 31 32	66 67 67 67
	60	746	17   9	244	33	10	120	427	243	314	34	66

1				.7	FABLE	X, Ai	ag. 3.— <i>C</i> e	ontinued				
	Arg.	(ρ.c.0)	(ρ.8.1)	(p.c.1)	(p.s.2)	(p.c.2)	Arg.	(p.c.0)	(p.s.1)	(p.c.1)	(p.s.2)	(p.c.2)
	120 121 122 123 124	427 417 407 397 387	243 247 250 254 257	314 309 303 298 292	34 35 37 38 39	66 66 65 65	180 181 182 183 184	11 10 9 9 8	172 168 165 162 159	66 66 67 67 68	26 25 25 24 24	33 33 34 35 36
	125 126 127 128 129	378 368 359 349 339	260 263 266 268 270	286 280 274 268 262	41 42 43 44 45	64 63 63 62 61	185 186 187 188 189	8 8 8 9	156 153 150 147 144	69 71 72 74 75	24 24 23 23 23	37 38 39 40 41
	130 131 132 133 134	330 320 310 301 292	272 274 275 277 278	256 250 244 238 232	46 47 48 49 50	60 59 58 57 56	190 191 192 193 194	10 11 13 14 16	141 138 136 133 131	77 79 81 84 86	23 24 24 24 24 24	42 43 44 45 46
The state of the s	135	282	279	225	50	55	195	18	129	89	25	47
	136	273	279	219	51	54	196	21	127	91	25	48
	137	263	280	213	52	52	197	23	125	94	26	49
	138	254	280	207	52	51	198	26	123	97	26	50
	139	245	280	201	52	50	199	29	121	99	27	51
	140	236	280	195	53	49	200	32	120	102	28	52
	141	227	280	189	53	47	201	36	118	105	28	52
	142	218	280	183	53	46	202	39	117	108	29	53
	143	209	279	177	53	45	203	43	116	112	30	54
	144	201	278	171	53	44	204	47	114	115	31	54
	145	193	277	165	53	42	205	51	113	118	32	55
	146	184	275	160	53	41	206	55	112	122	33	55
	147	176	274	154	52	40	207	60	112	125	34	56
	148	168	272	149	52	39	208	65	111	129	35	56
	149	160	271	144	52	38	209	69	111	132	36	57
	150	152	269	139	51	36	210	75	110	135	37	57
	151	145	267	134	51	35	211	80	110	139	38	57
	152	137	265	129	50	35	212	85	110	143	39	57
	153	130	263	124	49	34	213	91	110	146	40	57
	154	123	260	120	49	33	214	96	110	150	41	57
	155	116	257	115	48	32	215	102	110	153	42	57
	156	109	255	111	47	31	216	108	110	157	43	57
	157	103	252	107	46	30	217	114	110	160	44	57
	158	96	249	103	45	30	218	120	111	164	45	57
	159	90	246	100	45	29	219	126	111	168	46	57
	160	84	243	96	44	29	220	133	113	171	47	57
	161	78	240	93	43	28	221	139	114	175	48	56
	162	73	236	90	42	28	222	145	115	178	49	56
	163	67	233	87	41	27	223	152	116	182	50	55
	164	62	229	84	40	27	224	159	117	185	50	55
	165	57	226	81	39	27	225	166	118	188	51	54
	166	53	222	79	38	27	226	173	119	192	52	53
	167	48	219	77	36	27	227	180	120	195	53	52
	168	44	215	75	35	27	228	187	122	198	54	52
	169	40	212	73	34	27	229	194	123	201	54	51
	170	36	208	71	33	27	230	201	125	204	55	51
	171	32	204	70	32	27	231	208	127	207	55	50
	172	29	201	68	31	28	232	216	128	210	56	49
	173	26	197	67	30	28	233	223	130	213	56	49
	174	23	193	67	29	28	234	230	132	216	57	48
	175	21	190	66	28	29	235	238	134	218	57	47
	176	18	186	66	28	30	236	245	136	221	57	46
	177	16	182	65	27	30	237	253	138	224	58	45
	178	14	179	65	27	31	238	260	140	226	58	45
	179	12	175	65	26	32	239	268	142	228	58	44
	180	11	172	66	26	33	240	275	144	231	58	43

-				TA	BLE X	, Arg.	3.—Cont	inued.				
	Arg.	(p.c.0)	(ρ.ε.1)	(p.c.1)	(p.s.2)	(p.c.2)	Arg.	(p.c.0)	(ρ.8.1)	(p.c.1)	(p.s.2)	(p.c.2)
	240 241 242 243 244	275 283 290 298 305	144 146 148 150 152	231 233 235 237 239	58 58 58 58 58	43 42 41 40 40	300 301 302 303 304	562 562 562 561 560	208 208 208 208 208	250 250 250 250 250 250	42 42 42 42 41	32 32 32 32 32
	245 246 247 248 249	313 320 328 335 342	154 156 159 161 163	240 242 244 245 246	57 57 57 57 57	39 38 38 37 36	305 306 307 308 309	559 558 557 555 553	208 208 208 208 208	250 250 250 251 251	41 41 41 41 40	31 31 31 31 30
	250 251 252 253 254	350 357 364 371 378	165 167 169 171 173	248 249 250 251 252	56 56 55 55 54	36 35 34 34 33	310 311 312 313 314	551 549 547 544 542	208 209 209 209 210	251 251 251 251 251 251	40 40 39 39 39	30 30 30 29 29
	255 256 257 258 259	385 392 399 406 412	175 177 179 180 182	253 254 254 255 256	54 54 53 52 52	33 33 32 32 32	315 316 317 318 319	539 536 532 529 525	210 210 211 211 212	251 252 252 252 252 252	38 38 38 37 37	29 29 28 28 28
	260 261 262 263 264	419 426 432 438 444	184 185 187 189 190	256 256 257 257 257	51 51 50 50 50	31 21 31 31 31	320 321 322 323 324	521 517 513 509 504	213 213 214 215 216	252 252 252 252 252 252	36 36 35 34 34	28 28 28 28 28
	265 266 267 268 269	450 456 462 468 473	192 193 194 196 197	257 257 257 257 257	49 49 48 48 47	31 31 31 31 31	325 326 327 328 329	500 495 490 485 480	217 218 219 221 222	252 252 252 252 251 251	33 33 32 31 31	28 28 28 28 28
	270 271 272 273 274	478 484 489 494 499	198 199 200 201 202	257 257 257 257 257 256	47 46 46 45 45	31 31 31 31 31	330 331 332 333 334	474 469 463 457 451	223 224 225 227 228	251 250 249 249 248	30 30 29 29 28	28 28 29 29 29
	275 276 277 278 279	503 509 512 517 521	203 203 204 205 205	256 256 256 255 255	45 45 44 44 44	31 31 31 31 32	335 336 337 338 339	446 439 433 427 421	229 231 233 234 236	248 247 246 245 244	27 27 26 25 25	30 30 31 31 31
	280 281 282 283 284	524 528 531 535 538	206 206 207 207 207 207	255 254 254 253 253	44 43 43 43 43	32 32 32 32 32	340 341 342 343 344	414 407 401 394 387	238 239 241 243 244	243 242 241 240 238	24 24 24 23 23	32 33 33 34 35
No. of Contract of	285 286 287 288 289	541 544 546 549 551	208 208 208 208 208 208	253 252 252 252 252 251	43 43 43 43 42	32 33 33 33 33	345 346 347 348 349	380 373 366 359 352	246 248 249 251 253	236 235 233 231 229	23 22 22 22 22 -	35 36 37 38 38
	290 291 292 293 294	553 555 556 558 559	· 208 208 208 208 208 208	251 251 251 251 251 251	42 42 42 42 42	33 33 33 33 33	350 351 352 353 354	344 337 330 323 315	255 256 258 260 261	227 225 223 221 218	21 21 21 21 21 21	39 40 41 42 42
The state of the s	295 296 297 298 299	560 561 562 562 562	208 208 208 208 208 208	250 250 250 250 250 250	42 42 42 42 42	33 33 32 32 32	355 356 357 358 359	308 300 293 285 278	263 264 266 267 269	216 213 211, 208 205	22 22 22 22 22 23	43 44 45 46 47
	300	562	208	250	42	32	360	270	270	203	23	47

			TA	BLE X	, Arg.	3.—Con	tinued.				
Arg.	(p.c.0)	(ρ.8.1)	(p.c.1)	(p.s.2)	(p.c.2)	Arg.	(p.c.0)	(ρ.ε.1)	(µ.c.1)	(p.s.2)	(p.c.2)
360 361 362 363 364	270 263 255 248 241	270 272 273 274 275	203 200 197 194 190	23 23 24 25 25	47 48 49 50 50	420 421 422 423 424	14 16 18 20 22	183 180 176 173 170	69 70 72 74 76	44 44 43 42 41	32 32 32 32 32
365 366 367 368 369	233 226 219 211 204	276 277 278 278 278 279	187 184 181 177 174	26 26 27 28 29	51 52 52 53 53	425 426 427 428 429	24 27 30 33 36	166 163 160 157 153	78 81 83 86 89	41 40 39 38 38	32 32 32 33 33
370 371 372 373 374	197 190 183 176 169	280 280 281 281 281	171 167 164 160 157	29 30 31 32 33	54 54 54 55 55	430 431 432 433 434	40 44 48 53 57	150 147 144 142 139	92 95 99 103 106	37 36 35 35 34	33 34 34 35 36
375 376 377 378 379	162 155 149 142 136	281 281 281 281 281 281	153 150 146 142 139	34 35 36 37 38	55 55 55 55 55	435 436 437 438 439	62 67 72 77 83	136 134 132 130 128	111 115 119 124 128	34 33 33 32 32	36 37 38 39 40
380 381 382 383 384	129 123 117 111 105	280 280 279 278 278	135 132 128 125 122	39 40 41 42 42	55 55 55 55 55	440 441 442 443 444	89 95 102 108 115	126 124 122 121 120	133 138 143 148 153	32 32 31 31 31	40 41 42 43 44
385 386 387 388	99 94 89 83	277 276 274 273 272	118 115 111 108 105	43 44 45 46 47	54 54 53 53 53	445 446 447 448 449	121 128 135 142 150	118 118 117 116 116	159 164 170 176 181	31 31 31 32 32	45 46 47 48 49
389 390 391 392 393	78 73 68 63 59	270 268 266 265 263	102 99 97 94 91	47 48 48 49 49	52 51 50 50 49	450 451 452 453 454	157 165 173 181 189	115 115 115 116 117	187 193 199 205 211	32 33 33 34 34	50 51 52 53 54
394 395 396 397 398	54 50 46 42 39	261 258 256 254 251	88 86 83 81 79	50 50 51 51 51	48 47 47 46 45	455 456 457 458 459	197 206 215 223 232	117 118 120 121 123	217 223 229 236	35 36 36 37 38	55 56 57 58 58
399 400 401 402 403	35 32 29 27 24	248 246 243 240 237	77 75 73 72 70	52 52 52 52 52 52	45 44 43 42 41	460 461 462 463 464	241 250 259 268 278	125 127 129 131 134	248 254 260 265	39 40 41 42 43	59 60 60 61 61
404 405 406 407 408	19 17 15 14 13	234 231 228 225 221	69 68 67 66 65	52 52 51 51 51	40 39 38 38 38	465 466 467 468 469	287 296 306 315 324	137 140 143 147 150	277 283 288 294	44 45 47 48 49	62 62 62 62 62
409 410 411 412 413	12 11 11 10	218 215 211 208 204	64 64 64 64 64	50 50 49 49 48	36 36 35 34 34	470 471 472 473 474	334 343 353 362 372	154 158	305 310 2 315 320	51 52 53 54 55	62 62 62 62 62 62
414 415 416 417 418	10 10 11 12	201 197 194 190	64 65 66 67	48 47 46 46	33 33 33 32	475 476 477 478	382 391 401 411	170 181 180 19	329 1 334 6 338 1 342	57 58 59 60	62 61 61 60 60
419		187 183	68	45	32	479 480	420 430	20			59

			TA	BLE X	, Arg.	3.—Cone	cluded.				
Arg.	(p.c.0)	(ρ.s.1)	(p.c.1)	(p.s.2)	(p.c.2)	Arg.	(p.c.0)	(p.s.1)	(p.c.1)	(ρ. ε. 2)	(p.c.2)
480 481 482 483 484	430 439 449 458 468	202 207 213 218 223	349 353 356 359 361	62 63 64 65 66	59 58 57 56 55	540 541 542 543 544	741 739 737 735 732	381 378 375 372 368	186 181 176 171 167	29 28 27 26 25	19 20 21 22 23
485 486 487 488 489	477 486 496 505 514	230 236 242 248 254	364 366 368 370 371	67 68 69 69 70	54 53 52 51 50	545 546 547 548 549	730 727 724 721 717	365 361 357 353 350	162 158 153 149 145	24 24 23 22 22	24 25 26 27 28
490 491 492 493 494	523 532 540 549 558	260 266 272 278 284	373 374 374 375 375	70 71 71 72 72	49 48 46 45 44	550 551 552 553 554	714 710 706 702 698	346 342 338 333 329	141 137 133 130 126	21 21 21 20 20	29 30 31 32 33
495 496 497 498 499	566 574 583 591 599	289 295 301 307 313	375 374 374 373 872	72 72 72 72 72 72	42 41 39 38 37	555 556 557 558 559	693 689 684 679 674	325 321 316 312 308	123 120 117 114 112	20 20 19 19	34 35 36 38 39
500 501 502 503 504	606 614 621 629 636	318 324 329 334 339	371 369 367 365 363	72 71 71 71 70	35 34 33 31 30	560 561 562 563 564	669 664 659 654 649	303 299 295 290 286	109 107 105 103 101	20 20 20 20 20 20	40 41 42 43 44
505 506 507 508 509	643 649 656 662 668	344 349 353 358 362	360 357 354 351 347	70 69 68 68 67	29 28 27 25 24	565 566 567 568 569	644 638 633 628 623	282 278 274 270 266	99 97 96 94 93	20 21 21 22 22	45 46 47 48 49
510 511 512 513 514	674 680 686 691 696	366 370 374 377 380	344 340 336 332 327	66 65 64 63 62	23 22 21 20 19	570 571. 572 573 574	618 613 608 602 598	262 258 255 251 247	92 91 90 90 89	23 23 24 25 25	50 50 51 52 53
515 516 517 518 519	701 706 710 714 718	383 386 388 390 392	323 318 313 308 303	61 59 58 57 56	18 18 17 16 16	575 576 577 578 579	593 588 583 578 574	244 240 237 234 231	88 88 87 87	26 27 28 28 29	54 54 55 56 56
520 521 522 523 524	721 725 728 731 733	394 396 397 398 399	298 293 287 282 276	54 53 52 50 49	15 15 14 14 14	580 581 582 583 584	570 565 561 557 554	228 225 222 219 216	86 86 86 86	30 31 32 32 33	57 57 58 58 58
525 526 527 528 529	736 738 740 742 743	400 400 400 400 399	270 265 259 253 247	48 46 45 44 42	14 14 14 14 14	585 586 587 588 589	551 547 544 541 539	214 211 209 206 204	86 86 86 86	34 35 36 37 38	58 59 59 59
530 531 532 533 534	744 745 745 (46 746	399 398 397 396 394	242 236 230 225 219	41 40 38 37 36	14 14 14 15 15	590 591 592 593 594	536 534 532 530 528	202 199 197 195 193	87 87 87 88 88	39 40 41 42 43	60 60 60 60
535 536 537 538 539	745 745 744 743 742	392 390 388 386 383	213 208 202 197 192	34 33 32 31 30	16 17 17 18 19	595 596 597 598 599	527 526 525 525 524	190 188 186 184 182	88 88 88 89	44 45 46 47 48	59 59 59 59 59
540	741	381	186	29	19	600	524	180	89	49	58

7	ГАВ.	Х	I		XII.			XIII			XIV.	-		XV.			XVI	
1	IRG.	4			5.			6.			7.		-1.	8.			9.	
		(e.s.1)	(v.c.1)	(0.0.0)	(v.s.1)	(v,c,1)	(0, c.0)	(v.s.1)	(v.c.1)	(v.c.0)	(v.s 1)	(v.c.1)	(0, c.0)	(v.s.1)	(v c.1)	(0.0.0)	(v.s.1)	(v.c.1)
	0	0.67	0.19	1 11	0.03	0.91	0.00	0.19	0.19	0.10	0.10	0.10	0.05	0.15	0.14	0.12	0.10	0.19
ı	10	0.64	0.13	1.12	0.03	0.22	0.06	0.14	0.18	0.10	0.18	0.19	0.09	0.15	0.19	0.12	0.10	0.12
ı	20 30	0.58	0.16	1.11	0.03	0.26	0.07	0.16	0.18	0.10	0.18	0.19	0.22	0.11	0.31	0.11	0.09	0.11
ı	50								0.16									0.09
ı	00 70	0.47	0.21	1.06	0.04	0.31	0.08	0.17		0.10	0.18	0.19	0.50	0.11	0.52	0.09	0.08	0.07
ı	80	0.39	0.26	1.00	0.06	0.34	0.09	0.18	0.13	0.09	0.17	0.18	0.74	0.15	0.67	0.08	0.07	0.06
ı	90								0.12						0.75			0.04
	110 120								0.11									0.02
	130 140	0.20	0.40	0.79	0.12	0.38	0.09	0.18	0.09	0.07	0.14	0.14	1.42	0.34	1.06	0 06	0.06	0.01
L	150	0.14	0.46	0.68	0.16	0.38	0.09	0.18	0.07	0.06	0.12	0.12	1.70	0.45	1.19	0.05	0.06	0.01
	160 170																0.06	
_	180 190								0.04									0.00
_	200 210	0.04	0.59	0.41	0.25	0.35	0.08	0.16	0.04	0.03	0.03	0.07	2.31	0.78	1.43	0.04	0.07	0.00
ı	220	0.02	0.63	0.32	0.28	0.32	0.07	0.14	0.02	0.02	0.00	0.05	2.48	0.92	1.48	0.04	0.07	0.01
_	2:30 240								0.02									0.01
_	250 260																0.08	
Ł	270 280	0.06	0.68	0.14	0.35	0.24	0.05	0.10		0.01	0.03	0.02	2.70	1.21	1.46	0.06	0.09	
Т	290	0.10	0.68	0.10	0.36	0.21	0.04	0.08	0.01	0.00	0.02	0.01	2.68	1.29	1.40	0.06	0.10	0.06
_	300 310	0.16	0.67	0.08	0.37	0.18	0.04	0.06	$0.02 \\ 0.02$	0.00	0.02	0.01	2.61	1.35	1.31	0.08	0.10	0.07
_	320 330								0.02									0.09
	340 350		1						0.04						100000000000000000000000000000000000000			0.11
1	360	0.33	0.59	0.14	0.36	0.09	0.01	0.03	0.05	0.00	0.02	0.02	2.20	1.39	0.98	0.11	0.12	
Т	370 330	0.41	0.54	0.20	0.34	0.06	0.01	0.02	0.06	0.01	0.03	0.03	1.96	1.35	0.83	0.12	0.13	0.15
1	390 400								0.08									0.16
-	410 420	0.53	0.46	0.32	0.31	$0.03 \\ 0.03$	0.01	0.01	0.09	$0.02 \\ 0.03$	0.05	0.05	1.56 $1.42$	1.25	$0.59 \\ 0.52$	0.13	0.13	0.18
1	430 440	0.60	0.40	0.41	0.28	0.02	0.01	0.02	0.11 $0.12$	0.03	0.06	0.06	1.28	1.16	0.44	0.14	0.14	0.19
ı	450	0.66	0.34	0.52	0.24	0.02	0.01	0.09	0.13	0.04	0.08	0.08	1.00	1.05	0.31	0.15	0.14	0.19
_	460	0.71	0.29	0.63	0.21	0.03	0.02	0.03	0.14	0.05	0.10	0.10	0.74	0.92	0.19	0.16	0.14	0.20
-	480 490								0.16									0.20
1	500 510								0.17									0.20
	520	0.78	0.17	0.88	0.12	0.08	0.03	0.06	0.18	0.08	0.14	0.14	0.22	0.58	0.02	0.16	0.13	0.19
1	530 540	0.78	0.14	0.97	0.09	0.10	0.04	0.08	0.19	0.08	0.15	0.16	0.09	0.45	0.00	0.16	0.12	0.18
1	550 560	0.76	0.13	1.04	0.07	0.14	0.04	0.09	0.19	0.09	0.16	0.17	0.02	0.34	0.02	0.15	0.12 0.11	0.17
	570 580	0.74	0.12	1.00	0.06	0.16	0.05	0.10	0.19	0.09	0.17	0.18	0.00	$0.29 \\ 0.25$	0.04	$0.15 \\ 0.14$	0.11	0.16 0.15
1	590	0.70	0.12	1.10	0.04	0.19	0.06	0.19	0.19	0.10	0.18	0.19	0.02	0.21	0.10	0.14	0.10	0.14
L	600	0.67	0.13	1.11	0.03	0.21	0.06	0.13	0.18	[0.10	0.18	0.19	10.05	0.17	0.14	[0.13	0.10	0.13

		TABLE	XVII	<i>a</i> .			TABLE XV	II b.
Year.	(v.s.1)	(v.c.1)	Year.	(v.s.1)	(v.c.1)	Year.	(v.s.1)	(v.c.1)
	"	"		"	"		"	"
1800	240.33	-162.11	1850	183.57	189.69	1500	-560.44 550.95 + 9.59	- 96.24
1801	239.19	162.61	1851	182.44	190.29	1510	000.00	95.81 +0.43
1802	238.06	163.12	1852	181.30 180.17	190.89 191.50	1520 1530	541.17 9.03 531.40 9.77	95.54 95.44+0.10
1803 1804	236.92 $235.79$	$\begin{array}{c} 163.63 \\ 164.14 \end{array}$	1853 1854	179.04	192.10	1540	521 54 9.86	95.51 -0.07
			1855	177.91	192.71	1550	9.95	95.75
1805 1806	-234.65 $233.51$	-164.65 $165.16$	1856	176.78	193.32	1560	501 55 +10.04	96 16 -0.41
1807	232.38	165.68	1857	175.65	193.93	1570	491.42 10.13	96 75 0.59
1808	231.24	166.20	1858	174.51	194.54	1580	481.20	97.52 0.77
1809	230.11	166.72	1859	173.38	195.15	1590	470.90 10.38	98.47 1.13
1810	-228.97	-167.24	1860	-172.25	-195.77	1600	-460.52	99 60
1811	227.83	167.76	1861	171.12	196.39	1610 1620	450.06 +10.46	100.93 -1.33
1812 1813	226.70 $225.56$	$\frac{168.29}{168.82}$	1862 1863	169.99 168.86	197.01 197.63	1630	439.53 10.53 428.92 10.61	102.44 1.51 104.14 1.70
1814	224.43	169.35	1864	167.72	198.25	1640	418 94 10.68	106.02 1.88
1815	223.29	169.88	1865	166.59	_198.88	1650	_407.49	
1816	222.15	170.41	1866	165.46	199.51	1660	396 67 +10.82	$110.35^{-2.26}$
1817	221.02	170.95	1867	164.33	200.14	1670	385.79	112.80 2.45
1818	219.88	171.49	1868	163.20	200.77	1680	374.86 10.93	115.45 2.65 118.98 2.83
1819	218.75	172.03	1869	162.07	201.40	1690	11.04	3.02
1820	-217.61	-172.57	1870	-160.94	-202.04	1700	-352.83 341.74 +11.09	-121.30 $124.52$ $-3.22$
1821 1822	216.47 $215.34$	173.11 173.66	1871 1872	159.81 158.68	202.68 $203.32$	1710 1720	330.61	107 02 3.41
1823	214.20	174.21	1873	157.55	203.96	1730	319.43	131.53 3.00
1824	213.07	174.76	1874	156.42	204.60	1740	308.22 11.21	135.32 3.79 3.98
1825	211.93	175.31	1875	155.29	_205.24	1750	000 04	1 120 20
1826	210.80	175.86	1876	154.16	205.89	1760	$\begin{array}{c} -296.97 \\ 285.69 \\ 974.29 \\ 11.31 \end{array}$	143.48 -4.18
1827	209.66	176.42	1877	153.03	206.54	1770	274.38	147.85 4·37 159.49 4·57
1828 1829	208.53 207.39	176.97 177.53	1878 1879	151.91 150.78	207.19 207.84	1780 1790	951 60 11.35	152.42 4.57 157.17 4.75
	206.26	178.09	1880	_149.65	208.49	1800	11.30	4.94
1830 1831	205.13	178.65	1881	148.52	209.15	1810	-240.33 + 11.36 $228.97 + 11.36$	$-\frac{162.11}{167.24} - 5.13$
1832	203.99	179.22	1882	147.39	209.81	1820	917 61 3	179.57 5.33
1833	202.86	179.78	1883	146.27	210.47	1830	206.26 11.35	178.09 5.52
1834	201.72	180.35	1884	145.14	211.13	1840	194.91	183.80 5.89
1835	-200.59		1885	144.01	-211.79		183.57	-189.69
1836 1837	199.45 198.32	181.49	1886	142.89	212.45	1860	172.25 +11.32 160.94 11.31	100.11
1838	198.32	182.06 182.64	1887 1888	141.76 140.64	213.12 213.79	1870 1880	149.65	202.04 6.27 208.49 6.45
1839	196.05	183.22	1889	139.51	214.46		138.39 11.26	215.13 0.04
1840	194.91	183.80	1890	138.39	<u>215.13</u>		197 16	_221.95
1841	193.78	184.38	1891	137.27	215.80		115.98 +11.18	228.94 - 0.99
1842	192.64	184.96	1892	136.14	216.48		104.84	236.11 7.17
1843 1844	191.51 190.37	185.55	1893	135.02	217.17	1930	30.10	243.46 7·35 251 00 7·54
		186.13	1894	133.90	217.84	1940	10.98	7.72
1845 1846	-189.24 188.10	-186.72 $187.31$	1895 1896	-132.77 131.65	-218.52 $219.20$		- 71.74 60.82 +10.92	-258.72
1847	186.97	187.90	1897	130.53	219.20		49 97	274.68 8.07
1848	185.84	188.50	1898	129.40	220.57	1980	39.19 10.78	282.93 8.25
1849	184.70	189.09	1899	128.28	221.26	1990	28.49 10.70	291.35 8.42
1850	-183.57	189.69	1900	-127.16	-221.95	2000	17.88	299.95
No	The The	values of	(n s 1)	and (n.c.	1) must by	a talzan	from only one of t	ho two tables

Note.—The values of (v.s.1) and (v.c.1) must be taken from only one of the two tables XVII a and XVII b.

		T	ABLE X	VII b	-Concl	uded.					
Year.	(v.s.2)	(v.c.2)	(v,s,3)	(v.c.3)	(p.c.0)	(ρ.ε.1)	(p.c.1)	(p.8.2)	(p.c.2)	(p.s.3)	(p.c.3)
	,,	"	"	"							
1500 1510	-152.85 $152.43 + 0.42$	-124.83 $124.94$ $-0.11$	-10.39 $10.35$	-6.70 $-6.70$	+1379 $1369$		+2361 $2258$	-382 $382$	-158 165	- 96 96	- 80 80
1520	152 00 0.43	125.06 0.12	10.31	6.70	1359	881	2154	382	172	96	81
1530	151.57 0.43	125.19 0.13	10.28	6.69	1349		2047	381	179	96	81
1540	131.13 0.44	0.16	10.24	6.69	1338		1944	381	187	96	82
1550 1560	-150.69 $150.24$ $+0.45$	$\frac{-125.50}{125.67}$ $\frac{-0.17}{125.67}$	-10.20 $10.16$	0.69 6.69	+1328 $1318$		+1838 $1731$	-381 381	-195 $203$	- 96 96	- 82 83
1570	149 78 0.40	125.85	10.13	6.69	1307	886	1623	381	210	96	83
1580	149.32	126.04 0.19	10.09	6.69	1297	893	1513		218	96	84
1590	145.50 0.47	126.24 0.20	10.05	6.70	1286	901	1403	382	226	96	84
1600 1610	-148.39 $147.92 + 0.47$	-126.44 126.66 -0.22	-10.02 9.98	-6.70 $6.70$	+1275 $1264$	- 911 923	+1292 $1180$	-383 384	204 242	- 96 96	- 85 86
1620	147.44 0.48	126.89 0.23	9.94	6.71	1253		1067	385	250	96	86
1630	146.96 0.48	127.13 0.24	9.91	6.71	1241	954	954	386	258	96	87
1640	0.40	0.26	9.87	6.72	1230		2.3.	388	266	96	87
1650 1660	-145.99 $145.50 + 0.49$	-127.64 $127.91$ $-0.27$	- 9.83 9.79	-6.73 $6.74$	+1219 $1208$		+ 725 610	-389 391	274 282	— 96 96	— 88 89
1670	145.00 0.50	128.19 0.28	9.75	6.75	1197		495	392	290	96	89
1680	144.50 0.50	128.49 0.30	9.71	6.76	1185		379		298	96	90
1690	0.51	0.32	9.67	6.77	1174				306	96	90
1700	-143.49 142.98 +0.51	-129.12 $129.45$ $-0.33$	- 9.63 9.59	-6.78 6.79	+1163 $1152$			-398 400	314 323	- 97 97	$-\frac{91}{92}$
1710 1720	142.47	129.45	9.55	6.80	1141				331	97	92
1730	141.96 0.51	130.14 0.35	9.51	6.81	1130				339	. 97	93
1740	141.44 0.52	130.51 0.37	9.47	6.83	1119				348	98	93
1750	-140.93 140.41+0.52	_130.88	- 9.43	-6.84 6.85	+1108 1097				356 365	- 98 98	- 94 95
1760 1770	140.41 +0.52 139.88 0.53	131.27 -0.39	9,39 9,35	6.87	1086				373	98	95
1780	139.36 0.52	132.08 0.41	9.31	6.89	1074	1437	817	420	382	99	96
1790	138.83 0.53	132.50 0.42	9.27	6.90	1063				390	99	96
1800	100 01	-132.93	- 9.23	-6.92	+1052				399 408	- 99 99	- 97 98
1810 1820	137.79 +0.52 137.26 0.53	133 89 0.45	9.19 9.14	6.93 6.95	1041 1030			1	416	99	98
1830	136.74	134.28 0.40	9.10	6.96	1019	1699	1422	439	425	100	99
1840	136.21 0.53	134.76 0.48	9.06	6.98	1008	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	L-1007	1 1 1 1	433	100	99
1850	-135.69	_135.25	- 9.02	-7.00		1819			442	-100	-100
1860 1870	121.65 0.52	136.26 0.51	8.98 8.94	7.02	986 975				450 459	100	101 101
1880	134.13	136.78	8.90	7.07	964	2012	2027	461	467	101	102
1890	133.61 0.52	137.31 0.53	8.86	7.09	958		1	100000000000000000000000000000000000000	476	101	102
1900	_133 09	-137.85	- 8.82	-7.12					_484	-102	-103
1910 1920	132.57 +0.52 132.06 0.51	138.40 -0.55 138.96 0.56	8.78 8.74	7.15	931				492 500	102	104
1930	131.55 0.51	139.53 0.57	8.70	7.20	910	2379	2623	486	509	103	105
1940	131.04 0.51	140.11 0.58	8.66	7.22	100			1 - 7 - 7 -	517	103	105
1950	120 54	1 10 70	- 8.62	-7.25					525	-104	-106
1960	130.04 +0.50 129.55 0.49	141.31 -0.61	8.58 8.54	7.28					533 541	104	106
1970 1980	129.06 0.49	119 56 0.03	8.50	7.34	858	2780	320	515	550	105	107
1990	128.57 0.49	143.20 0.04	8 46	7.37				521	558	106	108
2000	-128.09	-143.85	- 8.42	-7.40	+ 83	8 —295	343	527	-566	106	108

		$11  191  6.49^{-0.31}  56  236  1.31^{+0.11}  101  281  13.51^{+0.31}  146  326  18.69^{-0.11}$													
I	и	и	R	u	11	R	u	u	R	и	u	R			
ľ	0	0	"	0	0	"	0	0	"	0	0	"	Area .		
1	0	180	10.00	45					10.00			19.37	0.07		
ı			0.01	2 40		U.UI OOT			10.33 70.33						
ı			9.02 0.3	3 48		0.68 0.03			10.98 0.33		-				
ı			8.70 0.3	2 49	1	0.79 0.04			11.30 0.32						
I				2					11.63				-0.07		
ı			0.00	2 01		0.04 0.07			11.95.						
ı			7 42 0.3	53		0.00			12 58 0.31						
ı	9	189			234	1.09	99	279		144		18.91			
۱	10	-	6.80	55					13.20				0.11		
	12	191	6.49 0.3	557	236	1.31 0.13	101	281	13.51 +0.30	146	$\frac{326}{327}$	18.69 <sup>-</sup> 18.56	0.13		
	13	193	5.89 0.3	58	238	1.58 0.14	103	283	14.11 0.30	148	328	18.42	0.14		
ı	14	194	5.60 0.2		239	1.73 0.15	104	284	14.40 0.29 0.28	149	329	18.27	0.15		
	15	195	5.32	8 60	240	1.88	105	285	14.68	150	330	18.12	0.74		
	16 17	196 197	5.04 -0.2 4.76 0.2		241 242	2.05 +0.17 2.23 0.18	106	286 287	14.96 +0.28	151 152	331	17.95	0.17		
	18	198	4.49 0.2	7 63	243	2.42 0.19	101	288	15.24 0.28 15.51 0.27	153	332 333	17.77 17.58	0.19		
	19	199	4.23 0.2	64	244	2.62 0.20	109	289	15.77 0.26 0.25	154	334	17.38	0.20		
	20	200	3.98	65	245	2.82	110	290	16.02	155	335	17.18			
	$\begin{bmatrix} 21 \\ 22 \end{bmatrix}$	201	3.73 -0.2 3.49 0.2	0.0	246 247	3.04 +0.22	111	291	16.27 +0.25	156	336	16.96	0.22		
	23	203	3.26 0.2	3 68	241	3.26 0.22 3.49 0.23	112 113	292 293	16.51 0.24 16.74 0.23	157 158	337 338	16.74 16.51	0.23		
ı	24	204	3.04 0.2	69	249	3.73 0.24 0.25	114	294	16.96 0.22	159	339	16.27	0.24		
L	25	205	2.82	70	250	3.98	115	295	17.18	160	340	16.02			
ı	$\begin{bmatrix} 26 \\ 27 \end{bmatrix}$	206	2.02	11	251	4.23+0.25	116	296	17.38 +0.20	161	341	15.77	0.25		
L	28	207 208	2.42 0.1 2.23 0.1		252 253	4.49 0.27	117	297 298	17.58 0.19 17.77 0.19	162 163	342 343	15.51 15.24	0.27		
	29	209	2.25 o.1 o.1	74	254	5.04 0.28	119	299	17.95 0.18	164	344	14.96	0.28		
1	30	210	1.88	75	255	5.32	120	300	10.10	165	345	14.68			
1	$\begin{vmatrix} 31 \\ 32 \end{vmatrix}$	211 212	1.73 — o. I 1.58 o. I	76	256	5.60 + 0.28 $5.60 + 0.29$	121	301	18.27 +0.15	166	346	14.40	0.29		
L	33	212	1 44 0.1	4 79	257 258	6 19 0.30	122 123	302	10.12 0.14	167 168	347	14.11	0.30		
ı	34	214	1.31 0.1	5 79	259	6.49 0.30	124	304	18.69 0.13	169	348 349	13.81 13.51	0.30		
	35	215	1.20	80	260	6.80	125	305	18.80	170	350	13.20			
1	36	216	1.09 -0.1	01	261	7.10 +0.30	126	306	18.91 +0.11	171	351	12.90	-0.30		
1	37 38	217 218	0.91 0.0		262	7.42 0.32	127	307	19.01 0.10	172	352	12.58	0.32		
1	39	219	0.84 0.0	7 84	263 264	7.73 0.31 8.05 0.32 0.32	$\frac{128}{129}$	308 309	19.09 0.07 19.16 0.07	173 174	353 354	12.27 11.95	0.32		
1	40	220	0.77	85	265	8 37	130	310	19 23	175	355	11.63	20.39		
1	41	221	0.72 -0.0		266	8.70 +0.33	131	311	19.28+0.05	176	356	11.30	-0.33		
1	42	222 223	0.68	. 81	267 268	9.02 °.32 9.35 °.33	132	312	19.32 0.04	177	357	10.98	0.32		
1	44	224	0.64 0.0	I 89	269	9.67 0.32	133 134	313	19.35 0.03 19.36 0.01	178 179	358 359	10.65	0.32		
	45	225	0.63	90	270	0.33			0.01				0.33		
	10	220	0.00	30	210	10.00	135	315	19.37	180	360	10.00			

	ŗ	ABI	LE :	X1X.—	Princii	PAL	TERM (	OF THE	LATIT	UDE.	A no	UMENT	u.	
14	1	ß			и	_	β			и		β	1	
180°	, ,			360°	190°	,	"		350°	200°	-,	"		340°
00	0 0.0	0 .		180°	10°	8	2.82		170°	20°	15	50.98		160°
10'	0 8.6	0 8	.09	50'	10'	8	10.78	7.96	50'	10'	15	58.58	7.60	50'
20	0 16.	0 -	.09	40	20	8	18.74	7.96	40	20	16	6.17	7.59	40
30	0 24.5	17 8	.09	30	80	8	26.69	7.95	30	30		13.75	7.58	30
40	0 32.3		80.	20	40	8	34,64	7.95	20	40	16	21.32	7-57	20
50	0 40.	4	.09	10	50	8	42.59	7.95	10	50	16	28.88	7.56	10
1°	0 48.	19	.09	179°	11°	8	50.54	7.95	169°	21°	16	36.43	7.55	159°
10'	0 56.6	2 8	.09	50'	10'	8	58.48	7.94	50'	10'	16	43.98	7.55	50'
20	1 4.	0 8	.08	40	20	9	6.41	7.93	40	20	16	51.52	7.54	40
30	1 12.	14	.09	30	30	9	14.34	7.93	30	30	16	59.05	7-53	30
40	1 20.5	7	.08	20	40	9	22.26	7.92	20	40	17	6.57	7.52	20
50	1 28.9	4.	.09	10	50	9	30.18	7.92	10	50	17	14.08	7.51	10
20	1 37.6	4		178°	12°	9	38.09	7.91	168°	22°	17	21.58	7.50	158°
10'	1 45.	0 0	80.8	50'	10'	9	45.99	7.90	50'	10'	17	29.07	7.49	50'
20	1 53.	0	.08	40	20	9	53.89	7.90	40	20	17	36.55	7.48	40
30	2 1.9	9 0	80.08	30	30	10	1.79	7.90	30	30	17	44.03	7.48	30
40	2 9.	26	8.08	20	40	10	9.68	7.89	20	40	17	51.50	7.47	20
50	2 17.	14 0	3.08	10	50	10	17.57	7.89	10	50	17	58.96	7.46	10
3°	2 25.	0	3.08	177°	13°	10	25.46	7.89	167°	23°	18	6.41	7.45	157°
10'	2 33.		8.08	50'	10'	10	33.34	7.88	50'	10'	18	13.85	7-44	50'
20	2 41.	7 8	3.07	40	20	10	41.21	7.87	40	20	18	21.28	7-43	40
30	2 49.	5 8	3.08	30	30	10	49,08	7.87	30	30	18	28.70	7.42	30
40	2 57.8	6.	3.07	20	40	10	56.94	7.86	20	40	18	36.11	7.41	20
50	3 5.1	9 8	.07	10	50	11	4.80	7.86	10	50	18	43.52	7.41	10
40	3 13.	8	3.07		14°	11	12.65	7.85	166°	24°	18	50.92	7.40	156°
10'	3 22	1,	3.07	176° 50′	10'	11	20.50	7.85	50'	10'	18	58.31	7-39	50'
20	3 30.	0	3.06		20	11	28.34	7.84	40	20	19	5.68	7-37	40
30	3 38.		3.07	40 30	30	11	36.17	7.83	30	30	19	13.05	7.37	30
40	3 46.5	00 8	3.06	20	40	11	44.00	7.83	20	40	19	20.40	7.35	20
50	3 54.5	8 8	3.06	10	50	11	51.82	7.82	10	50	19	27.75	7-35	10
		0	3.06					7.81		25°	19	35.08	7-33	155°
5°	4 2.3	×	3.05	175°	15°	11	59.63	7.80	165° 50′	10'	19	42.41	7.33	50'
10'	4 10.3	0 0	3.06	50'	10'	12	7.43	7.81	40	20	19	49.72	7.31	40
20	4 26.		3.05	40	20	12	23.04	7.80	30	30	19	57.02	7.30	30
30	4 34.	0	3.06	30	30	12	30.83	7.79	20	40	20	4.32	7.30	20
50	4 42.		3.05	20	40 50		38.61	7.78	. 10	50	20	11.61	7.29	10
		Ö	3.04	10				7.79			-		7.27	154°
6°	4 50.		3.04	174°	16°		46.40	7.78	164°	26°	20	18.88	7.26	50'
10'	4 58.	19 8	3.04	50'	10'		54.18	7-77	50'	10'		26.14	7.26	40
20	5 6.	0 0	3.03	40	20	13	1.95	7-75	40	20	20	33.40 40.64	7.24	30
30	5 14.	8	3.03	30	30	13	9.70 17.45	7-75	30 20	30	20	47.88	7.24	20
40		8	3.03	20	40	13	25.19	7-74	10	-50		55.10	7.22	10
50		8	3.03	10	50			7-74					7.21	
7°	5 33.	35 g	3.03	173°	17°		32.93	7-73	163°	27°	21	2.31	7.20	153°
10'	5 46.	90 9	3.02	50'	10'	-	40.66	7.73	50'	10'	21	9.51	7.19	50' 40
20	5 54.	00 8	3.02	40	20		48.39	7.72	40	20 30	21	23.88	7.18	30
30	6 2.	11 0	3.02	30	30		56.11	7.71	30 20	40	21	31.05	7.17	20
40	6 10.	14 8	B.or	20	40	14	3.82	7.70	10	50	21	38.21	7.16	10
50	6 18.	C	3.01	10	50		11.52	7.69					7.14	
80	6 26.		3.01	172°	18°		19.21	7.69	162°	28°	21	45.35	7.14	152°
10'	6 34.	7 I C	3.00	50'	10'	14	26.90	7.68	50'	10'	21	52.49	7.12	50' 40
20	6 42.	91 9	3.00	40	20	14	34.58	7.67	40	20 30	21	59.61 6.73	7.12	30
30	6 50.	04 0	3.00	30	30	14	42.25	7.67	30 20	40	22	13.83	7.10	20
40	6 58.	96 "	7.99	20	40	14	49.92	7.66	10	50	22	20.92	7.09	10
50	7 6.	8	3.00	10	50		57.58	7.65					7.08	
9°	7 14.		7.99	171°	19°	15	5.23	7.65	161°	29°	22	28.00	7.07	151°
10'	7 22.	200	7.93	50'	10'	15	12.88	7.64	50'	10'	22	85.07	7.05	50'
20	7 30.	(e)	7.98	40	20	15	20.52	7.63	40	20	22	42.12	7.05	40 30
30	7 38.	7 1	7.97	30	30	15	28.15	7.62	30	30 40	22	56.20	7.03	20
40	7 46.	30	7-97	20	40	15	35.77	7.61	20	50	23	3.23	7.03	10
50	7 54.	20 7	7.97	10	50		43.38	7.60		22			7.01	
10°	8 2.	32		170°	20°	15	50.98		160°	30°	23	10.24		150°
190°	β		12.	350°	200°		β		340°	210°		β		330°
				u					26				100	u
											1			

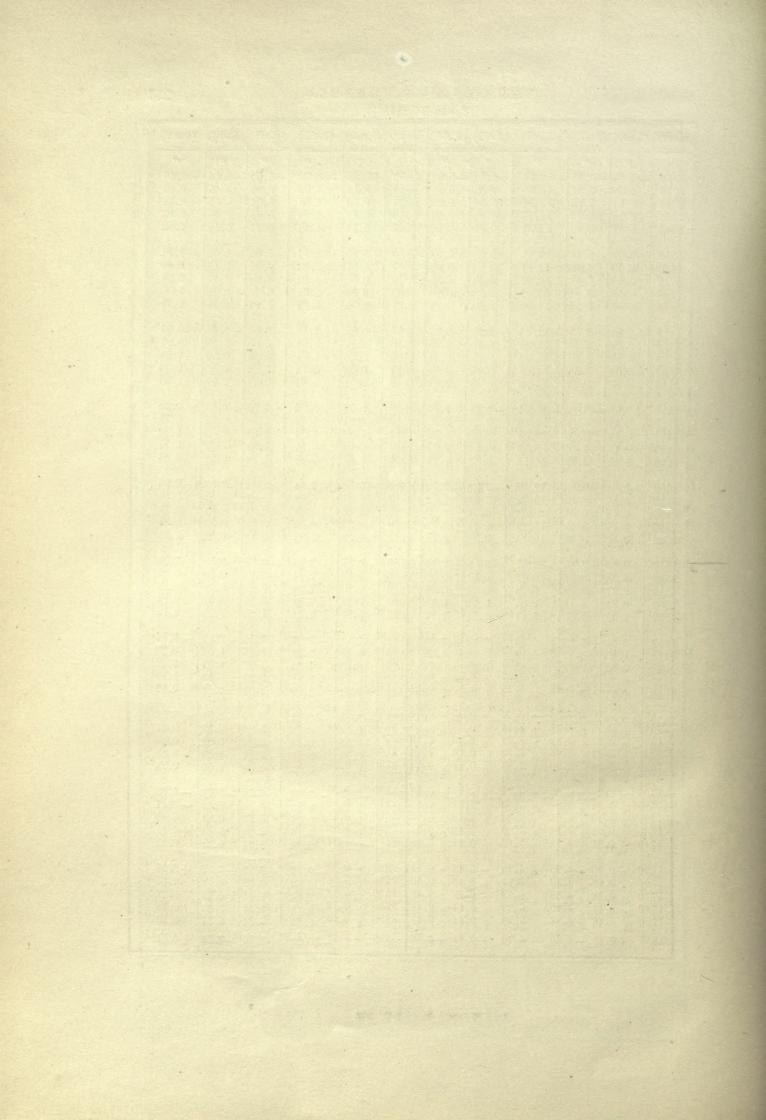
				7	TABLE	X	IX, AR	ig. u	Conti	nued.					-
	и	β			u		β			и		β			
	210°	1 11		330°	220°	,	"		320°	230		, ,,		310°	
	30°	23 10.24		150°	40°	29		6.19	140		3			130°	
	10' 20	23 17.24 23 24.23	6	50'	10' 20	29		. 6.17	7 40	$\begin{array}{c c} 10' \\ 20 \end{array}$	3	-	F 7 10	30	
	30	23 31.20	6.97	30	30	30		6.16	30	30	3		5.15	30	=
	40	23 38.17	6.97	20	40		11.93	6.12	40	40	3	50.63	5.13	20	
	50	23 45.12	6.04	10	50		13.06	6.11	10	50	3		5.10	10	
	31° 10′	23 52.06 23 58.99	6.93	149° 50′	41° 10′	30	24.17 30.27	6.10	139°	51°	3		0	129°	
	20	24 5.90	6.91	40	20	1	36.35	6.08	40	20	3		5.07	50' 40	
	30	24 12.80	6.80	30	30	30	42.41	6.06	90	30	3	6 16.05	5.05	30	
ı	40	24 19.69 24 26.57	6.88	20 10	40 50		48.46 54.49	6.03	40	40	3			20	
	50 <b>32°</b>	24 33.43	6.86	148°	42°	31		6.02	10	50	3		4.00	10	
1	10'	24 40.28	6.85	50'	10'	31	$0.51 \\ 6.51$	6.00	138° 50′	52°	30			128° 50′	
1	20	24 47.12	6.84	40	20	31	12.50	5.99	40	20	36		4.95	40	П
1	30	24 53.95	6.83	30	30	31	18.47	5.97 5.96	00	30	36			30	П
	40 50	25 0.77 25 7.57	6.80	$\begin{array}{c} 20 \\ 10 \end{array}$	40 50	31	24.43 30.37	5.94		40 50	30		4.91	20	
	33°	25 14.36	6.79	147°	43°	31	36.29	5.92	137°	53°	3		4.88	10 127°	
ı	10'	25 21.14	6.78	50'	10'	31	42.20	5.91	501	10'	3		4.86	50'	1
I	20	25 27.90	6.76	40	20		48.09	5.89	10	20	37	10.31	4.84	40	ı
1	30 40	25 34.65 25 41.39	6.74	30 20	30 40		53.96 59.82	5.86	30 20	30 40	37		4.80	30	1
1	50	25 48.11	6.72	10	50	32	5.66	5.84	10	50	37		4.79	20 10	ı
1	34°	25 54.82	6.71	146°	44°	32	11.49	5.83	136°	54°	37		4.76	126°	1
ı	10'	26 1.52	6.70	50'	10'		17.30	5.81 5.79	50'	10'	37	34.22	4.74	50'	1
4	20 30	26 8.20 26 14.88	6.68	40 30	20 30	32 32	23.09 28.87	5.78	30	20	37		4·73 4·71	40	1
П	40	26 21.54	6.66	20	40	32	34.63	5.76	20	30	37		4.68	$\begin{array}{c} 30 \\ 20 \end{array}$	ı
ı	50	26 28.19	6.65	10	50	32	40.38	5.75	10	50	37		4.67	10	ı
Ł	35°	26 34.82	6.62	145°	45°		46.11	5·73 5·71	135°	55°	37	57.66	4.65	125°	I
	10' 20	26 41.44 26 48.04	6.60	50' 40	10' 20		51.82	5.69	50'	10'	38		4.63	50'	ı
ı	30	26 54.63	6.59	30	30	33	57.51 3.19	5.68	40 30	20 30	38	6.90 $11.49$	4.59	40	ı
	40	27 1.21	6.58	20	40	33	8.85	5.66	20	40	38		4.58	$\begin{array}{c} 30 \\ 20 \end{array}$	
l	50	27 7.77	6.55	10	50		14.49	5.63	10	50	38	20.62	4·55 4·53	10	1
E	36° 10′	27 14.32 27 20.86	6.54	144° 50′	46° 10′		20.12	5.61	134°	56°	38	25.15	4.51	124°	H
ı	20	27 27.38	6.52	40	20	33	25.73 31.32	5.59	50'	10' 20	38	29.66 34.16	4.50	50'	1
ı	30	27 33.89	6.50	30	30	33	36.90	5.58	30	30		38.63	4.47	40 30	ı
ı	40 50	27 40.39 27 46.87	6.48	20	40		42.46	5.56 5.54	20	40	38	43.08	4.45	20	ı
L	37°	27 53.34	6.47	10	50		48.00	5.53	10	50	38	47.52	4.41	10	۱
1	10'	27 59.79	0.45	143° 50′	47° 10′		53.53 59.04	5.51	133° 50′	57° 10′	38 38	51.93 56.33	4.40	123°	1
1	20	28 6.23	6.44	40	20	34	4.53	5.49	40	20	39	0.70	4.37	50' 40	
	30 40	28 12.65 28 19.06	6.41	30	30		10.00	5.47	30	30	39	5.06	4.36	30	
	50	28 25.46	6.40	20 10	40 50		$15.46 \\ 20.90$	5.44	20 10	40 50	39 39	$9.40 \\ 13.71$	4.34	20	1
	38°	28 31.84	6.38	142°			26.32	5.42	132°	58°	39	18.01	4.30	10	1
	10'	28 38.21	6.37	50'	10'	34	31.72	5.40	50'	10'	39	22.29	4.28	122° 50′	
		28 44.56 28 50.89	6.33	40 30	20		37.11	5·39 5·37	40	20	39	26.54	4.25	40	
	40	28 57.22	6.33	20			42.48 47.83	5.35	30 20	30 40	39	30.78 34.99	4.24	30	
		29 3.53	6.31	10	50		53.16	5.33	10	50		39.19	4.20	20 10	
		29 9.82	6.28	141°		34 8	58.47	5.31	131°	59°		43.36	4.17	121°	
	-	29 16.10 29 22.36	6.26	50'		35	3.77	5.30	50'	10'	39	47.52	4.16	50'	
		29 28.61	6.25	40 30		35 35 ]		5.26	40 30	20		51.65	4.13	40	
	40	29 34.85	6.24	20	40	35	19.55	5.24	20	30 40		55.77 59.87	4.10	30 20	
		29 41.07	6.20	10		35 9	24.78	5.23	10	50	40	3.94	4.07	10	
		29 47.27		140°			29.99	5.21	130°	60°	40	8.00	4.06	120°	
1	220°	β			230°		β	H. 4	310°	240°		β		300°	
_				и					u			learn's		u	
												THE RESERVE			

1												100
				'n	CABLE	XIX, AR	в. и.—	-Contin	ued.			
	u	β			ш	β			lu	β		
	240°	, ,,		300°	250°	1 11		290°	260°	, ,,		280°
ı	60°	40 8.00	4.03	120°	70°	43 32.84	2.76	110°	80°	45 38.29	4 00	100°
ľ	10'	40 12.03 40 16.04	4.01	50'	10'	43 35.60	2.73	50'	10'	45 39.68	1.39	50'
ı	30	40 16.04	4.00	30	20 30	48 38.33 43 41.04	2.71	30	20 30	45 41.05 45 42.40	1.35	40 30
ı	40	40 24.01	3.97	20	40	43 43.73	2.69	20	40	45 43.73	1.33	20
ı	50	40 27.96	3.95	10	50	43 46.40	2.64	10	50	45 45.03	1.30	10
ı	61°	40 31.89	3.91	119°	71°	43 49.04	2.62	109°	81°	45 46.30	1.26	99°
ı	10'	40 35.80	3.89	50'	10'	43 51.66	2.60	50'	10'	45 47.56	1.23	50'
ı	20 30	40 39.69 40 43.56	3.87	40 30	20 30	43 54.26 43 56.84	2.58	30	20 30	45 48.79 45 50.00	1.21	40 30
ı	40	40 47.41	3.85	20	40	43 59.40	2.56	20	40	45 51.18	1.18	20
ı	50	40 51.24	3.83	10	50	44 1.93	2.53	10	50	45 52.34	1.16	10
I	62°	40 55.05	3.79	118°	72°	44 4.44	2.49	108°	82°	45 53.48	1.11	98°
	10'	40 58.84	3.76	50'	10'	44 6.93	2.46	50'	10'	45 54.59	1.00	50'
1	20 30	41 2.60 41 6.35	3.75	40 30	20 30	44 9.39	2.44	40 30	20 30	45 55.68 45 56.75	1.07	40 30
1	40	41 10.07	3-72	20	40	44 14.25	2.42	20	40	45 57.79	1.04	20
	50	41 13.78	3.71	10	50	44 16.65	2.40	10	50	45 58.81	0.99	10
H	63°	41 17.46		117°	73°	44 19.03		107°	83°	45 59.80		97°
1	10'	41 21.13	3.67	50'	10'	44 21.38	2.35	50'	10'	46 0.78	0.98	50'
1	20 30	41 24.77 41 28.39	3.62	40 30	20 30	44 23.71 44 26.02	2.31	40 30	20 30	46 1.73 46 2.66	0.93	30
ı	40	41 31.99	3.60	20	40	44 28.30	2.28	20	40	46 3.56	0.90	20
1	50	41 35.56	3-57	10	50	44 30.57	2.27	10	50	46 4.44	0.88	10
1	64°	41 39.12	3.56	116°	74°	44 32.82	2.25	106°	84°	46 5.30	0.86	98°
1	10'	41 42.65	3.53	50'	10'	44 35.04	2.22	50'	10'	46 6.14	0.84	50'
1	20 30	41 46.17 41 49.66	3.49	40 30	20 30	44 37.23 44 39.40	2.17	40 30	20 30	46 6.95	0.79	40 30
	40	41 53.13	3-47	20	40	44 41.55	2.15	20	40	46 8.50	0.76	20
	50	41 56.58	3.45	10	50	44 43.68	2.13	10	50	46 9.24	0.74	10
1	65°	42 0.01	3.43	115°	75°	44 45.79	2.11	105°	85°	46 9.96	0.72	95°
1	10'	42 3.42	3.41	50'	10'	44 47.87	2.08	50'	10'	46 10.65	0.69	50'
1	20	42 6.80	3.30	40	20	44 49.93	2.04	40	20	46 11.32	0.65	40
1	30	42 10.17 42 13.51	3.34	30 20	30 40	44 51.97 44 53.98	2.01	30 20	30 40	46 11.97 46 12.59	0.62	30 20
1	50	42 16.83	3.32	10	50	44 55.97	1.99	10	50	46 13.19	0.60	10
1	66°	42 20.13	3.30	114°	76°	44 57.94	1.97	104°	86°	46 13.76	0.57	94°
1	10'	42 23.41	3.28	50'	10'	44 59.89	1.95	50'	10'	46 14.3I	0.55	50'
1	20	42 26.67	3.26	40	20	45 1.81	1.92	40	20	46 14.84	0.53	40
1	30	42 29.91 42 33.12	3.21	30 20	30 40	45 3.71 45 5.59	1.88	30 20	30 40	46 15.35 46 15.83	0.48	30 20
1	50	42 36.32	3.20	10	50	45 5.59 45 7.44	1.85	10	50	46 16.29	0.46	10
1	67°	42 39.49	3.17	113°	77°	45 9.27	1.83	103°	87°	46 16.72	0.43	93°
	10'	42 42.64	3.15	50'	10'	45 11.08	1.81	50'	10'	46 17.13	0.41	50'
1	20	42 45.77	3.13	40	20	45 12.86	1.78	40	20	46 17.52	0.39	40
1	30	42 48.87	3.10	30	30	45 14.62	1.76	30	30	46 17.89 46 18.23	0.37	30 20
1	40 50	42 51.96 42 55.02	3.06	20 10	40 50	45 16.36 45 18.08	1.72	20	40 50	46 18.23 46 18.55	0.32	10
1	68°	42 58.06	3.04	112°	78°	45 19.77	1.69	102°	88°	46 18.84	0.29	92°
1	10'	43 1.08	3.02	50'	10'	45 21.44	1.67	50'	10'	46 19.11	0.27	50'
1	20	43 4.08	3.00	40	20	45 23.09	1.65	40	20	46 19.36	0.25	40
1	30	43 7.05	2.97	30	30	45 24.71	1.60	30	30	46 19.59	0.20	30 20
1	40 50	43 10.01 43 12.94	2.93	20 10	40 50	45 26.31 45 27.89	1.58	20 10	40 50	46 19.79 46 19.97	0.18	10
1	69°	43 15.85	2.91	111°	79°	45 29.45	1.56	101°	89°	46 20.12	0.15	91°
	10'	43 18.74	2.89	50'	10'	45 30.98	1.53	50'	10'	46 20.12	0.13	50'
1	20	43 21.60	2.86	40	20	45 32.49	1.51	40	20	46 20.36	0.11	40
1	30	43 24.45	2.85	30	30	45 33.97	1.48	30	30	46 20.44	0.06	30
-	40 50	43 27.27 43 30.06	2.79	20 10	40 50	45 35.43 45 36.87	1.44	20 10	40 50	46 20.50	0.03	20 10
		The second of	2.78		80°	45 38.29	1.42	100°	90°	46 20.54	0.01	90°
	70°	43 32.84		110°			TIME				IGI	270°
	250°	β	11.55	290°	260°	β	1	280°	270°	β	1	210°
		10.1	Philippine.	и				L4				

Í	TABLE	X	X.			XXI.					XXII.		
	ARG.	1				2					3		14.0
		(b.s.1)	(b.c.1)	(b.c.0)	(b.s.1)	(b.c.1)	(b.s.2)	(b.c.2)	(b.c.0)	(b.s.1)	(b.c.1)	(b.s.2)	(b.c.2)
1		"	"	"	"	"	"	0.35	"	"	"	"	"
1	0 10	1.20 1.15	1.12 1.17	0.04	5.99 6.13	5.42 5.23	$0.21 \\ 0.19$	$0.17 \\ 0.18$	$0.06 \\ 0.06$	1.58 1.63	1.34 1.14	0.07 0.08	$0.17 \\ 0.23$
ı	20 30	1.10 1.04	$1.21 \\ 1.25$	0.03	$\begin{array}{c} 6.25 \\ 6.34 \end{array}$	5.04 4.84	$0.18 \\ 0.17$	0.18 0.18	$0.05 \\ 0.04$	1.67 1.68	$0.93 \\ 0.72$	$0.11 \\ 0.15$	$0.29 \\ 0.32$
۱	40	0.98	1.28	0.02	6.41	4.62	0.16	0.18	0.03	1.67	0.51	0.21	0.33
۱	50 60	$0.92 \\ 0.86$	1.31 1.33	$0.02 \\ 0.02$	$6.45 \\ 6.45$	4.40	0.15	0.18	$0.03 \\ 0.02$	1.60 1.48	0.33	$0.27 \\ 0.32$	$0.32 \\ 0.28$
	70 80	$0.79 \\ 0.72$	1.34 1.35	$0.02 \\ 0.02$	$\begin{array}{c} 6.40 \\ 6.32 \end{array}$	3.94 3.69	$0.16 \\ 0.16$	$0.18 \\ 0.17$	0.01	1.32 1.13	0.09	0.35 0.36	0.23
1	90	0.66	1.35	0.03	6.19	3.43	0.17	0.16	0.00	0.94	0.13	0.35	0.13
ı	100 110	$0.59 \\ 0.52$	1.34 1.32	$0.03 \\ 0.04$	$6.02 \\ 5.81$	3.15 2.87	$0.17 \\ 0.18$	0.15 0.14	$0.01 \\ 0.02$	0.77	0.25 0.41	$0.32 \\ 0.29$	0.09
1	120	0.46	1.30	0.04	5.56	2.57 2.26	0.19	0.12 0.11	$0.04 \\ 0.06$	0.62 0.64	0.60	$0.25 \\ 0.22$	0.06
ı	130 140	0.40 0.34	1.27 1.24	0.04 0.05	5.29 4.99	1.96	0.20	0.10	0.08	0.72	0.91	0.20	0.07
ı	150 160	$0.28 \\ 0.23$	1.20 1.15	0.05 0.05	4.68	1.66 1.38	$0.20 \\ 0.20$	0.09	0.09	0.83	1.00	0.18	0.08
	170	0.19	1.10	0.06	4.03	1.11	$0.20 \\ 0.19$	0.08 0.07	0.11	1.04	1.04	0.17	0.10 0.10
1	180 190	$0.15 \\ 0.12$	1.04 0.98	0.06	3.69 3.36	0.65	0.13	0.07	0.11	1.14	0.97	0.16	0.11
1	200 210	0.09	0.92	0.06	$\frac{3.03}{2.71}$	$0.56 \\ 0.32$	0.16 0.14	0.08	$0.11 \\ 0.11$	1.14	0.93	0.13	0.12 0.13
1	220	0.06	0.79	0.06	2.39 2.08	0.20	0.12 0.11	0.09	0.10	1.07	0.91	0.10	0.15
	230 240	0.05	$0.72 \\ 0.66$	0.06	1.77	0.12	0.09	0.11	0.10	0.98	0.96	0.10	0.21
	250 260	$0.06 \\ 0.08$	$0.59 \\ 0.52$	0.07	1.48 1.21	0.08	0.07	0.15 0.17	$0.09 \\ 0.08$	0.96 0.95	1.00	$0.12 \\ 0.14$	0.23 0.25
	270 280	0.10	0.46	0.08	1.05	0.16	0.03	$0.20 \\ 0.22$	0.08	0.94	1.09	0.16	0.26
	290	0.13 0.16	$0.40 \\ 0.34$	0.08	$0.72 \\ 0.52$	0.38	0.02	0.25	0.07	0.95	1.16	0.13	0.25
1	300 310	$\begin{bmatrix} 0.20 \\ 0.25 \end{bmatrix}$	$0.28 \\ 0.23$	0.10	$0.35 \\ 0.22$	0.54 0.73	0.01	$0.27 \\ 0.29$	0.06	0.94	1.18	0.23 0.24	0.23 0.21
	320 330	0.30	0.19 0.15	0.12 0.13	$0.12 \\ 0.06$	0.94	0.02	0.31 0.33	0.07	0.91	1.22 1.25	$0.23 \\ 0.22$	0.19 0.18
١	340	0.42	0.12	0.14	0.04	1.44	0.05	0.35	0.09	0.86	1.28	0.20	0.17
1	350 360	0.48 0.54	0.09	0.15	$0.06 \\ 0.12$	1.72 2.01	0.07	0.36 0.37	0.09	0.84	1.34	0.18	0.17
	370 380	0.61 0.68	0.06 0.05	0.17 0.18	$0.21 \\ 0.34$	2.31 2.62	0.13 0.16	0.37 0.37	0.11 0.12	0.88	1.46	0.15	0.19
۱	390	0.74	0.05	0.19	0.50	2.92	0.19	0.36	0.12	0.98	1.54	0.13	0.21
	400 410	0.81	0.06	$0.20 \\ 0.20$	$0.70 \\ 0.92$	3.24 3.54	$0.23 \\ 0.26$	0.35 0.34	0.11 0.10	1.03	1.54 1.50	0.13	0.22 0.23
	420 430	$0.94 \\ 1.00$	0.10 0.13	$0.21 \\ 0.21$	1.17 1.45	3.84 4.14	0.30 0.33	0.33	0.08	1.06	1.44	$0.12 \\ 0.12$	0.25 0.27
	440	1.06	0.16	0.21	1.75	4.42	0.36	0.29	0.04	0.91	1.30	0.12	0.29
	450 460	1.12 1.17	$0.20 \\ 0.25$	$0.21 \\ 0.21$	2.06 2 39	4.70 4.96	0.38	0.27 0.25	$0.03 \\ 0.02$	0.77	1.28 1.31	0.12 0.14	0.32 0.35
	470 480	$\frac{1.21}{1.25}$	$0.30 \\ 0.36$	$0.20 \\ 0.19$	2.72	5.20 5.42	$0.41 \\ 0.42$	0.23	0.01	0.47	1.40 1.56	0.17 0.21	0.38
	490	1.28	0.42	0.18	3.39	5.62	0.42	0.20	0.01	0.32	1.76	0.27	0.39
	500 510	1.31	0.48 0.54	$0.17 \\ 0.16$	3.71 4.02	5.79 5.92	0.42 0.41	0.18	0.01	0.36	1.96 $2.15$	0.32	0.37
	520 530	1.34 1.35	0.61 0.68	0.14 0.13	4.31	6.01	0.39	0.16	$0.02 \\ 0.02$	0.62 0.81	2.21 2.35	0.40	0.27 5.20
	540	1.35	0.74	0.11	4.84	6.08	0.35	0.15	0.03	1.00	2.34	0.38	0.14
	550 560	1.34 1.32	0.81 0.88	0.10	5.07 5.28	6.04 5.98	0.33	0.15	0.03 0.04	1.18	2.26 2.11	0.33	0.08
	570 580	$1.30 \\ 1.27$	0.94	0.07	5.48 5.67	5.88 5.75	0.28	0.16	$0.04 \\ 0.05$	1.41 1.48	1.94 1.74	0.20 0.14	0.04
	590	1.24	1.06	0.05	5.84	5,59	0.23	0.17	0.06	1.53	1.54	0.10	0.11
	600	1.20	1.12	0.04	5.99	5.42	0.21	0.17	0.06	1.58	1.34	0.07	0.17

TABLE XXIII.

			-			TABLE .	AAUI.					
١	Year.	(b.c.0)	(b.s.1)	(b.c.1)	(b.s.2)	(b.c.2)	Year.	(b.c.0)	(b.s.1)	(b.c.1)	(b.s.2)	(b.c.2)
ŀ		11	"	- 11	"	. 11:		"	"	***	"	"
ı	1300	+0.66	_3.85	_12.74	-0.34	_0.97	1800					-0.46
ı	1310	0.65	3.81	12.65	0.34	0.96	1810	$+0.15 \\ 0.14$	-4.60 4.68	-6.00 5.80	-0.44 0.45	0.45
ı	1320	0.64	3.78	12.56	0.34	0.95	1820	0.13	4.75	5.61	0.45	0.43
ı	1330	0.62	3.74	12.46	0.34	0.94	1830	0.13	4.83	5.41	0.45	0.43
ı	1340	0.61	3.70	12.37	0.34	0.93		0.11	4.92	5.21	0.46	0.42
۱									1.02	0.21	0.10	
ı	1350	+0.60			-0.34	-0.92	1850	+0.10	-5.00	-5.00	-0.46	-0.41
ı	1360	0.59	3.63	12.17	0.34	0.90		0.09	5.09	4.79		0.40
١	1370	0.58	3.60	12.07	0.34	0.89		0.08	5.18	4.58		0.39
ı	1380	0.57	3.57	11.97	0.34	0.88		0.07	5.27	4.36		0.38
ı	1390	0.56	3.54	11.86	0.34	0.87	1890	0.06	5.36	4.14	0.48	0.37
ı	1400	+0.55	_3.51	_11.76	-0.35	_0.86	1900	1005	E 45	-3.92	-0.49	-0.36
۱	1410	0.54	3.48	11.65	0.35	0.85		+0.05 $0.04$	-5.45 5.55	3.69		0.35
١	1420	0.53		11.54	0.35	0.84		0.03	5.64	3.46		0.34
1	1430	0.52		11.43	0.35	0.83		0.03	5.74	3.22		0.33
1	1440	0.51	3.43	11.32	0.35	0.82		+0.01	5.84	2.97		0.32
1					0.00			1 3.01	7.02	1	0.00	
1	1450		-3.42		-0.35	_0.80	1950	0.00	-5.94	-2.73	-0.51	-0.30
1	1460	0.49	3.41	11.10	0.35	0.79	1960	-0.01	6.04	2.48	0.51	0.29
1	1470	0.48			0.36	0.78	A TOTAL COLUMN	0.02	6.14	2.24		0.28
1	1480	0.46			0.36	0.77		0.04	6.25	1.99		0.27
ı	1490	0.45	3.40	10.74	0.36	0.76	1990	0.05	6.36	1.73	0.52	0.26
ı	1500	+0.44	_3.40	_10.62	_0.36	_0.75	2000	_0.06	-6.47	_1.47	_0.53	-0.25
1	1510	0.43		10.50	0.36	0.74		0.07	6.58	1.21		0.24
١	1520	0.43			0.36	0.73		0.08	6.69	0.94		0.23
1	1530	0.41			0.37	0.72		0.09	6.80	0.66		0.22
1	1540	0.40		10.14	0.37	0.71		0.10	6.92	0.38		0.20
ı												
ı	1550	+0.39			-0.37			-0.11		-0.10		
П	1560	0.38		9.88	0.37	0.70		0.12	7.14	+0.18		0.18
8	1570	0.37			0.37	0.69		0.13	7.26	0.47		0.17
1	1580	0.36			0.37	0.68		0.15	7.37	0.76		0.16
ı	1590	0.35	3.53	9.47	0.38	0.67	2090	0.16	7.48	1.05	0.56	0.15
ı	1600	+0.34	3 56	_ 9.33	0.38	_0.66	2100	_0.17	_7.60	+1.35	_0.57	-0.14
8	1610	0.33			0.38	0.65		0.18	7.72	1.65		0.13
8	1620	0.32			0.39			0.19	7.84	1.96		0.12
	1630	0.32			0.39			0.21	7.97	2.27		
	1640	0.31			0.39			0.22	8.09	2.58		
	7.83	1		1000	11 11 11				-	100	1	0.00
	1650	+0.30			-0.39			-0.23	-8.21	+2.90		-0.08
	1660	0.29		8.44	0.40	0.60		0.24	8.33	3.22		0.07
	1670	0.28		8.29	0.40	0.59		0.25	8.44	3.54		0.06
	1680 1690	0.27		8.13	0.40			0.27	8.56	3.87 4.20		0.03
	1030	0.26	3.90	1.00	0.41	0.57	2130	0.28	8.68	1,20	0.00	0.00
	1700	+0.25	-3.95	_ 7.79	_0.41	_0.56	2200	_0.29	-8.80	+4.54	-0.60	-0.02
	1710	0.24		7.63	0.41	0.55		0.30	8.92	4.88	0.60	-0.01
	1720	0.23	4.06	7.46	0.42	0.54		0.31	9.04	5.23		0.00
1	1730	0.22		7.29	0.42	0.53		0.33	9.16	5 58		+0.01
	1740	0.21	4.18	7.12	0.42	0.52	2240	0.34	9.28	5.94	0.61	0.03
	1750	10.00	_4.25	_ 6.95	_0.43	_0.51	2250	_0.35	-9.40	+6.29	_0.62	+0.04
	1750 1760	$+0.20 \\ 0.19$	4.32	6.77	0.43	0.50		0.36	9.52	6.65		0.05
	1770	0.19	4.38	6.58	0.43	0.30		0.38	9.64	7.01	0.63	0.07
1	1780	0.18	4.45	6.39	0.44	0.48		0.39	9.76	7.37	0.63	0.08
	1790	0.16	4.53	6.20	0.44	0.47		0.40	9.88	7.74	0.63	0.10
1			STORM	The second	1		2300	-0.42	_10.00	+8.10		+0.11
1	1800	+0.15	-4.60	- 6.00	-0.44	-0.46	2300	-0.42	-10.00	70.10	-0.04	T 0.11
L						-	-				-	



## TABLE FOR FORMING THE PRODUCTS OF GIVEN NUMBERS BY THE SINE OR COSINE OF A GIVEN ANGLE.

This table is formed for the especial purpose of facilitating the formation of the products  $(v.s.3) \sin 3g$ ,  $(v.c.3) \cos 3g$ , etc.,  $(\rho.s.1) \sin g$ ,  $(\rho.c.1) \cos g$ , for entire degrees of g. It is so arranged that the required products can be taken out at sight. Supposing the number to be given in seconds and decimal fractions of a second, we first seek the given angle at the top or bottom of the page, and then enter one of the first nine lines of the table with the fraction part of the second, interpolating for the hundredths. We then add the result mentally to the number corresponding to the entire seconds. The algebraic signs at the sides of the angles are those of the sines or cosines corresponding to the angle and to the column above or below. If the number does not exceed 3" we can enter the table as if it were ten times greater, and remove the decimal point one place to the left in the result.

For example, to find the value of

 $21''.67 \sin 280^{\circ} + 2''.25 \cos 280^{\circ}$ 

we find the angle 280° at the bottom of a pair of columns, the right hand one being the sine column. Entering this column with 0.67 as the argument, we find 0.66. Entering with 2.1, we find 20.68, to which adding 0.66, we have 21".34 as the sine product. Entering the other column with 22.5, and moving the decimal point, we find 0".39 for the cosine product. Noticing the algebraic signs on each side of 280°, we find the result to be -21".34 + 0".39 = -20".95.

	+1	1°+ 179 — 181 — 159 4	+1 -1	2°+ .78 — .82 — .58 +	+1	3°+ 177 — 183 — 157 +	+	4°+ 176 — 84 — 856 +	+:	5°+ 175 — 185 — 855 +	-
840	sin	cos									
0.1 0.2 0.3 0.4	0.00 0.00 0.01 0.01	0.10 0.20 0.30 0.40	0.01	0.10 0.20 0.30 0.40	$0.01 \\ 0.01 \\ 0.02 \\ 0.02$	0.10 0.20 0.30 0.40	0.01 $0.01$ $0.02$ $0.03$	0.10 0.20 0.30 0.40	0.01 0.02 0.03 0.03	0.10 0.20 0.30 0.40	0.1 0.2 0.3 0.4
0.5 0.6 0.7 0.8	0.01 0.01 0.01 0.01	0.50 0.60 0.70 0.80	0.02 0.02 0.02 0.03	0.50 0.60 0.70 0.80	0.03 0.03 0.04 0.04	0.50 0.60 0.70 0.80	0.03 0.04 0.05 0.06	0.50 0.60 0.70 0.80	0.04 0.05 0.06 0.07	0.50 0.60 0.70 0.80	0.5 0.6 0.7 0.8
0.9	0.02	~0.90	0.03	0.90	0.05	0.90	0.06	0.90	0.08	0.90	0.9
1.0 2.0 3.0 4.0	0.02 0.03 0.05 0.07	1.00 2.00 3.00 4.00	0.03 0.07 0.10 0.14	1.00 2.00 3.00 4.00	0.05 0.10 0.16 0.21	1.00 2.00 3.00 3.99	0.07 0.14 0.21 0.28	1.00 2.00 2.99 3.99	0.09 0.17 0.26 0.35	1.00 1.99 2.99 3.98	1.0 2.0 3.0 4.0
5.0 6.0 7.0 8.0	0.09 0.10 0.12 0.14	5.00 6.00 7.00 8.00	0.17 0.21 0.24 0.28	5.00 6.00 7.00 8.00	0.26 0.31 0.37 0.42	4.99 5.99 6.99 7.99	0.35 0.42 0.49 0.56	4.99 5.99 6.98 7.98	0.44 0.52 0.61 0.70	4.98 5.98 6.97 7.97	5.0 6.0 7.0 8.0
9.0	0.16	9.00	0.31	8.99	0.47	8.99	0.63	8.98	0.78	8.97	9.0
11.0 12.0 13.0	0.17 0.19 0.21 0.23	10.00 11.00 12.00 13.00	0.35 $0.38$ $0.42$ $0.45$	9.99 10.99 11.99 12.99	0.52 0.58 0.63 0.68	9.99 10.98 11.98 12.98	$0.70 \\ 0.77 \\ 0.84 \\ 0.91$	9.98 10.97 11.97 12.97	0.87 $0.96$ $1.05$ $1.13$	9.96 10.96 11.95 12.95	10.0 11.0 12.0 13.0
14.0	0.24	14.00	0.49	13.99	0.73	13.98	0.98	13.97	1.22	13.95	14.0
15.0 16.0 17.0 18.0 19.0	0.26 0.28 0.30 0.31 0.33	15.00 16.00 17.00 18.00 19.00	0.52 0.56 0.59 0.63 0.66	14.99 15.99 16.99 17.99 18.99	0.79 0.84 0.89 0.94 0.99	14.98 15.98 16.98 17.98 18.97	1.05 1.12 1.19 1.26 1.33	14.96 15.96 16.96 17.96 18.95	1.31 1.39 1.48 1.57 1.66	14.94 15.94 16.94 17.93 18.93	15.0 16.0 17.0 18.0 19.0
20.0 21.0 22.0 23.0	0.35 0.37 0.38 0.40	20.00 21.00 22.00 23.00	0.70 0.73 0.77 0.80	19.99 20.99 21.99 22.99	1.05 1.10 1.15	19.97 20.97 21.97	1.40 1.46 1.53	19.95 20.95 21.95	1.74 1.83 1.92	19.92 20.92 21.92	20.0 21.0 22.0
24.0	0.42	24.00	0.84	23.99	1.20 1.26	22.97 23.97	1.60 1.67	22.94 23.94	2.00 2.09	22.91 23.91	23.0 24.0
25.0 26.0 27.0 28.0 29.0	0.44 0.45 0.47 0.49 0.51	25.00 26.00 27.00 28.00 29.00	0.87 0.91 0.94 0.98 1.01	24.98 25.98 26.98 27.98 28.98	1.31 1.36 1.41 1.47 1.52	24.97 25.96 26.96 27.96 28.96	1.74 1.81 1.88 1.95 2.02	24 94 25.94 26.93 27.93 28.93	2.18 2.27 2.35 2.44 2.53	24.90 25.90 26.90 27.89 28.89	25.0 26.0 27.0 28.0 29.0
30.0	0.52	30.00	1.05	29.98	1.57	29.96	2.09	29.93	2.61	29.89	20.0
	cos	sin									
	+27 -26 - 9 + 8	9 - 1 +	+279 -268 - 99 + 88	3 - 2 +	+27 -26 - 9 + 8	7 - 3 +	+27 $-26$ $-9$ $+8$	6 — 4 +	+27 $-26$ $-9$ $+8$	5 — 5 +	

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		+	6°+		7°+	+	8°+		9°+		10°+	
				The second second	The same of the same of							
			74 —		73 —		72 —		71 —		70 —	
		-1	86 —	-1	87 —	-1	88 —	-10	89 —	-1	90 —	
		-3	54 +	-3	53 +	-3	52 +	-3	51 +	-3	50 +	
						3						
			1 25	nin.	1	nin.	1		1	-1-	1	
1		sin	cos	sin	cos	sin	cos	sin	cos	sin	cos	
0	1.1	0.01	0.10	0.01	0.10	0.01	0.10	0.02	0.10	0.02	0.10	0.1
	.2	0.02	0.20	0.02	0.20	0.03	0.20	0.03	0.20	0.03	0.20	0.2
	.3	0.03	0.30	0.04	0.30	0.04	0.30	0.05	- 0.30	0.05	0.30	0.3
0	.4	0.04	0.40	0.05	0.40	0.06	0.40	0.06	0.40	0.07	0.39	0.4
1 -		0.0=	800	0.00	0.50	0.07	0.50	0.00	0.40	0.00	0.40	
	.5	0.05	0.50	0.06	0.50	0.07	0.50	0.08	0.49 0.59	0.09	0.49	0.5
	.6	0.06	0.70	0.01	0.69	0.10	0.69	0.03	0.69	0.10	0.59	0.6
	.7	0.01	0.80	0.09	0.69	0.10	0.79	0.11	0.79	0.12	0.69	0.7
	.9	0.08	0.90	0.10	0.19	0.11	0.19	0.14	0.19	0.14	0.19	0.8
1	. 0	0.03	0.00	0.11	0.00	0.10	0.00	0.14	0.00	0.10	0.00	0.9
1	.0	0.10	0.99	0.12	0.99	0.14	0.99	0.16	0.99	0.17	0.98	1.0
	.0	0.21	1.99	0.24	1.99	0.28	1.98	0.31	1.98	0.35	1.97	2.0
	.0	0.31	2.98	0.37	2.98	0.42	2.97	0.47	2.96	0.52	2.95	3.0
	.0	0 42	3.98	0.49	3.97	0.56	3.96	0.63	3.95	0.69	3.94	4.0
1 .		0.00	1 200	0.703	4.00	0.00		0.00	4.04	0.05	1.00	
	.0	0.52	4.97	0.61	4.96	0.70	4.95	0.78	4.94	0.87	4.92	5.0
	.0	0.63	5.97	0.73	5.96	0.84	5.94	0.94	5.93	1.04	5.91	6.0
	.0	0.73	6.96	0.85	6.95	0.97	6.93	1.10	6.91	1.22	6.89	7.0
	.0	0.84	7.96	0.97	7.94	1.11	7.92 8.91	1.25	7.90	1.39	7.88	8.0
1 9	.0	0.94	8.95	1.10	8.93	1.25	0.91	1.41	8.89	1.50	8.86	9.0
10	0	1.05	9.95	1.22	9.93	1.39	9.90	1.56	9.88	1.74	9.85	10.0
11		1.15	10.94	1.34	10.92	1.53	10.89	1.72	10.86	1.91	10.83	11.0
12		1.25	11.93	1.46	11.91	1.67	11.88	1.88	11.85	2.08	11.82	12.0
13.		1.36	12.93	1.58	12.90	1.81	12.87	2.03	12.84	2.26	12.80	13.0
14.		1.46	13.92	1.71	13.90	1.95	13.86	2.19	13.83	2.43	13.79	14.0
15.		1.57	14.92	1.83	14.89	2.09	14.85	2.35	14.82	2.60	14.77	15.0
16.		1.67	15.91	1.95	15.88	2.23	15.84	2.50	15.80	2.78	15.76	16.0
17.		1.78	16.91	2.07	16.87	2.37	16.83	2.66	16.79	2.95	16.74	17.0
18.		1.88	17.90	2.19	17.87	2.51	17.82	2.82	17.78	3.13	17.73	18.0
19.	.0	1.99	18.90	2.32	18.86	2.64	18.82	2.97	18.77	3.30	18.71	19.0
20.	0	2.09	19.89	2.44	19.85	2.78	19.81	3.13	19.75	3.47	19.70	20.0
21.	_	2.20	20.88	2.56	20.84	2.92	20.80	3.29	20.74	3.65	20.68	21.0
22		2.30	21.88	2.68	21.84	3.06	21.79	3.44	21.73	3.82	21.67	22.0
23.		2.40	22.87	2.80	22.83	3.20	22.78	3.60	22.72	3.99	22.65	23.0
24.		2.51	23.87	2.92	23.82	3.34	23.77	3.75	23.70	4.17	23.64	24.0
						1		1				
25.	.0	2.61	24.86	3.05	24.81	3.48	24.76	3.91	24.69	4.34	24.62	25.0
26.		2.72	25.86	3.17	25.81	3.62	25.75	4.07	25.68	4.51	25.61	26.0
27.		2.82	26.85	3.29	26.80	3.76	26.74	4.22	26.67	4.69	26.59	27.0
28,	_	2.93	27.85	3.41	27.79	3.90	27.73	4.38	27.66	4.86	27.57	28.0
29.	.0	3.03	28.84	3.53	28.78	4.04	28.72	4.54	28.64	5.04	28.56	29.0
30.	0	3.14	29.84	3.66	29.78	4.18	29.71	4.69	29.63	5.21	29.54	20.0
30.	.0						1000000	3 ,	ALL AND DE		10.7 ( T. O.)	30.0
	- 6	cos	sin	cos	sin	cos	sin	cos	sin	cos	sin	
	NO E			2	0027	19	-1950	18	TO SERVICE STATE OF THE PARTY O	2 10	THE P	
	-0	+ 27	76 —	+27	7 —	+ 27	8 -	+ 27	9 -	+ 28	0 -	
	100		34 —	- 26		CONTRACTOR OF THE PARTY OF THE	32 -		1 -	- 26	0 -	
	1 3		6 +	_ 9			3 +	- 9		- 10		
	1 6	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	34 +		33 +		2 +	+ 8		+ 8		
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	. 36		ust, 1873.		-					-		

36 August, 1873.

	+ 1   - 1	11°+ .69 — .91 — 49 +	+1 -1	12°+ 68 92 48 +	+ 1 - 1	13°+ 67 — .93 — 47 +	+1	14°+ 66 — 94 — 46 +	+1 -1	15°+ 65 — 95 — 45 +	
	sin	cos	sin	cos	sin	cos	sin	cos	sin	cos	
0.1	0.02	0.10	$0.02 \\ 0.04$	0.10	$0.02 \\ 0.04$	0.10	$0.02 \\ 0.05$	0.10	0.03 0.05	0.10 0.19	0.1
0.3	0.06	0.29	0.06	0.29	0.07	0.29	0.07	0.29	0.08	0.29	0.3
0.4	0.08	0.39	0.08	0.39	0.09	0.39	0.10	0.39	0.10	0.39	0.4
0.5	0.10	0.49	$0.10 \\ 0.12$	0.49 0.59	0.11 0.13	0.49 0.58	$0.12 \\ 0.15$	0.49 0.58	0.13 0.16	0.48 0.58	0.5.
0.7	0.13	0.69	0.15	0.68	0.16	0.68	0.17	0.68	0.18	0.68	0.7
0.8	0.15 0.17	0.79	$0.17 \\ 0.19$	0.78	0.18 0.20	0.78	$0.19 \\ 0.22$	0.78	$0.21 \\ 0.23$	0.77	0.8
1.0	0.19	0.98	0.21	0.98	0.22	0.97	0.24	0.97	0.26	0.97	1.0
2.0	0.38	1.96	0.42	1.96	0.45	1.95	0.48	1.94	0.52	1.93	2.0
3.0	0.57 0.76	2.94 3.93	0.62 0.83	2.93 3.91	0.67	2.92 3.90	$0.73 \\ 0.97$	2.91 3.88	0.78 1.04	2.90 3.86	3.0 4.0
5.0	0.95	4.91	1.04	4.89	1.12	4.87	1.21	4.85	1.29	4.83	5.0
6.0	1.14 1.34	5.89 6.87	1.25 1.46	5.87 6.85	1.35 1.57	5.85 6.82	$1.45 \\ 1.69$	5.82 6.79	1.55 1.81	5.80	6.0
8.0	1.53	7.85	1.66	7 83	1.80	7.79	1.94	7.76	2.07	6.76	7.0 8.0
9.0	1.72	8.83	1.87	8.80	2.02	8.77	2.18	8.73	2.33	8.69	9.0
10.0 11.0	1.91 2.10	9.82 10.80	2.08 2.29	9.78 10.76	2.25 2.47	9.74 $10.72$	2.42 2.66	9.70 10.67	2.59	9.66	10.0
12.0	2.29	11.78	2.49	11.74	2.70	11.69	2.90	11.64	2.85 3.11	10.63	$11.0 \\ 12.0$
13.0 14.0	2.48 2.67	12.76 13.74	$2.70 \\ 2.91$	12.72 13.69	2.92 3.15	12.67 13.64	3.14	12.61 13.58	3.36 3.62	12.56 13.52	13.0 14.0
15.0	2.86	14.72	3.12	14.67	3.37	14.62	3.63	14.55	3.88		
16.0	3.05	15.71	3.33	15.65	3.60	15.59	3.87	15.52	4.14	14.49 15.45	15.0 16.0
17.0 18.0	3.24	16.69 17.67	3.53 3.74	16.63 17.61	$\frac{3.82}{4.05}$	16.56 17.54	4.11 4.35	16.50 17.47	4.40	16.42 17.39	17.0 18.0
19.0	3.63	18.65	3.95	18.58	4.27	18.51	4.60	18.44	4.92	18.35	19.0
20.0	3.82	19.63	4.16	19.56	4.50	19.49	4.84	19.41	5.18	19.32	20.0
21.0 22.0	4.01 4.20	$20.61 \\ 21.60$	4.37	20.54 $21.52$	4.72	20.46	5.08 5.32	20.38 $21.35$	5.44 5.69	20.28 21.25	$21.0 \\ 22.0$
23.0 24.0	4.39 4.58	22.58 23.56	4.78	22.50	5.17	22.41	5.56	22.32	5.95	22.22	23.0
				23.48	5.40	23.38	5.81	23.29	6.21	23.18	24.0
25.0 26.0	4.77	24.54 25.52	5.20 5.41	24.45 25.43	5.62 5.85	24.36 25.33	6.05	24.26 25.23	6.47 6.73	24.15 25.11	25.0 26.0
27.0	5.15 5.34	26.50 27.49	5.61	26.41	6.07	26.31	6.53	26.20	6.99	26.08	27.0
29.0	5.53	28.47	5.82 6.03	27.39 28.37	$6.30 \\ 6.52$	27.28 28.26	6.77 7.02	27.17 28.14	7.25 7.51	27.05 28.01	$28.0 \\ 29.0$
30.0	5.72	29.45	6.24	29.34	6.75	29.23	7.26	29.11	7.76	28.98	30.0
	cos	sin	cos	sin	cos	sin	cos	sin	cos	sin	00.0
	1.00	27	1.00			0					
-3	+28 $-25$		+28 $-25$		+28 $-25$		+28 $-25$		+28 $-25$		
	- 10	)1 +	- 10	2 +	- 10	3 +	- 10		- 10		
	+ 7	9 +	+ 7	8 +	+ 7	7 +	+ 7	6 +	+ 7		

		+ 1 + 16 - 19 - 34	4 — 6 —	+ 1 + 16 - 19 - 34	3 - 7 -	+ 1 + 163 - 19 - 34	2 - 8 -	+ 16 + 16 - 19 - 34	9 —	+ 2 + 166 - 200 - 34	0 - 0 -	
L			* +	-04	* +	-04	4 +	-04	1+	- 34	0 +	
L		sin	cos	sin	cos	sin	cos	sin	cos	sin	cos	
ľ	0.1	0.03	0.10	0.03	0.10	0.03	0.10	0.03	0.09	0.03	0.09	0.1
١	0.3	0.08	0.29	0.09	0.29	0.09	0.29	0.10	0.28	0.10	0.28	0.3
ı	0.4	0.11	0.38	0.12	0.38	0.12	0.38	0.13	0.38	0.14	0.38	0.4
١	. 0.5	0.14	0.48	0.15	0.48	0.15	0.48	0.16	0.47	0.17	0.47	0.5
ı	0.6	0.17	0.58	0.18	0.57	0.19	0.57	0.20 0.23	0.57	0.21 0.24	0.56	0.6
ı	0.8	0.22	0.77	0.23	0.77	0.25	0.76	0.26	0.76	0.27	0.75	0.8
ı	0.9	0.25	0.87	0.26	0.86	0.28	0.86	0.29	0.85	0.31	0.85	0.9
1	1.0	0.28	0.96	0.29	0.96	0.31	0.95	0.33	0.95	0.34	0.94	1.0
1	2.0	0.55	1.92	0.58	1.91	0.62	1.90	0.65	1.89	0.68	1.88	2.0
1	3:0 4.0	0.83 1.10	2.88 3.85	0.88	2.87 3.83	0.93	2.85 3.80	0.98 1.30	2.84 3.78	1.03 1.37	2.82 3.76	3.0 4.0
1	5.0	1.38	4.81	1.46	4.78	1.55	4.76	1.63	4.73	1.71	4.70	5.0
ı	6.0	1.65	5.77	1.75	5.74	1.85	5.71	1.95	5.67	2.05	5.64	6.0
١	7.0	1.93 2.21	6.73 7.69	2.05	6.69 7.65	2.16	6.66	2.28	6.62 7.56	2.39 2.74	6.58 7.52	7.0
١	9.0	2.48	8.65	2.63	8.61	2.78	8.56	2.93	8.51	3.08	8.46	9.0
I	10.0	2.76	9.61	2.92	9.56	3.09	9.51	3.26	9.46	3.42	9.40	10.0
1	11.0	3.03	10.57	3.22	10.52	3.40	10.46	3.58	10.40	3.76	10.34	11.0
١	12.0 13.0	3.31 3.58	11.54 12.50	3.51 3.80	11.48 12.43	3.71 4.02	11.41 12.36	3.91 4.23	11.35 12.29	4.10	11.28 12.22	12.0 13.0
ı	14.0	3.86	13.46	4.09	13.39	4.33	13.31	4.56	13.24	4.79	13.16	14.0
1	15.0	4.13	14.42	4.39	14.34	4.64	14.27	4.88	14.18	5.13	14.10	15.0
1	16.0	4.41	15.38	4.68	15.30	4.94	15.22	5.21	15.13	5.47	15.04 15.97	16.0 17.0
ı	17.0 18.0	4.69	16.34 17.30	4.97 5.26	16.26 17.21	5.25 5.56	16.17 17.12	5.53 5.86	16.07 17.02	5.81 6.16	16.91	18.0
ı	19.0	5.24	18.26	5.56	18.17	5.87	18.07	6.19	17.96	6.50	17.85	19.0
ı	20.0	5.51	19.23	5.85	19.13	6.18	19.02	6.51	18.91	6.84	18.79	20.0
ı	21.0	5.79	20.19	6.14	20.08	6.49	19.97	6.84 7.16	19.86 20.80	7.18 7.52	19.73 20.67	21.0 22.0
١	23.0	6.06	21.15		22.00		21.87		21.75	7.87	21.61	23.0
ı	24.0	6.62	23.07	7.02	22.95	7.42	22.83	7.81	22.69	8.21	22.55	24.0
1	25.0	6.89	24.03	7.31	23.91	7.73	23.78	8.14	23.64	8.55	23.49	25 0
-	26.0	7.17	24.99	7.60	24.86	8.03	24.73	8.46	24.58	8.89 9.23	24.43 25.37	26.0 27.0
-	27.0 28.0	7.44	25.95 26.92	7.89	25.82 26.78	8.34	25.68 26.63	8.79 9.12	25.53 26.47	9.23	26.31	28.0
-	29.0	7.99	27.88	8.48	27.73	8.96	27.58	9.44	27.42	9.92	27.25	29.0
1	30.0	8.27	28.84	8.77	28.69	9.27	28.53	9.77	28.37	10.26	28.19	30.0
1		cos	sin	cos	sin	cos	sin	cos	sin	cos	sin	
1		+2	86 —	+2	87 —	+ 2	88 —	+2	89 —	+2	90 —	
1			54 —		53 —		52 —		51 —	-2	50 —	
1		-1	06 +		07 +		08 +		09 +		10 +	
1		+ 1	74 +	+	73 +	+	72 +	+	71 +	+ '	70 +	
L		-				-	-	-		-		•

	+ 21°+ + 159 - - 201 - - 339 +	+ 158 — -202 —	+ 157 — - 203 —		+ 25°+ + 155 — - 205 — - 335 +	
	sin cos	sin cos	sin cos	sin cos	sin cos	
0.1	0.04 0.0			0.04 0.09 0.08 0.18	0.04 0.09 0.08 0.18	0.1
$0.2 \\ 0.3$	$egin{array}{ c c c c c c c c c c c c c c c c c c c$		0.12 0.28	0.12 0.27	0.13 0.27	$\begin{array}{c} 0.2 \\ 0.3 \end{array}$
0.4	0.14 0.3	7 0.15 0.3	0.16 0.37	0.16 0.37	0.17 0.36	0.4
0.5	0.18 0.4			0.20 0.46	0.21 0.45	0.5
0.6	$egin{array}{ c c c c c c c c c c c c c c c c c c c$			$\begin{array}{c cccc} 0.24 & 0.55 \\ 0.28 & 0.64 \\ \end{array}$	0.25 0.54 0.30 0.63	0.6
0.8	0.29 0.7	5 0.30 0.74		$\begin{array}{c cccc} 0.33 & 0.73 \\ 0.37 & 0.82 \\ \end{array}$	$\begin{array}{c cccc} 0.34 & 0.73 \\ 0.38 & 0.82 \end{array}$	0.8
	0.32 0.8					
$\frac{1.0}{2.0}$	$egin{array}{ c c c c c c c c c c c c c c c c c c c$			0.41 0.91 0.81 1.83	$\begin{array}{c cccc} 0.42 & 0.91 \\ 0.85 & 1.81 \\ \end{array}$	1.0 2.0
3.0	1.08 2.8	0 1.12 2.78	1.17 2.76	1.22 2.74	1.27 2.72	3.0
4.0	1.43 3.7			1.63 3.65	1.69 3.63	4.0
5.0 6.0	1.79 4.6 2.15 5.6			2.03 4.57 2.44 5.48	2.11 4.53 2.54 5.44	5.0 6.0
7.0	2.51 6.5	4 2.62 6.49	2.74 6.44	2.85 6.39	2.96 6.34	7.0
8.0 9.0	2.87 7.4 3.23 8.4			$egin{array}{ c c c c c c c c c c c c c c c c c c c$	3.38 7.25 3.80 8.16	8.0 9.0
10.0 11.0	$\begin{vmatrix} 3.58 & 9.3 \\ 3.94 & 10.2 \end{vmatrix}$			4.07 9.14 4.47 10.05	4.23 9.06 4.65 9.97	10.0 11.0
12.0 13.0	4.30 11.2	0 4.50 11.13	4.69 11.05	4.88 10.96	5.07 10.88	12.0
14.0	$\begin{array}{c cccc} 4.66 & 12.1 \\ 5.02 & 13.0 \end{array}$			5.29 11.88 5.69 12.79	5.49 11.78 5.92 12.69	13.0 14.0
15.0	5.38 14.0	5.62 13.93	5.86 13.81	6.10 13.70	6.34 13.59	15.0
16.0	5.73 14.9	4 5.99 14.83	6.25 14.73	6.51 14.62	6.76 14.50	16.0
17.0 18.0	6.09 15.8 6.45 16.8			6.91 15.53 7.32 16.44	7.18   15.41 7.61   16.31	17.0 18.0
19.0	6.81 17.7			7.73 17.36	8.03 17.22	19.0
20.0	7.17 18.6	7 7.49 18.5	7.81 18.41	8.13 18.27	8.45 18.13	20.0
21.0 22.0	7.53 19.6	1 7.87 19.4	8.21 19.33	8.54 19.18	8.87 19.03	21.0
23.0	8.24 21.4	7 8.62 21.3	8.99 21.17	9.35 21.01	$\begin{array}{c cccc} 9.30 & 19.94 \\ 9.72 & 20.85 \end{array}$	$22.0 \\ 23.0$
24.0	8.60 22.4	1 8.99 22.2	9.38 22.09	9.76 21.93	10.14 21.75	24.0
25.0	8.96 23.3			10.17 22.84	10.57 22.66	25.0
$26.0 \\ 27.0$	$   \begin{array}{c cccc}     9.32 & 24.3 \\     9.68 & 25.3 \\   \end{array} $			10.58 23.75 10.98 24.67	10.99 23.56 11.41 24.47	$26.0 \\ 27.0$
28.0 29.0	10.03 26.1	4 10.49 25.9	6 10.94 25.77	11.39 25.58	11.83 25.38	28.0
	10.39 27.0		- B - S	11.80 26.49	12.26 26.28	29.0
30.0	10.75 28.0			12.20 27.41	12.68 27.19	30.0
	cos sin	cos sin	cos sin	cos sin	cos sin	
	+ 291 -	+ 292 -	+ 293 —	+294 —	+295 -	
	-249 -	-248 -	-247 -	-246 -	-245 -	
	- 111 + + 69 +		- 113 +	-114 +	<b>— 115</b> +	
	1 00 4	7 00 +	+ 67 +	+ 66 +	+ 65 +	

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ı		+15 $-20$		+15 $-20$		+15		+ 15		+ 15		
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ı		-00	* T	- 00	· T	- 00	4 +	_ 00	T T	- 00	U T	
I		sin	cos	sin	cos	sin	cos	sin	cos	sin	cos	
ı	0.1	0.04	0.09	0.05	0.09	0.05	0.09	0.05	0.09	0.05	0.09	0.1
ı	0.2	0.09	0.18	0.09	0.18	0.09	0.18	0.10	0.17	0.10	0.17	0.2
ı	0.3	0.13	0.27 0.36	0.14	0.27 0.36	0.14 0.19	0.26 0.35	0.15	0.26 0.35	0.15 0.20	0.26 0.35	0.3
ı												
ı	0.5	0.22	0.45 0.54	0.23	0.45 0.53	0.23	0.44 0.53	0.24 0.29	$0.44 \\ 0.52$	0.25	0.43 0.52	0.5
ı	0.7	0.20	0.63	0.32	0.62	0.33	0.62	0.34	0.61	0.35	0.61	0.7
ı	0.8	0.35	0.72	0.36	0.71	0.38	0.71	0.39	0.70	0.40	0.69	0.8
ı	0.9	0.39	0.81	0.41	0.80	0.42	0.79	0.44	0.79	0.45	0.78	0.9
1	1.0	0.44	0.90	0.45	0.89	0.47	0.88	0.48	0.87	0.50	0.87	1.0
1	2.0	0.88	1.80	0.91	1.78	0.94	1.77	0.97	1.75	1.00	1.73 2.60	2.0 3.0
1	3.0	1.32	2.70 3.60	1.36 1.82	2.67 3.56	1.41	2.65 3.53	1.45 1.94	2.62 3.50	1.50 2.00	3.46	4.0
1				1								
ı	5.0	2.19 2.63	4.49 5.39	2.27	4.46 5.35	2.35	4.41 5.30	2.42 2.91	4.37 5.25	2.50 3.00	4.33 5.20	5.0 6.0
ı	7.0	3.07	6.29	3.18	6.24	3.29	6.18	3.39	6.12	3.50	6.06	7.0
ı	8.0	3.51	7.19	3 63	7.13	3.76	7.06	3.88	7.00	4.00	6.93	8.0
ı	9.0	3.95	8.09	4.09	8.02	4.23	7.95	4.36	7.87	4.50	7.79	9.0
ı	10.0	4.38	8.99	4.54	8.91	4.69	8.83	4.85	8.75	5.00	8.66	10.0
١	11.0	4.82	9.89	4.99	9.80	5.16	9.71 $10.60$	5.33	9.62 10.50	5.50 6.00	9.53 10.39	11.0 12.0
١	12.0 13.0	5.26 5.70	10.79	5.45 5.90	10.69 11.58	5.63 6.10	11.48	5.82 6.30	11.37	6.50	11.26	13.0
١	14.0	6.14	12.58	6.36	12.47	6.57	12.36	6.79	12.24	7.00	12.12	14.0
١	15.0	6.58	13.48	6.81	13.37	7.04	13.24	7.27	13.12	7.50	12.99	15.0
ı	16.0	7.01	14.38	7.26	14.26	7.51	14.13	7.76	13.99	8.00	13.86	16.0
ı	17.0	7.45	15.28	7.72	15.15	7.98	15.01 15.89	8.24	14.87	8.50 9.00	14.72 15.59	17.0 18.0
ı	18.0 19.0	7.89 8.33	16.18 17.08	8.17 8.63	16.04 16.93	8.45 8.92	16.78	8.73 9.21	16.62	9.50	16.45	19.0
ı							17.66			1	17.32	20.0
ı	20.0 21.0	8.77 9.21	17.98 18.87	9.08 9.53	17.82 18.71	9.39 9.86	18.54	9.70	17.49 18.37	10.00 10.50	18.19	21.0
1	22.0	9.64	19.77			10.33	19.42	10.67	19.24	11.00	19.05	22.0
	. 23.0	10.08	20.67	10.44	20.49	10.80	20.31	11.15	20.12	11.50	19.92	23.0
	24.0	10.52	21.57	10.90	21.38	11.27	21.19	11.64	20.99	12.00	20.78	24.0
	25.0	10.96	22.47	11.35		11.74	22.07	12.12	21.87	12.50	21.65	25 0
1	26.0	11.40		11.80	23.17	12.21	22.96	12.61	22.74 23.61	13.00 13.50	22.52 23.38	26.0 27.0
	27.0 28.0	11.84	24.27 25.17	12.26 $12.71$	24.06 24.95	12.68 13.15	23.84 24.72	13.09 13.57	24.49	14.00	24.25	28.0
-	29.0	12.71	26.07	13.17	25.84		25.61	14.06	25.36	14.50	25.11	29.0
	30.0	13.15	26.96	13.62	26.73	14.08	26.49	14.54	26.24	15.00	25.98	30.0
		cos	sin	cos	sin	cos	sin	cos	sin	cos	sin	
			00	1.0	07		98 —	100	99 —	1 20	00 —	
			96 — 44 —		97 — 43 —	ALC DE LA CONTRACTOR DE	42 —	The second second	41 —		10 —	
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				-2	48 — 212 —		147 — 213 —		146 — 214 —		145 — 215 —	
		-:	329 +	-3	28 +	-8	327 +		326 +	-	325 +	
1		sin	cos	sin	cos		cos	sin	cos	sin	cos	
1	0.1	0.03	0.17	0.11	0.17	0.11	0.17	0.11	0.17	0.06 0.11	0.16	0.1
1	0.3	0.15							0 25 0.33	0.17 0.23		0.3
ı	0.5 0.6	0.26			0.42				0.41 0.50	0.29 0.34		0.5
1	0.7	0.36	0.60	0.37		0.38	0.59	0.39	0.58	0.40 0.46	0.57	0.7 0.8
1	0.9	0.46			0.76			0.50	0.75	0.52	0.74	0.9
1	1.0 2.0	0.52 1.03			0.85			0.56 1.12	0.83	0.57 1.15	0.82	1.0 2.0
	3.0	1.55 2.06	2.57	1.59	2.54 3.39		2.52	1.68 2.24	2.49 3.32	1.72 2.29	2.46 3.28	3.0 4.0
	5.0	2.58	4.29	2.65	4.24	2.72	4.19	2.80	4.15	2.87	4.10	5.0
l	$\frac{6.0}{7.0}$	3.09 3.61	5.14 6.00	3.18 3.71	5.09 5.94	3.27 $3.81$	5.03 5.87		4.97 5.80	3.44 4.02	4.91 5.73	6.0
	8.0 9.0	4.12 4.64			6.78 7.63	4.36 4.90	6.71 7.55		6.63	4.59 5.16	6.55	8.0 9.0
ı	10.0	5.15	8.57		8.48	5.45	8.39		8.29	5.74	8.19	10.0
	11.0	5.67		6.36	9.33	5.99 6.54	9.23 10.06	6.71	9.12 9.95	6.31	9.01 9.83	11.0 12.0
	13.0 14.0	6.70 7.21	11.14 12.00	6.89 7.42	11.02 11.87	7.08 7.62	10.90	7.27 7.83	10.78	7.46 8.03	10.65	13.0 14.0
	15.0 16.0	7.73 8.24	12.86 13.71		12.72 13.57	8.17 8.71	12.58 13.42	8.39	12.44	8.60	12.29	15.0
ĺ	17.0 18.0	8.76 9.27	14.57 15.43	9.01	14.42	9.26	14.26	8.95 9.51	13.26 14.09	9.18 9.75	13.11	16.0 17.0
	19.0	9.79	16.29	9.54	15.26 16.11	9.80 10.35	15.10 15.93	10.07	14.92 15.75	10.32 10.90	14.74 15.56	18.0 19.0
	20.0 21.0	10.30 10.82			16.96 17.81	10.89	16.77 17.61	11.18 11.74	16.58 17.41	11.47 12.05	16.38 17.20	20.0 21.0
	22.0 23.0			11.66 12.19	18.66 19.51	11.98 12.53	18.45	12.30	18.24	12.62	18.02	22.0
	24.0	12.36	20.57	12.72	20.35	13.07	19.29 20.13	$12.86 \\ 13.42$	19.07 19.90	13.19 13.77	18.84 19.66	23.0 24.0
	25.0 26.0	12.88 13.39	21.43 22.29	13.25 13.78	$21.20 \\ 22.05$	13.62 14.16	20.97 21.81	13.98	20.73	14.34	20.48	25.0
1	27 0 28.0	13.91	23.14	14.31	22.90	14.71	22.64	14.54 15.10	21.55 22.38	14.91 15.49	$21.30 \\ 22.12$	$\frac{26.0}{27.0}$
	29.0	14.42	24.00 24.86	14.84 15.37	23.75 24.59	15.25 15.79	23.48 24.32	15.66 16.22	23.21 24.04	16.06 16.63	$22.94 \\ 23.76$	28.0 29.0
	30.0	15.45	25.71	15.90	25.44	16.34	25.16	16.78	24.87	17.21	24.57	30.0
_		cos	sin	cos	sin	cos	sin	cos	sin	cos	sin	
		+301°— +302 — -239 — -238 —				+30		+30			5 —	Y
	-635	-239 - -121 +		-129	2 +	-23 $-12$		-23 $-12$	66 — 4 +		5 — · · · · · · · · · · · · · · · · · ·	
		+ 59 + + 58		3 +	+ 5	7 +	+ 5		+ 5			
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	+ 3 +14 - 21 - 32	4 —		The second second	+ 8 + 14 - 21 - 32	2 - 8 -	+ 3 + 14 - 21 - 32	1 —	+ 4 + 14 - 22 - 32	0 - 0 - 0	
	sin	cos	sin	cos	sin	cos.	sin	cos	sin	cos	
0.1	0.06	0.08	0.06	0.08	0.06	0.08	0.06	0.08	0.06	0.08	0.1
0.2	0.12 0.18	0.16 0.24	0.12	$0.16 \\ 0.24$	0.12	$0.16 \\ 0.24$	0.13	$0.16 \\ 0.23$	0.13 0.19	0.15 0.23	0.2
0.4	0.18	0.32	0.16	0.24	0.16	0.32	0.25	0.31	0.15	0.23	0.4
0.5	0.29	0.40	0.30	0.40	0.31	0.39	0.31	0.39	0.32	0.38	0.5
0.6	0.35	0.49	0.36	0.48	0.37	0.47	0.38	0.47	0.39	0.46	0.6
0.7	0.41	0.57	0.42	0.56	0.43	0 55	0.44	0.54	0.45	0.54	0.7
0.8	0.47 0.53	0.65 0.73	0.48	$0.64 \\ 0.72$	0.49 0.55	0.63	0.50 0.57	$0.62 \\ 0.70$	0.51 0.58	0.61 0.69	0.8
							0.00	0 40	0.04		10
1.0	0.59	0.81 1.62	0.60 1.20	0.80 1.60	0.62 1.23	0.79 1.58	$0.63 \\ 1.26$	0.78 1.55	0.64	0.77 1.53	1.0 2.0
3.0	1.76	2.43	1.81	2.40	1.85	2.36	1.89	2.33	1.93	2.30	3.0
4.0	2.35	3.24	2.41	3.19	2.46	3.15	2.52	3.11	2.57	3.06	4.0
5.0	2.94	4.05	3.01	3.99	3.08	3.94	3.15	3.89	3.21	3.83	5.0
6.0	3.53	4.85	3.61	4.79	3.69	4.73	3.78	4.66	3.86	4.60	6.0 7.0
7.0 8.0	4.11	5.66 6.47	4.21	5.59 6.39	4.31	5.52 6.30	4.41 5.03	5.44 6.22	4.50 5.14	5.36 6.13	8.0
9.0	5.29	7.28	5.42	7.19	5.54	7.09	5.66	6.99	5.79	6.89	9.0
10.0	5.88	8.09	6.02	7.99	6.16	7.88	6.29	7.77	6.43	7.66	10.0
11.0	6.47	8.90	6.62	8.78	6.77	8.67	6.92	8.55	7.07	8.43	11.0
12.0 13.0	7.05	$9.71 \\ 10.52$	7.22	9.58	7.39	9.46	7.55 8.18	9.33	7.71 8.36	9.19 9.96	12.0 13.0
14.0	8.23	11.33	8.43	11.18	8.62	11.03	8.81	10.88	9.00	10.72	14.0
15.0	8.82	12.14	9.03	11.98	9.23	11.82	9.44	11.66	9.64	11.49	15.0
16.0	9.40	12.94	9.63	12.78	9.85	12.61	10.07	12.43	10.28	12.26	16.0
17.0	9.99	13.75	10.23	13.58	10.47	13.40	10.70	13.21	10.93	13.02 13.79	17.0 18.0
18.0 19.0	10.58 11.17	14.56 15.37	10.83	14.38 15.17	11.08 11.70	14.18	11.33 11.96	13.99	11.57 12.21	14.55	19.0
			10.04		10.01	15 70	10.50	15.54	12.86	15.32	20.0
20.0	11.76 $12.34$		12.04 $12.64$	15.97 16.77	12.31 12.93	15.76 16.55		15.54 16.32	13.50	16.09	21.0
22.0	12.93	17.80	13.24	17.57	13.54	17.34	13.85	17.10	14.14	16.85	22.0
23.0	13.52		13.84 14.44			18.12 18.91	14.47 15.10	17.87 18.65	14.78 15.43	17.62 18.39	23.0 24.0
24.0	14.11	19.42	14.44	19.17	14.78		15.10				
25.0	14.69	20.23	15.05	19.97		19.70	15.73	19.43	16.07	19.15 19.92	25.0 26.0
26.0 27.0	15.28 15.87	21.03	15.65 16.25	20.76 21.56	16.01 16.62	20.49 21.28	16.36 16.99	20.21 20.98	16.71 17.36	20.68	27.0
28.0	16.46	22.65	16.85	22.36	17.24	22.06	17.62	21.76	18.00	21.45	28.0
29.0	17.05	23.46	17.45	23.16	17.85	22.85	18.25	22.54	18.64	22.22	29.0
30.0	17.63	24.27	18.05	23.96	18.47	23.64	18.88	23.31	19.28	22.98	30.0
	cos	sin	cos	sin	cos	sin	cos	sin	cos	sin	
	-28 - 19	06 — 34 — 26 + 54 +	-28 - 19	07 — 33 — 27 + 53 +	-28 - 19	08 — 32 — 28 + 52 +	$-2 \\ -19$	09 — 31 — 29 + 51 +	- 28 - 18	10 — 30 — 30 + 50 +	

	+13 $-22$	11°+ 39 — 21 — .9 +	-22	12°+ 38 — 22 — 18 +	+ 18 - 29	13°+ 37 — 23 — 17 +	+13 $-22$	4°+ 36 — 44 — 16 +	+ 13 22	45°+ 85 — 25 — 15 +	
0.1	sin 0.07	cos 0.08	sin 0.07	cos 0.07	sin 0.07	cos 0.07	sin 0.07	cos 0.07	sin 0.07	cos 0.07	0.1
0.2 0.3 0.4	0.13 0.20 0.26	0.15 0.23 0.30	0.13 0.20 0.27	0.15 0.22 0.30	0.14 $0.20$ $0.27$	0.15 0.22 0.29	$0.14 \\ 0.21 \\ 0.28$	$0.14 \\ 0.22 \\ 0.29$	$0.14 \\ 0.21 \\ 0.28$	$0.14 \\ 0.21 \\ 0.28$	$0.2 \\ 0.3 \\ 0.4$
0.5 0.6 0.7 0.8 0.9	0.33 0.39 0.46 0.52 0.59	0.38 0.45 0.53 0.60 0.68	0.33 0.40 0.47 0.54 0.60	0.37 0.45 0.52 0.59 0.67	0.34 0.41 0.48 0.55 0.61	0.37 0.44 0.51 0.59 0.66	0.35 $0.42$ $0.49$ $0.56$ $0.63$	0.36 0.43 0.50 0.58 0.65	0.35 0.42 0.49 0.57 0.64	0.35 $0.42$ $0.49$ $0.57$ $0.64$	0.5 0.6 0.7 0.8 0.9
1.0	0.66	0.75	0.67	0.74	0.68	0.73	0.69	0.72	0.71	0.71	1.0
2.0	1.31	1.51	1.34	1.49	1.36	1.46	1.39	1.44	1.41	1.41	2.0
3.0	1.97	2.26	2.01	2.23	2.05	2.19	2.08	2.16	2.12	2.12	3.0
4.0	2.62	3.02	2.68	2.97	2.73	2.93	2.78	2.88	2.83	2.83	4.0
5.0	3.28	3.77	3.35	3.72	3.41	3.66	3.47	3.60	3.54	3.54	5.0
6.0	3.94	4.53	4.01	4.46	4.09	4.39	4.17	4.32	4.24	4.24	6.0
7.0	4.59	5.28	4.68	5.20	4.77	5.12	4.86	5.04	4.95	4.95	7.0
8.0	5.25	6.04	5.35	5.95	5.46	5.85	5.56	5.75	5.66	5.66	8.0
9.0	5.90	6.79	6.02	6.69	6.14	6.58	6.25	6.47	6.36	6.36	9.0
10.0	6.56	7.55	6.69	7.43	6.82	7.31	6.95	7.19	7.07	7.07	10.0
11.0	7.22	8.30	7.36	8.17	7.50	8.04	7.64	7.91	7.78	7.78	11.0
12.0	7.87	9.06	8.03	8.92	8.18	8.78	8.34	8.63	8.49	8.49	12.0
13.0	8.53	9.81	8.70	9.66	8.87	9.51	9.03	9.35	9.19	9.19	13.0
14.0	9.18	10.57	9.37	10.40	9.55	10.24	9.73	10.07	9.90	9.90	14.0
15:0	9.84	11.32	10.04	11.15	10.23	10.97.	10.42	10.79	10.61	10.61	15.0
16:0	10.50	12.08	10.71	11.89	10.91	11.70	11.11	11.51	11.31	11.31	16.0
17:0	11.15	12.83	11.38	12.63	11.59	12.43	11.81	12.23	12.02	12.02	17.0
18:0	11.81	13.58	12.04	13.38	12.28	13.16	12.50	12.95	12.73	12.73	18.0
19:0	12.47	14.34	12.71	14.12	12.96	13.90	13.20	13.67	13.44	13.44	19.0
20.0	13.12	15.09	13.38	14.86	13.64	14.63	13.89	14.39	14.14	14.14	20.0
21.0	13.78	15.85	14.05	15.61	14.32	15.36	14.59	15.11	14.85	14.85	21.0
22.0	14.43	16.60	14.72	16.35	15.00	16.09	15.28	15.83	15.56	15.56	22.0
23.0	15.09	17.36	15.39	17.09	15.69	16.82	15.98	16.54	16.26	16.26	23.0
24.0	15.75	18.11	16.06	17.84	16.37	17.55	16.67	17.26	16.97	16.97	24.0
25.0	16.40	18.87	16.73	18.58	17.05	18.28	17.37	17.98	17.68	17.68	25.0
26.0	17.06	19.62	17.40	19.32	17.73	19.02	18.06	18.70	18.38	18.38	26.0
27.0	17.71	20.38	18.07	20.06	18.41	19.75	18.76	19.42	19.09	19.09	27.0
28.0	18.37	21.13	18.74	20.81	19.10	20.48	19.45	20.14	19.80	19.80	28.0
29.0	19.03	21.89	19.40	21.55	19.78	21.21	20.15	20.86	20.51	20.51	29.0
30.0	19.68 cos	22.64 sin	20.07 cos	22.29 sin	20.46 cos	21.94 sin	20.84 cos	21.58 sin	21.21 cos	21.21 sin	30.0
	-22 $-13$		-29 $-13$	12 — 28 — 32 + 48 +	- 29 - 18	13 — 27 — 33 + 47 +	-29 $-13$	4 — 26 — 4 + 46 +	22 13	15 — 25 — 35 + 45 +	

